

INPUT PROTECTION

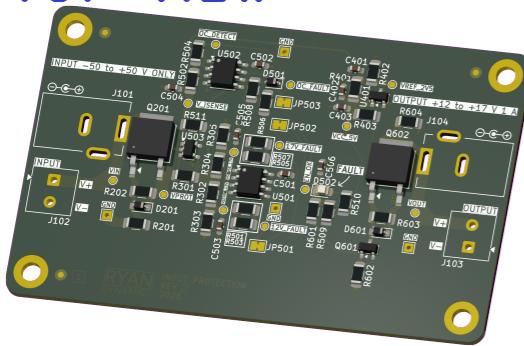
VARIANT: RELEASED

2026-02-18

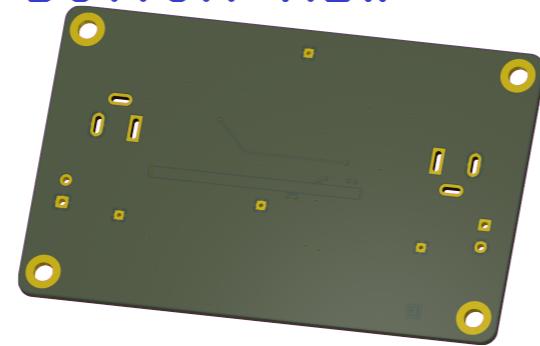
REV 1.0.0+ (Unreleased)

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TOP VIEW



BOTTOM VIEW



NOTES

COMMENT

NOT FITTED COMPONENTS MARKED AS

DRAFT – EARLY STAGE SCHEMATIC CAPTURE

PRELIMINARY – LATE STAGE SCHEMATIC CAPTURE

CHECKED – PCB LAYOUT CHECKED, CONTACT ENGINEER IF MISTAKE FOUND

RELEASED – READY FOR PRODUCTION

DESIGN CONSIDERATIONS

DESIGN NOTE:
Example text for informational design notes.

DESIGN NOTE:
Example text for debug notes.

DESIGN NOTE:
Example text for cautionary design notes.

DESIGN NOTE:
Example text for critical design notes.

LAYOUT NOTE:
Example text for critical layout guidelines.

PROJECT
ASSIGNMENT 1

DRN
2025-01-12 R. HICKS

CHK

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MFR APP

SHEET PATH

FILENAME

Input-Protection.kicad_sch

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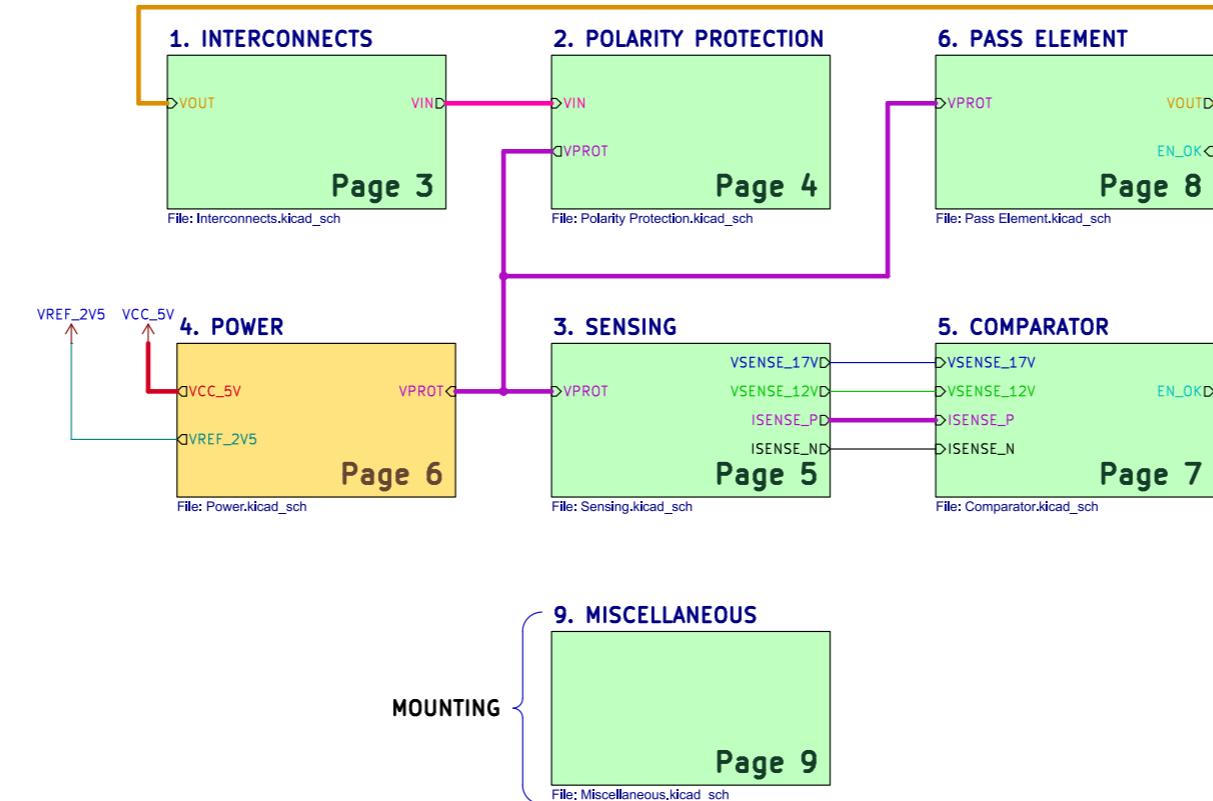
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[2] ARCHITECTURE



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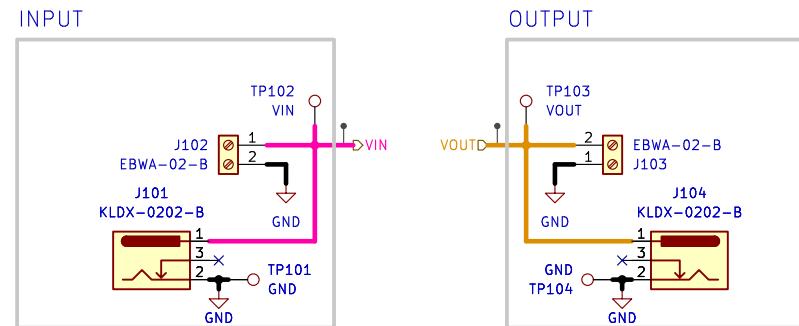


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/ARCHITECTURE/	63a4f02	ARCHITECTURE				
FILENAME	VARIANT	RELEASED	REVISION	(Unreleased)	SHEET	2 OF 10

A3

[3] 1. INTERCONNECTS



LAYOUT NOTE:
Large traces for VIN and VOUT, with 1oz copper a track width of >0.8mm is required to handle 2A of current with a FoS=2.

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/ARCHITECTURE/1. INTERCONNECTS/

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1. INTERCONNECTS

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FILENAME Interconnects.kicad_sch

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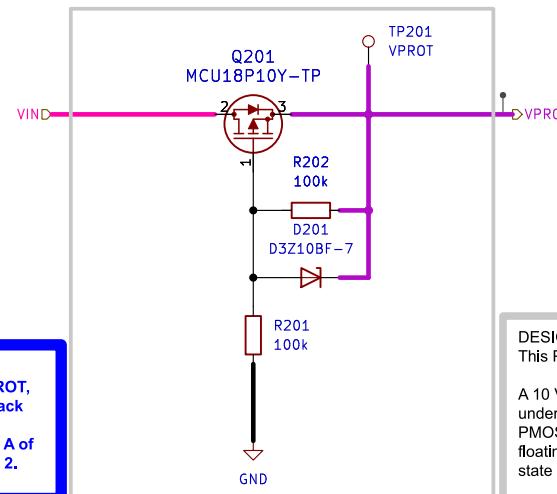
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SHEET

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[4] 2. POLARITY PROTECTION



LAYOUT NOTE:
Large traces for VPROT, with 1oz copper a track width of >0.8 mm is required to handle 2 A of current with a FoS = 2.

DESIGN NOTE:
This PMOS is acting as an ideal diode [1].

A 10 V zener from gate to source limits $V_{GS} \leq 10$ V under all VIN and transient conditions to protect the PMOS. A 100k gate to source resistor stops the gate floating. A 100k gate pulldown resistor sets default state to OFF when no voltage at VIN is present.

[1] <https://www.ti.com/lit/an/slvae57b/slvae57b.pdf?ts=1770319054914>

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/ARCHITECTURE/ 2. POLARITY PROTECTION/

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63a7f02 POLARITY PROTECTION

FILENAME Polarity Protection.kicad_sch

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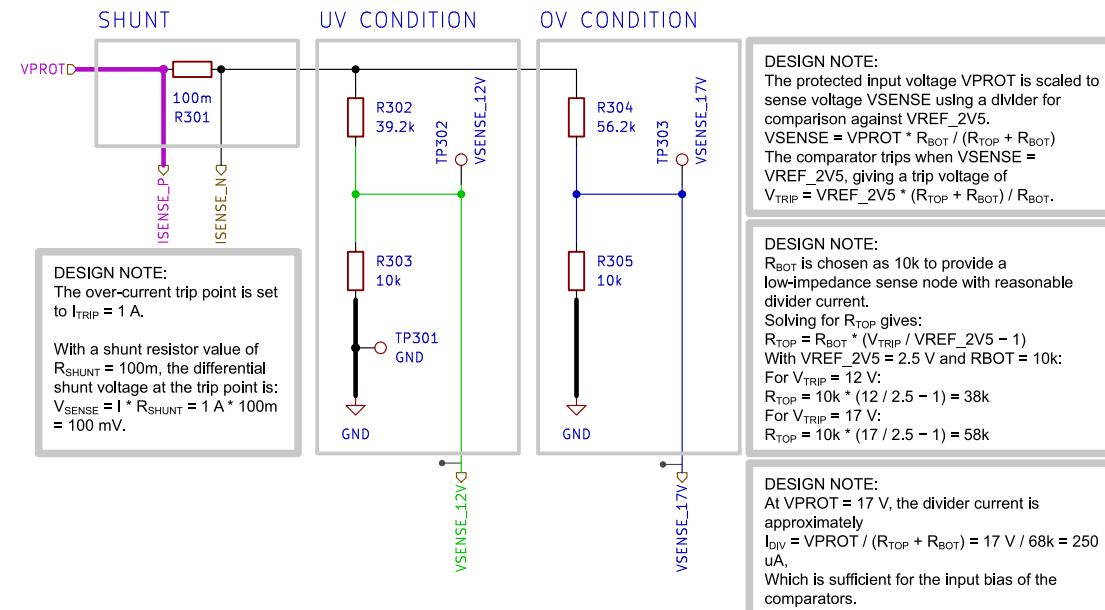
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[5] 3. SENSING



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/ARCHITECTURE/3. SENSING/

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3. SENSING

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FILENAME Sensing.kicad_sch

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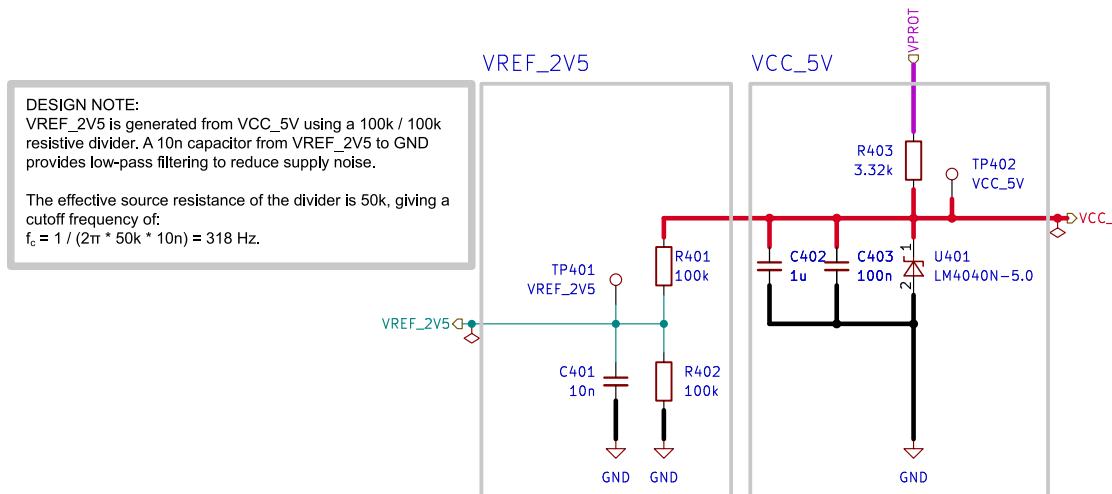
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[6] 4. POWER



DESIGN NOTE:
Per TI [2], choose the series resistor R_s such that $I_{RMIN} < I_R < I_{RMAX}$ across the full input range, while supplying the worst-case load current from VCC_5V.

Assume:
 $V_{IN,MIN} = 12 \text{ V}$, $V_{IN,MAX} = 50 \text{ V}$, $V_{OUT} = 5 \text{ V}$
 $I_{RMAX} = 15 \text{ mA}$, $I_{RMIN} = 75 \mu\text{A}$
Worst-case VCC_5V load current with EN_OK high is estimated as:
 $I_{LOAD,MAX} = I_{DIV,2V5} + I_{Q,LM393} + I_{Q,INA169} + I_{B,NPN}$
where:
 $I_{DIV,2V5} = 5 \text{ V} / (100k + 100k) = 25 \mu\text{A}$
 $I_{Q,LM393} = 2 * 600 \mu\text{A} = 1.2 \text{ mA}$ (two LM393 packages)
 $I_{Q,INA169} = 125 \mu\text{A}$
 $I_{B,NPN} = (5 \text{ V} - 0.7 \text{ V}) / 10k = 430 \mu\text{A}$

Note:
The fault LED current is drawn only when EN_OK is low and is therefore not included in the EN_OK-high load budget.
Thus:
 $I_{LOAD,MAX} = 25 \mu\text{A} + 1.2 \text{ mA} + 125 \mu\text{A} + 430 \mu\text{A} = 1.78 \text{ mA}$
This gives:
 $R_s,MAX = (V_{IN,MIN} - V_{OUT}) / (I_{LOAD,MAX} + I_{RMIN}) = 7 \text{ V} / (1.78 \text{ mA} + 0.075 \text{ mA}) = 3.8k$
 $R_s,MIN = (V_{IN,MAX} - V_{OUT}) / I_{RMAX} = 45 \text{ V} / 15 \text{ mA} = 3k$
 R_s (R403) is selected as 3.32k to ensure regulation at $V_{IN,MIN}$ while limiting shunt current at $V_{IN,MAX}$.

[2] <https://www.ti.com/lit/ds/symlink/lm4040-n.pdf?ts=1752678691365>

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/ARCHITECTURE/4. POWER/

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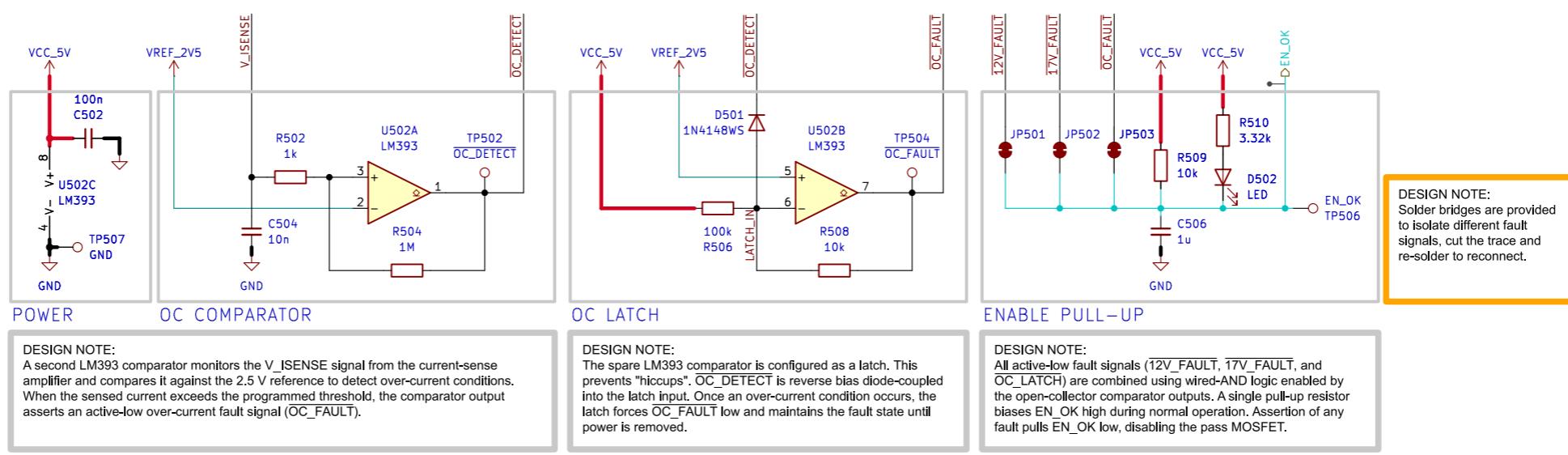
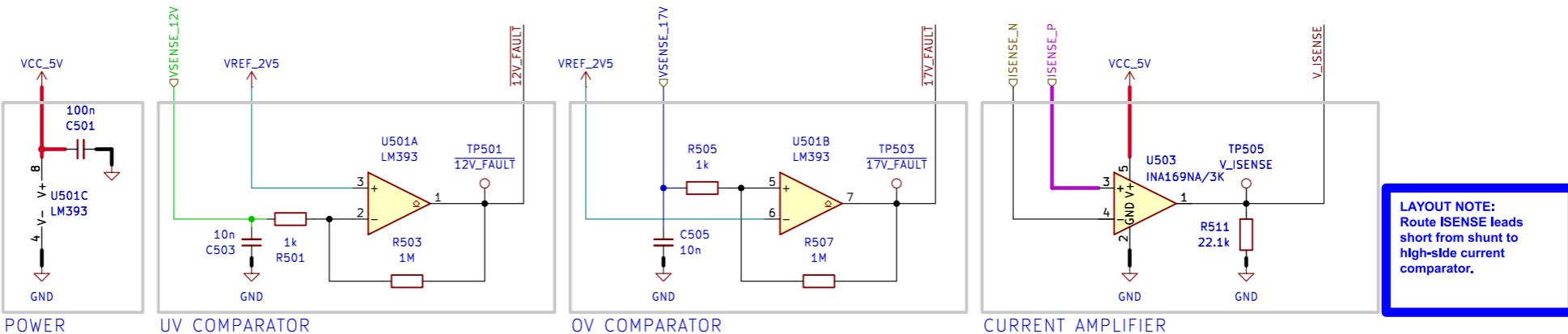
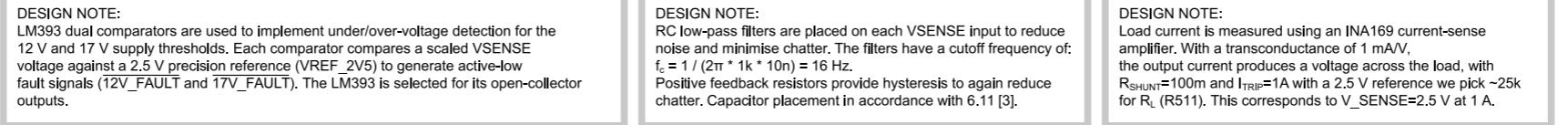
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4. POWER

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[7] 5. COMPARATOR

[3] <https://www.ti.com/lit/an/sn0aa35f/sn0aa35f.pdf?ts=1770697404856>



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SHEET PATH	GIT HASH
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FILENAME	VARIANT
Comparator.kicad_sch	RELEASED
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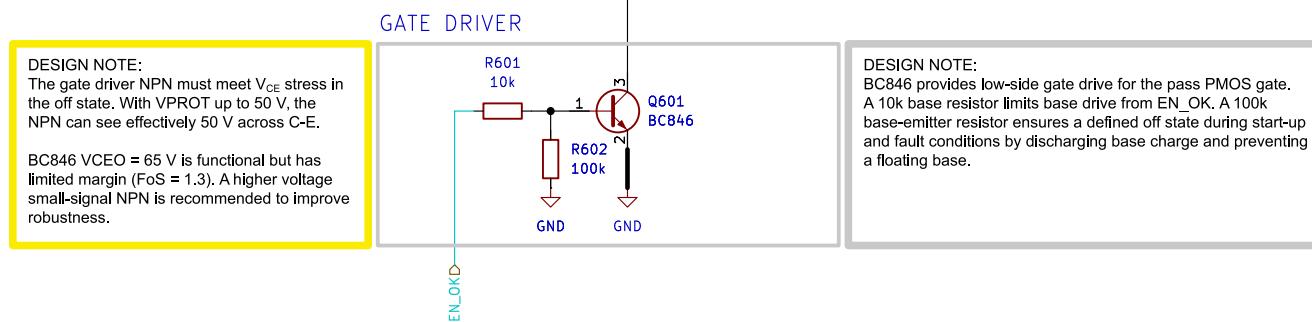
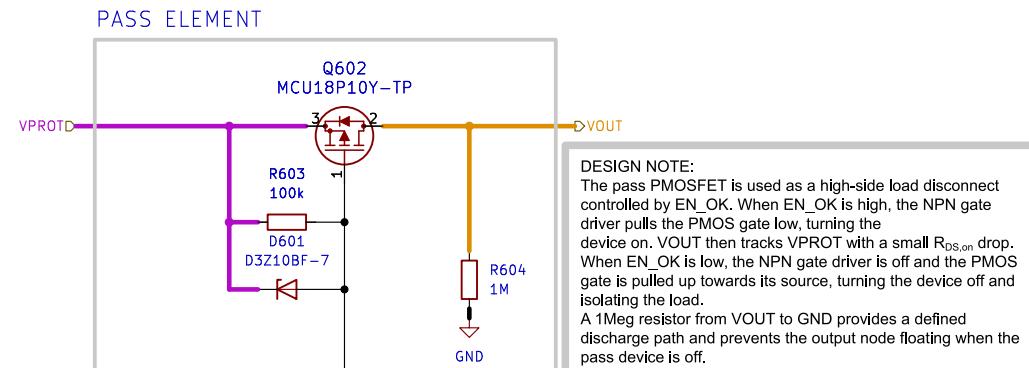


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[8] 6. PASS ELEMENT



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6. PASS ELEMENT

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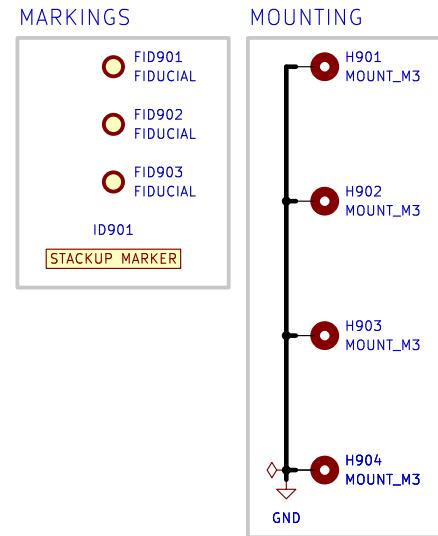


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[9] 9. MISCELLANEOUS



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9. MISCELLANEOUS

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FILENAME Miscellaneous.kicad_sch

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[10] REVISION HISTORY

A

Version 1.0.0 – 2026-02-11

Fixed

- Tidied up some routing issues

B

Added

- N/A

C

Changed

- Changed fiducials to be circular
- Changed info block

Removed

- N/A

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Revision History.kicad_sch

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