

1 Theory

FIRST LINE OF THEORY ANOTHER LINE OF THEORY

1.1 Notations

In this study, the distribution network is accounted as a tree (connected graph) having N number of buses (indexed with i , j , and k) and the study is conducted for T time steps (indexed by t). The distribution line connecting two buses i and j are denoted by ij and magnitude of the current flowing through the line at time t is denoted by I_{ij}^t ($l_{ij}^t = (I_{ij}^t)^2$). The voltage magnitude of bus i at time t is given by V_i^t ($v_i^t = (V_i^t)^2$).

1.2 Centralized Multi-Period OPF with Batteries

1.2.1 Network Model

On similar lines to the branch flow equations in [?], the network is modeled as a function of time, considering the interaction of batteries.

$$p_j^t = \sum_{(j,k) \in \mathcal{L}} P_{jk}^t - \sum_{(i,j) \in \mathcal{L}} \{P_{ij}^t - r_{ij} l_{ij}^t\} - P_{d_j}^t + P_{c_j}^t \quad (1)$$

$$q_j^t = \sum_{(j,k) \in \mathcal{L}} Q_{jk}^t - \sum_{(i,j) \in \mathcal{L}} \{Q_{ij}^t - x_{ij} l_{ij}^t\} - q_{D_j}^t - q_{B_j}^t \quad (2)$$

$$v_j^t = v_i^t + \{r_{ij}^2 + x_{ij}^2\} l_{ij}^t - 2(r_{ij} P_{ij}^t + x_{ij} Q_{ij}^t) \quad (3)$$

$$l_{ij}^t = \frac{(P_{ij}^t)^2 + (Q_{ij}^t)^2}{v_i^t} \quad (4)$$

where $P_{ij}^t, Q_{ij}^t, l_{ij}^t$ denote the sending-end real power, reactive power and the square of the magnitude of the current flowing in the branch (i, j) respectively. v_j^t denotes the square of the magnitude of the voltage at node j . The superscript t specifies the time-period for the corresponding variable. Node i denotes the ‘parent’ node of node j , which itself may be the parent of a set of k ‘children’ nodes (the set may contain one, many or even zero nodes, if j is a leaf node). It may be noted that for a radial distribution system, each node j can have only one ‘parent’ node i , and thus the summation for the second term in (1) to (4) may be dropped.

1.2.2 DER Model

DERs are modeled as photovoltaic (PV) modules interfacing with the network via inverters operating in two quadrants. The DERs inject a time-varying, non-controllable real power p_D^t into the network. Based on the maximum apparent power capacity of their corresponding inverter, S_D , they can output controllable reactive power q_D , whose limits are given by (5).

$$q_{D_j}^t \in \left[-\sqrt{S_{D_j}^2 - p_{D_j}^t{}^2}, \sqrt{S_{D_j}^2 - p_{D_j}^t{}^2} \right] \quad (5)$$

(Integer Constraint Relaxed) Naive Brute Force Full Optimization Model - Full Horizon

$$\begin{aligned} \min \quad & \sum_{t=1}^T \sum_{(i,j) \in \mathcal{L}} (r_{ij} l_{ij}^t) \\ & + \alpha \sum_{t=1}^T \sum_{j \in \mathcal{B}} \left\{ (1 - \eta_c) P_{c_j}^t + \left(\frac{1}{\eta_d} - 1 \right) P_{d_j}^t \right\} \\ & + \gamma \sum_{j \in \mathcal{B}} \left\{ (B_j^T - B_{ref_j})^2 \right\} \end{aligned} \quad (6)$$

s.t.

$$(1) \text{ to } (4) \quad (7)$$

$$B_j^t = B_j^{t-1} + \Delta t \eta_c P_{c_j}^t - \Delta t \frac{1}{\eta_d} P_{d_j}^t \quad (8)$$

$$\text{where,} \quad (9)$$

$$(i, j) : \text{Branch connecting nodes } i \text{ and } j \quad (10)$$

$$p_j^t = p_{D_j}^t - p_{L_j}^t \quad (11)$$

$$q_j^t = -q_{L_j}^t \quad (12)$$

$$t = \{1, 2, \dots, T\} \quad (13)$$

1.3 ENApp based Distributed Multi-Period OPF with Batteries