# Cheetah MPC

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## Conventions

Notation	
i	ith leg
$\mathcal{B}$	left subscript for body coordinate system
$[\mathbf{x}]_{\times} \in \mathbb{R}^{3 \times 3}$	skew-symmetric matrix, $[\mathbf{x}]_{\times}\mathbf{y} = \mathbf{x} \times \mathbf{y}$
$\mathbf{\Theta} = [\phi, \theta, \psi]^T$	orientation as ZYX Euler angles
$\mathbf{J}_i \in \mathbb{R}^{3 imes 3}$	foot Jacobain
$oldsymbol{\Lambda}_i \in \mathbb{R}^{3 imes 3}$	operational space inertia matrix
$\mathbf{K}_p, \mathbf{K}_d \in \mathbb{R}^{3 \times 3}$	diagonal positive definite pd gain matrices

#### **Dynamics** $\mathbf{2}$

$$\ddot{\mathbf{p}} = \frac{\sum_{i=1}^{n} \mathbf{f}_i}{m} - \mathbf{g} \tag{1}$$

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$$\frac{\mathrm{d}}{\mathrm{d}t}(\mathbf{I}\boldsymbol{\omega}) = \sum_{i=1}^{n} \mathbf{r}_{i} \times \mathbf{f}_{i}$$
(2)

$$\dot{\mathbf{R}} = [\boldsymbol{\omega}]_{\times} \mathbf{R} \tag{3}$$

$$\mathbf{R} = \mathbf{R}_z(\psi)\mathbf{R}_y(\theta)\mathbf{R}_x(\phi) \tag{4}$$

$$\mathbf{R} = \mathbf{R}_{z}(\psi)\mathbf{R}_{y}(\theta)\mathbf{R}_{x}(\phi)$$

$$\frac{\mathrm{d}}{\mathrm{d}t}(\mathbf{I}\boldsymbol{\omega}) = \mathbf{I}\dot{\boldsymbol{\omega}} + \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega}) \approx \mathbf{I}\dot{\boldsymbol{\omega}}$$
(5)

$$\boldsymbol{\omega} = \begin{bmatrix} \cos(\theta)\cos(\psi) & -\sin(\psi) & 0\\ \cos(\theta)\sin(\psi) & \cos(\psi) & 0\\ -\sin(\theta) & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi}\\ \dot{\theta}\\ \dot{\psi} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} \cos(\psi)/\cos(\theta) & \sin(\psi)/\cos(\theta) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi)\tan(\theta) & \sin(\psi)\tan(\theta) & 1 \end{bmatrix} \boldsymbol{\omega}$$

$$\approx \begin{bmatrix} \cos(\psi) & \sin(\psi) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \boldsymbol{\omega} \approx \mathbf{R}_{z}^{\mathsf{T}}(\psi)\boldsymbol{\omega}$$

$$(6)$$

$$\approx \begin{bmatrix} \cos(\psi) & \sin(\psi) & 0 \\ -\sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \boldsymbol{\omega} \approx \mathbf{R}_z^{\top}(\psi) \boldsymbol{\omega}$$
 (7)

## 3 State Space Model

$$\frac{\mathrm{d}}{\mathrm{d}t}\hat{\mathbf{\Theta}} = R_z(\psi)\hat{\mathbf{\Theta}} \tag{8}$$

$$\frac{\mathrm{d}}{\mathrm{d}t}\hat{\mathbf{p}} = \hat{\mathbf{p}} \tag{9}$$

$$\frac{\mathrm{d}}{\mathrm{d}t}\hat{\omega} = \hat{\mathbf{I}}^{-1} \sum_{i=1}^{n} \mathbf{r}_{i} \times \mathbf{f}_{i} = \hat{\mathbf{I}}^{-1} \left( \left[ \mathbf{r}_{1} \right]_{\times} \mathbf{f}_{1} + \dots + \left[ \mathbf{r}_{n} \right]_{\times} \mathbf{f}_{n} \right)$$
(10)

$$\frac{\mathrm{d}}{\mathrm{d}t}\hat{\hat{\mathbf{p}}} = \frac{\sum_{i=1}^{n} \mathbf{f}_{i}}{m} - \mathbf{g} = \frac{\mathbf{f}_{1} + \dots + \mathbf{f}_{n}}{m} - \mathbf{g}$$
(11)

$$\frac{\mathrm{d}}{\mathrm{d}t} \begin{bmatrix} \hat{\mathbf{\Theta}} \\ \hat{\mathbf{p}} \\ \hat{\mathbf{p}} \\ \hat{\mathbf{p}} \\ \mathbf{g} \end{bmatrix} = \begin{bmatrix} \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{R}_{z}(\psi) & \mathbf{0}_{3} & \mathbf{0}_{3\times1} \\ \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{I}_{3} & \mathbf{0}_{3\times1} \\ \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3\times1} \\ \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3} & \mathbf{0}_{3} & [0 \ 0 \ 1]^{T} \\ \mathbf{0}_{1\times3} & \mathbf{0}_{1\times3} & \mathbf{0}_{1\times3} & \mathbf{0}_{1\times3} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \hat{\mathbf{\Theta}} \\ \hat{\mathbf{p}} \\ \hat{\mathbf{p}} \\ \hat{\mathbf{p}} \\ \mathbf{g} \end{bmatrix}$$
(12)

$$+\begin{bmatrix} \mathbf{0}_{3} & \cdots & \mathbf{0}_{3} \\ \mathbf{0}_{3} & \cdots & \mathbf{0}_{3} \\ \hat{\mathbf{I}}^{-1} \left[ \mathbf{r}_{1} \right]_{\times} & \cdots & \hat{\mathbf{I}}^{-1} \left[ \mathbf{r}_{4} \right]_{\times} \\ \mathbf{I}_{3}/m & \cdots & \mathbf{I}_{3}/m \\ \mathbf{0}_{1\times3} & \cdots & \mathbf{0}_{1\times3} \end{bmatrix} \begin{bmatrix} \mathbf{f}_{1} \\ \vdots \\ \mathbf{f}_{4} \end{bmatrix}$$

$$(13)$$

$$\dot{\mathbf{x}}(t) = \mathbf{A}_c(\psi)\mathbf{x}(t) + \mathbf{B}_c(\mathbf{r}_1, \dots, \mathbf{r}_n, \psi)\mathbf{u}(t)$$

where  $\mathbf{A}_c \in \mathbb{R}^{13 \times 13}$  and  $\mathbf{B}_c \in \mathbb{R}^{13 \times 3n}$ 

### 4 ZOH Discretization

Given a linear system  $\dot{x} = Ax + Bu$  and its solution

$$\mathbf{x}(t) = e^{\mathbf{A}(t-t_0)}\mathbf{x}(t_0) + \int_{t_0}^{t} e^{\mathbf{A}(t-\tau)}\mathbf{B}\mathbf{u}(\tau)d\tau$$

Let  $t_0 = t_k, t = t_{k+1}$ , and  $t_{k+1} - t_k = T$ . Therefore,

$$\mathbf{x}_{k+1} = e^{\mathbf{A}T}\mathbf{x}_k + \int_{t_k}^{t_{k+1}} e^{\mathbf{A}(t_{k+1} - \tau)} \mathbf{B} \mathbf{u}(\tau) d\tau$$
$$= e^{\mathbf{A}T}\mathbf{x}_k + \int_{t_k}^{t_{k+1}} e^{\mathbf{A}(t_{k+1} - \tau)} \mathbf{B} d\tau \mathbf{u}_k$$

Let  $\tau' = t_{k+1} - \tau$ , we have

$$\int_{t_k}^{t_{k+1}} e^{\mathbf{A}(t_{k+1}-\tau)} \mathbf{B} d\tau = \int_{T}^{0} e^{\mathbf{A}\tau'} \left(-d\tau'\right) \mathbf{B} = \int_{0}^{T} e^{\mathbf{A}\tau} d\tau \mathbf{B}$$

Thus,  $\mathbf{x}_{k+1} = \mathbf{A}_d \mathbf{x}_k + \mathbf{B}_d \mathbf{u}_k$ , where  $\mathbf{A}_d = e^{\mathbf{A}T}$  and  $\mathbf{B}_d = \int_0^T e^{\mathbf{A}\tau} d\tau \mathbf{B}$ 

$$\mathbf{x}_{k+1} = \mathbf{A}_d \mathbf{x}_k + \mathbf{B}_d \mathbf{u}_k \tag{14}$$

$$\mathbf{A}_d = e^{\mathbf{A}T} \tag{15}$$

$$\mathbf{B}_d = \int_0^T e^{\mathbf{A}\tau} d\tau \mathbf{B} \tag{16}$$

## 5 MPC Formulation

$$\begin{aligned} \min_{\mathbf{x}, \mathbf{u}} \sum_{i=0}^{k-1} \|\mathbf{x}_{i+1} - \mathbf{x}_{i+1, \text{ref}}\|_{\mathbf{Q}_i} + \|\mathbf{u}_i\|_{\mathbf{R}_i} \\ subject \ to \quad \mathbf{x}_{i+1} &= \mathbf{A}_i \mathbf{x}_i + \mathbf{B}_i \mathbf{u}_i, i = 0 \dots k-1 \\ \underline{\mathbf{c}}_i &\leq \mathbf{C}_i \mathbf{u}_i \leq \overline{\mathbf{c}}_i, i = 0 \dots k-1 \\ \mathbf{D}_i \mathbf{u}_i &= 0, i = 0 \dots k-1 \\ f_{\min} &\leq f_z \leq f_{\max} \\ -\mu f_z &\leq \pm f_x \leq \mu f_z \\ -\mu f_z &\leq \pm f_y \leq \mu f_z \end{aligned}$$

## 6 QP Formulation

$$\begin{aligned} \boldsymbol{x_k} &= \mathbf{A}^k \boldsymbol{x}_0 + \sum_{i=0}^{k-1} \mathbf{A}^{k-1-i} \mathbf{B} \mathbf{u}_i \\ \begin{bmatrix} \boldsymbol{x}_1 \\ \boldsymbol{x}_2 \\ \vdots \\ \boldsymbol{x}_k \end{bmatrix} &= \begin{bmatrix} \mathbf{A}^1 \\ \mathbf{A}^2 \\ \vdots \\ \mathbf{A}^k \end{bmatrix} \boldsymbol{x}_0 + \begin{bmatrix} \mathbf{0} & & \cdots & \mathbf{0} \\ \mathbf{B} & \mathbf{0} & & \cdots & \mathbf{0} \\ \mathbf{A} \mathbf{B} & \mathbf{B} & \mathbf{0} & \cdots & \mathbf{0} \\ \vdots & & & \ddots & \vdots \\ \mathbf{A}^{k-1} \mathbf{B} & \mathbf{A}^{k-1} \mathbf{B} & \mathbf{0} & \cdots & \mathbf{B} \end{bmatrix} \begin{bmatrix} \mathbf{u}_0 \\ \mathbf{u}_1 \\ \vdots \\ \mathbf{u}_{k-1} \end{bmatrix} \\ & & & & & \\ \min_{\mathbf{U}} & \frac{1}{2} \mathbf{U}^{\mathsf{T}} \mathbf{H} \mathbf{U} + \mathbf{U}^{\mathsf{T}} \mathbf{g} \\ \text{s. t.} & & & & \\ \mathbf{c} \leq \mathbf{C} \mathbf{U} \leq \overline{\mathbf{c}} \end{aligned}$$

$$\mathbf{H} = 2\left(\mathbf{B}_{qp}^{L}\mathbf{B}_{qp} + \mathbf{K}\right) \tag{17}$$

$$\mathbf{g} = 2\mathbf{B}_{\mathrm{qp}}^{\mathsf{T}} \mathbf{L} \left( \mathbf{A}_{\mathrm{qp}} \mathbf{x}_{0} - \mathbf{y} \right) \tag{18}$$

### 7 Ground Normal Estimation

To enable the ability to traverse stairs and sloped terrain without vision, we use measurements of each footstep location

$$\boldsymbol{p}_i = (p_i^x, p_i^y, p_i^z)$$

to approximate the local slope of the walking surface.

The walking surface is modeled as a plane:

$$z(x,y) = a_0 + a_1 x + a_2 y$$

Coefficients  $\boldsymbol{a} = (a_0, a_1, a_2)^T$  are obtained through the solution of the least squares problem

$$oldsymbol{a} = egin{pmatrix} oldsymbol{W}^T oldsymbol{W}^T oldsymbol{p}^z \ oldsymbol{W} = egin{bmatrix} oldsymbol{1} & oldsymbol{p}^x & oldsymbol{p}^y \end{bmatrix}_{4 imes 3}$$

where  $\mathbf{p}^{x} = (p_{1}^{x}, p_{2}^{x}, p_{3}^{x}, p_{4}^{x})$