

Comparative Analysis of Linear vs. Nonlinear Multi-Period OPF Models for Active Distribution Systems

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Abstract—

Index Terms—Battery energy storage systems, distribution system, optimal power flow, distributed energy resources.

I. INTRODUCTION

II. PROBLEM FORMULATION

A. Notations

In this study, the distribution system is modeled as a tree (connected graph) with N number of buses (indexed with i , j , and k); the study is conducted for T time steps (indexed by t), each of interval length Δt . The sets of buses with DERs and batteries are D and B respectively, such that $D, B \subseteq N$. A directed edge from bus i to j in the tree is represented by ij and the set for edges is given by \mathcal{L} . Line resistance and reactance are r_{ij} and x_{ij} , respectively. Magnitude of the current flowing through the line at time t is denoted by I_{ij}^t and $I_{ij}^t = (I_{ij}^t)^2$. The voltage magnitude of bus j at time t is given by V_j^t and $v_j^t = (V_j^t)^2$. Apparent power demand at a node j at time t is $s_{L_j}^t = (p_{L_j}^t + jq_{L_j}^t)$. The active power generation from the DER present at bus j at time t is denoted by $p_{D_j}^t$ and controlled reactive power dispatch from the DER inverter is $q_{D_j}^t$. DER inverter capacity is $S_{D_{R_j}}$. The apparent power flow through line ij at time t is $S_{ij}^t = (P_{ij}^t + jQ_{ij}^t)$. The real power flowing from the substation into the network is denoted by P_{Subs}^t and the associated cost involved per kWh is C^t . The battery energy level is B_j^t . Charging and discharging active power from battery inverter (of apparent power capacity $S_{B_{R_j}}$) are denoted by $P_{c_j}^t$ and $P_{d_j}^t$, respectively and their associated efficiencies are η_c and η_d , respectively. The energy capacity of the batteries is denoted by B_{R_j} , and the rated battery power is $P_{B_{R_j}}$. soc_{min} and soc_{max} are fractional values for denoting safe soc limits of a battery about its rated state-of-charge (soc) capacity. The reactive power support of the battery inverter is indicated by $q_{B_j}^t$.

B. MPCOPF with Batteries

The OPF problem aims to minimize two objectives as shown in (1). The first term in (1) aims to minimize the total energy cost for the entire horizon. Including the ‘Battery Loss’ cost as the second term ($\alpha > 0$) helps eliminate the need for binary (integer) variables typically used to prevent

simultaneous charging and discharging. The resulting OPF problem is a non-convex optimization problem [1].

$$\min \sum_{t=1}^T \{f_0^t + f_{SCD}^t\} \quad (1)$$

where

$$f_0^t = C^t P_{Subs}^t \Delta t$$

$$f_{SCD}^t = \alpha \sum_{j \in B} \left\{ (1 - \eta_c) P_{c_j}^t + \left(\frac{1}{\eta_d} - 1 \right) P_{d_j}^t \right\} \quad (2)$$

Subject to the constraints ?? 3–II-B as given below:

$$\sum_{(j,k) \in \mathcal{L}} \{P_{jk}^t\} - (P_{ij}^t - r_{ij} I_{ij}^t) = p_j^t \quad (3)$$

where

$$\begin{aligned} p_j^t &= (P_{d_j}^t - P_{c_j}^t) + p_{D_j}^t - p_{L_j}^t \\ \sum_{(j,k) \in \mathcal{L}} \{Q_{jk}^t\} - (Q_{ij}^t - x_{ij} I_{ij}^t) &= q_{D_j}^t + q_{B_j}^t - q_{L_j}^t \\ v_j^t &= v_i^t - 2(r_{ij} P_{ij}^t + x_{ij} Q_{ij}^t) + \{r_{ij}^2 + x_{ij}^2\} I_{ij}^t \end{aligned}$$

$$(P_{ij}^t)^2 + (Q_{ij}^t)^2 = I_{ij}^t v_i^t$$

$$P_{Subs}^t \geq 0$$

$$v_j^t \in [V_{min}^2, V_{max}^2]$$

$$q_{D_j}^t \in \left[-\sqrt{S_{D_{R,j}}^2 - p_{D_j}^t{}^2}, \sqrt{S_{D_{R,j}}^2 - p_{D_j}^t{}^2} \right]$$

$$B_j^t = B_j^{t-1} + \Delta t \eta_c P_{c_j}^t - \Delta t \frac{1}{\eta_d} P_{d_j}^t$$

$$P_{c_j}^t, P_{d_j}^t \in [0, P_{B_{R_j}}], \quad B_j^0 = B_j^T$$

$$q_{B_j}^t \in \left[-\sqrt{0.44} P_{B_{R,j}}, \sqrt{0.44} P_{B_{R,j}} \right]$$

$$B_j^t \in [soc_{min} B_{R,j}, soc_{max} B_{R,j}]$$

A branch power flow model, given by ?? 3–II-B, is used to represent power flow in distribution system. Constraints (3) and section II-B model the active and reactive power balance at node j , respectively.

TABLE I: Parameter values

Parameter	Value
V_{min}, V_{max}	0.95 pu, 1.05 pu
p_{DR_j}	$0.33p_{LR_j}$
s_{DR_j}	$1.2p_{DR_j}$
P_{BR_j}	$0.33p_{LR_j}$
s_{BR_j}	$1.2P_{BR_j}$
BR_j	$T_{fullCharge} \times P_{BR_j}$
$T_{fullCharge}$	4 h
Δt	1 h
η_c, η_d	0.95, 0.95
soc_{min}, soc_{max}	0.30, 0.95
α	0.001

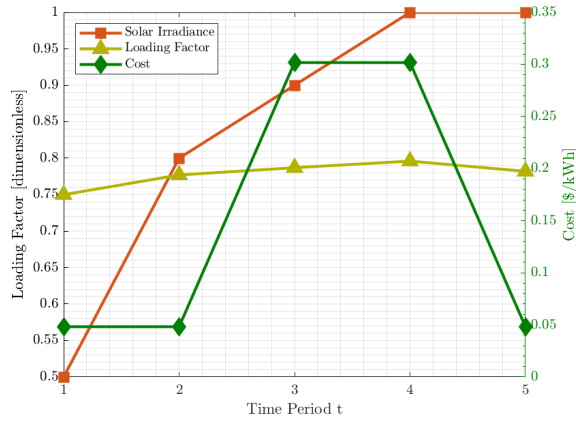


Fig. 1: Forecasts for demand power, irradiance and cost of substation power over a 5 hour horizon

The KVL equation for branch (ij) is represented by section II-B, while the equation describing the relationship between current magnitude, voltage magnitude and apparent power magnitude for branch (ij) is given by section II-B. Backflow of real power into the substation from the distribution system is avoided using the constraint section II-B. The allowable limits for bus voltages are modeled via section II-B. section II-B describes the reactive power limits of DER inverters. The trajectory of the battery energy versus time is given by section II-B (this is a time-coupled constraint). Battery charging and discharging powers are limited by the battery's rated power capacity, as given by section II-B. section II-B also says that the initial and final energy levels for battery must be the same at the end of the optimization time horizon. Every battery's reactive power is also constrained by the corresponding inverter's rated capacity, modeled in section II-B. For the safe and sustainable operation of the batteries, the energy B_j^t is constrained to be within some percentage limits of the rated battery SOC capacity, modeled using section II-B

TABLE II: Comparative analyses between BFM-NL and LinDistFlow - 5 time-period horizon

Metric	BFM-NL	LinDistFlow
Largest subproblem		
Decision variables	3150	1320
Linear constraints	5831	2451
Nonlinear constraints	635	265
Simulation results		
Substation power cost (\$)	576.31	576.30
Substation real power (kW)	4308.28	4308.14
Line loss (kW)	75.99	76.12
Substation reactive power (kVAR)	574.18	656.24
PV reactive power (kVAR)	116.92	160.64
Battery reactive power (kVAR)	202.73	76.01
Computation		
Number of Iterations	-	5
Total Simulation Time (s)	521.25	49.87

TABLE V: ACOPF feasibility analyses - 10 hour

Metric	MPDOPF	OpenDSS
Full horizon		
Substation real power (kW)	8544.04	8544.40
Line loss (kW)	148.94	148.87
Substation reactive power (kVAR)	1252.03	1243.36
Max. all-time discrepancy		
Voltage (pu)		0.0002
Line loss (kW)		0.0132
Substation power (kW)		0.4002

III. CASE STUDY DEMONSTRATION

TABLE III: ACOPF feasibility analyses - 5 hour

Metric	MPDOPF	OpenDSS
Full horizon		
Substation real power (kW)	4308.14	4308.35
Line loss (kW)	76.12	76.09
Substation reactive power (kVAR)	656.24	652.49
Max. all-time discrepancy		
Voltage (pu)		0.0002
Line loss (kW)		0.0139
Substation power (kW)		0.3431

TABLE IV: Comparison between Nonlinear BFM and LinDistFlow - 10 hour

Metric	Nonlinear BFM	LinDistFlow
Largest subproblem		
Decision variables	6300	2640
Linear constraints	11636	4891
Nonlinear constraints	1270	530
Simulation results		
Substation power cost (\$)	1197.87	1197.87
Substation real power (kW)	8544.28	8544.04
Line loss (kW)	148.67	148.94
Substation reactive power (kVAR)	1092.39	1252.03
PV reactive power (kVAR)	222.59	139.81
Battery reactive power (kVAR)	388.52	310.94
Computation		
Number of Iterations	-	5
Total Simulation Time (s)	4620.73	358.69

IV. CONCLUSIONS

V. ACKNOWLEDGEMENT

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REFERENCES

- [1] N. Nazir and M. Almassalkhi, “Guaranteeing a Physically Realizable Battery Dispatch Without Charge-Discharge Complementarity Constraints,” IEEE Trans. Smart Grid, vol. 14, no. 3, pp. 2473–2476, Sep. 2021.