Objectives of the WorkShop

For the same structure:

Learn to do a modeling with membrane elements, Learn to do a modeling with 3D elements, Learn to do a modeling with beam elements, Learn to do a modeling with shell elements.

Work to do

Using a 2D modelling with membrane elements verify that the assumptions of the beam theory are verified for this structure, Create a modelling with beam elements and compare the results with the previous one,

Create a modelling with shell elements and compare the results with the previous ones,

Create a 3D modelling with a cross section such as b=5 mm e=20 mm, Verify that the shear stress is constant along b and quadratic along e as the beam theory teach us.

Structure to Design

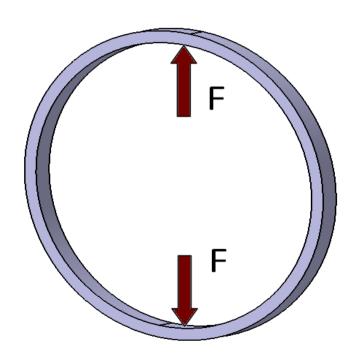
Dynamometer Ring

Width: b = 30 mm

Internal radius: Ri = 240 mm External radius: Re = 260 mm Thickness: e = (Re-Ri) = 20 mm Young Modulus: E = 200 000 MPa

Poisson's ratio: 1/3

F = 2000 N

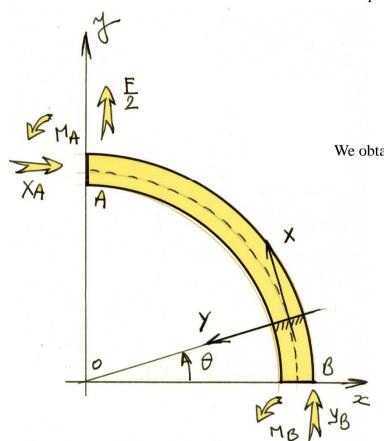


Analytical Modelling with the theory of beams

The hyperstatic structure is a closed beam, with two planes of symmetry.

Hence, we can study a quarter part of the ring.

If we write the equilibrium of this structure we obtain 3 equations for 4 reactions unknown.



$$\begin{cases} X_A = 0 \\ \frac{F}{2} + Y_B = 0 \\ M_A + M_B + RY_B = 0 \end{cases}$$

We obtain a new equation by using the theorem of Castigliano.

$$\theta_A^z = \frac{\partial W}{\partial M_A} = 0$$

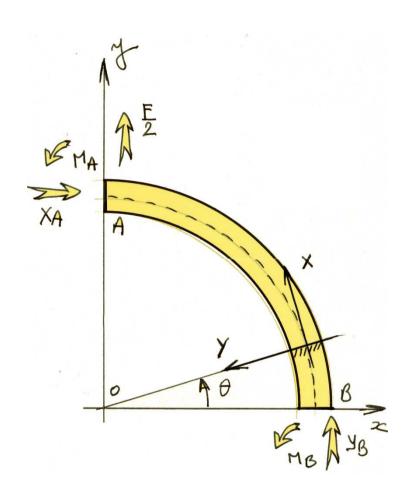
The internal energy is equal to:

$$W = \int_0^{\pi/2} \left(\frac{1}{2} \frac{N_X^2}{ES} + \frac{1}{2} \frac{T_Y^2}{Gk_Y S} + \frac{1}{2} \frac{M_Z^2}{EI_Z} \right) r d\theta$$

With

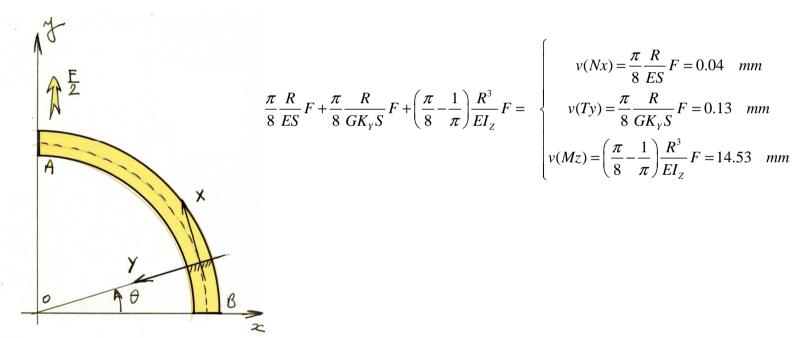
$$\begin{cases} N_X = \frac{F\cos\theta}{2} \\ T_Y = -\frac{F\sin\theta}{2} \\ M_Z = -\frac{FR\cos\theta}{2} + M_A \end{cases}$$

Analytical Results: Reactions



Reactions
$$\begin{cases} X_A = 0 \\ Y_B = -\frac{F}{2} = -25000 \quad N \\ M_A = \frac{FR}{\pi} = 3979 \quad m.N \\ M_B = \frac{FR}{2} \left(\frac{\pi - 2}{\pi}\right) = 2271 \quad m.N \end{cases}$$

Analytical Results: Displacement of the cross section in A



$$v(Nx) = \frac{\pi}{8} \frac{R}{ES} F = 0.04 \quad mm$$

$$v(Ty) = \frac{\pi}{8} \frac{R}{GK_Y S} F = 0.13 \quad mm$$

$$v(Mz) = \left(\frac{\pi}{8} - \frac{1}{\pi}\right) \frac{R^3}{EI_Z} F = 14.53 \quad mm$$

Analytical Results: Stresses

Normal Force **Shear Force** Bending Moment

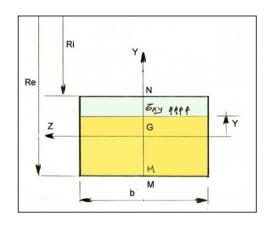
$$\begin{cases} N_X = \frac{F\cos\theta}{2} \\ T_Y = -\frac{F\sin\theta}{2} \\ M_Z = FR\left(\frac{1}{\pi} - \frac{\cos\theta}{2}\right) \end{cases}$$

Normal Stresses in the principal axis: $\sigma_X = \frac{N_X}{eh} - \frac{6M_Z}{he^3}Y$

$$\sigma_X = \frac{N_X}{eb} - \frac{6M_Z}{be^3} Y$$

Shear Stresses in the principal axis :

$$\tau_{XY} = \frac{12T_{Y}}{be^{3}} \left(\frac{e^{2}}{8} - \frac{Y^{2}}{2} \right)$$



Results

E	200000	MPa	Young's modulus
ν	0,33		Poisson's ratio
G	75187,96992	MPa	Shear modulus
b	30	mm	Width
R_e	260	mm	External radius
R_{i}	240	mm	Internal radius
$e = (R_e - R_i)$	20	mm	Thickness
$R = (R_e + R_i)/2$	250	mm	Average Radius
$I_Z = be^3/12$	20000	mm4	Quadratic moment
S = eb	600	mm2	Area of the cross section
F	50000	N	Load Applied on the ring
θ	0		Angle in degre
θ	0		Angle in radian
Nx	25000	N	Normal <u>Load</u>

		——	
Ţχ	0	N	Shear Force
M_A	3978873,6	mm.N	Reaction
Mz	-2271126,4	mm.N	Bending moment
Y max	10	mm	Maximum of Y
Y min	-10	mm	Minimum of Y
$\sigma_{_{\!X}}$	41,7	MPa	Normal Stress by Nx
$\sigma_{\!\scriptscriptstyle X}$	1135,6	MPa	Max normal stress by Mz
$\sigma_{\!\scriptscriptstyle X}$	-1135,6	MPa	Min stresse by Mz
$\sigma_{\!\scriptscriptstyle X}$	1177,2	MPa	MPa
$\sigma_{\!\scriptscriptstyle X}$	-1093,9	MPa	MPa
Ку	0,83333333		Coefficient of reduced Section
$\sigma_{_{\!X}}$	0,04	mm	Displacement by Nx
$\nu_{r_{\mathcal{V}}}$	0,13	mm	Displacement by Ty
v _{Mz}	14,53	mm	Displacement by Mz

Geometry

Points

Point Identifier	x	у
PT 1	0	0
PT 2	0	140
PT 3	0	160
PT 4	160	0
PT 5	140	0

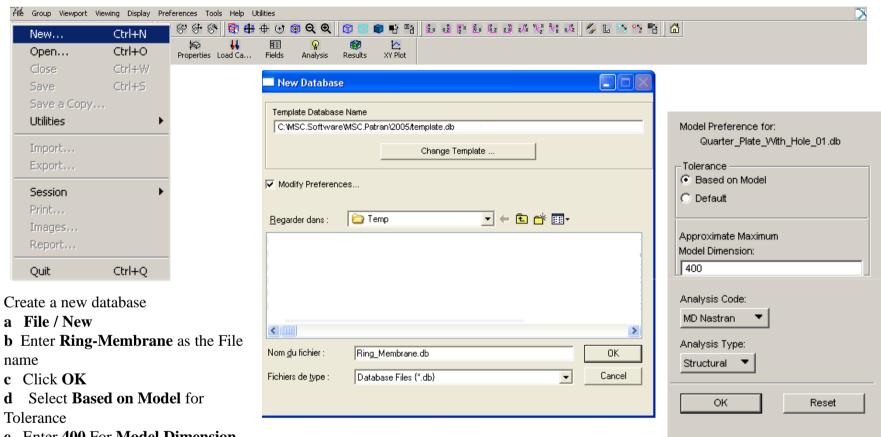
Curves

Curve identifier	Center	1° Point	2° Point
CRV 1	PT 1	PT 2	PT 3
CRV 2	PT 1	PT 5	PT 4

Surfaces

Surface identifier	1° Curve	2° Curve
SUR 1	CRV 1	CRV 2

Step 1: Creation of a New Database

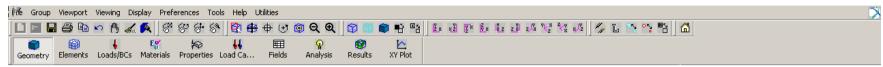


- e Enter 400 For Model Dimension
- f Select MD Nastran as the Analysis

Code

- g Select Structural as the Analysis Type
- h Click OK

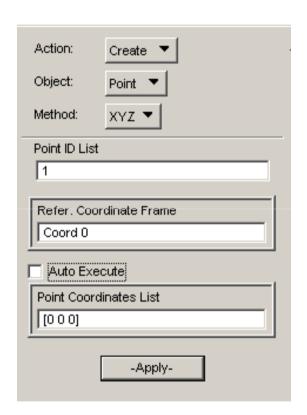
Step 1: Creation of Geometry - Points



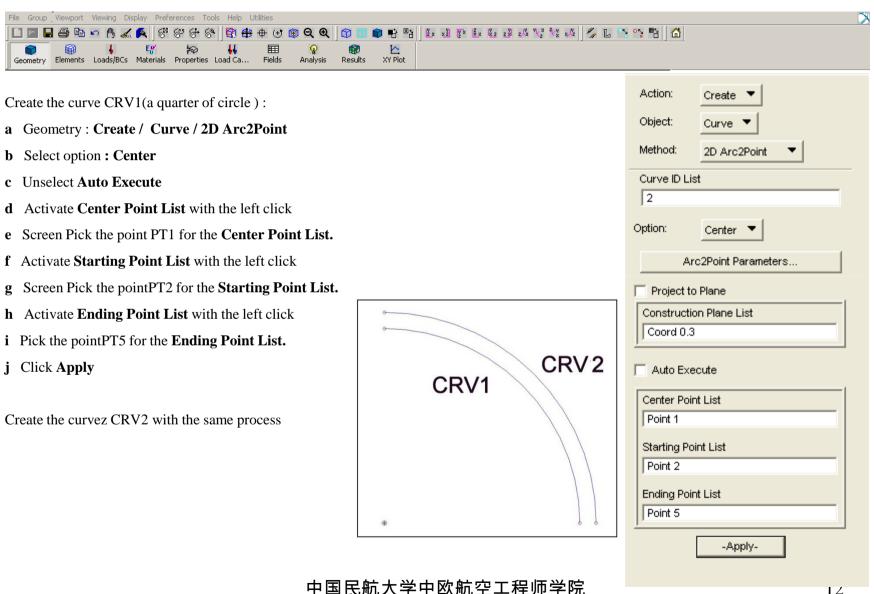
Create the first point:

- a Geometry: Create / Point / XYZ
- b Unselect Auto Execute
- c Enter [0,0,0] for the **Point Coordinate List**.
- d Click Apply

Create the other points (PT1....PT5) with the same method.



Step 1: Creation of Geometry – Curves

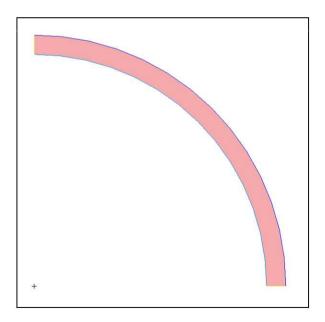


Step 1 : Creation of Geometry - Surface



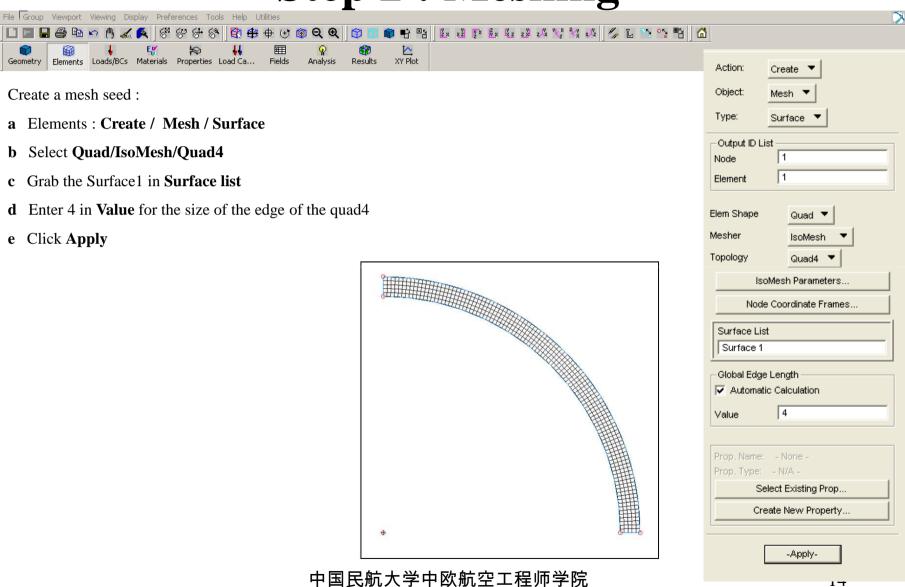
Create Surfaces with 2 curvilinear boundaries:

- a Geometry: Create / Surface / Curve
- **b** Select Option : **2 Curves**
- c Unselect Auto Execute
- **d** Screen Pick the Curve 1 CRV1in **Starting Curve List**.
- e Screen Pick the Curve 2 CRV2 in **Ending Curve List**.
- f Click Apply
- **g** Use the shading Icon to visualize the surface

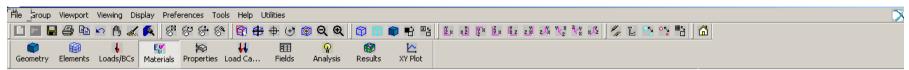




Step 2: Meshing

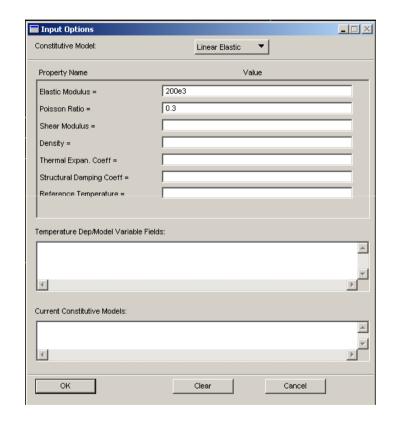


Step 4 Create material



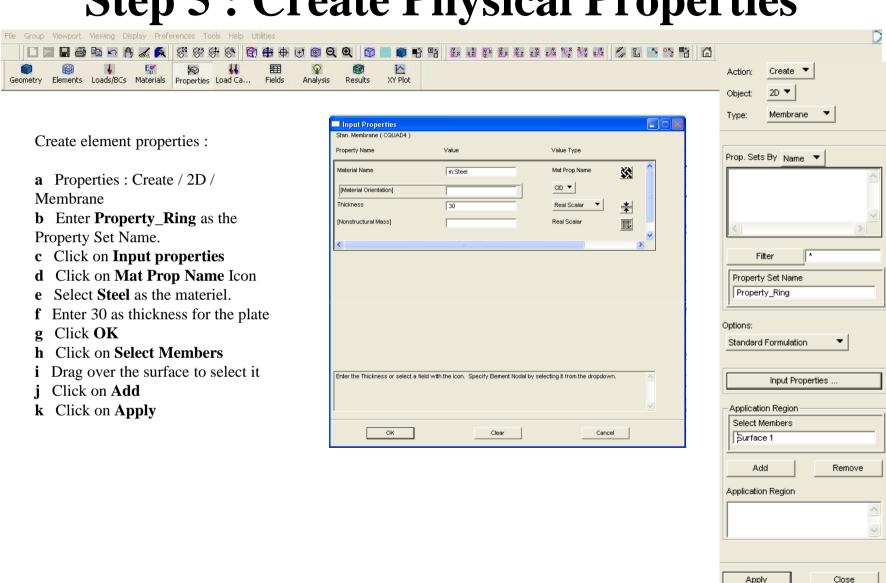
Create an isotropic material:

- **a** Material : Create / Isotropic / Manual Input
- **b** Enter **Steel** as the Material Name
- c Click on **Input properties**
- d Enter 200e3 for Elastic Modulus
- e Enter 0.3 for Poisson's Ratio
- f Click OK
- g Click Apply
- **h** Verify that the material has been created in the field **Existing Materials**



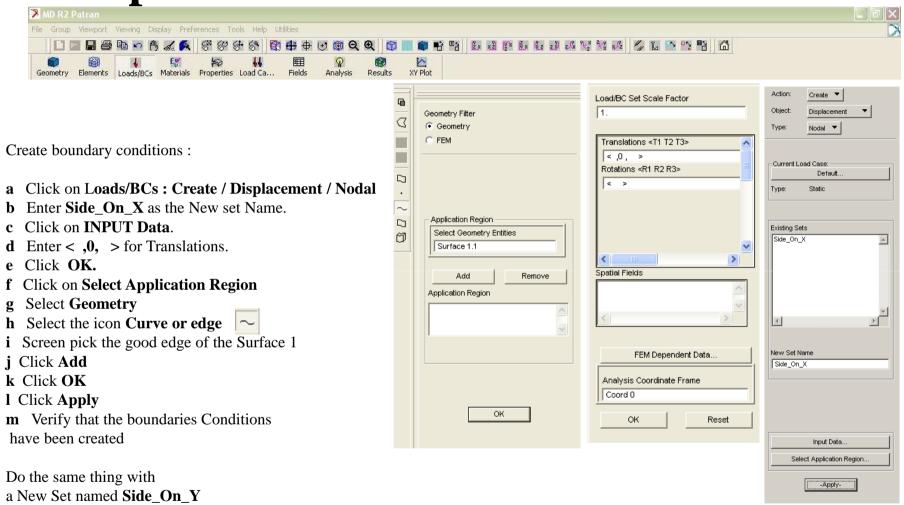


Step 5 : Create Physical Properties

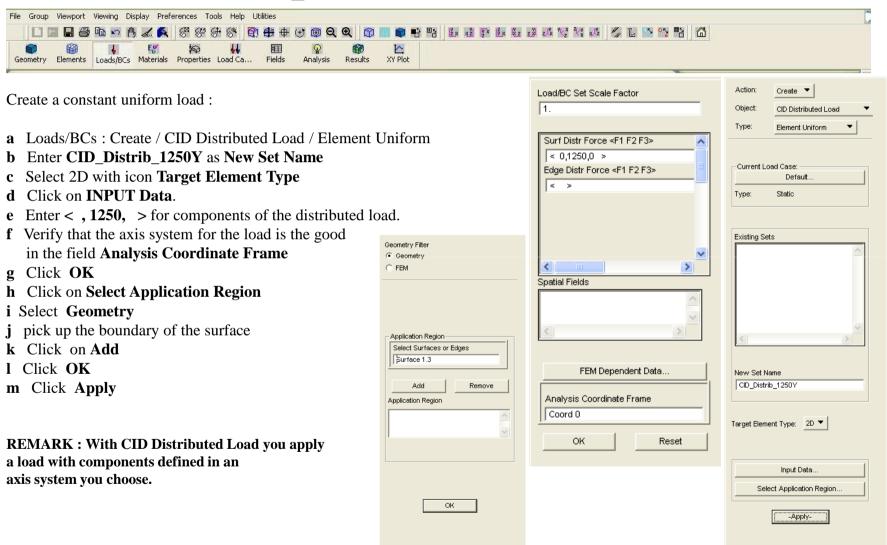


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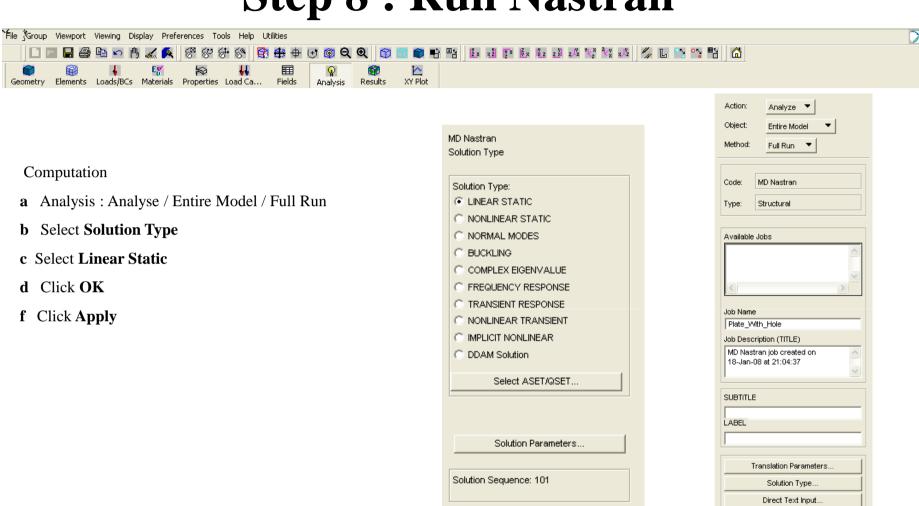
Step 6: Create Boundaries Conditions



Step 7: Create Load



Step 8: Run Nastran



OK

Cancel

Select Superelements..

Subcases...
Subcase Select.

Apply

Analysis of the results

Before creating images, graph and data files to store the results you must:

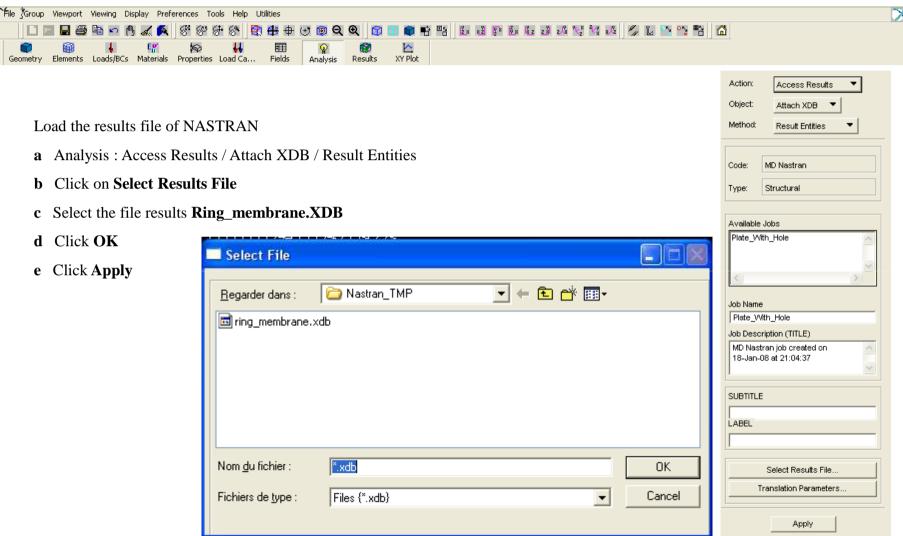
- * Open the BDF file to verify if the nodes, the elements, the material, the properties, the load, the boundary conditions have been defined correctly.
- * Open the F06 file to verify if your model has been computed correctly, with the good accuracy. Verify if OLAOD and EPSILON are good. Verify that the model performs.

After that you can import a specific output file inside Patran to analyse the results. Two different output files can be generated by NASTRAN:

- *. XDB output file (used at ISAE)
- *.OP2

To import the output file in Patran see the following slide

Step 8: Load Nastran Results in Patran



How to identify a membrane element

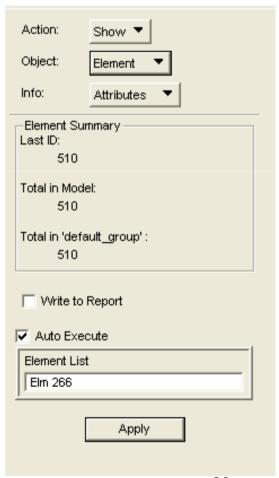


If you want to find in the F06 file the results in one or more elements you can find the identifier of this element with the following process

Identify one (or More) element(s)

:

- a Elements: Show / Element / Attributes
- **b** Screen Select the element you want to know the identifier
- c Click Apply
- **d** Read the identification number of the element in the windows that appears.
- e Open the file job.F06
- **f** Find the data of the element(s)
- **g** Analyse the results



Step 9: Results - Deformation



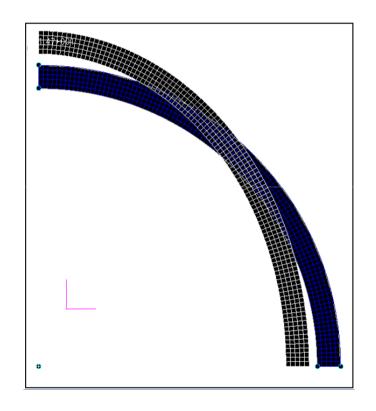
Verify the displacement:

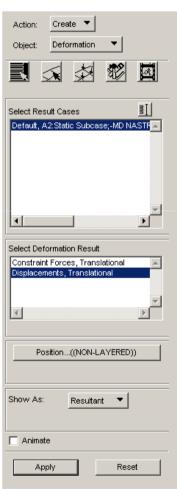
a Results: Create / Deformation

b Select Displacements,Translational in SelectDeformation Result

c Click Apply

Remark Verify the shape of the displacement, Verify the boundary conditions.





Analysis of the results

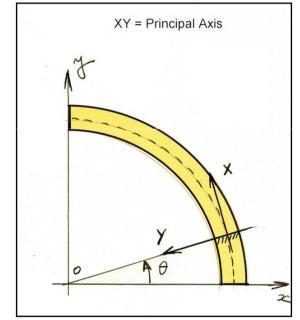
In the principal axis of the cross section we know that, according to the beam theory, we have

the following results.

$$\sigma_X = -\frac{M_z}{I_z}Y + \frac{N_X}{S}$$

$$\sigma_{\rm Y} = 0$$

$$\tau_{XY} = \frac{T_Y}{I_Z} \left(\frac{e^2}{8} - \frac{Y^2}{2} \right)$$



To verify if these results are accurate, we need to create an cylindrical axis system and then to create the images described on the following page.

Results: Creation of images

- 1 : Create a Cylindrical axis system to analyse the stresses on the cross section of the ring
- 2 : Create an image of σ_{θ}
- 3 : Create an image of σ_r
- 4 : Create an image of $\tau_{r\theta}$

Create a Cylindrical Axis System



There are several solutions to create a cylindrical axis system, for instance :

- a Geometry: Create / Coord / Axis
- **b** Select **Cylindrical** as Type
- **c** Verify the axis system in witch you will define the vector of the new axis system (**Coordinate Frame**)
- **d** With the **KeyBoard** enter the coordinates of the center of the axis system : [0 0 0]
- e With the **KeyBoard** enter the components of a vector for r direction : [0 0 1]

f With the **KeyBoard** enter the components of a vector for Theta direction : [0 1 0]

- g Click Apply
- **h** Verify that the axis system has been created

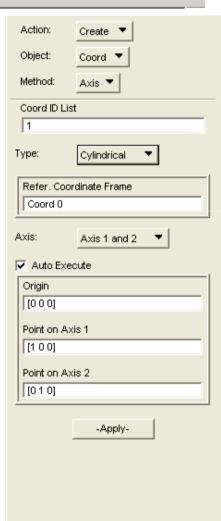


Image for the shear stress



- a Results: Create / Fringe
- **b** Select the Icon Select results
- c Select Stress tensor in Field Fringe Result
- **d** Select the quantity XY component
- e Click Apply
- f Select the Icon Target Entities
- g Select Elements as Target Entity
- **h** Select the elemenst on the model with the mouse
- i Click Apply
- j Select the Icon Plot options
- k Select CID as Coordinate Transformation
- 1 Select the cylindrical axis system on the model
- m Click Apply

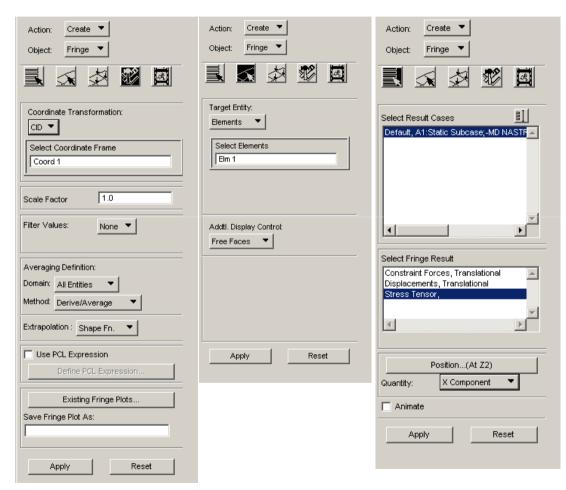


Image for the normal stress in X direction

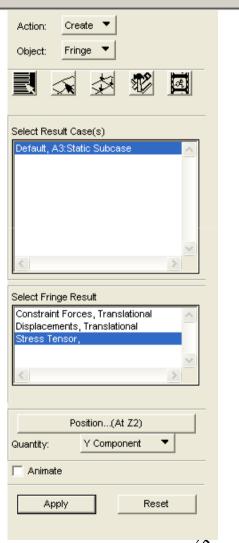


Remark : The direction X of the principal axis of the cross section is the second direction of the cylindrical axis system (the direction θ)

Principal Axis of the cross	Cylindrical axis
section	system
X	θ
Υ	r
Z	Z

Cylindrical axis	Name in PATRAN for
system	Images
r	X
θ	Υ
Z	Z

- a Results : Create / Fringe
- **b** Select the Icon Select results
- c Select Stress tensor in Field Fringe Result
- **d** Select the quantity XY component
- e Click Apply



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Image for the normal stress in Y direction

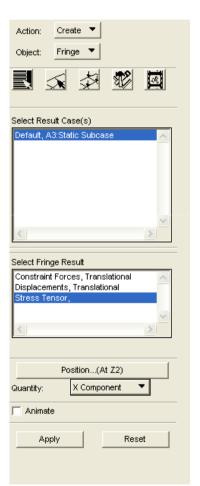


Remark : The direction Y of the principal axis of the cross section is the first direction of the cylindrical axis system (the direction r)

Principal Axis of the cross	Cylindrical axis
section	system
Х	θ
Υ	r
Z	Z

Cylindrical axis	Name in PATRAN for
system	Images
r	X
θ	Υ
Z	Z

- a Results: Create / Fringe
- **b** Select the Icon Select results
- c Select Stress tensor in Field Fringe Result
- **d** Select the quantity X component
- e Click Apply



Displacement

