# 1 Theory

#### FIRST LINE OF THEORY ANOTHER LINE OF THEORY

## 1.1 Notations

In this study, the distribution network is accounted as a tree (connected graph) having N number of buses (indexed with i, j, and k) and the study is conducted for T time steps (indexed by t). The distribution line connecting two buses i and j are denoted by ij and magnitude of the current flowing through the line at time t is denoted by  $I_{ij}^t$  ( $l_{ij}^t = \left(I_{ij}^t\right)^2$ ). The voltage magnitude of bus i at time t is given by  $V_i^t$  ( $v_i^t = \left(V_i^t\right)^2$ ).

## 1.2 Centralized Multi-Period OPF with Batteries

#### 1.2.1 Network Model

On similar lines to the branch flow equations in [?], the network is modeled as a function of time, considering the interaction of batteries.

$$p_j^t = \sum_{(j,k)\in\mathcal{L}} P_{jk}^t - \sum_{(i,j)\in\mathcal{L}} \left\{ P_{ij}^t - r_{ij} l_{ij}^t \right\} - P_{d_j}^t + P_{c_j}^t$$
 (1)

$$q_j^t = \sum_{(j,k)\in\mathcal{L}} Q_{jk}^t - \sum_{(i,j)\in\mathcal{L}} \left\{ Q_{ij}^t - x_{ij} l_{ij}^t \right\} - q_{D_j}^t - q_{B_j}^t$$
 (2)

$$v_j^t = v_i^t + \left\{ r_{ij}^2 + x_{ij}^2 \right\} l_{ij}^t - 2(r_{ij}P_{ij}^t + x_{ij}Q_{ij}^t)$$
(3)

$$l_{ij}^{t} = \frac{(P_{ij}^{t})^{2} + (Q_{ij}^{t})^{2}}{v^{t}}$$

$$\tag{4}$$

where  $P_{ij}^t$ ,  $Q_{ij}^t$ ,  $l_{ij}^t$  denote the sending-end real power, reactive power and the square of the magnitude of the current flowing in the branch (i,j) respectively.  $v_j^t$  denotes the square of the magnitude of the voltage at node j. The superscript t specifies the time-period for the corresponding variable. Node i denotes the 'parent' node of node j, which itself may be the parent of a set of k 'children' nodes (the set may contain one, many or even zero nodes, if j is a leaf node). It may be noted that for a radial distribution system, each node j can have only one 'parent' node i, and thus the summation for the second term in equations Equations (1) to (4) may be dropped.

### 1.2.2 DER Model

DERs are modeled as photovoltaic (PV) modules interfacing with the network via inverters operating in two quadrants. The DERs inject a time-varying, non-controllable real power  $p_D^t$  into the network. Based on the maximum apparent power capacity of their corresponding inverter,  $S_D$ , they can output controllable reactive power  $q_D$ , whose limits are given by eq. (5).

$$q_{D_j}^t \in \left[ -\sqrt{S_{D_j}^2 - p_{D_j}^t}^2, \sqrt{S_{D_j}^2 - p_{D_j}^t}^2 \right]$$
 (5)

(Integer Constraint Relaxed) Naive Brute Force Full Optimization Model - Full Horizon

$$\min \sum_{t=1}^{T} \sum_{(i,j)\in\mathcal{L}} (r_{ij}l_{ij}^{t})$$

$$+ \alpha \sum_{t=1}^{T} \sum_{j\in\mathcal{B}} \left\{ (1 - \eta_c) P_{c_j}^{t} + \left(\frac{1}{\eta_d} - 1\right) P_{d_j}^{t} \right\}$$

$$+ \gamma \sum_{j\in\mathcal{B}} \left\{ \left(B_j^T - B_{ref_j}\right] \right)^2 \right\}$$
(6)

s.t.

$$eqs. (1)to (4)$$
 (7)

$$B_{j}^{t} = B_{j}^{t-1} + \Delta t \eta_{c} P_{c_{j}}^{t} - \Delta t \frac{1}{\eta_{d}} P_{d_{j}}^{t}$$
(8)

where, 
$$(9)$$

$$(i, j)$$
: Branch connecting nodes  $i$  and  $j$  (10)

$$p_{j}^{t} = p_{D_{j}}^{t} - p_{L_{j}}^{t} \tag{11}$$

$$q_j^t = -q_{Lj}^t \tag{12}$$

$$t = \{1, 2, \dots T\} \tag{13}$$

1.3 ENApp based Distributed Multi-Period OPF with Batteries