

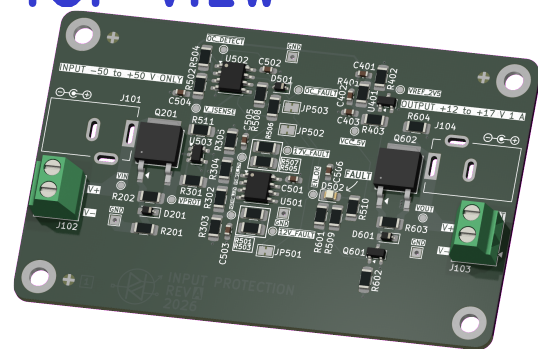
# INPUT PROTECTION

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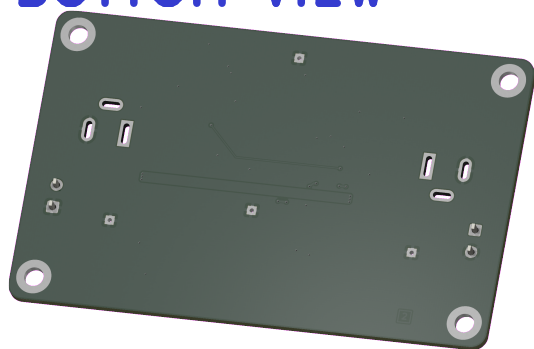
2026-02-10  
Rev + (Unreleased)

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TOP VIEW



BOTTOM VIEW



## NOTES

Comment

Not fitted components are marked as **X**

- DRAFT – Very early stage of schematic, ignore details.
- PRELIMINARY – Close to final schematic.
- CHECKED – There shouldn't be any mistakes. Contact the engineer if found.
- RELEASED – A board with this schematic has been sent to production.

## DESIGN CONSIDERATIONS

DESIGN NOTE:

Example text for informational design notes.

DESIGN NOTE:

Example text for debug notes.

DESIGN NOTE:


Example text for cautionary design notes.

DESIGN NOTE:

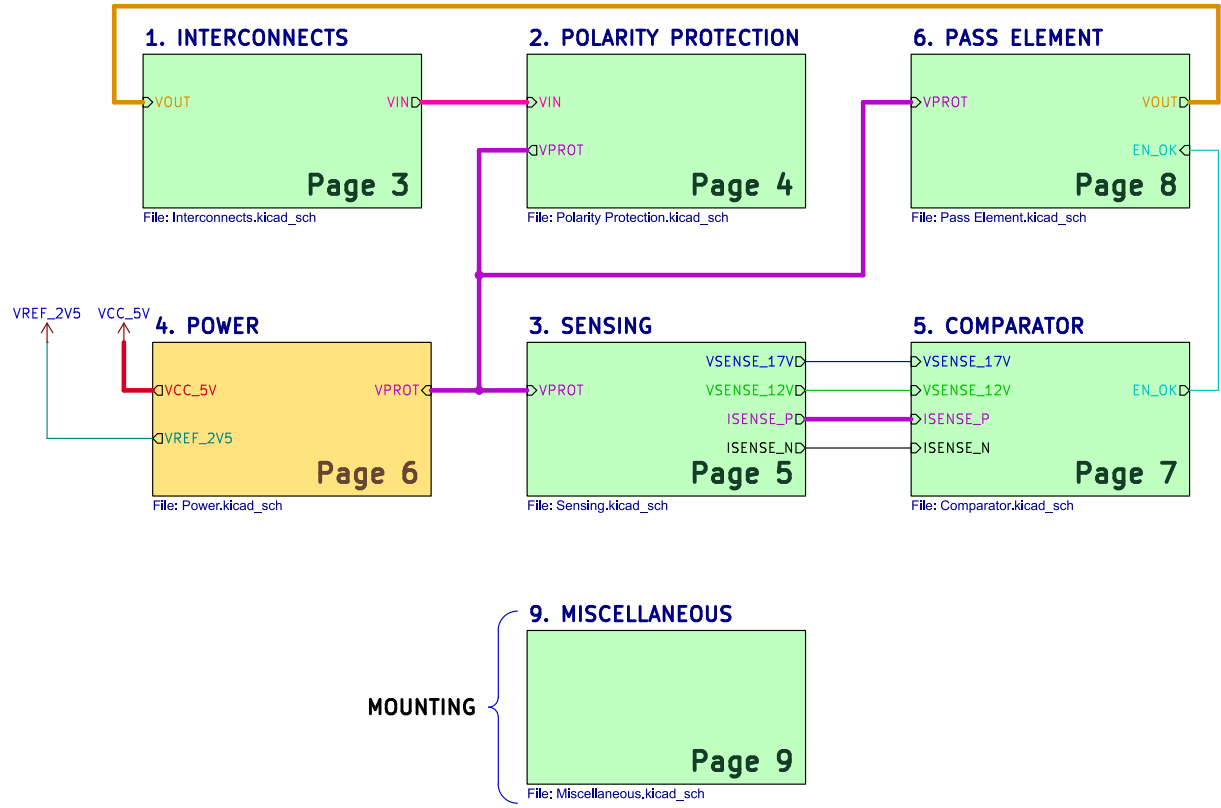
Example text for critical design notes.


LAYOUT NOTE:

Example text for critical layout guidelines.

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FILENAME	Input-Protection.kicad_sch	VARIANT	CHECKED
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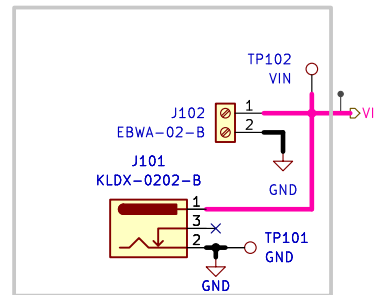
# [2] ARCHITECTURE



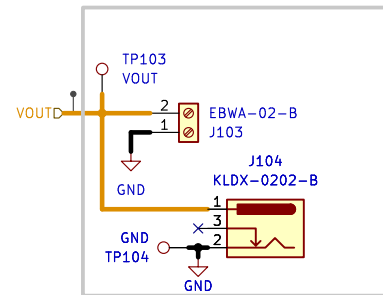
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# [3] 1. INTERCONNECTS

INPUT



OUTPUT



**LAYOUT NOTE:**  
Large traces for VIN and VOUT, with 1oz copper a track width of >0.8mm is required to handle 2A of current with a FoS=2.

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/ARCHITECTURE/1. INTERCONNECTS/

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1. INTERCONNECTS

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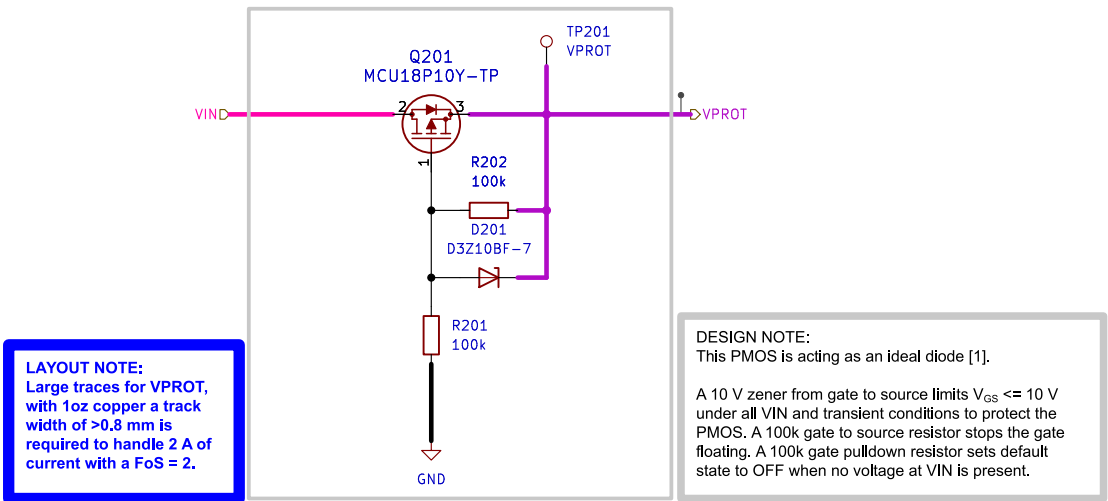
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# [4] 2. POLARITY PROTECTION



[1] <https://www.ti.com/lit/an/slvae57b/slvae57b.pdf?ts=1770319054914>

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/ARCHITECTURE/2. POLARITY PROTECTION/

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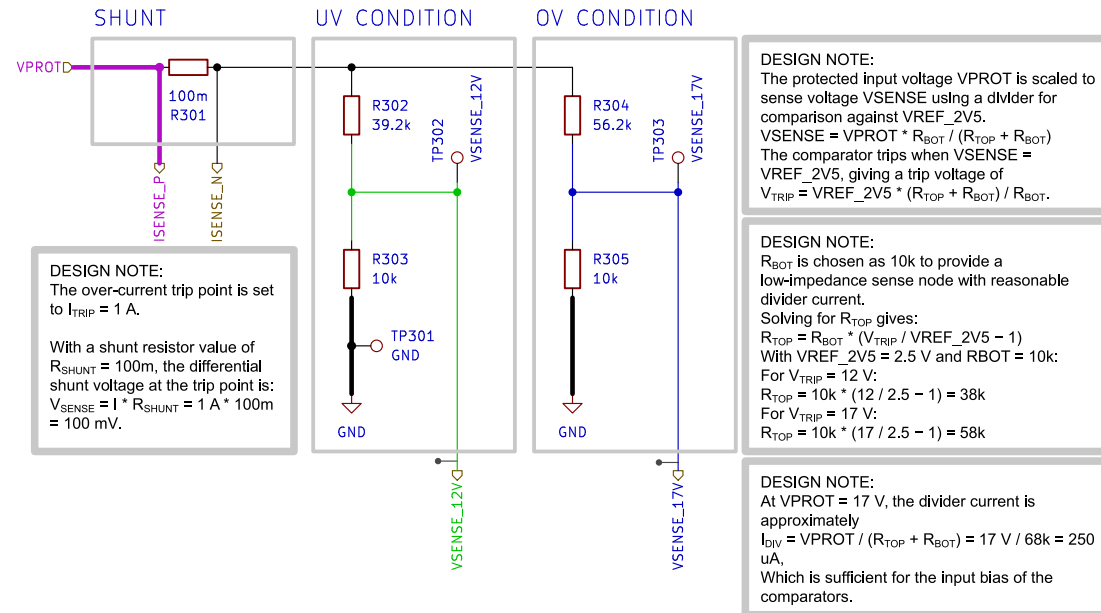
POLARITY PROTECTION

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# [5] 3. SENSING



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/ARCHITECTURE/3. SENSING/

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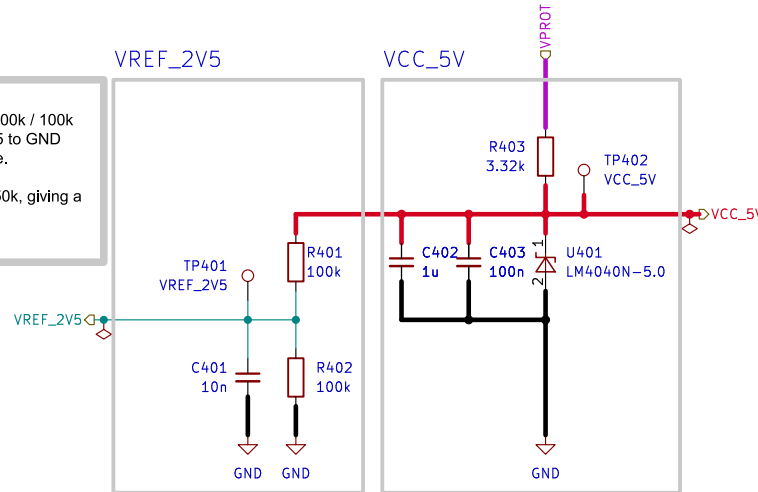
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# [6] 4. POWER

DESIGN NOTE:  
VREF\_2V5 is generated from VCC\_5V using a 100k / 100k resistive divider. A 10n capacitor from VREF\_2V5 to GND provides low-pass filtering to reduce supply noise.

The effective source resistance of the divider is 50k, giving a cutoff frequency of:  
 $f_c = 1 / (2\pi * 50k * 10n) = 318 \text{ Hz}$ .



## DESIGN NOTE:

Per TI [2], choose the series resistor  $R_S$  such that  $I_{RMIN} < I_R < I_{RMAX}$  across the full input range, while supplying the worst-case load current from VCC\_5V.

Assume:

$V_{IN,MIN} = 12 \text{ V}$ ,  $V_{IN,MAX} = 50 \text{ V}$ ,  $V_{OUT} = 5 \text{ V}$

$I_{RMAX} = 15 \text{ mA}$ ,  $I_{RMIN} = 75 \text{ uA}$

Worst-case VCC\_5V load current with EN\_OK high is estimated as:

$I_{LOAD,MAX} = I_{DIV,2V5} + I_{Q,LM393} + I_{Q,INA169} + I_{B,NPN}$

where:

$I_{DIV,2V5} = 5 \text{ V} / (100k + 100k) = 25 \text{ uA}$

$I_{Q,LM393} = 2 * 600 \text{ uA} = 1.2 \text{ mA}$  (two LM393 packages)

$I_{Q,INA169} = 125 \text{ uA}$

$I_{B,NPN} = (5 \text{ V} - 0.7 \text{ V}) / 10k = 430 \text{ uA}$

Note:

The fault LED current is drawn only when EN\_OK is low and is therefore not included in the EN\_OK-high load budget.

Thus:

$I_{LOAD,MAX} = 25 \text{ uA} + 1.2 \text{ mA} + 125 \text{ uA} + 430 \text{ uA} = 1.78 \text{ mA}$

This gives:

$R_{S,MAX} = (V_{IN,MIN} - V_{OUT}) / (I_{LOAD,MAX} + I_{RMIN}) = 7 \text{ V} / (1.78 \text{ mA} + 0.075 \text{ mA}) = 3.8k$

$R_{S,MIN} = (V_{IN,MAX} - V_{OUT}) / I_{RMAX} = 45 \text{ V} / 15 \text{ mA} = 3k$

$R_S$  (R403) is selected as 3.32k to ensure regulation at  $V_{IN,MIN}$  while limiting shunt current at  $V_{IN,MAX}$ .

[2] <https://www.ti.com/lit/ds/symlink/lm4040-n.pdf?ts=1752678691365>

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/ARCHITECTURE/4. POWER/

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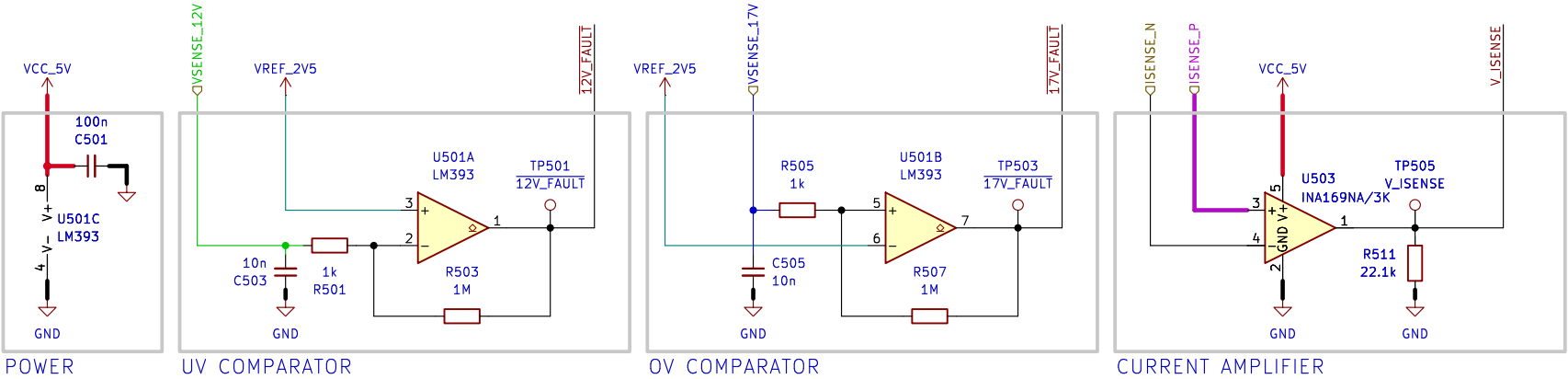
[7] 5. COMPARATOR

[3] <https://www.ti.com/lit/an/snoaa35f/snoaa35f.pdf?ts=1770697404856>

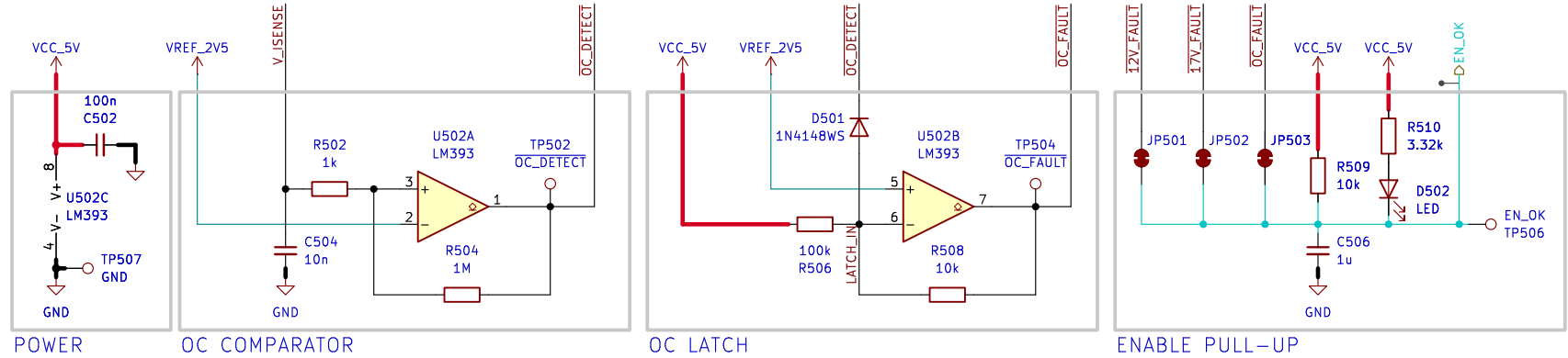
DESIGN NOTE:  
LM393 dual comparators are used to implement under/over-voltage detection for the 12 V and 17 V supply thresholds. Each comparator compares a scaled VSENSE voltage against a 2.5 V precision reference (VREF\_2V5) to generate active-low fault signals (12V\_FAULT and 17V\_FAULT). The LM393 is selected for its open-collector outputs.

DESIGN NOTE:  
RC low-pass filters are placed on each VSENSE input to reduce noise and minimise chatter. The filters have a cutoff frequency of:  $f_c = 1 / (2\pi * 1k * 10n) = 16 \text{ Hz}$ . Positive feedback resistors provide hysteresis to again reduce chatter. Capacitor placement in accordance with 6.11 [3].

DESIGN NOTE:  
Load current is measured using an INA169 current-sense amplifier. With a transconductance of 1 mA/V, the output current produces a voltage across the load, with  $R_{SHUNT}=100m$  and  $I_{TRIP}=1A$  with a 2.5 V reference we pick ~25k for  $R_L$  (R511). This corresponds to  $V_{SENSE}=2.5 \text{ V}$  at 1 A.



LAYOUT NOTE:  
Route ISENSE leads short from shunt to high-side current comparator.



DESIGN NOTE:  
Solder bridges are provided to isolate different fault signals, cut the trace and re-solder to reconnect.

DESIGN NOTE:  
A second LM393 comparator monitors the V\_ISENSE signal from the current-sense amplifier and compares it against the 2.5 V reference to detect over-current conditions. When the sensed current exceeds the programmed threshold, the comparator output asserts an active-low over-current fault signal (OC\_FAULT).

DESIGN NOTE:  
The spare LM393 comparator is configured as a latch. This prevents "hiccups". OC\_DETECT is reverse bias diode-coupled into the latch input. Once an over-current condition occurs, the latch forces OC\_FAULT low and maintains the fault state until power is removed.

DESIGN NOTE:  
All active-low fault signals (12V\_FAULT, 17V\_FAULT, and OC\_FAULT) are combined using wired-AND logic enabled by the open-collector comparator outputs. A single pull-up resistor biases EN\_OK high during normal operation. Assertion of any fault pulls EN\_OK low, disabling the pass MOSFET.

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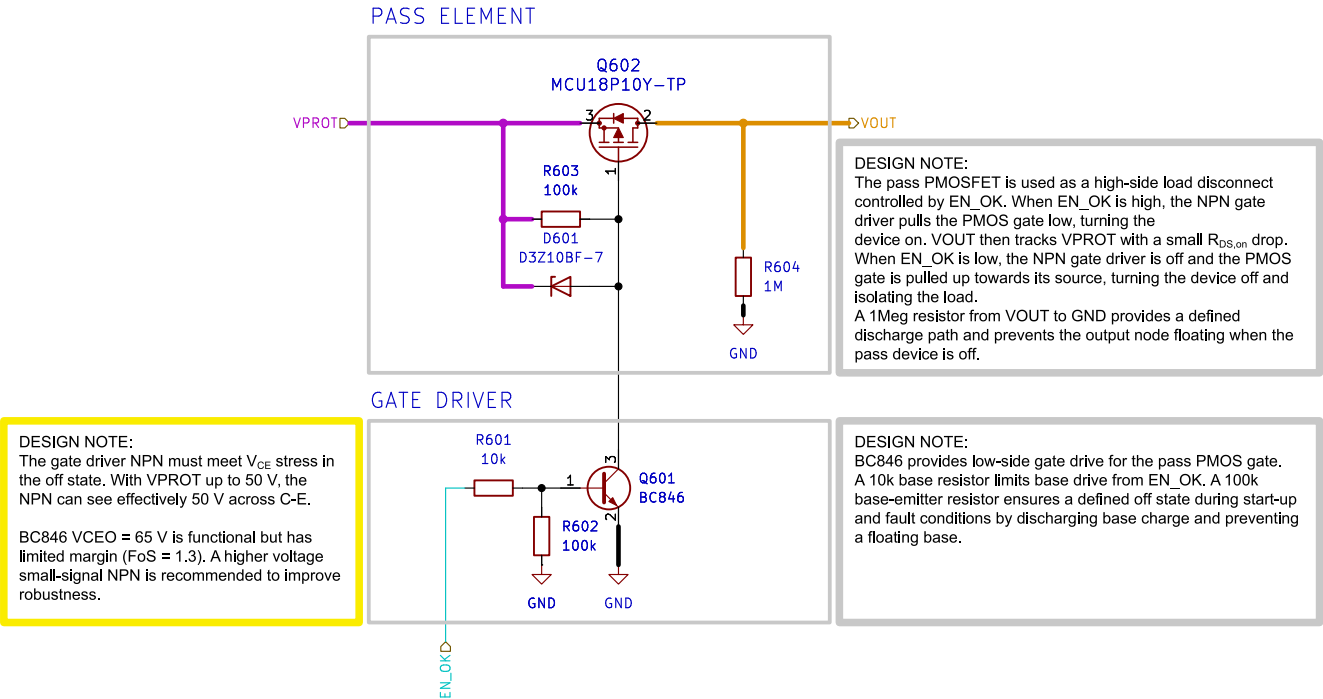
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/ARCHITECTURE/5. COMPARATOR/

[8] 6. PASS ELEMENT



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/ARCHITECTURE/6. PASS ELEMENT/

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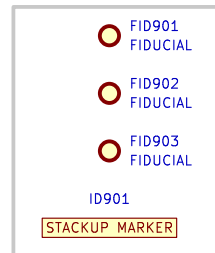
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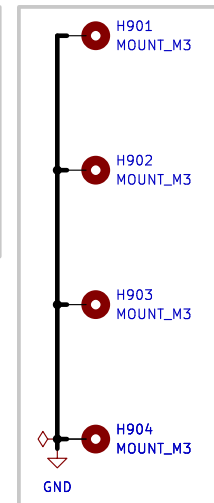



# [9] 9. MISCELLANEOUS

## MARKINGS



## MOUNTING



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FILENAME Miscellaneous.kicad_sch	VARIANT	CHECKED		
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# [10] REVISION HISTORY

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