

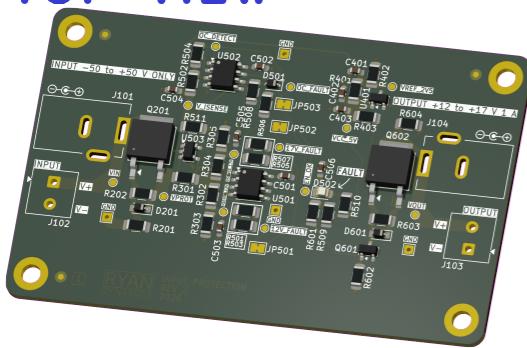
# INPUT PROTECTION

## VARIANT: RELEASED

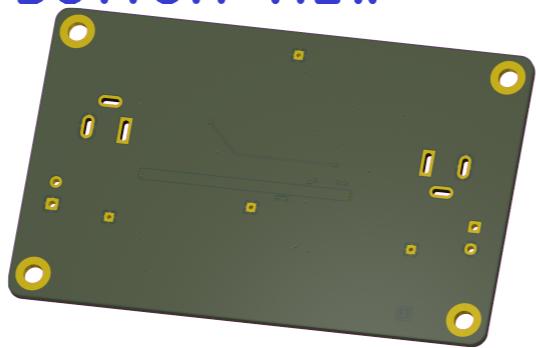
2026-02-18  
REV 1.1.0

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### TOP VIEW



### BOTTOM VIEW



### NOTES

COMMENT

NOT FITTED COMPONENTS MARKED AS

DRAFT – EARLY STAGE SCHEMATIC CAPTURE

PRELIMINARY – LATE STAGE SCHEMATIC CAPTURE

CHECKED – PCB LAYOUT CHECKED, CONTACT ENGINEER IF MISTAKE FOUND

RELEASED – READY FOR PRODUCTION

### DESIGN CONSIDERATIONS

DESIGN NOTE:  
Example text for informational design notes.

DESIGN NOTE:  
Example text for debug notes.

DESIGN NOTE:  
Example text for cautionary design notes.

DESIGN NOTE:  
Example text for critical design notes.

LAYOUT NOTE:  
Example text for critical layout guidelines.

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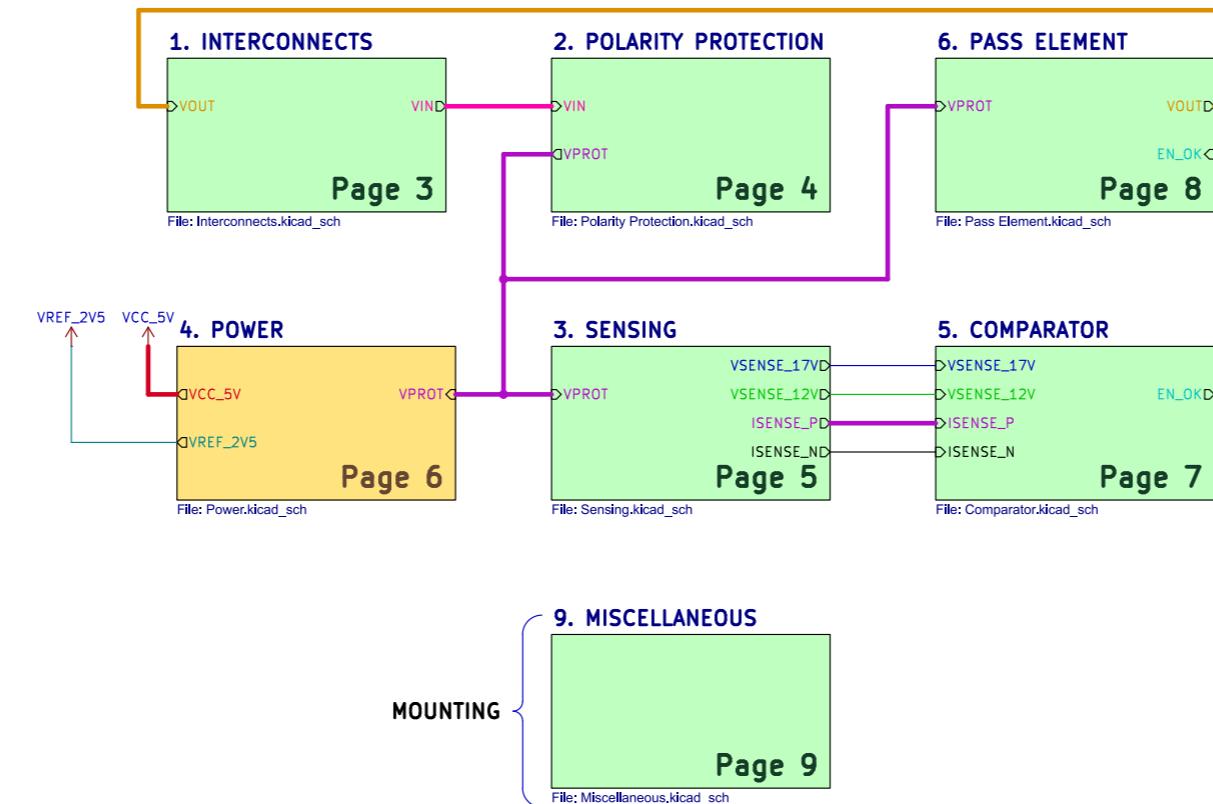
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/	0313524		
FILENAME	VARIANT	RELEASED	REVISION
Input-Protection.kicad_sch			1.1.0

# [2] ARCHITECTURE



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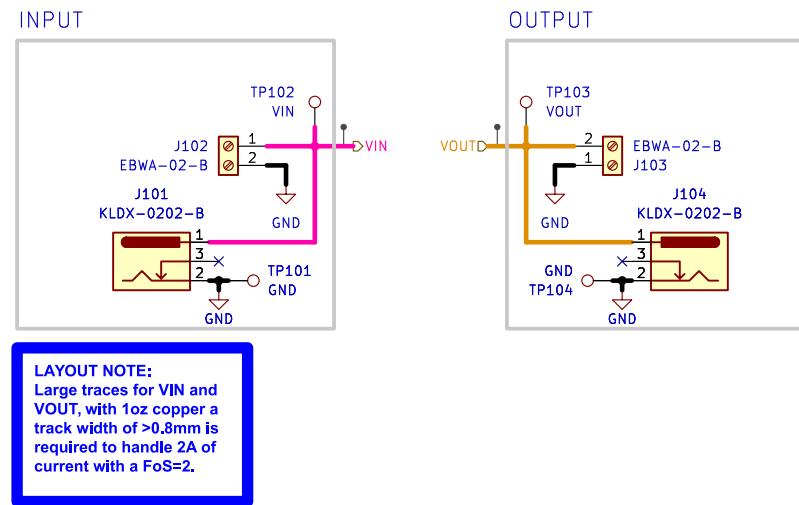
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/ARCHITECTURE/	0313524	ARCHITECTURE			
FILENAME	VARIANT	RELEASED	REVISION	SHEET	F
Project Architecture.kicad_sch			1.1.0	2 OF 10	A3

# [3] 1. INTERCONNECTS



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/ARCHITECTURE/1. INTERCONNECTS/

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DRAWING No  
1. INTERCONNECTS

FILENAME Interconnects.kicad\_sch

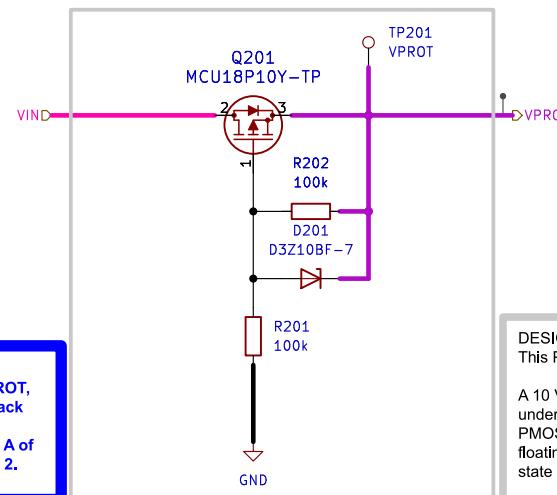
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# [4] 2. POLARITY PROTECTION



**LAYOUT NOTE:**  
Large traces for VPROT, with 1oz copper a track width of >0.8 mm is required to handle 2 A of current with a FoS = 2.

**DESIGN NOTE:**  
This PMOS is acting as an ideal diode [1].

A 10 V zener from gate to source limits  $V_{GS} \leq 10$  V under all VIN and transient conditions to protect the PMOS. A 100k gate to source resistor stops the gate floating. A 100k gate pulldown resistor sets default state to OFF when no voltage at VIN is present.

[1] <https://www.ti.com/lit/an/slvae57b/slvae57b.pdf?ts=1770319054914>

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/ARCHITECTURE/ 2. POLARITY PROTECTION/

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0313524 POLARITY PROTECTION

FILENAME Polarity Protection.kicad\_sch

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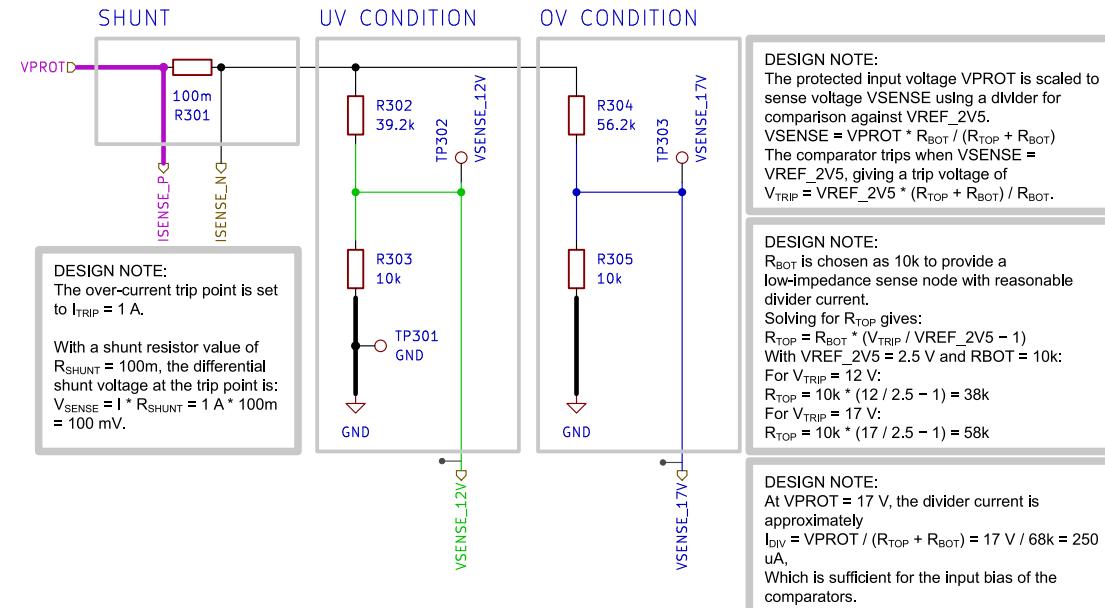
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# [5] 3. SENSING



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/ARCHITECTURE/3. SENSING/

FILENAME Sensing.kicad\_sch

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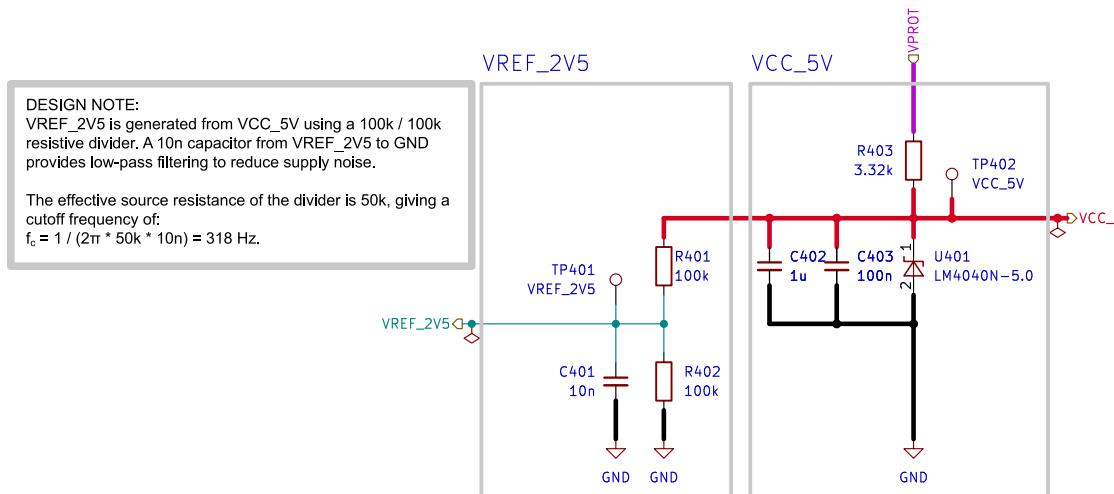
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# [6] 4. POWER



**DESIGN NOTE:**  
Per TI [2], choose the series resistor  $R_s$  such that  $I_{RMIN} < I_R < I_{RMAX}$  across the full input range, while supplying the worst-case load current from VCC\_5V.

Assume:  
 $V_{IN,MIN} = 12 \text{ V}$ ,  $V_{IN,MAX} = 50 \text{ V}$ ,  $V_{OUT} = 5 \text{ V}$   
 $I_{RMAX} = 15 \text{ mA}$ ,  $I_{RMIN} = 75 \mu\text{A}$   
Worst-case VCC\_5V load current with EN\_OK high is estimated as:  
 $I_{LOAD,MAX} = I_{DIV,2V5} + I_{Q,LM393} + I_{Q,INA169} + I_{B,NPN}$   
where:  
 $I_{DIV,2V5} = 5 \text{ V} / (100k + 100k) = 25 \mu\text{A}$   
 $I_{Q,LM393} = 2 * 600 \mu\text{A} = 1.2 \text{ mA}$  (two LM393 packages)  
 $I_{Q,INA169} = 125 \mu\text{A}$   
 $I_{B,NPN} = (5 \text{ V} - 0.7 \text{ V}) / 10k = 430 \mu\text{A}$   
Note:  
The fault LED current is drawn only when EN\_OK is low and is therefore not included in the EN\_OK-high load budget.  
Thus:  
 $I_{LOAD,MAX} = 25 \mu\text{A} + 1.2 \text{ mA} + 125 \mu\text{A} + 430 \mu\text{A} = 1.78 \text{ mA}$   
This gives:  
 $R_s,MAX = (V_{IN,MIN} - V_{OUT}) / (I_{LOAD,MAX} + I_{RMIN}) = 7 \text{ V} / (1.78 \text{ mA} + 0.075 \text{ mA}) = 3.8k$   
 $R_s,MIN = (V_{IN,MAX} - V_{OUT}) / I_{RMAX} = 45 \text{ V} / 15 \text{ mA} = 3k$   
 $R_s$  (R403) is selected as 3.32k to ensure regulation at  $V_{IN,MIN}$  while limiting shunt current at  $V_{IN,MAX}$ .

[2] <https://www.ti.com/lit/ds/symlink/lm4040-n.pdf?ts=1752678691365>

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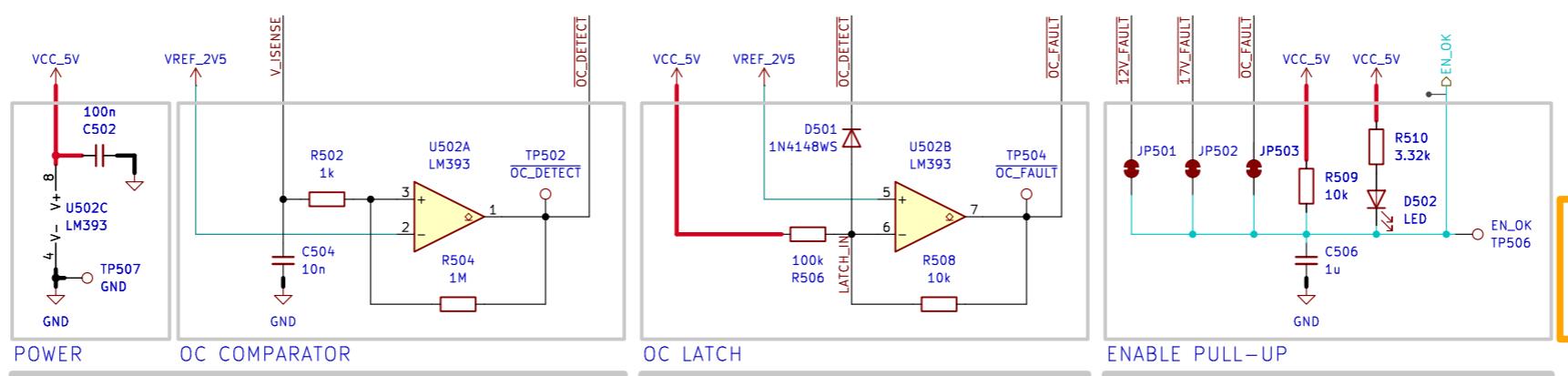
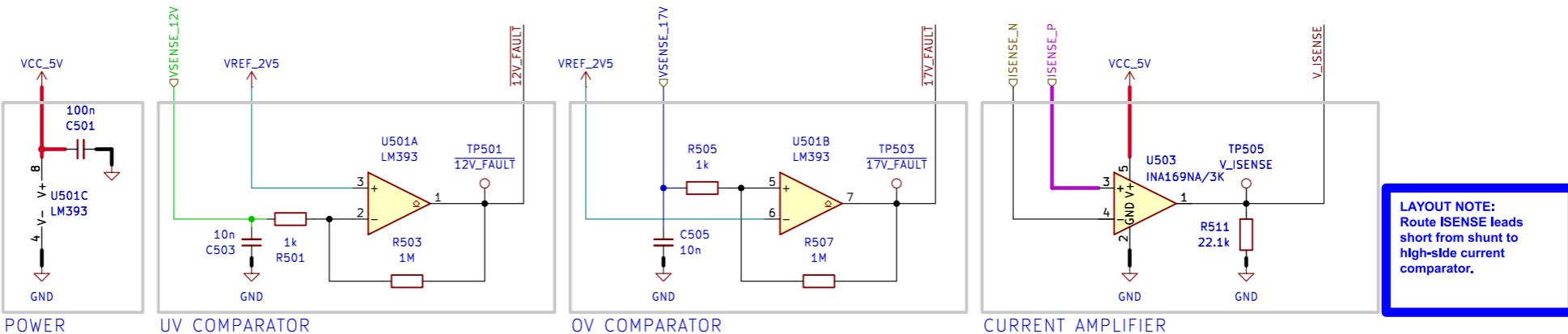
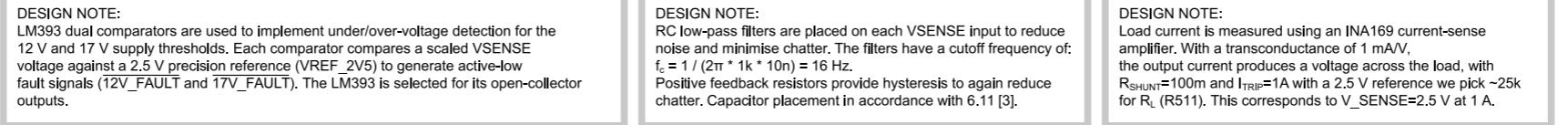
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/ARCHITECTURE/4. POWER/	0313524			
FILENAME	VARIANT	RELEASED	REVISION	SHEET
Power.kicad_sch			1.1.0	6 OF 10

# [7] 5. COMPARATOR

[3] <https://www.ti.com/lit/an/sn0aa35f/sn0aa35f.pdf?ts=1770697404856>



**DESIGN NOTE:**  
A second LM393 comparator monitors the V\_ISENSE signal from the current-sense amplifier and compares it against the 2.5 V reference to detect over-current conditions. When the sensed current exceeds the programmed threshold, the comparator output asserts an active-low over-current fault signal (OC\_FAULT).

**DESIGN NOTE:**  
The spare LM393 comparator is configured as a latch. This prevents "hiccupps". OC\_DETECT is reverse bias diode-coupled into the latch input. Once an over-current condition occurs, the latch forces OC\_FAULT low and maintains the fault state until power is removed.

**DESIGN NOTE:**  
All active-low fault signals (12V\_FAULT, 17V\_FAULT, and OC\_FAULT) are combined using wired-AND logic enabled by the open-collector comparator outputs. A single pull-up resistor biases EN\_OK high during normal operation. Assertion of any fault pulls EN\_OK low, disabling the pass MOSFET.

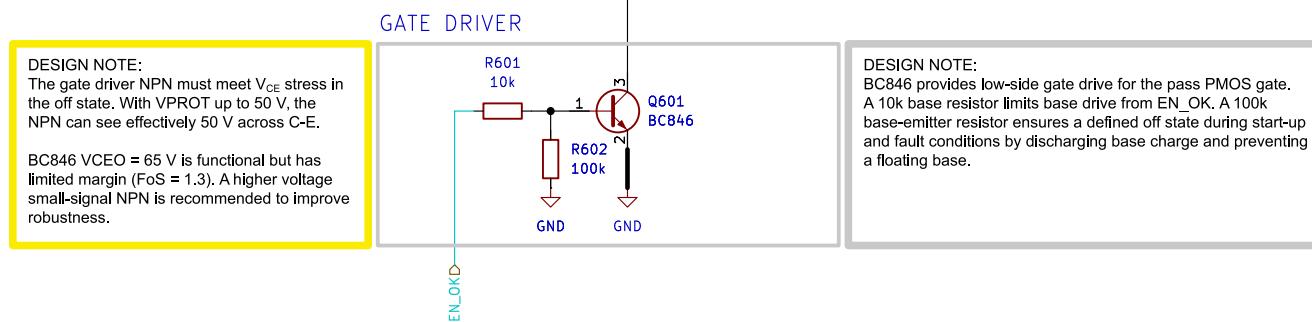
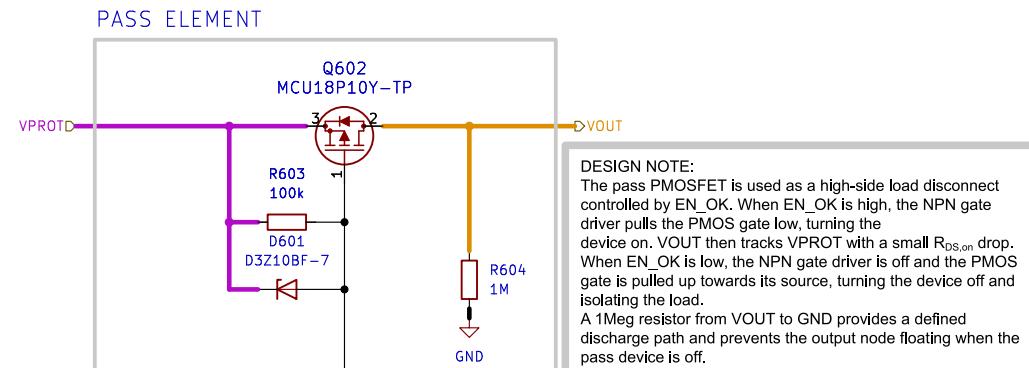
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FILENAME	Comparator.kicad_sch
DRAWING No	
0313524	5. COMPARATOR
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RELEASED	REVISION
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# [8] 6. PASS ELEMENT



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6. PASS ELEMENT

FILENAME

Pass Element.kicad\_sch

VARIANT

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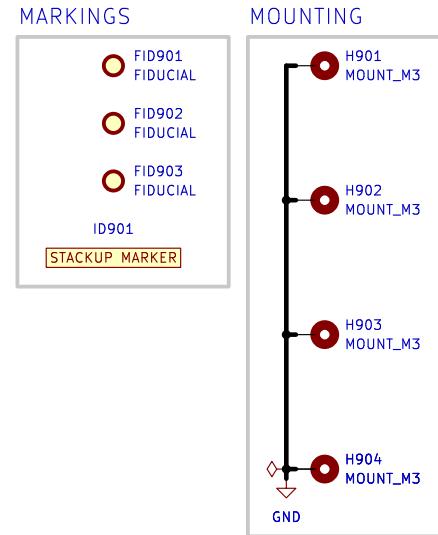
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# [9] 9. MISCELLANEOUS



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9. MISCELLANEOUS

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FILENAME Miscellaneous.kicad\_sch

VARIANT

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# [10] REVISION HISTORY

## A Version 1.0.0 – 2026–02–11

### Fixed

- N/A

### Added

- Schematic capture and layout of a -50 to +50 V input +12 to +17 V output 1A protection PCBA

### Changed

- N/A

### Removed

- N/A

## B Version 1.1.0 – 2026–02–18

### Fixed

- Tidied up some routing issues

### Added

- N/A

### Changed

- Changed fiducials to be circular
- Changed info block

### Removed

- N/A

## C Version 1.1.0 – 2026–02–18

### Fixed

- Tidied up some routing issues

### Added

- N/A

### Changed

- Changed fiducials to be circular
- Changed info block

### Removed

- N/A

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FILENAME Revision History.kicad\_sch

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