

§ 5 线性系统的频域分析

- § 5.1 频率特性的基本概念
- § 5.2 幅相频率特性 (Nyquist图)
- § 5.3 对数频率特性 (Bode图)
- § 5.4 频域稳定判据
- § 5.5 稳定裕度
- § 5.6 利用开环频率特性分析系统的性能
- § 5.7 利用闭环频率特性分析系统的性能

§ 5.1 频率特性的基本概念

频域分析法特点

- (1) 研究稳态正弦响应的幅值和相角随频率的变化规律
- (2) 由开环频率特性研究闭环稳定性及性能
- (3) 图解分析法
- (4) 有一定的近似性

§ 5.1 频率特性的基本概念 (1)

例1 RC 电路如图所示, $u_r(t)=A\sin\omega t$, 求 $u_c(t)=?$

$$G(s) = \frac{U_c(s)}{U_r(s)} = \frac{1}{CRs + 1} \stackrel{T=CR}{=} \frac{1}{Ts + 1} = \frac{1/T}{s + 1/T}$$

$$U_c(s) = \frac{1/T}{s + 1/T} \cdot \frac{A\omega}{s^2 + \omega^2} = \frac{C_0}{s + 1/T} + \frac{C_1s + C_2}{s^2 + \omega^2}$$

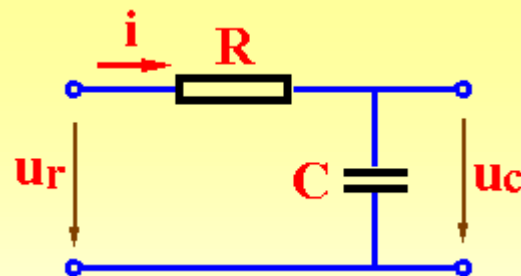
$$C_0 = \lim_{s \rightarrow -1/T} \frac{A\omega/T}{s^2 + \omega^2} = \frac{A\omega T}{1 + \omega^2 T^2}$$

$$C_1 = \frac{-A\omega T}{1 + \omega^2 T^2} \quad C_2 = \frac{A\omega}{1 + \omega^2 T^2}$$

$$U_c(s) = \frac{A\omega T}{1 + \omega^2 T^2} \cdot \frac{1}{s + 1/T} + \frac{A}{\sqrt{1 + \omega^2 T^2}} \left[\frac{1}{\sqrt{1 + \omega^2 T^2}} \cdot \frac{\omega}{s^2 + \omega^2} - \frac{T\omega}{\sqrt{1 + \omega^2 T^2}} \cdot \frac{s}{s^2 + \omega^2} \right]$$

$$u_c(t) = \frac{A\omega T}{1 + \omega^2 T^2} e^{\frac{-t}{T}} + \frac{A}{\sqrt{1 + \omega^2 T^2}} [\sin \omega t \cdot \cos \alpha - \cos \omega t \cdot \sin \alpha]$$

$$= \frac{A\omega T}{1 + \omega^2 T^2} e^{\frac{-t}{T}} + \frac{A}{\sqrt{1 + \omega^2 T^2}} \sin(\omega t - \arctan \omega T)$$



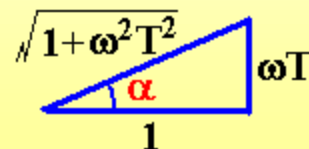
建模

$$u_r = Ri + u_c$$

$$\downarrow i = C\dot{u}_c$$

$$u_r = CR\dot{u}_c + u_c$$

$$U_r = [CRs + 1] U_c$$



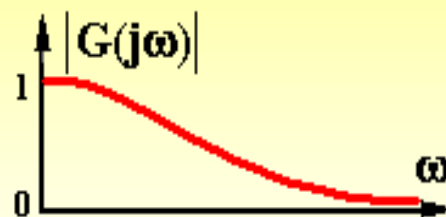
§ 5.1 频率特性的基本概念 (2)

§ 5.1.1 频率特性 $G(j\omega)$ 的定义

$$c_s(t) = \frac{A}{\sqrt{1 + \omega^2 T^2}} \sin(\omega T - \arctan \omega T)$$

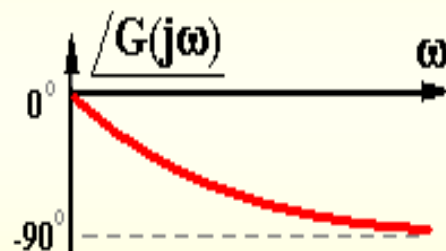
$G(j\omega)$ 定义一: $G(j\omega) = |G(j\omega)| \angle G(j\omega)$

幅频特性



$$\begin{cases} |G(j\omega)| = \frac{|c_s(t)|}{|r(t)|} = \frac{1}{\sqrt{1 + \omega^2 T^2}} \\ \angle G(j\omega) = \angle c_s(t) - \angle r(t) = -\arctan \omega T \end{cases}$$

相频特性

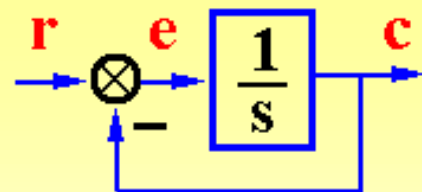


$G(j\omega)$ 定义二: $G(j\omega) = G(s)|_{s=j\omega}$

$$\frac{1}{\sqrt{1 + \omega^2 T^2}} \angle -\arctan \omega T = \left| \frac{1}{1 + j\omega T} \right| \angle \frac{1}{1 + j\omega T} = \frac{1}{1 + j\omega T} = \frac{1}{Ts + 1} \Big|_{s=j\omega}$$

§ 5.1 频率特性的基本概念 (3)

例2 系统结构图如图所示, $r(t)=3\sin(2t+30^\circ)$,
求 $c_s(t)$, $e_s(t)$ 。



$$\text{解. } \Phi(s) = \frac{1}{s+1} \left\{ \begin{array}{l} |\Phi(j\omega)| = \left| \frac{1}{1+j\omega} \right| = \frac{1}{\sqrt{1+\omega^2}} \stackrel{\omega=2}{=} \frac{1}{\sqrt{5}} = \frac{|c_s(t)|}{3} \\ \angle\Phi(j\omega) = -\arctan \omega \stackrel{\omega=2}{=} -63.4^\circ = \angle c_s(t) - \angle r(t) = \angle c_s(t) - 30^\circ \end{array} \right.$$

$$\left\{ \begin{array}{l} |c_s(t)| = 3/\sqrt{5} \\ \angle c_s(t) = -63.4^\circ + 30^\circ = -33.4^\circ \end{array} \right. \quad c_s(t) = \frac{3}{\sqrt{5}} \sin(2t - 33.4^\circ)$$

$$\Phi_e(s) = \frac{s}{s+1} \left\{ \begin{array}{l} |\Phi_e(j\omega)| = \left| \frac{j\omega}{1+j\omega} \right| = \frac{\omega}{\sqrt{1+\omega^2}} \stackrel{\omega=2}{=} \frac{2}{\sqrt{5}} = \frac{|e_s(t)|}{3} \\ \angle\Phi_e(j\omega) = 90^\circ - \arctan \omega \stackrel{\omega=2}{=} 90^\circ - 63.4^\circ = \angle e_s(t) - 30^\circ \end{array} \right.$$

$$\left\{ \begin{array}{l} |e_s(t)| = 6/\sqrt{5} \\ \angle e_s(t) = 26.6^\circ + 30^\circ = 56.6^\circ \end{array} \right. \quad e_s(t) = \frac{6}{\sqrt{5}} \sin(2t + 56.6^\circ)$$

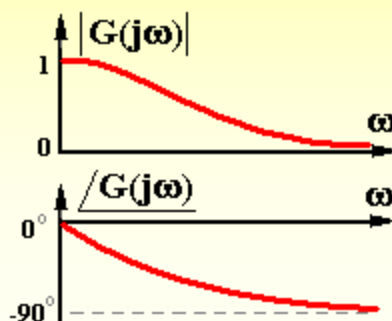
§ 5.1 频率特性的基本概念 (4)

§ 5.1.2 频率特性 $G(j\omega)$ 的表示方法

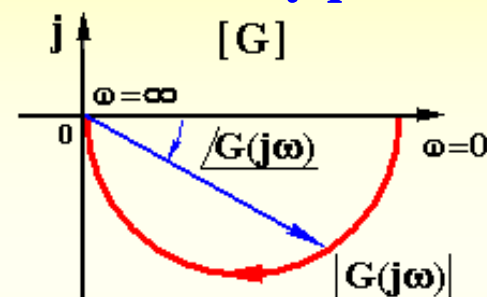
以 $G(j\omega) = \frac{1}{Ts + 1} \Big|_{s=j\omega}$ 为例。

频率特性

幅频 $|G(j\omega)|$
相频 $\angle G(j\omega)$

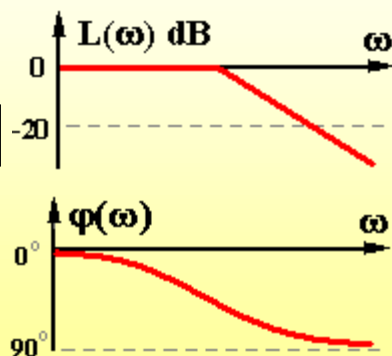


α. 幅相特性 (Nyquist)

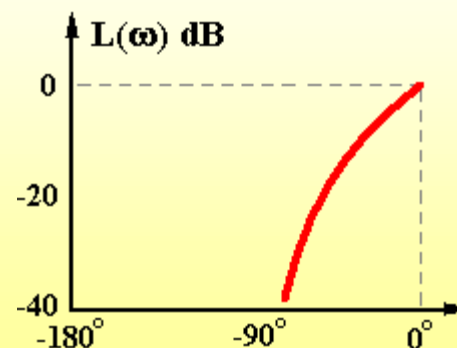


β. 对数频率特性 (Bode)

对数幅频
 $L(\omega) = 20\lg|G(j\omega)|$
对数相频
 $\varphi(\omega) = \angle G(j\omega)$

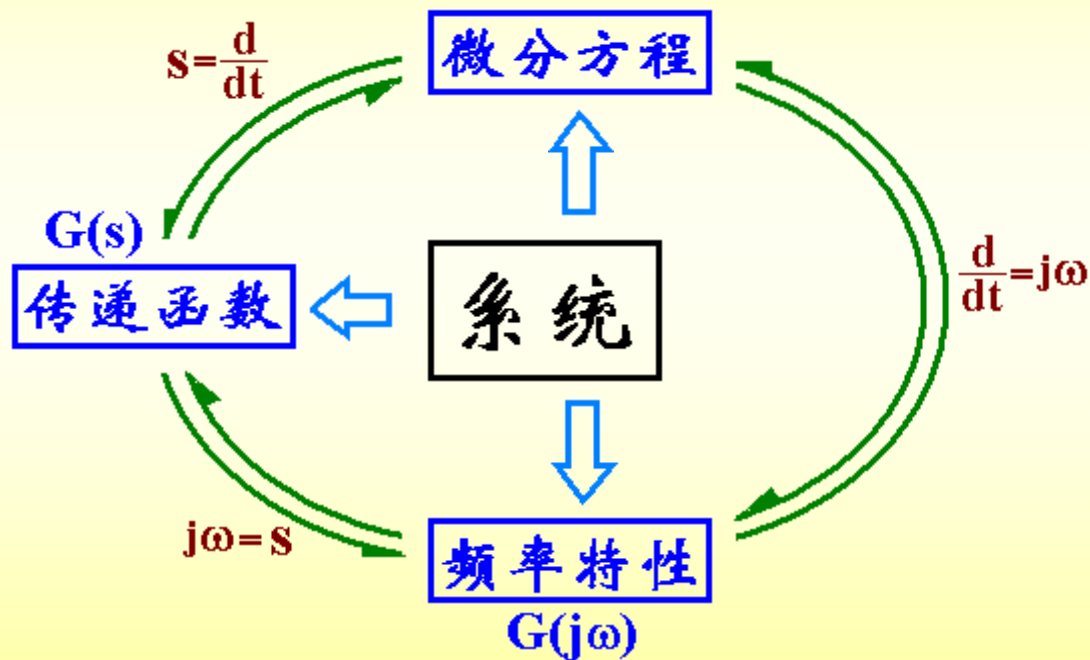


χ. 对数幅相特性 (Nichols)



§ 5.1 频率特性的基本概念 (5)

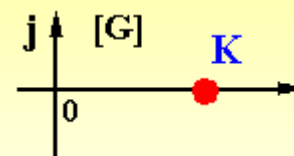
系统模型间的关系



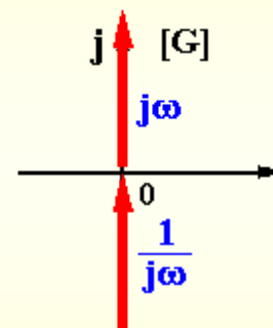
§ 5.2 幅相频率特性 (Nyquist)

§ 5.2.1 典型环节的幅相频率特性

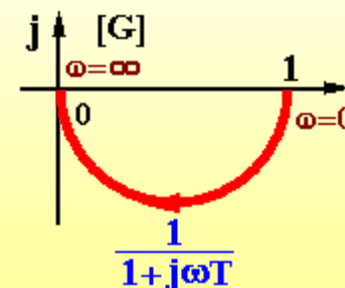
(1) 比例环节 $G(s) = K$ $G(j\omega) = K$ $\begin{cases} |G| = K \\ \angle G = 0^\circ \end{cases}$



(2) 微分环节 $G(s) = s$ $G(j\omega) = j\omega$ $\begin{cases} |G| = \omega \\ \angle G = 90^\circ \end{cases}$

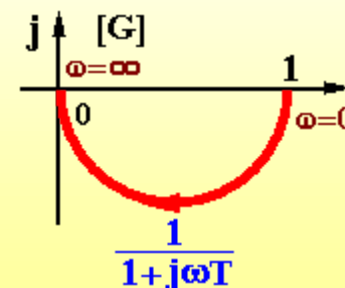


(3) 积分环节 $G(s) = \frac{1}{s}$ $G(j\omega) = \frac{1}{j\omega}$ $\begin{cases} |G| = 1/\omega \\ \angle G = -90^\circ \end{cases}$



(4) 惯性环节 $G(s) = \frac{1}{Ts + 1}$

$$G(j\omega) = \frac{1}{1 + j\omega T} \begin{cases} |G| = \frac{1}{\sqrt{1 + \omega^2 T^2}} \\ \angle G = -\arctan \omega T \end{cases}$$



§ 5.2.1 典型环节幅相频率特性 (Nyquist) (2)

例3 证明：惯性环节 $G(j\omega) = \frac{1}{1+j\omega T}$ 的幅相特性为半圆

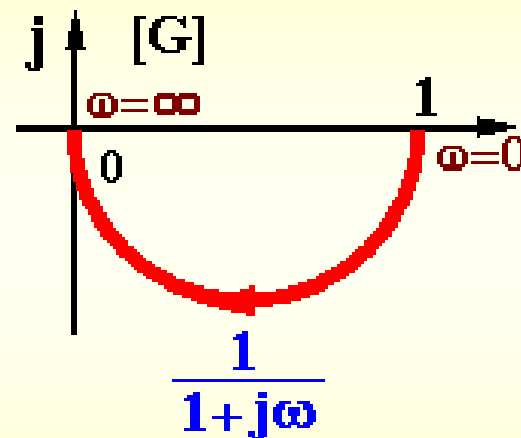
$$G(j\omega) = \frac{1}{1+j\omega T} = \frac{1-j\omega T}{1+\omega^2 T^2} = X + jY$$

$$Y = \frac{-\omega T}{1+\omega^2 T^2} = -\omega T X \Rightarrow \omega T = -\frac{Y}{X}$$

$$X = \frac{1}{1+\omega^2 T^2} = \frac{1}{1+(Y/X)^2}$$

$$X^2 - X + Y^2 = 0$$

$$\left(X - \frac{1}{2}\right)^2 + Y^2 = \left(\frac{1}{2}\right)^2 \xrightarrow{Y = -\omega T X} \quad (\text{下半圆})$$



§ 5.2.1 典型环节幅相频率特性 (Nyquist) (3)

$G(j\omega) \Leftrightarrow$ 幅相特性

例4 系统的幅相曲线如图所示，求系统的传递函数。

由曲线形状有 $G(s) = \frac{K}{Ts + 1}$

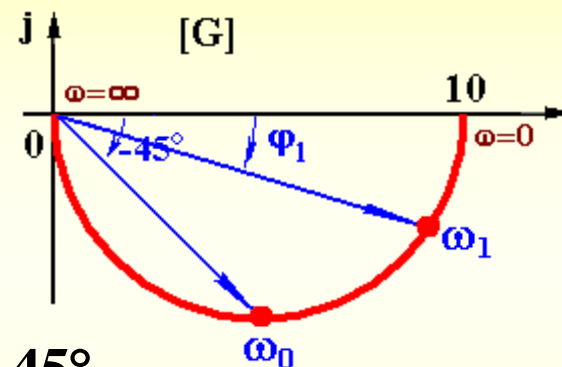
由起点: $G(j0) = \frac{K}{1 + j0T} = K = 10 \angle 0^\circ$ $K = 10$

由 φ_0 : $\angle G(j\omega_0) = \angle \frac{K}{1 + j\omega_0 T} = -\arctan \omega_0 T = -45^\circ$

$\omega_0 T = \tan 45^\circ = 1$ $T = 1/\omega_0$

由 φ_1 : $\angle G(j\omega_1) = \angle \frac{K}{1 + j\omega_1 T} = -\arctan \omega_1 T = \varphi_1$

$\omega_1 T = \tan \varphi_1$ $T = \tan \varphi_1 / \omega_1$



§ 5.2.1 典型环节幅相频率特性 (Nyquist) (4)

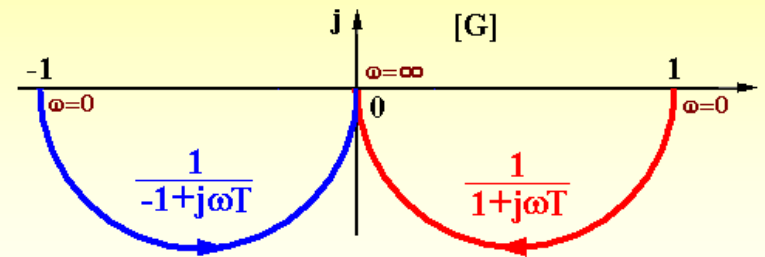
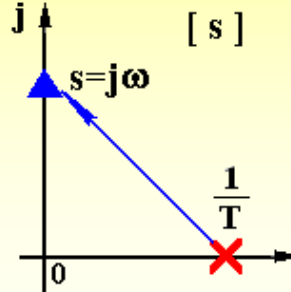
不稳定惯性环节

$$G(s) = \frac{1}{Ts - 1}$$

$$G(j\omega) = \frac{1}{-1 + j\omega T}$$

$$\begin{cases} |G| = \frac{1}{\sqrt{1 + \omega^2 T^2}} \end{cases}$$

$$\begin{cases} \angle G = -\arctan \frac{\omega T}{-1} = -180^\circ + \arctan \omega T \end{cases}$$

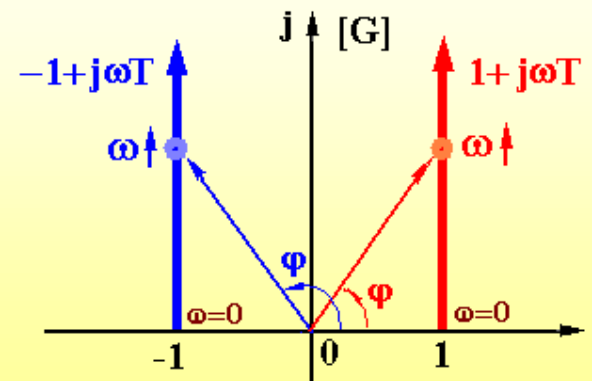


(5) 一阶复合微分 $G(s) = Ts \pm 1$

$$G(j\omega) = j\omega T \pm 1$$

$$\begin{cases} |G| = \sqrt{1 + \omega^2 T^2} \end{cases}$$

$$\begin{cases} \angle G = \begin{cases} \arctan \omega T \\ 180^\circ - \arctan \omega T \end{cases} \end{cases}$$



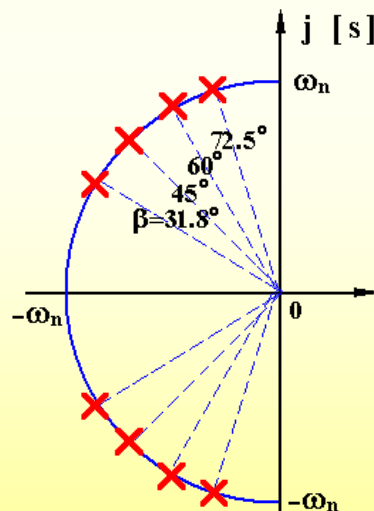
§ 5.2.1 典型环节幅相频率特性 (Nyquist) (5)

(6) 振荡环节

$$G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} = \frac{1}{\left(\frac{s}{\omega_n}\right)^2 + 2\xi \frac{s}{\omega_n} + 1}$$

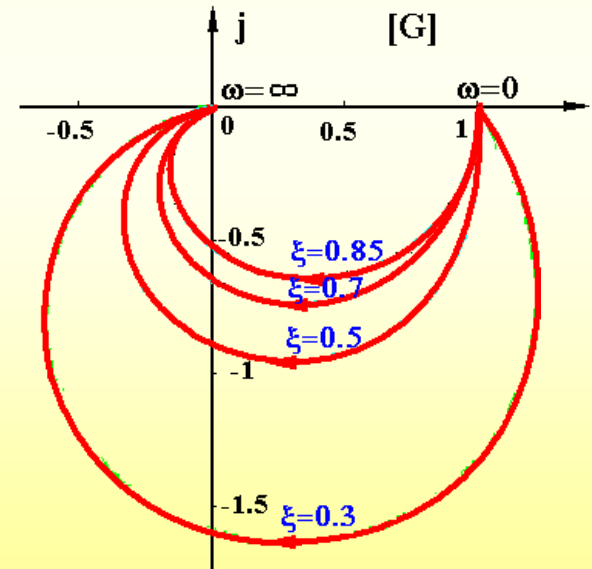
$$G(j\omega) = \frac{1}{1 - \frac{\omega^2}{\omega_n^2} + j2\xi \frac{\omega}{\omega_n}}$$

$$\left\{ \begin{array}{l} |G| = \frac{1}{\sqrt{\left[1 - \frac{\omega^2}{\omega_n^2}\right]^2 + \left[2\xi \frac{\omega}{\omega_n}\right]^2}} \\ \angle G = -\arctan \frac{2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \end{array} \right.$$



$$G(j0) = 1 \angle 0^\circ$$

$$G(j\infty) = 0 \angle -180^\circ$$



§ 5. 2典型环节幅相频率特性 (Nyquist) (6)

谐振频率 ω_r 和谐振峰值 M_r

$$|G| = 1 / \sqrt{[1 - \frac{\omega^2}{\omega_n^2}]^2 + [2\xi \frac{\omega}{\omega_n}]^2}$$

$$\frac{d}{d\omega} |G| = 0$$

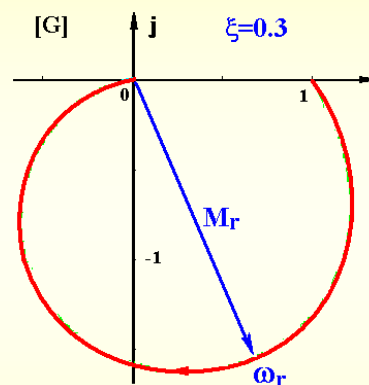
$$\frac{d}{d\omega} \left\{ [1 - \frac{\omega^2}{\omega_n^2}]^2 + [2\xi \frac{\omega}{\omega_n}]^2 \right\} = 0$$

$$2[1 - \frac{\omega^2}{\omega_n^2}][-2(\frac{\omega}{\omega_n^2})] + 2[2\xi \frac{\omega}{\omega_n}](\frac{2\xi}{\omega_n}) = 0$$

$$\frac{4\omega}{\omega_n^2} [-1 + \frac{\omega^2}{\omega_n^2} + 2\xi^2] = 0$$

$$\frac{\omega^2}{\omega_n^2} = 1 - 2\xi^2$$

$$\begin{cases} \omega_r = \omega_n \sqrt{1 - 2\xi^2} \\ M_r = |G(j\omega_r)| = \frac{1}{2\xi \sqrt{1 - \xi^2}} \end{cases}$$



例4: 当 $\xi = 0.3$, $\omega_n = 1$, 时

$$\begin{cases} \omega_r = 1 \times \sqrt{1 - 2 \times 0.3^2} = 0.9055 \\ M_r = \frac{1}{2 \times 0.3 \sqrt{1 - 0.3^2}} = 1.832 \end{cases}$$

§ 5.2.1 典型环节幅相频率特性 (Nyquist) (7)

$G(j\omega) \Leftrightarrow$ 幅相特性

例5 系统的幅相曲线如图所示，求传递函数。

由曲线形状有 $G(s) = \frac{K}{\frac{s^2}{\omega_n^2} + 2\xi \frac{s}{\omega_n} + 1}$

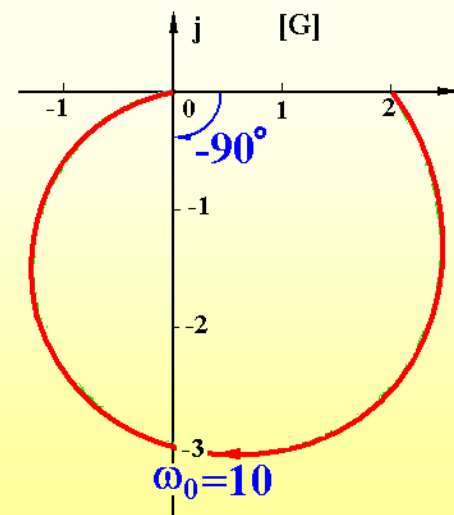
$$\left\{ \begin{array}{l} |G| = \frac{K}{\sqrt{[1 - \frac{\omega^2}{\omega_n^2}]^2 + [2\xi \frac{\omega}{\omega_n}]^2}} \\ \angle G = -\arctan \frac{2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \end{array} \right.$$

由起点: $G(j0) = K \angle 0^\circ$ $K = 2$

由 $\phi(\omega_0)$: $\angle G(j\omega_0) = -90^\circ$ $\omega_0 = \omega_n = 10$

由 $|G(\omega_0)|$: $|G(\omega_0)| = 3 = \frac{K}{2\xi} = \frac{2}{2\xi}$ $\xi = \frac{1}{3}$

$$G(s) = \frac{2 \times 10^2}{s^2 + 2 \times \frac{1}{3} \times 10s + 10^2} = \frac{200}{s^2 + 6.67s + 100}$$



§ 5.2.1 典型环节幅相频率特性 (Nyquist) (8)

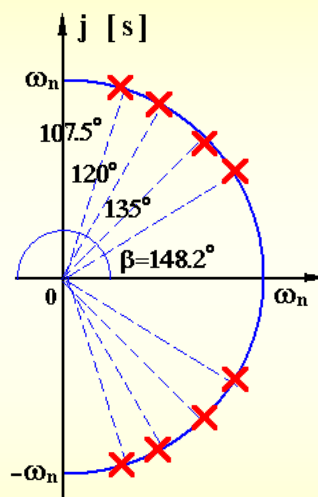
不稳定振荡环节 $G(s) = \frac{\omega_n^2}{s^2 - 2\xi\omega_n s + \omega_n^2}$

$$G(s) = \frac{1}{\left(\frac{s}{\omega_n}\right)^2 - 2\xi \frac{s}{\omega_n} + 1}$$

$$G(j\omega) = \frac{1}{1 - \frac{\omega^2}{\omega_n^2} - j2\xi \frac{\omega}{\omega_n}}$$

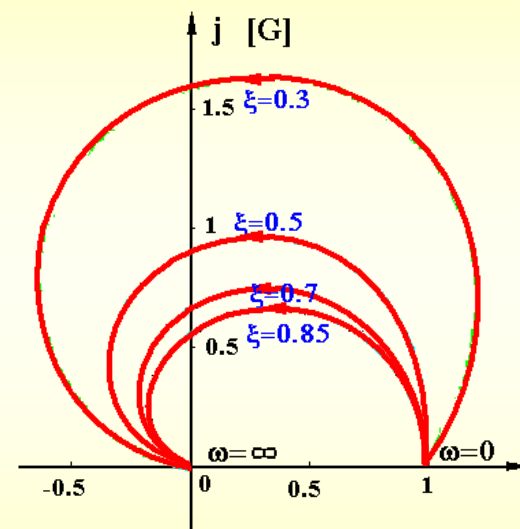
$$\left\{ \begin{aligned} |G| &= \frac{1}{\sqrt{\left[1 - \frac{\omega^2}{\omega_n^2}\right]^2 + \left[2\xi \frac{\omega}{\omega_n}\right]^2}} \end{aligned} \right.$$

$$\left\{ \begin{aligned} \angle G &= -\arctan \frac{-2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} = \arctan \frac{2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \end{aligned} \right.$$



$$G(j0) = 1 \angle 0^\circ$$

$$G(j\infty) = 0 \angle 180^\circ$$



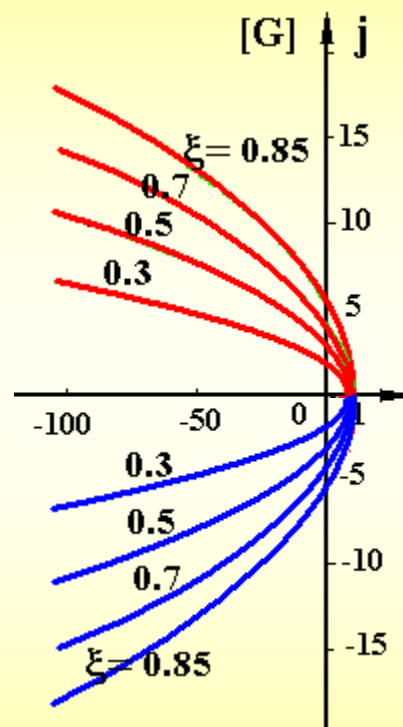
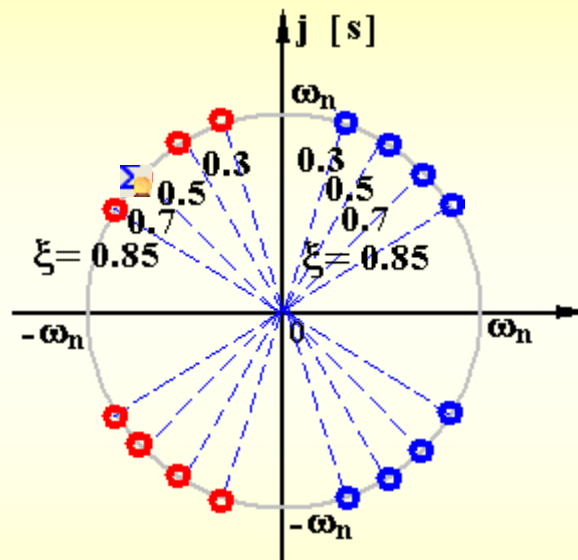
§ 5.2.1 典型环节幅相频率特性 (Nyquist) (9)

(7) 二阶复合微分

$$G(s) = T^2 s^2 + 2\xi Ts + 1 \quad T=1/\omega_n \quad = \left(\frac{s}{\omega_n}\right)^2 + 2\xi \frac{s}{\omega_n} + 1$$

$$G(j\omega) = 1 - \frac{\omega^2}{\omega_n^2} + j2\xi \frac{\omega}{\omega_n}$$

$$\left\{ \begin{array}{l} |G| = \sqrt{\left[1 - \frac{\omega^2}{\omega_n^2}\right]^2 + \left[2\xi \frac{\omega}{\omega_n}\right]^2} \\ \angle G^+ = \arctan \frac{2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \\ \angle G^- = \arctan \frac{-2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \end{array} \right.$$



$$G(j) = 1 \angle 0^\circ$$

$$G(j\infty) = 0 \angle 180^\circ$$

$$G(j) = 1 \angle 0^\circ$$

$$G(j\infty) = 0 \angle -180^\circ$$

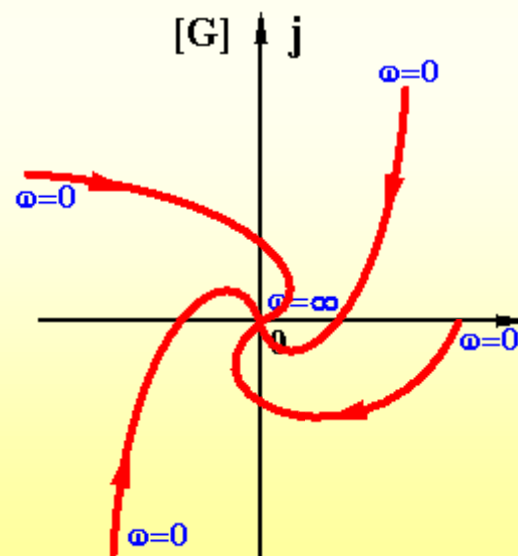
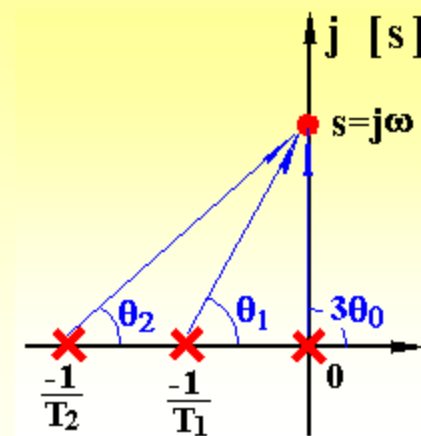
§ 5.2.2 开环系统的幅相频率特性 (1)

§ 5.2.2 开环系统的幅相频率特性

例6 $G(s) = \frac{K}{s^v (T_1 s + 1)(T_2 s + 1)} = \frac{K/(T_1 T_2)}{s^v (s + 1/T_1)(s + 1/T_2)}$

v	$G(j\omega)$	$G(j0)$	$G(j\infty)$
0	$\frac{K}{(1+j\omega T_1)(1+j\omega T_2)}$	$K \angle 0^\circ$	$0 \angle -180^\circ$
I	$\frac{K}{j\omega(1+j\omega T_1)(1+j\omega T_2)}$	$\infty \angle -90^\circ$	$0 \angle -270^\circ$
II	$\frac{K}{(j\omega)^2(1+j\omega T_1)(1+j\omega T_2)}$	$\infty \angle -180^\circ$	$0 \angle -360^\circ$
III	$\frac{K}{(j\omega)^3(1+j\omega T_1)(1+j\omega T_2)}$	$\infty \angle -270^\circ$	$0 \angle -450^\circ$

起点 $\begin{cases} K \angle 0^\circ & v = 0 \\ \infty \angle -90^\circ v & v > 0 \end{cases}$
 终点 $0 \angle -90^\circ(n-m)$



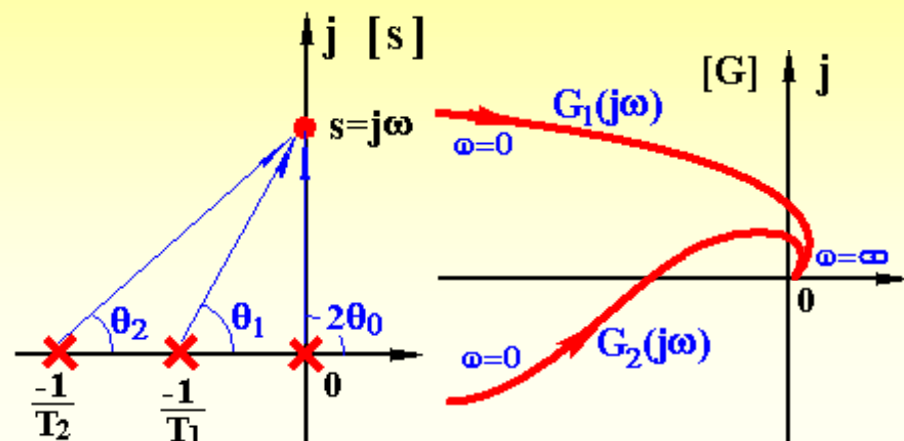
§ 5.2.2 开环系统的幅相频率特性 (2)

例7 $G_1(s) = \frac{K}{s^2(T_1s + 1)(T_2s + 1)}$

$$G_1(j0) = \infty \angle -180^\circ$$

$$\downarrow |G_1| \downarrow \quad \angle G_1 \downarrow$$

$$G_1(j\infty) = 0 \angle -360^\circ$$



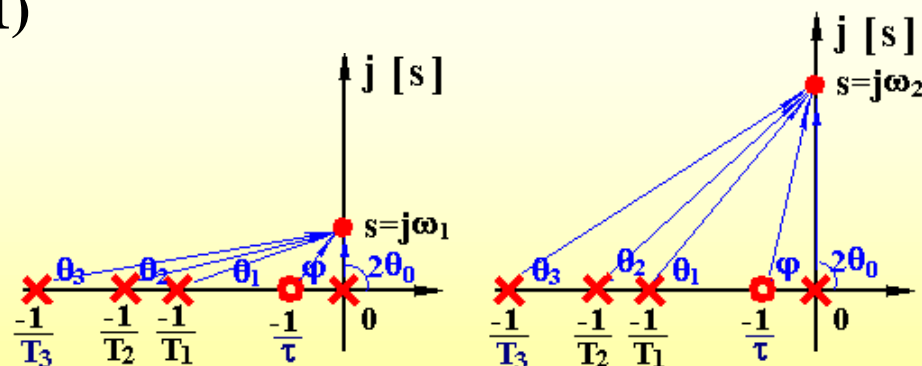
$$G_2(s) = \frac{K(\tau s + 1)}{s^2(T_1s + 1)(T_2s + 1)(T_3s + 1)}$$

$$G_2(j0) = \infty \angle -180^\circ$$

$$\downarrow |G_2| \downarrow \quad \angle G_2 \downarrow (> -180^\circ)$$

$$\downarrow |G_2| \downarrow \quad \angle G_2 \downarrow (< -180^\circ)$$

$$G_2(j\infty) = 0 \angle -360^\circ$$



§ 5.2.2 开环系统的幅相频率特性 (3)

例8 $G(s) = \frac{5}{s(s+1)(2s+1)}$, 画 $G(j\omega)$ 曲线。

$$\begin{aligned} \text{解 } G(j\omega) &= \frac{5}{j\omega(1+j\omega)(1+j2\omega)} = \frac{-j5(1-j\omega)(1-j2\omega)}{\omega(1+\omega^2)(1+4\omega^2)} \\ &= \frac{-15}{(1+\omega^2)(1+4\omega^2)} - j \frac{5(1-2\omega^2)}{\omega(1+\omega^2)(1+4\omega^2)} \end{aligned}$$

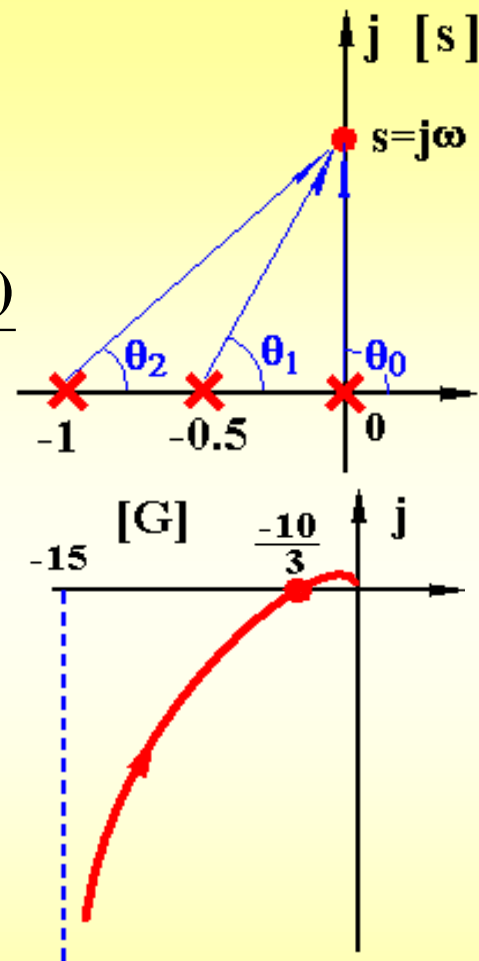
$$G(j0) = \infty \angle -90^\circ$$

$$G(j\infty) = 0 \angle -270^\circ$$

渐近线: $\text{Re}[G(j0)] \Rightarrow -15$

与实轴交点: $\text{Im}[G(j\omega)] = 0 \Rightarrow \omega = 1/\sqrt{2} = 0.707$

$$\text{Re}[G(j0.707)] = \frac{-15}{(1+0.5)(1+4 \times 0.5)} = -\frac{10}{3}$$



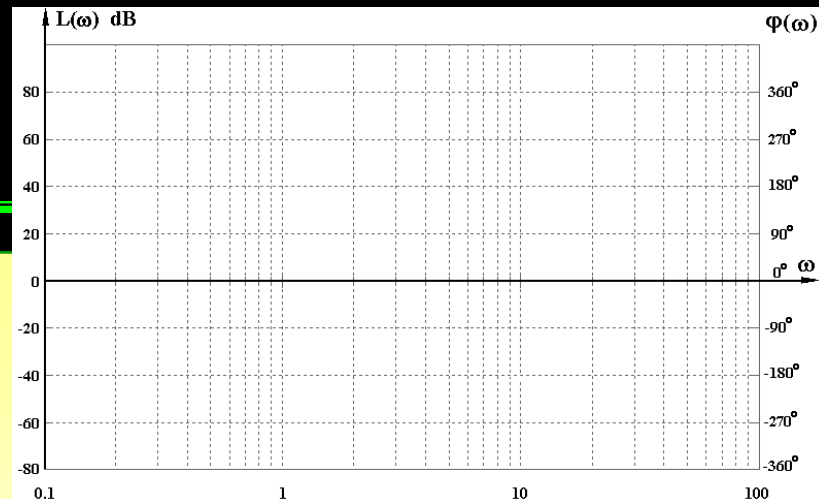
§ 5.3

对数频率特性 (Bode) (1)

Bode图介绍



§ 5.3 对数频率特性 (Bode)

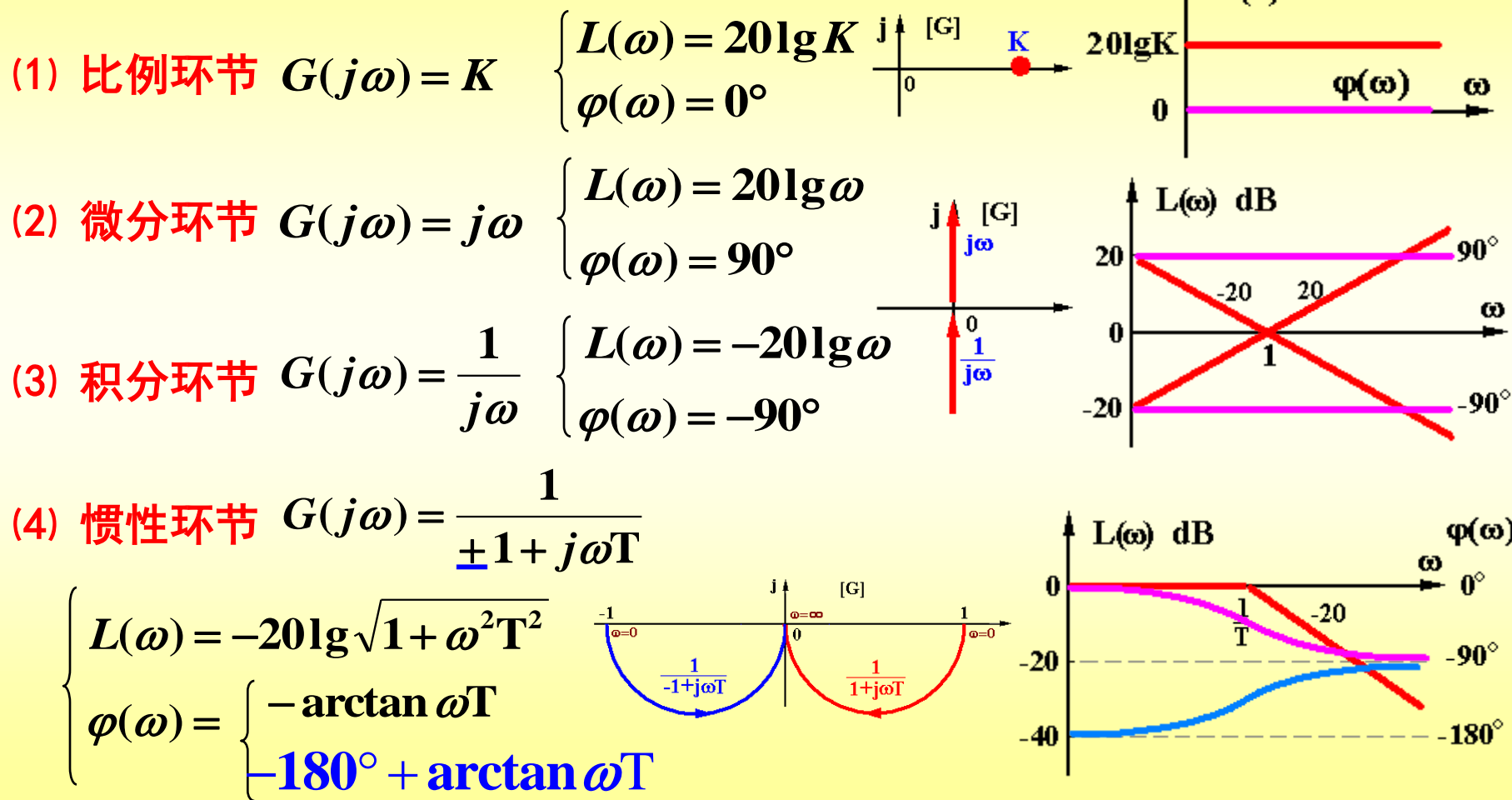


Bode图介绍

- 坐标特点
- 横轴
 - 按 $\lg \omega$ 刻度, dec “十倍频程”
 - 按 ω 标定, 等距等比
 - 纵轴
 - $L(\omega) = 20 \lg |G(j\omega)|$ dB “分贝”
 - 线性刻度
 - 特点
 - (1) 幅值相乘 = 对数相加, 便于叠加作图;
 - (2) 可在大范围内表示频率特性;
 - (3) 利用实验数据容易确定 $L(\omega)$, 进而确定 $G(s)$ 。

§ 5.3.1 典型环节的对数频率特性 (Bode) (1)

§ 5.3.1 典型环节的Bode图



§ 5.3.1 典型环节的对数频率特性 (Bode) (2)

惯性环节对数相频特性 $\varphi(\omega)$ 关于 $(\omega=1/T, \varphi=-45^\circ)$ 点斜对称

$$\varphi(\omega) = -\arctan \omega T$$

证明: $\varphi(\frac{1}{TK}) + \varphi(\frac{K}{T}) = -90^\circ$

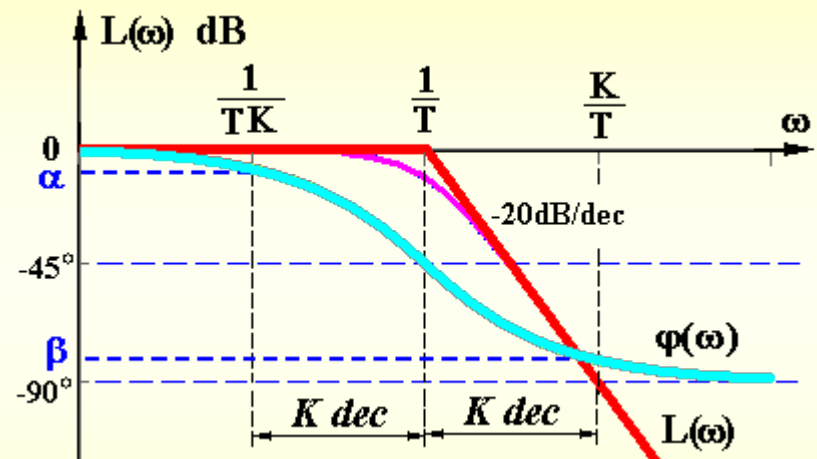
设 $\alpha = \varphi(\frac{1}{TK}) = -\arctan(T \cdot \frac{1}{TK})$

$$= -\arctan \frac{1}{K}$$

$$\beta = \varphi(\frac{K}{T}) = \arctan(T \cdot \frac{K}{T})$$

$$= \arctan K$$

$$\tan(\alpha + \beta) = \frac{\tan \alpha + \tan \beta}{1 - \tan \alpha \cdot \tan \beta} = \frac{-\frac{1}{K} - K}{1 - \frac{1}{K} K} = \infty \quad \alpha + \beta = -90^\circ$$



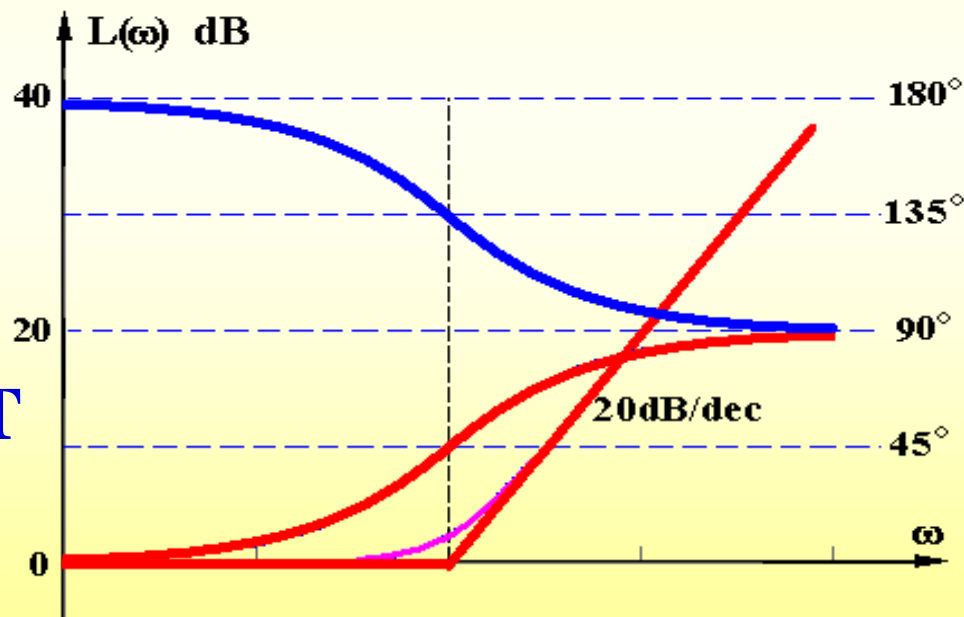
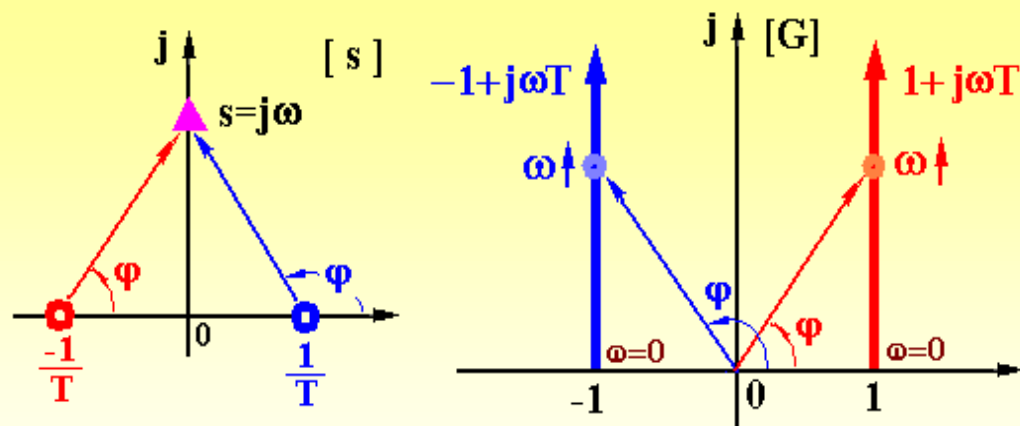
§ 5.3.1 典型环节的对数频率特性 (Bode) (3)

(5) 一阶复合微分

$$G(s) = Ts + 1$$

$$G(j\omega) = \underline{\pm}1 + j\omega T$$

$$\begin{cases} L(\omega) = 20\lg\sqrt{1 + \omega^2 T^2} \\ \varphi(\omega) = \begin{cases} \arctan \omega T \\ 180^\circ - \arctan \omega T \end{cases} \end{cases}$$



§ 5.3.1 典型环节的对数频率特性 (Bode) (4)

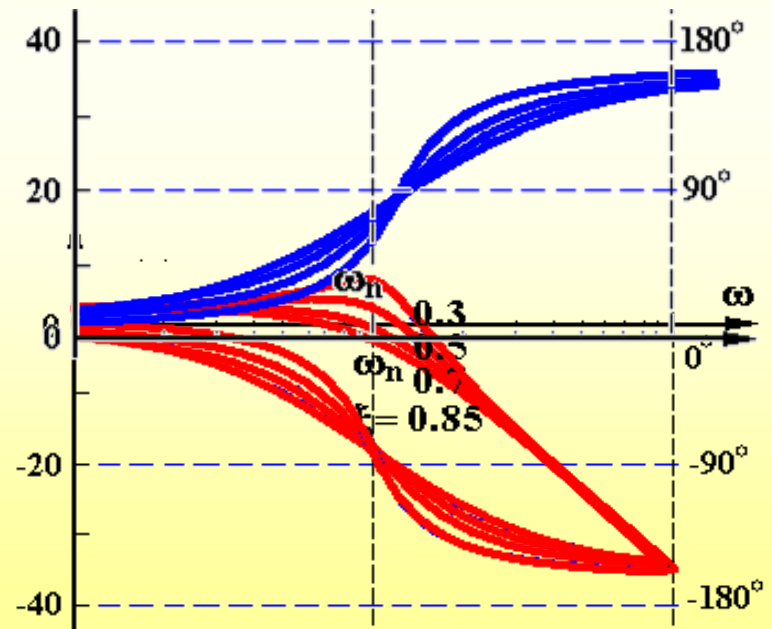
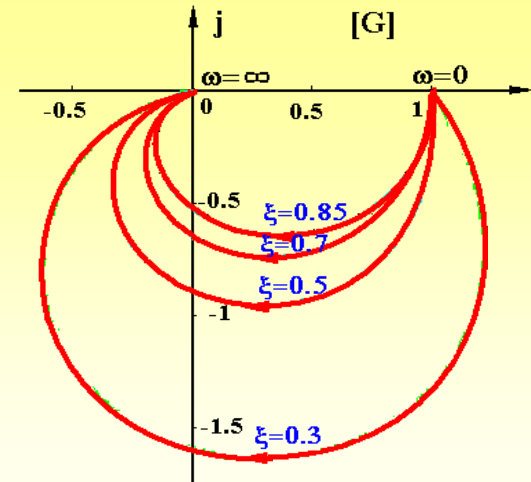
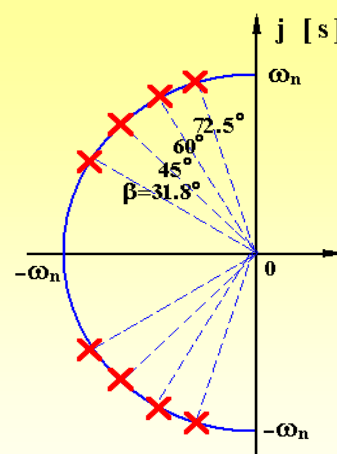
(6) 振荡环节 $G(s) = \frac{\omega_n^2}{s^2 \pm 2\xi\omega_n s + \omega_n^2}$

$$G(j\omega) = \frac{1}{1 - \frac{\omega^2}{\omega_n^2} \pm j2\xi \frac{\omega}{\omega_n}}$$

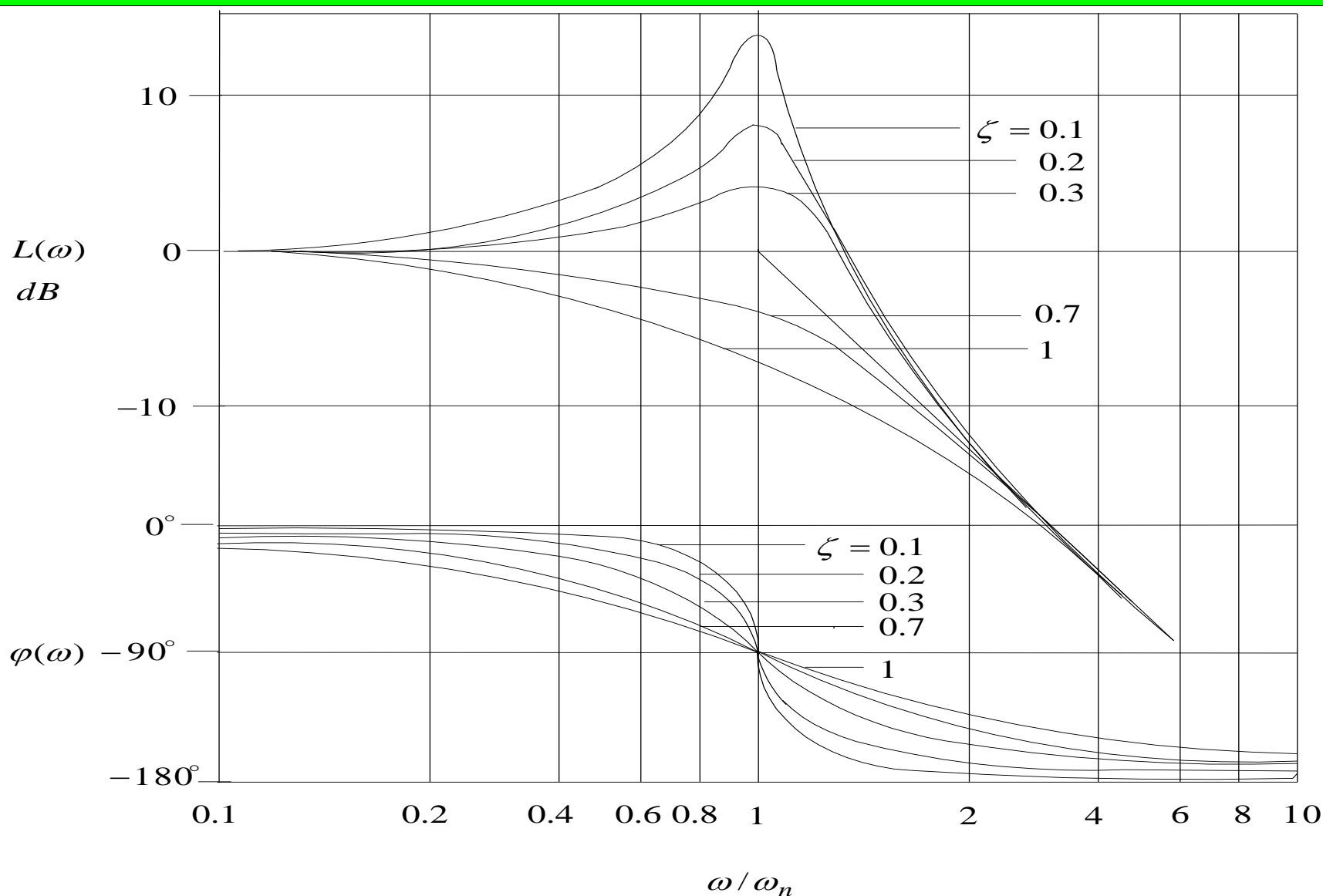
$$\begin{cases} L(\omega) = -20\lg \sqrt{\left[1 - \frac{\omega^2}{\omega_n^2}\right]^2 + \left[2\xi \frac{\omega}{\omega_n}\right]^2} \\ \varphi(\omega) = \begin{cases} -\arctan \left[\left(2\xi \frac{\omega}{\omega_n}\right) / \left(1 - \frac{\omega^2}{\omega_n^2}\right) \right] \\ \arctan \left[\left(2\xi \frac{\omega}{\omega_n}\right) / \left(1 - \frac{\omega^2}{\omega_n^2}\right) \right] \end{cases} \end{cases}$$

$$\frac{\omega}{\omega_n} \ll 1 \quad \begin{cases} L(\omega) \approx 0 \\ \varphi(\omega) \approx 0^\circ \end{cases}$$

$$\frac{\omega}{\omega_n} \gg 1 \quad \begin{cases} L(\omega) \approx -40\lg(\omega/\omega_n) \\ \varphi(\omega) \approx -180^\circ \end{cases}$$



§ 5.3.1 典型环节的对数频率特性 (Bode) (4)



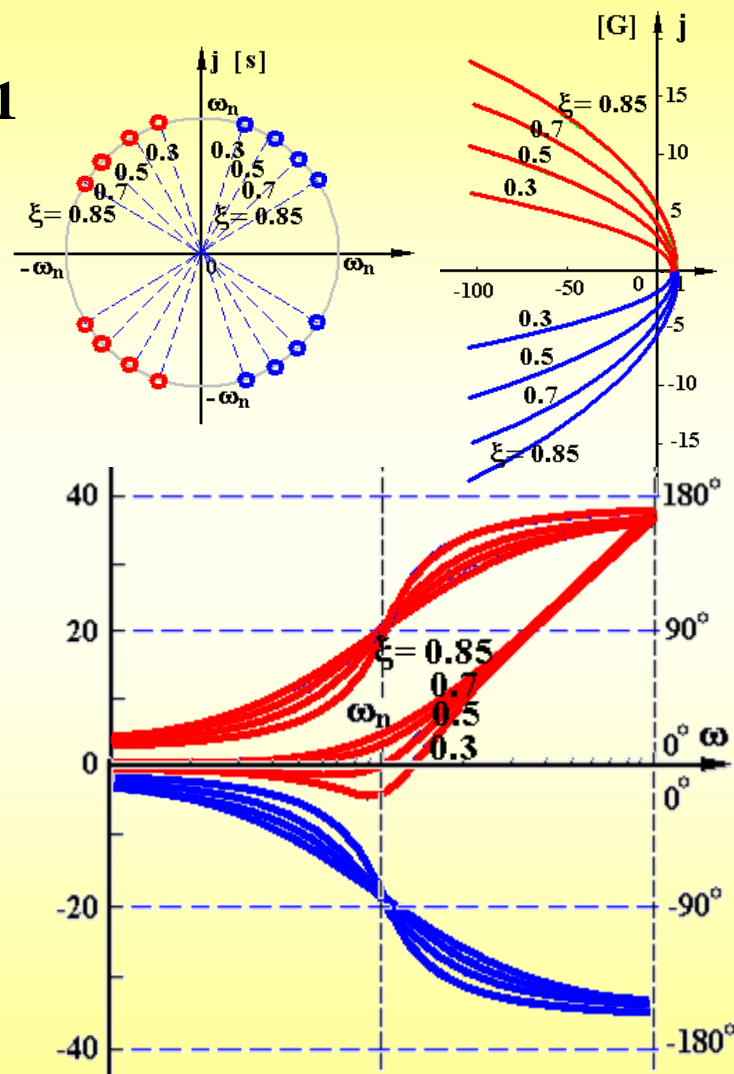
§ 5.3.1 典型环节的对数频率特性 (Bode) (5)

(7) 二阶复合微分 $G(s) = \left(\frac{s}{\omega_n}\right)^2 \pm 2\xi \frac{s}{\omega_n} + 1$

$$G(j\omega) = 1 - \frac{\omega^2}{\omega_n^2} \pm j2\xi \frac{\omega}{\omega_n}$$

$$L(\omega) = 20 \lg \sqrt{\left[1 - \frac{\omega^2}{\omega_n^2}\right]^2 + \left[2\xi \frac{\omega}{\omega_n}\right]^2}$$

$$\varphi(\omega) = \begin{cases} \arctan \frac{2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \\ \arctan \frac{-2\xi \frac{\omega}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}} \end{cases}$$



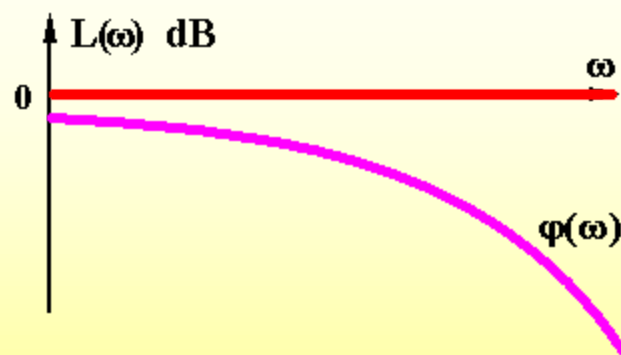
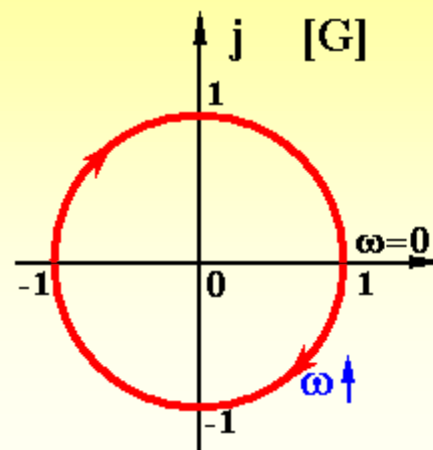
§ 5.3.1 典型环节的对数频率特性 (Bode) (6)

(8) 延迟环节

$$G(s) = e^{-\tau s}$$

$$G(j\omega) = e^{-j\omega \tau}$$

$$\begin{cases} L(\omega) = 20\lg 1 = 0 \\ \varphi(\omega) = -57.3^\circ \times \tau \omega \end{cases}$$



§ 5.3.1 典型环节的对数频率特性 (Bode) (7)

例1 根据Bode图确定系统传递函数。

解. 依图有 $G(s) = \frac{K}{Ts + 1}$

$$20\lg K = 30 \Rightarrow K = 10^{\frac{30}{20}} = 31.6$$

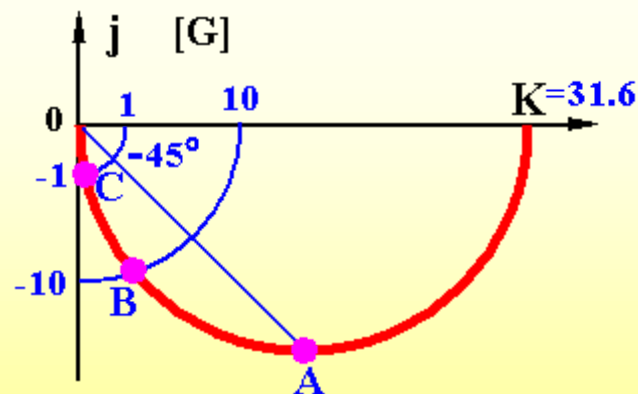
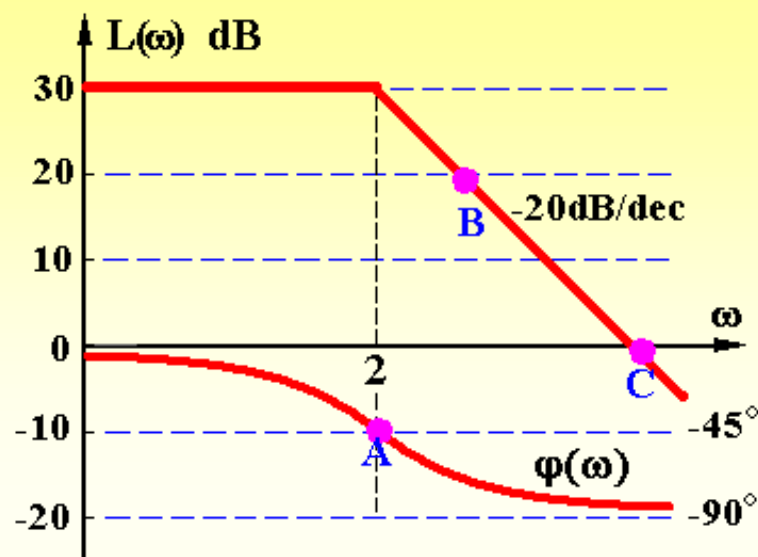
• 转折频率 $\omega = 2 = 1/T$ $G(s) = \frac{3.16}{\frac{s}{2} + 1}$

• Bode图与Nyquist图之间的对应关系：

截止频率 ω_c : $|G(j\omega_c)| = 1$

$$30\text{dB} = 20(\lg \omega_c - \lg 2) = 20\lg \frac{\omega_c}{2}$$

$$\lg \frac{\omega_c}{2} = \frac{30}{20} = 1.5 \quad \omega_c = 2 \times 10^{1.5} = 63.2 \text{ rad/s}$$



§ 5.3.1 典型环节的对数频率特性 (Bode) (8)

例2 根据Bode图确定系统传递函数。

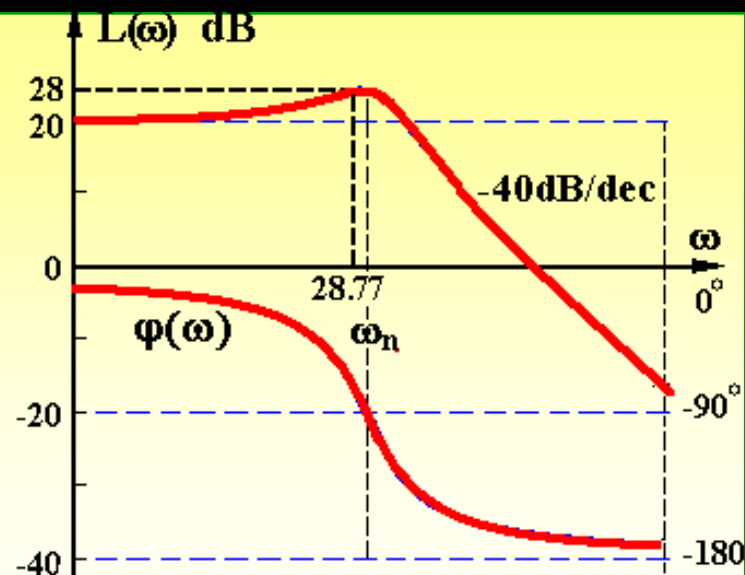
解. 依图有 $G(s) = \frac{K}{\frac{s^2}{\omega_n^2} + 2\xi \frac{s}{\omega_n} + 1}$

$$20\lg K = 20 \Rightarrow K = 10$$

$$\begin{cases} 20\lg M_r = 20\lg \frac{K}{2\xi\sqrt{1-\xi^2}} = 28 \text{ dB} \\ 20\lg \frac{1}{2\xi\sqrt{1-\xi^2}} = 8 \text{ dB} \end{cases}$$

$$2\xi\sqrt{1-\xi^2} = 10^{-\frac{8}{20}}$$

$$\xi^4 - \xi^2 + 0.04 = 0 \quad \begin{cases} \xi_1 = 0.979 \\ \xi_2 = 0.203 \end{cases}$$



$$\omega_r = \omega_n \sqrt{1-2\xi^2} = 28.77 \quad \omega_n = \frac{\omega_r}{\sqrt{1-2\xi^2}} = 30$$

$$G(s) = \frac{10 \times 30^2}{s^2 + 2 \times 0.203 \times 30 s + 30^2} = \frac{9000}{s^2 + 12.18 s + 900}$$

§ 5.3.1 典型环节的对数频率特性 (Bode) (9)

• Bode图与Nyquist图之间的对应关系:

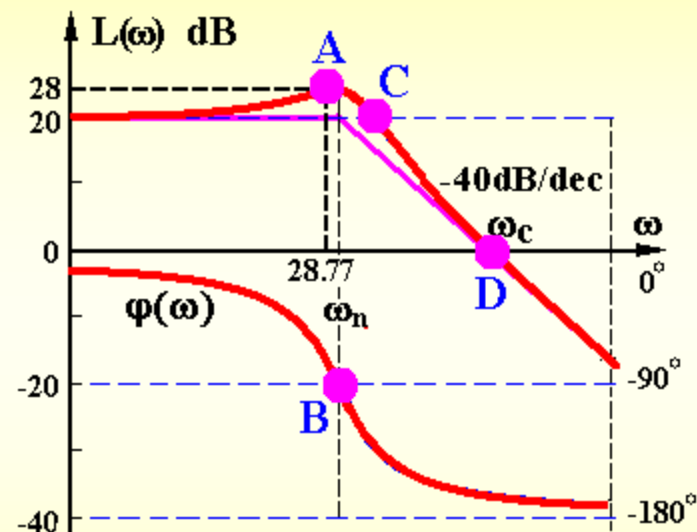
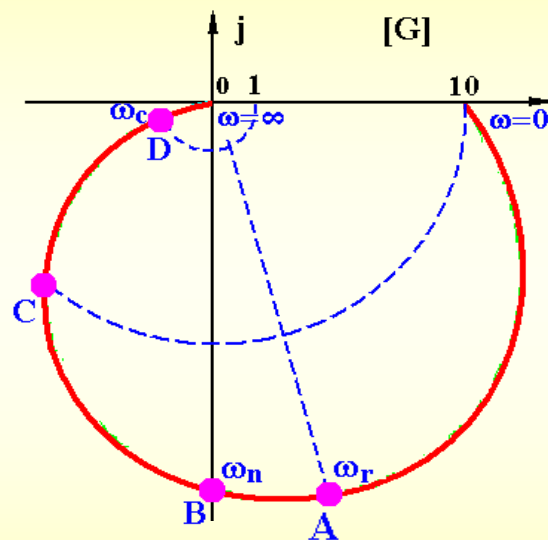
截止频率 ω_c :

$$40 \times \lg\left(\frac{\omega_c}{\omega_n}\right) = 20$$

$$\lg\left(\frac{\omega_c}{30}\right) = \frac{20}{40}$$

$$\frac{\omega_c}{30} = 10^{\frac{1}{2}}$$

$$\omega_c = 30 \times \sqrt{10} = 94.87 \text{ rad/s}$$



§ 5.3.2 开环系统对数频率特性 (Bode) (1)

§ 5.3.2 开环系统的Bode图

$$G(s) = \frac{K(\tau_1 s + 1) \cdots (\tau_m s + 1)}{s^v (T_1 s + 1) \cdots (T_{n-v} s + 1)}$$

$$\left\{ \begin{array}{l} L(\omega) = 20 \lg |G| \\ \quad = 20 \lg K + 20 \lg |1 + j\tau_1 \omega| + \cdots + 20 \lg |1 + j\tau_m \omega| \\ \quad \quad - 20v \lg |\omega| - 20 \lg |1 + jT_1 \omega| - \cdots - 20 \lg |1 + jT_{n-v} \omega| \\ \varphi(\omega) = \angle G \\ \quad = \arctan \tau_1 \omega + \cdots + \arctan \tau_m \omega \\ \quad \quad - 90^\circ v - \arctan T_1 \omega - \cdots - \arctan T_{n-v} \omega \end{array} \right.$$

§ 5.3.2 开环系统对数频率特性 (Bode) (2)

绘制开环系统Bode图的步骤

(1) 化 $G(j\omega)$ 为尾1标准型

(2) 顺序列出转折频率

(3) 确定基准线 $\left\{ \begin{array}{l} \text{最小转折频率之左} \\ \text{的特性及其延长线} \end{array} \right.$

(4) 叠加作图 $\left\{ \begin{array}{l} \text{一阶} \left\{ \begin{array}{ll} \text{惯性环节} & -20\text{dB/dec} \\ \text{复合微分} & +20\text{dB/dec} \end{array} \right. \\ \text{二阶} \left\{ \begin{array}{ll} \text{振荡环节} & -40\text{dB/dec} \\ \text{复合微分} & +40\text{dB/dec} \end{array} \right. \end{array} \right.$

例1
$$G(s) = \frac{40(s + 0.5)}{s(s + 0.2)(s^2 + s + 1)}$$

$$G(s) = \frac{100\left(\frac{s}{0.5} + 1\right)}{s\left(\frac{s}{0.2} + 1\right)(s^2 + s + 1)}$$

$$\left\{ \begin{array}{ll} 0.2 & \text{惯性环节} \\ 0.5 & \text{一阶复合微分} \\ 1 & \text{振荡环节} \end{array} \right.$$

$$\left\{ \begin{array}{ll} \text{基准点} & (\omega = 1, \quad L(1) = 20\lg K) \\ \text{斜率} & -20 \cdot \nu \quad \text{dB/dec} \end{array} \right.$$

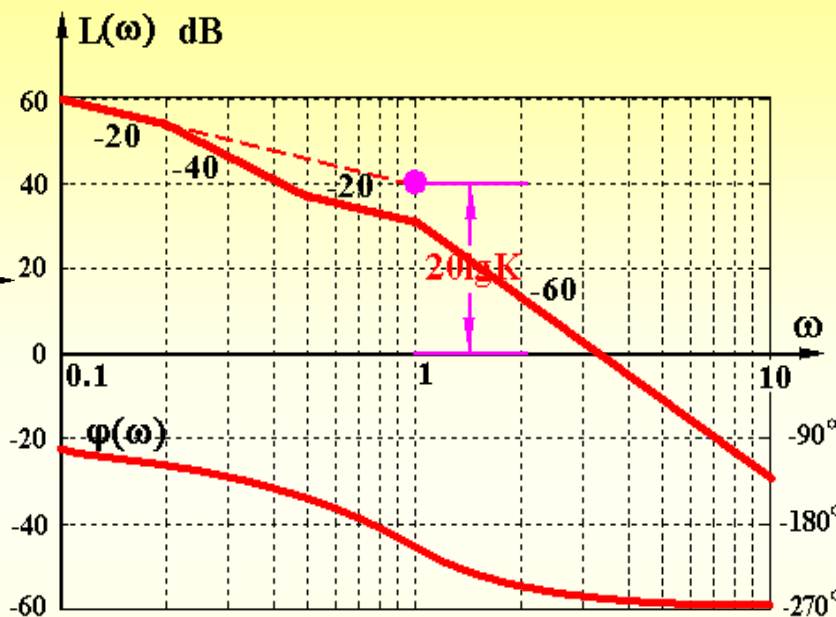
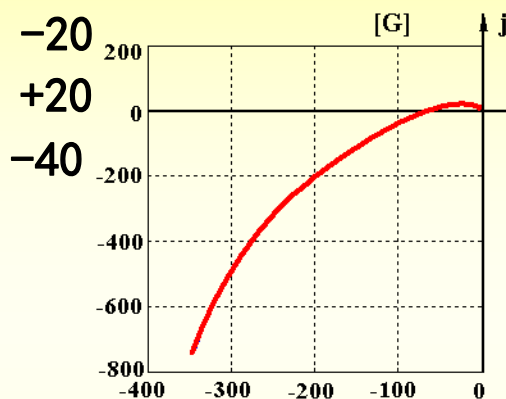
$$\left\{ \begin{array}{lll} \omega=0.2 & \text{惯性环节} & -20 \\ \omega=0.5 & \text{一阶复合微分} & +20 \\ \omega=1 & \text{振荡环节} & -40 \end{array} \right.$$

§ 5.3.2 开环系统对数频率特性 (B)

$$G(s) = \frac{100(\frac{s}{0.5} + 1)}{s(\frac{s}{0.2} + 1)(s^2 + s + 1)}$$

{ 基准点 ($\omega = 1$, $L(1) = 20\lg K$)
 斜率 $-20 \cdot \nu$ dB/dec

{ $\omega=0.2$ 惯性环节
 $\omega=0.5$ 一阶复合微分
 $\omega=1$ 振荡环节



(5) 修正： 需要时可修正误差，得出较准确的特性曲线

(6) 检查 { ① $L(\omega)$ 最右端曲线斜率 $= -20(n-m)$ dB/dec
 ② 转折点数 $= (\text{惯性}) + (\text{一阶复合微分}) + (\text{振荡}) + (\text{二阶复合微分})$
 ③ $\varphi(\omega) \Rightarrow -90^\circ (n-m)$

§ 5.3.2 开环系统对数频率特性 (Bode) (4)

例2 $G(s) = \frac{s^3}{(s+0.2)(s+1)(s+5)}$ ，绘制Bode图。

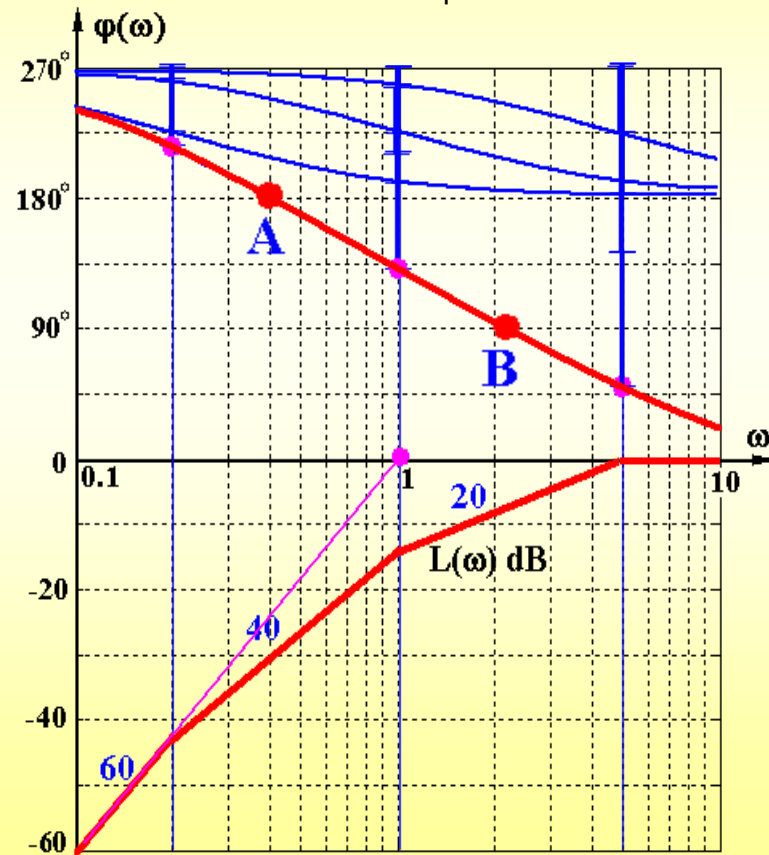
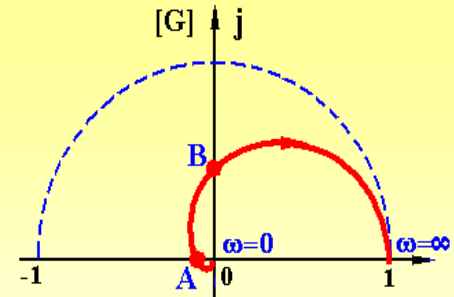
解 ① 标准型 $G(s) = \frac{s^3}{(\frac{s}{0.2}+1)(s+1)(\frac{s}{5}+1)}$

② 转折频率 $\begin{cases} \omega_1 = 0.2 \Rightarrow -20 \\ \omega_2 = 1 \Rightarrow -20 \\ \omega_3 = 5 \Rightarrow -20 \end{cases}$

③ 基准线 $\begin{cases} \text{基点 } (\omega=1, 20\lg 1 = 0 \text{ dB}) \\ \text{斜率 } -20 \times (-3) = 60 \text{ dB/dec} \end{cases}$

④ 作图

⑤ 检查 $\begin{cases} L(\omega) \text{ 最右端斜率} = -20(n-m) = 0 \\ \text{转折点数} = 3 \\ \varphi(\omega) \text{ 最终趋于 } -90^\circ(n-m) = 0^\circ \end{cases}$



§ 5.3.2 开环系统对数频率特性 (Bode) (5)

例3 已知 Bode 图, 确定 $G(s)$ 。

解:

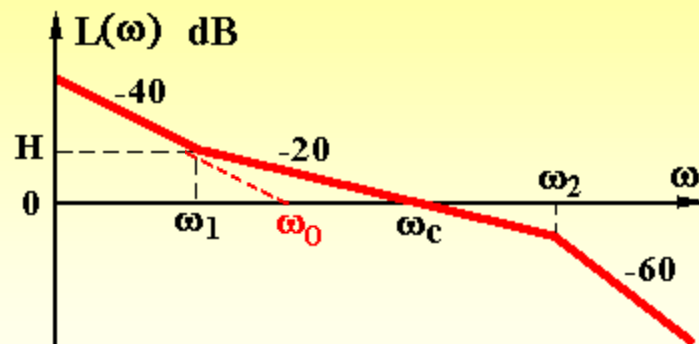
$$G(s) = \frac{K \left(\frac{s}{\omega_1} + 1 \right)}{s^2 \left(\frac{s^2}{\omega_n^2} + 2\xi \frac{s}{\omega_n} + 1 \right)}$$

解法 I $20 \lg \frac{K}{\omega_0^2} = 0 \quad K = \omega_0^2$

解法 II $H = 40[\lg \omega_0 - \lg \omega_1]$
 $= 20(\lg \omega_c - \lg \omega_1)$

$$40 \lg \frac{\omega_0}{\omega_1} = 20 \lg \frac{\omega_c}{\omega_1}$$

$$\left(\frac{\omega_0}{\omega_1} \right)^2 = \frac{\omega_c}{\omega_1} \quad K = \omega_0^2 = \omega_1 \omega_c$$



解法 III $|G(j\omega_c)| = 1 = \frac{K \frac{\omega_c}{\omega_1}}{\omega_c^2 \cdot 1} = \frac{K}{\omega_1 \omega_c}$

注: 本例无法确定阻尼比 ξ

低频段有: $20 \lg \left| \frac{K}{s^v} \right| = 20 \lg \left| \frac{K}{\omega_0^v} \right| = 0$
 $K = \omega_0^v \quad \omega_0 = K^{\frac{1}{v}}$

§ 5.3.2 开环系统对数频率特性 (Bode) (6)

例4 已知 $L(\omega)$, 写出 $G(s)$, 绘制 $\varphi(\omega)$ 以及系统幅相特性曲线。

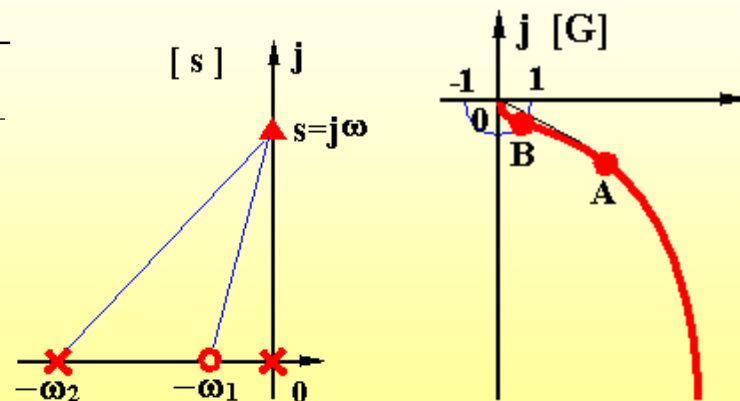
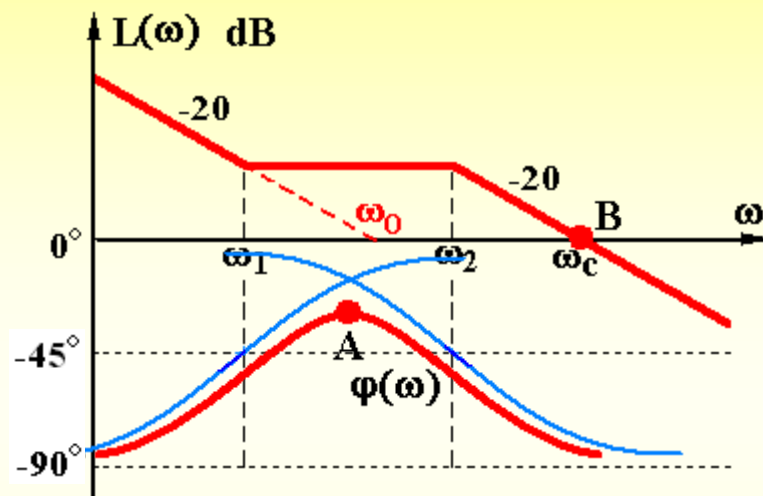
解 (1) $G(s) = \frac{K(\frac{s}{\omega_1} + 1)}{s(\frac{s}{\omega_2} + 1)}$

解法I $\frac{\omega_c}{\omega_2} = \frac{\omega_0}{\omega_1} \quad K = \omega_0 = \frac{\omega_1 \omega_c}{\omega_2}$

解法II $|G(j\omega_c)| = 1 = \frac{K \frac{\omega_c}{\omega_1}}{\omega_c \cdot \frac{\omega_c}{\omega_2}} = \frac{K}{\frac{\omega_1 \omega_c}{\omega_2}}$

(2) 叠加作图如右

(3) $G(j\omega_c) \begin{cases} G(j0) = \infty \angle -90^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$



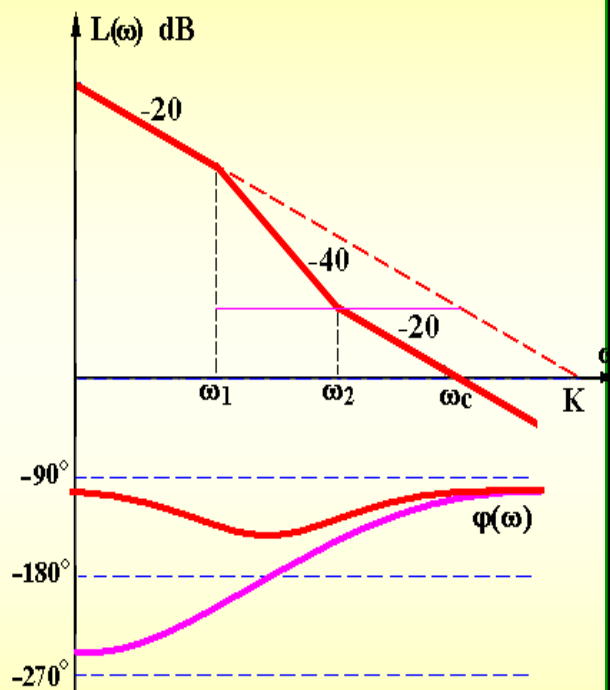
§ 5.3.2 开环系统对数频率特性 (Bode) (7)

最小相位 (角) 系统

—— 在右半 s 平面不存在开环零点和开环极点且没有纯时间延迟环节的系统

最小相位系统特征:

1. 在 $n > m$ 且幅频特性相同的情况下, 最小相位系统的相角变化范围最小。
2. 当 $\omega = \infty$ 时, 其相角等于 $-90^\circ (n-m)$, 对数幅频特性曲线的斜率为 $-20(n-m)$ dB/dec。有时用这一特性来判别该系统是否为最小相位系统。
3. 对数幅频特性与相频特性之间存在确定的对应关系。最小相位系统可由 $L(\omega)$ 惟一确定 $G(s)$ 。

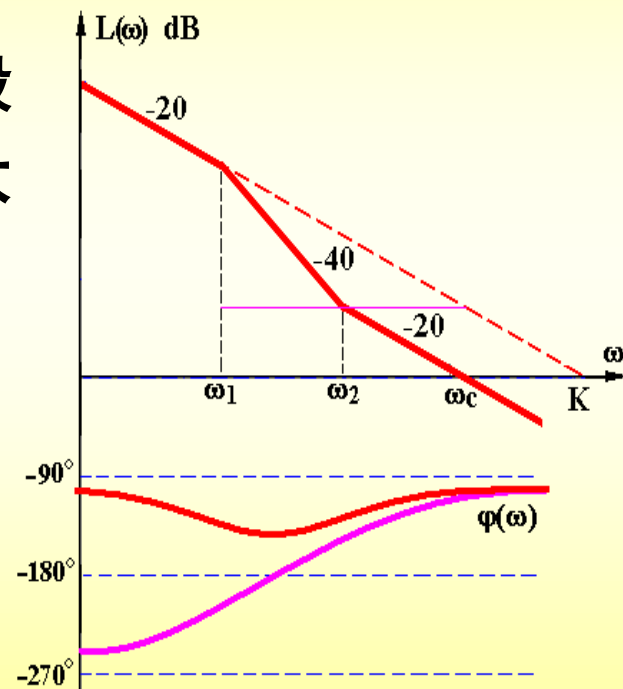


§ 5.3.2 开环系统对数频率特性 (Bode) (8)

非最小相位 (角) 系统

—— 在右半 s 平面存在开环零点或开环极点的系统

- ★ 非最小相位系统相角变化的绝对值一般比最小相位系统的相角变化的绝对值大
- ★ 非最小相位系统未必不稳定
- ★ 非最小相位系统由 $L(\omega)$ 不能惟一确定 $G(s)$



§ 5.3.2 开环系统对数频率特性 (Bode) (9)

例5 已知最小相位系统 $\varphi(\omega)$ 表达式, 求 $G(s)$ 。

$$\varphi(\omega) = \arctan \omega - 90^\circ - \arctan \frac{\omega}{2} - \arctan \frac{2\omega}{1-4\omega^2}$$

解
$$G(s) = \frac{K(s+1)}{s(\frac{s}{2}+1)[(2s)^2+2s+1]}$$

$$= \frac{K(s+1)}{s(\frac{s}{2}+1)[(\frac{s^2}{0.5^2})+2 \times 0.5 \times \frac{s}{0.5}+1]}$$

注意: K 不影响 $\varphi(\omega)$ 表达式。

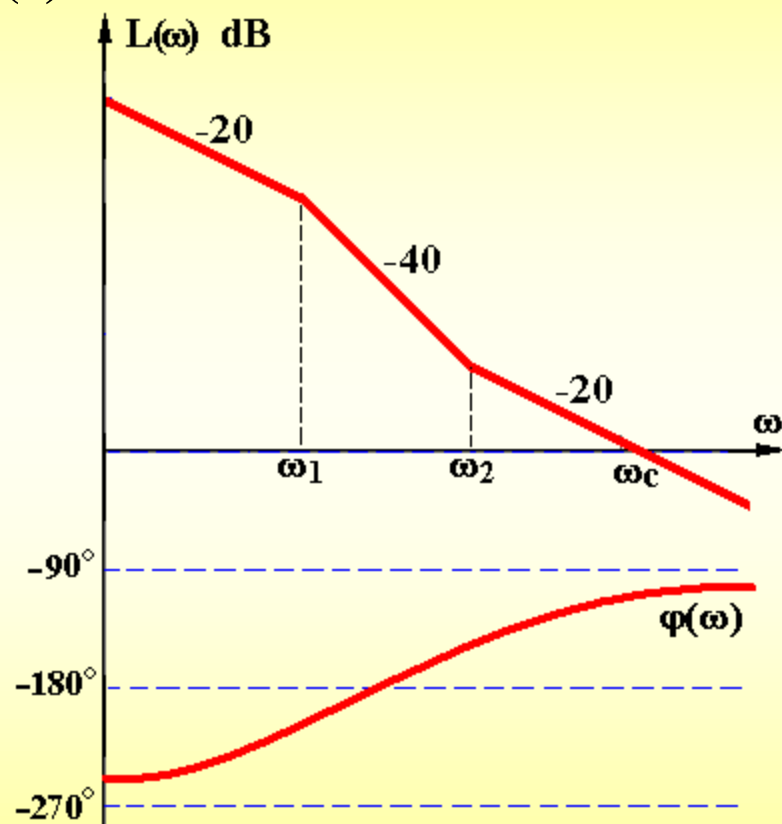
§ 5.3.2 开环系统对数频率特性 (Bode) (11)

例6 开环系统Bode图如图所示, 求 $G(s)$ 。

解 依题有 $G(s) = \frac{K(\frac{s}{\omega_2} \pm 1)}{s(\frac{s}{\omega_1} \pm 1)}$

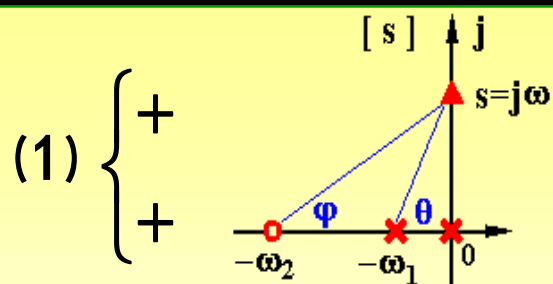
求K: $|G(j\omega)| = \frac{\omega_2}{\omega_c \frac{\omega_c}{\omega_1}} = \frac{K}{\frac{\omega_c \omega_2}{\omega_1}} = 1$

$$K = \frac{\omega_c \omega_2}{\omega_1}$$

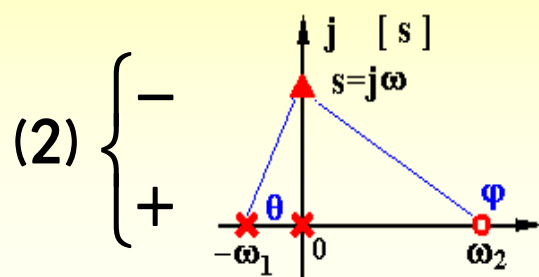
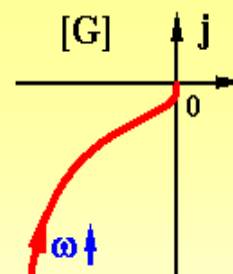


§ 5.3.2 开环系统对数频率特性 (Bode)

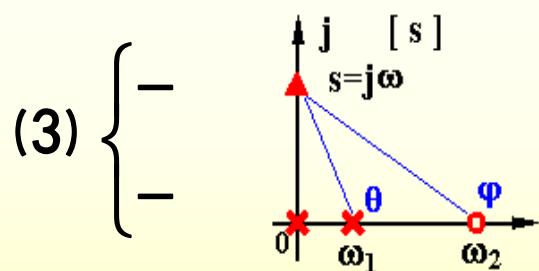
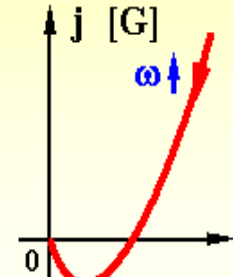
$$G(s) = \frac{K \left(\frac{s}{\omega_2} \pm 1 \right)}{s \left(\frac{s}{\omega_1} \pm 1 \right)}$$



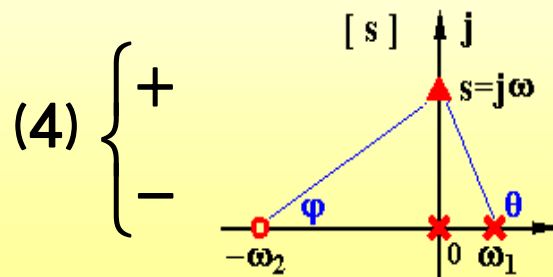
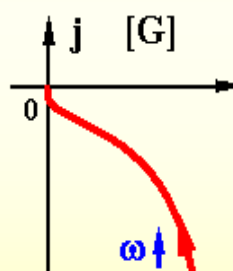
$$\begin{cases} G(j0) = \infty \angle -90^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$$



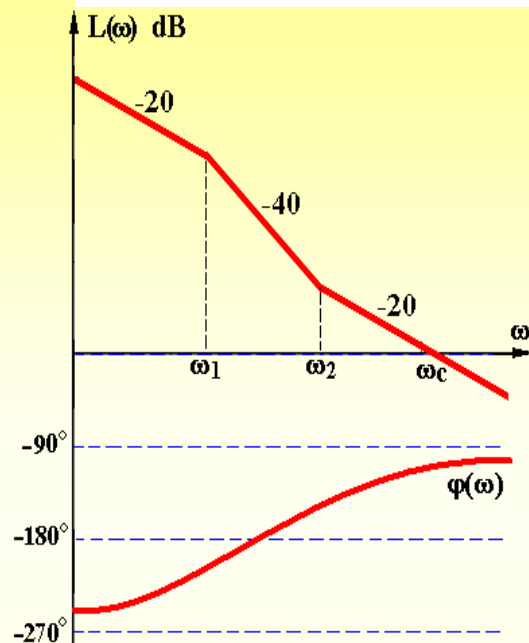
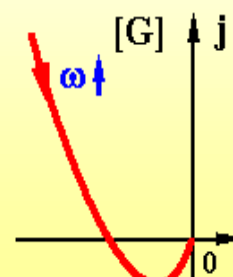
$$\begin{cases} G(j0) = \infty \angle 90^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$$



$$\begin{cases} G(j0) = \infty \angle -90^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$$



$$\begin{cases} G(j0) = \infty \angle -270^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$$



$$G(s) = \frac{K \left(\frac{s}{\omega_2} + 1 \right)}{s \left(\frac{s}{\omega_1} - 1 \right)}$$

课程小结

绘制开环系统对数复频特性曲线的步骤

(1) 化 $G(j\omega)$ 为尾1标准型

(2) 顺序列出转折频率

(3) 确定基准线 $\left\{ \begin{array}{l} \text{基准点} \quad (\omega = 1, \quad L(1) = 20\lg K) \\ \text{斜率} \quad -20 \cdot \nu \quad \text{dB/dec} \end{array} \right. \left[\begin{array}{l} \text{第一转折频率之左} \\ \text{的特性及其延长线} \end{array} \right]$

(4) 叠加作图 $\left\{ \begin{array}{l} \text{一阶} \left\{ \begin{array}{l} \text{惯性环节} \quad -20\text{dB/dec} \\ \text{复合微分} \quad +20\text{dB/dec} \end{array} \right. \\ \text{二阶} \left\{ \begin{array}{l} \text{振荡环节} \quad -40\text{dB/dec} \\ \text{复合微分} \quad +40\text{dB/dec} \end{array} \right. \end{array} \right.$

(5) 修正： 需要时可修正误差，绘出较准确的特性曲线

(6) 检查 $\left\{ \begin{array}{l} \text{① } L(\omega) \text{ 最右端曲线斜率} = -20(n-m) \text{ dB/dec} \\ \text{② 转折点数} = (\text{惯性}) + (\text{一阶复合微分}) + (\text{振荡}) + (\text{二阶复合微分}) \\ \text{③ } \varphi(\omega) \Rightarrow -90^\circ (n-m) \end{array} \right.$

§ 5.4 频域稳定判据

系统稳定的充要条件 — 全部闭环极点均具有负的实部

代数稳定判据 — Routh判据

由闭环特征多项式系数（不解根）判定系统稳定性

不能用于研究如何调整系统结构参数来改善系统稳定性及性能的问题

频域稳定判据 — { Nyquist 判据
对数稳定判据

由开环频率特性直接判定闭环系统的稳定性

可研究如何调整系统结构参数改善系统稳定性及性能问题

§ 5.4 频域稳定判据

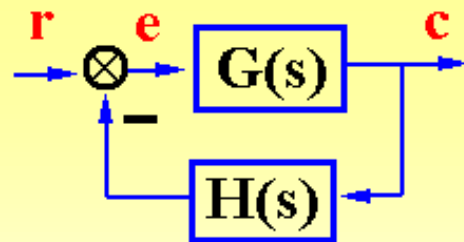
构造辅助函数 $F(s)$

$$F(s) = 1 + GH(s) = 1 + \frac{K^* M(s)}{N(s)} = \frac{N(s) + K^* M(s)}{N(s)}$$

$$= \frac{(s - p_1)(s - p_2)(s - p_3) \cdots + K^* M(s)}{(s - p_1)(s - p_2)(s - p_3) \cdots}$$

$$F(s) = \frac{D(s)}{N(s)} = \frac{(s - \lambda_1)(s - \lambda_2)(s - \lambda_3) \cdots}{(s - p_1)(s - p_2)(s - p_3) \cdots}$$

$$F(s) \text{ 的特点 } \left\{ \begin{array}{l} \text{① } F(s) \text{ 的 } \left\{ \begin{array}{l} \text{零点 } \lambda_i: \text{ 闭环极点} \\ \text{极点 } p_i: \text{ 开环极点} \end{array} \right\} \text{ 个数相同} \\ F(j\omega) = 1 + GH(j\omega) \\ \text{② } F(j\omega) \text{ 的坐标原点是 } G \text{ 平面 } GH(j\omega) \text{ 的 } (-1, 0j) \text{ 点} \end{array} \right.$$



$$\Phi(s) = \frac{G(s)}{1 + GH(s)}$$

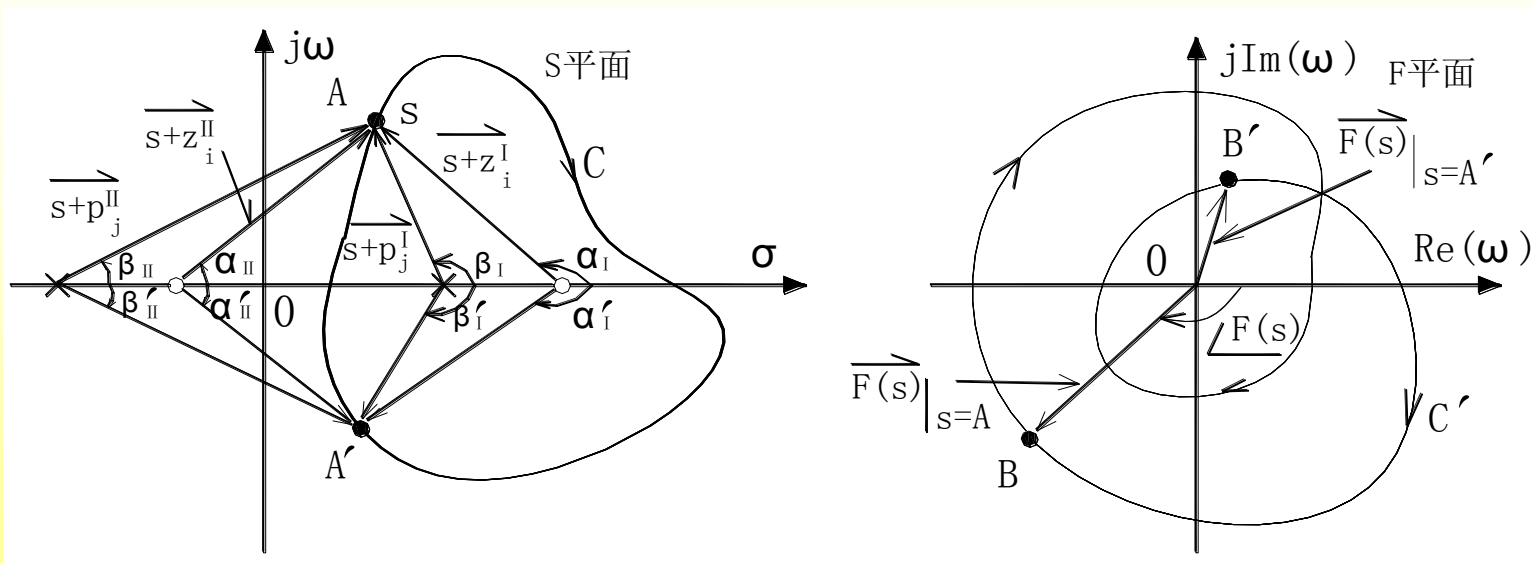
$$= \frac{G(s)}{F(s)} = \frac{G(s)N(s)}{D(s)}$$

§ 5.4 频域稳定判据

幅角定理：

设 $F(s)$ 是 s 的单值有理函数，在 s 平面内任一闭合路径包围了 $F(s)$ 的 Z 个零点和 P 个极点，并且不经过 $F(s)$ 的任一零点和极点，则在 s 平面内当 s 沿闭合路径**顺时针**方向旋转一圈时，映射到 $F(s)$ 平面内的 $F(s)$ 曲线**顺时针绕原点** $(Z - P)$ 圈（或逆时针绕原点 $(P - Z)$ 圈）。

$$\Delta \angle F(s) = \sum_{i=1}^Z \angle(s + z_i^I) - \sum_{j=1}^P \angle(s + p_j^I) = Z \times (-2\pi) - P \times (-2\pi) = (Z - P) \times (-2\pi)$$



§ 5.4.1 奈奎斯特稳定判据 (1)

奈氏路径(奈氏轨迹)：

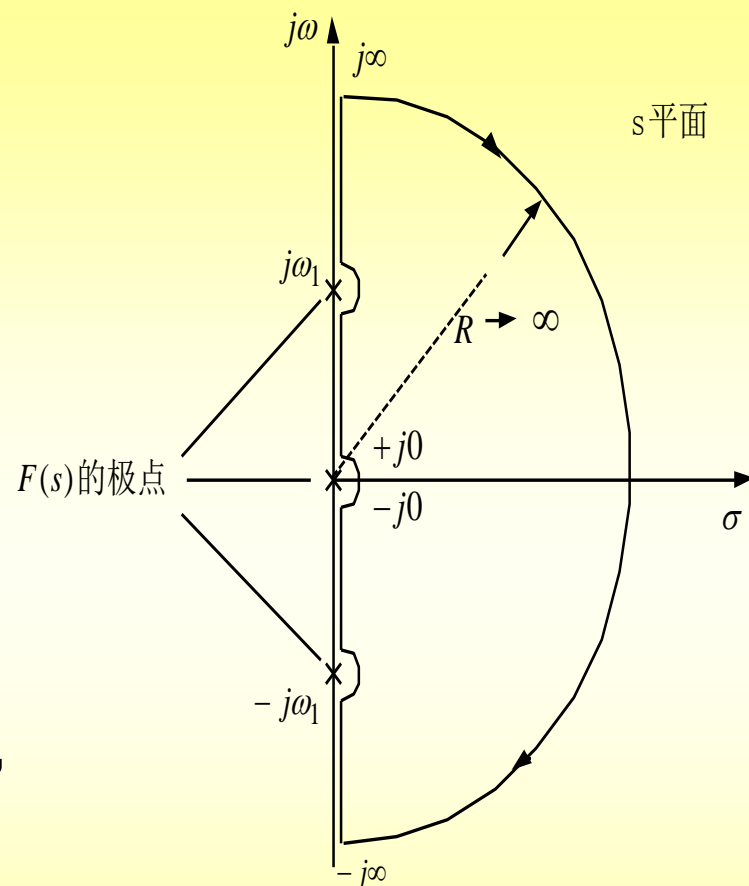
$$s = -j\infty \rightarrow -j0 \rightarrow +j0 \rightarrow +j\infty \rightarrow -j\infty$$

顺时针方向包围整个s右半面，形成奈氏路径。

说明：

1. 奈氏路径不通过 $F(s)$ 的任何零、极点。
2. 当 $F(s)$ 有若干个极点（包括原点），而没有零点处于s平面虚轴上时，奈氏路径则以这些点为圆心，作半径为无穷小的半圆，按逆时针方向从右侧绕过这些点。

(当 s 从 $-j0$ 转到 $+j0$ 时， $G(s)H(s)$ 的奈氏曲线以半径为无穷大，顺时针转过 $\nu\pi$ 。)



§ 5.4.1 奈奎斯特稳定判据 (2)

设 $F(s)$ 在右半 s 平面有 $\begin{cases} Z \text{个零点 (闭环极点)} & Z=2 \\ P \text{个极点 (开环极点)} & P=1 \end{cases}$

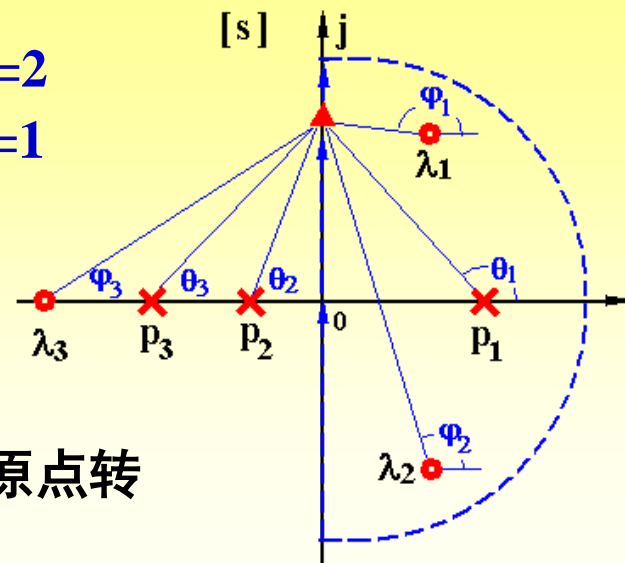
$$F(j\omega) = \frac{(s - \lambda_1)(s - \lambda_2)(s - \lambda_3)}{(s - p_1)(s - p_2)(s - p_3)}$$

-2π
 -2π
 0

-2π
 0
 0

s 顺时针绕奈氏路径转过一周, $F(j\omega)$ 绕 $[F]$ 平面原点转过的角度 **变化量** 为:

$$\angle F(j\omega) = -2\pi(Z - P) = 2\pi(P - Z) = 2\pi N$$



$$Z = P - N = P - 2R$$

N : s 顺时针绕奈氏路径一周时, $F(j\omega)$ 包围 $[F]$ 平面 $(0, j0)$ 点的圈数, **N 为正表示逆时针包围, 为负表示顺时针包围。**

R : 开环幅相曲线 $GH(j\omega)$ 包围 $[G]$ 平面 $(-1, j0)$ 点的圈数, **为正表示逆时针包围, 为负表示顺时针包围。**

§ 5.4.1 奈奎斯特稳定判据 (3)

奈氏判据一：

闭环系统稳定的**充要条件**是：s沿着奈氏路径绕一圈， $G(j\omega)H(j\omega)$ 曲线不穿过 $(-1, j0)$ 点，且**逆时针**包围 $(-1, j0)$ 点的圈数N等于开环传递函数的正实部极点数P（即 $G(s)H(s)$ 位于s右半平面的极点数）。

$$Z = P - N = P - 2R = 0$$

解释：

1. 若 $P=0$ ，且 $N=0$ ，即GH曲线不包围 $(-1, j0)$ 点，则闭环系统稳定；
2. 若 $P \neq 0$ ，且 $N=P$ ，即GH曲线逆时针绕 $(-1, j0)$ 点P圈，则闭环系统稳定，否则是不稳定系统。不稳定系统分布在s右半平面极点的个数为： $Z=P-N$

§ 5.4.1 奈奎斯特稳定判据 (4)

奈氏判据二：

当 $F(s)$ 有若干个**零点**处于 s 平面虚轴（包括原点）上时， s 沿着奈氏路径绕一圈，映射曲线 $G(j\omega)H(j\omega)$ **经过** $(-1, 0j)$ 点。若 $G(j\omega)H(j\omega)$ 曲线通过 $(-1, j0)$ 点 L 次，则说明闭环系统有 L 个极点分布在 s 平面的虚轴上，闭环系统处于临界稳定状态。

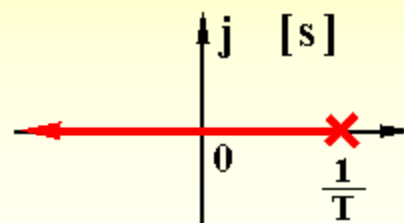
§ 5.4.2 奈氏判据的应用 (1)

例1 已知单位反馈系统开环传递函数, 分析系统稳定性。

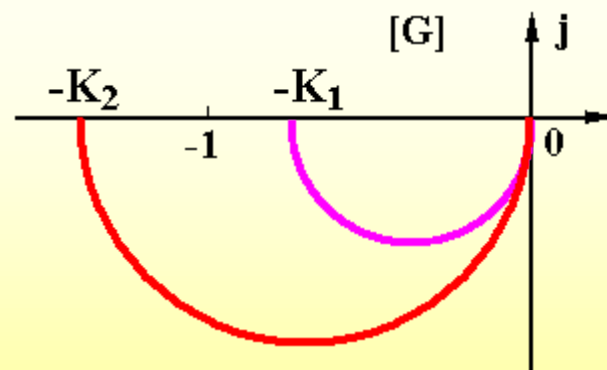
$$G(s) = \frac{K}{Ts - 1} \quad D(s) = Ts - 1 + K = 0$$

解: 依题有

$$\begin{cases} G(j0) = -K \angle -180^\circ \\ G(j\infty) = 0 \angle -90^\circ \end{cases}$$



$$K = \begin{cases} K_1 < 1 & R = 0 & \text{(不稳定)} \\ Z = P - 2R = 1 - 2 \times 0 = 1 \\ K_2 > 1 & R = \frac{1}{2} & \text{(稳定)} \\ Z = P - 2R = 1 - 2 \times \frac{1}{2} = 0 \end{cases}$$



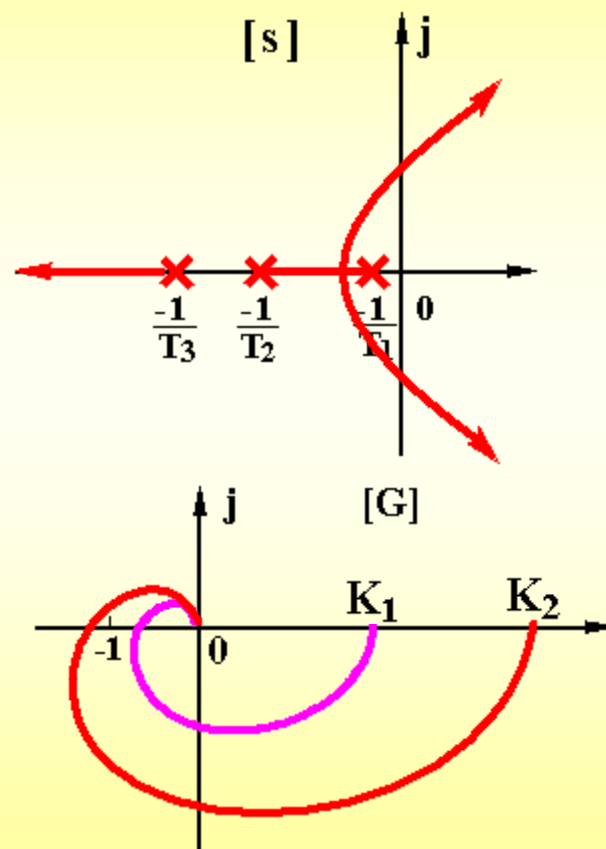
§ 5.4.2 奈氏判据的应用 (2)

例2 已知单位反馈系统开环传递函数, 分析系统稳定性。

$$G(s) = \frac{K}{(T_1s + 1)(T_2s + 1)(T_3s + 1)}$$

解 依题有
$$\begin{cases} G(j0) = K \angle 0^\circ \\ G(j\infty) = 0 \angle -270^\circ \end{cases}$$

$$K = \begin{cases} K_1 \text{ (小)} & R = 0 & \text{(稳定)} \\ Z = P - 2R = 0 - 2 \times 0 = 0 \\ K_2 \text{ (大)} & R = -1 & \text{(不稳定)} \\ Z = P - 2R = 0 - 2(-1) = 2 \end{cases}$$



§ 5.4.2 奈氏判据的应用 (3)

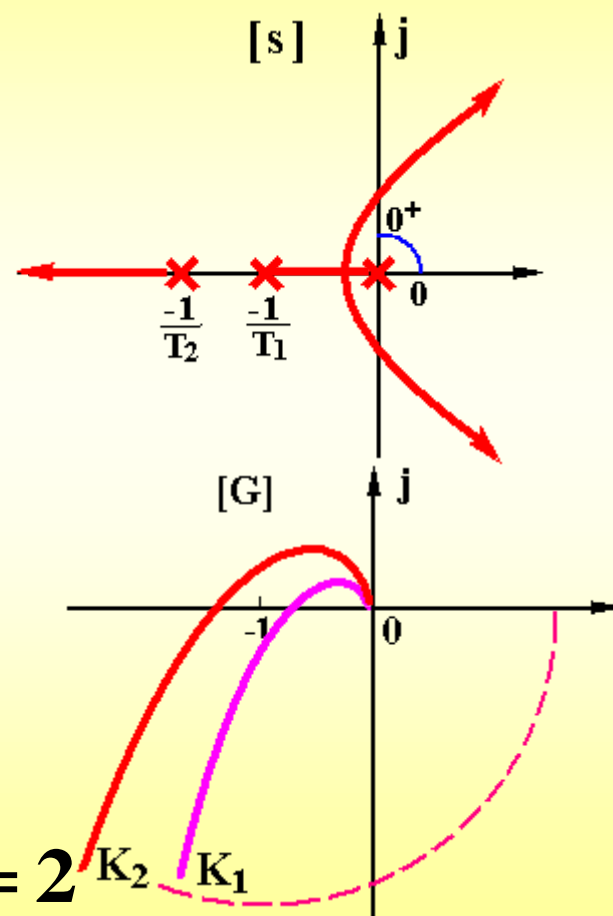
例3 已知单位反馈系统开环传递函数, 分析系统稳定性。

$$G(s) = \frac{K}{s(T_1s + 1)(T_2s + 1)}$$

解 依题有

$$\begin{cases} G(j0) = \infty \angle 0^\circ \\ G(j0^+) = \infty \angle -90^\circ \\ G(j\infty) = 0 \angle -270^\circ \end{cases}$$

$$K = \begin{cases} K_1 \text{ (小)} & R = 0 & \text{(稳定)} \\ Z = P - 2R = 0 - 2 \times 0 = 0 \\ K_2 \text{ (大)} & R = -1 & \text{(不稳定)} \\ Z = P - 2R = 0 - 2 \times (-1) = 2 \end{cases}$$



§ 5.4.2 奈氏判据的应用 (4)

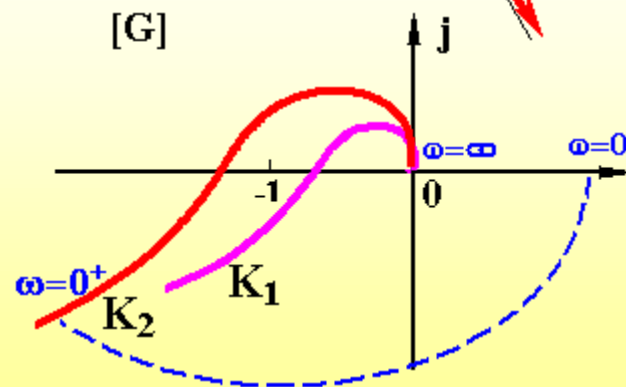
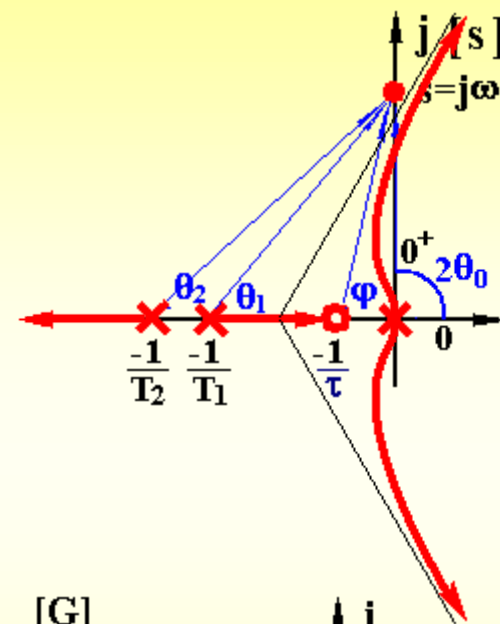
例4 已知单位反馈系统开环传递函数, 分析系统稳定性。

$$G(s) = \frac{K(\tau s + 1)}{s^2(T_1 s + 1)(T_2 s + 1)} \quad \tau > T_1 > T_2$$

解 依题有

$$\begin{cases} G(j0) = \infty \angle 0^\circ \\ G(j0^+) = \infty \angle -180^\circ \\ G(j\infty) = 0 \angle -270^\circ \end{cases}$$

$$K = \begin{cases} K_1 \text{ (小)} & R = 0 & \text{(稳定)} \\ Z = P - 2R = 0 - 2 \times 0 = 0 \\ K_2 \text{ (大)} & R = -1 & \text{(不稳定)} \\ Z = P - 2R = 0 - 2 \times (-1) = 2 \end{cases}$$



§ 5.4.3 对数稳定判据 (1)

伯德图上的奈氏判据

奈氏图

伯德图

单位圆 \rightarrow 0db线 (幅频特性图)

单位圆内 \rightarrow 0db线以下区域

单位圆外 \rightarrow 0db线以上区域

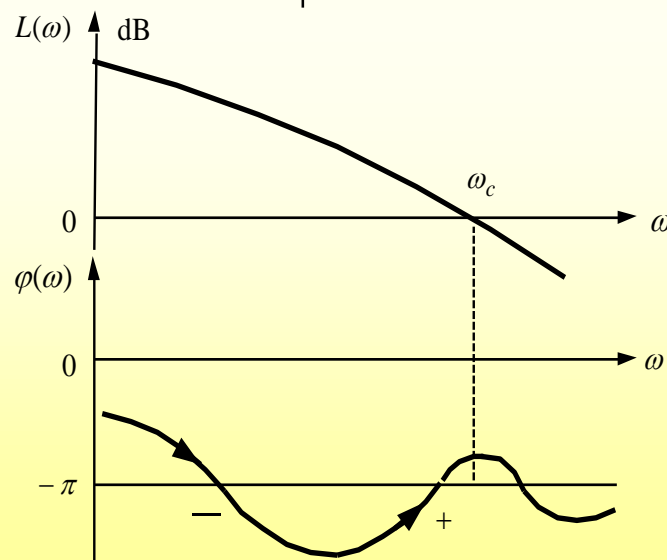
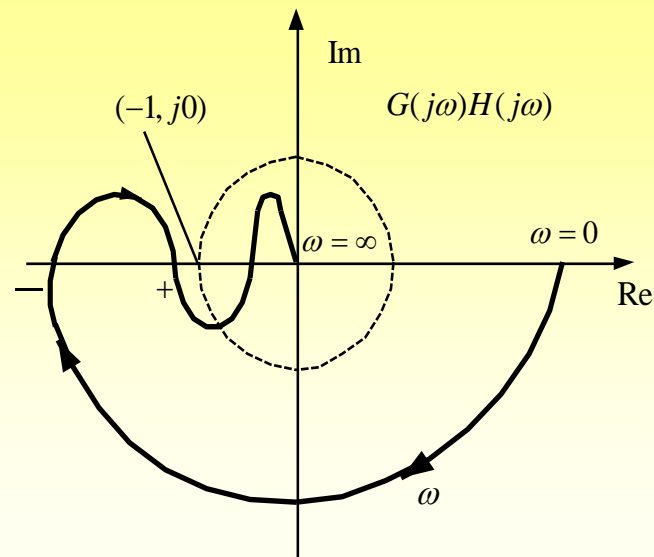
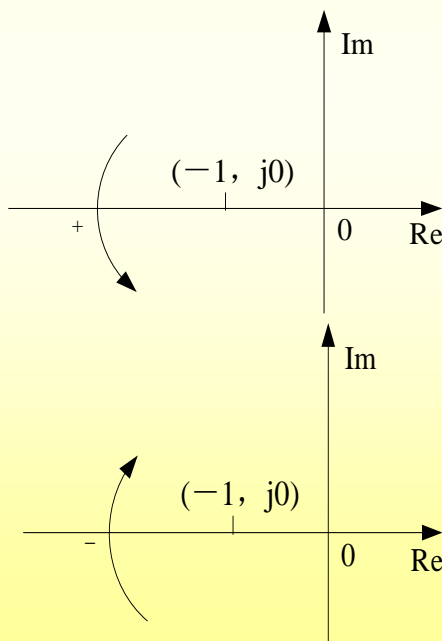
负实轴 $\rightarrow -180^\circ$ 线 (相频特性图)

正穿越:

ω 增加时, 奈氏曲线从上而下穿越 $(-\infty, -1)$ 区间一次 (相角增加), 用 N^+ 表示。

负穿越:

ω 增加时, 奈氏曲线从下而上穿越 $(-\infty, -1)$ 区间一次 (相角增加为负), 用 N^- 表示。



§ 5.4.3 对数稳定判据 (2)

伯德图上的奈氏判据：对数稳定判据

闭环系统稳定的充要条件是：当 ω 由0变到 ∞ 时，在开环对数幅频特性 $L(\omega) \geq 0$ 的频段内，相频特性 $\varphi(\omega)$ 穿越 -180° 线的次数（正穿越 N^+ 与负穿越 N^- 次数之差）为 $P/2$ （ P 为开环传递函数在 s 右半平面的极点数）。

$$N^+ - N^- = P/2$$

若 $G(j\omega)H(j\omega)$ 轨迹起始或终止于 $(-1, j0)$ 以左的负轴上，则穿越次数为半次，即 N^+ 或 N^- 为 $1/2$ 。

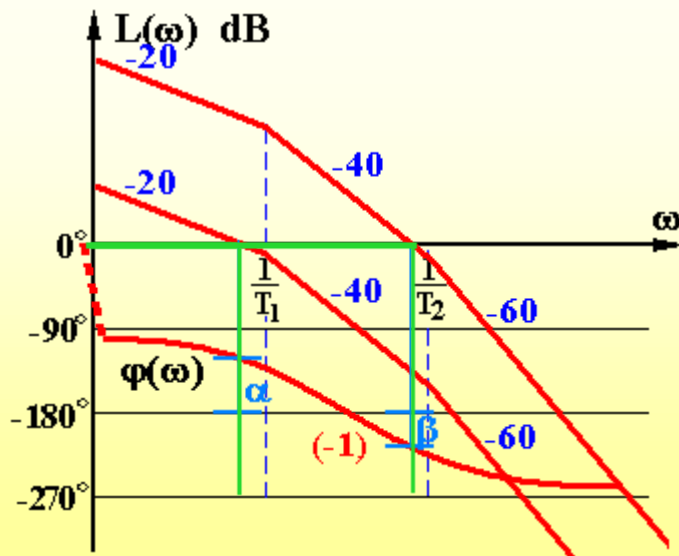
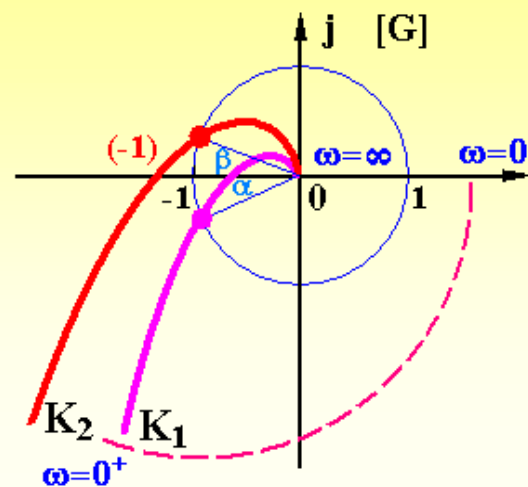
§ 5.4.3 对数稳定判据 (3)

例5 已知单位反馈系统开环传递函数, 分析系统稳定性。

$$G(s) = \frac{K}{s(T_1s + 1)(T_2s + 1)}$$

对数稳定判据 $\begin{cases} Z = P - N = P - 2R \\ R = N_+ - N_- \end{cases}$

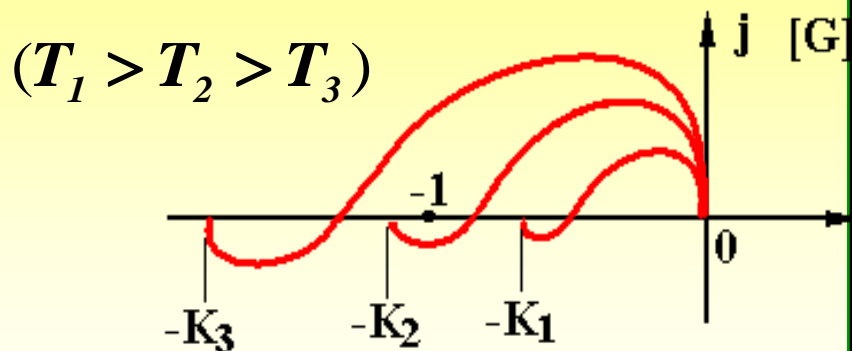
$$K = \begin{cases} K_1 \begin{cases} R = N_+ - N_- = 0 - 0 = 0 \\ Z = P - N = P - 2R = 0 \\ \text{(稳定)} \end{cases} \\ K_2 \begin{cases} R = N_+ - N_- = 0 - 1 = -1 \\ Z = P - 2R = 0 - 2 \times (-1) = 2 \\ \text{(不稳定)} \end{cases} \end{cases}$$



§ 5.4.3 对数稳定判据 (4)

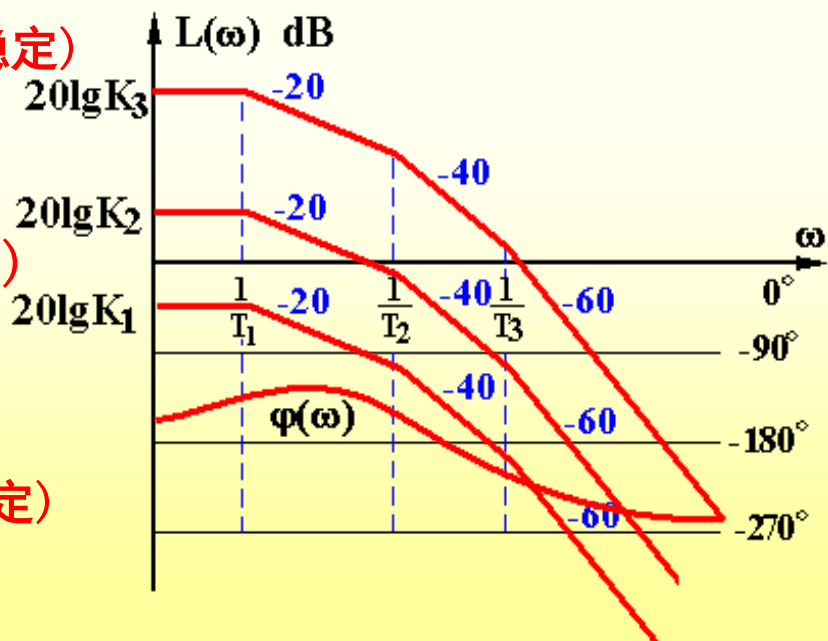
例6 已知单位反馈系统开环传递函数, 分析系统稳定性。

$$G(s) = \frac{K}{(T_1 s - 1)(T_2 s + 1)(T_3 s + 1)} \quad (T_1 > T_2 > T_3)$$



$$\begin{cases} G(j0) = K \angle -180^\circ \\ G(j\infty) = 0 \angle -270^\circ \end{cases}$$

$$K = \begin{cases} K_1 \begin{cases} R = N_+ - N_- = 0 - 0 = 0 \text{ (不稳定)} \\ Z = P - 2R = 1 - 2 \times 0 = 1 \end{cases} \\ K_2 \begin{cases} R = N_+ - N_- = \frac{1}{2} - 0 = \frac{1}{2} \text{ (稳定)} \\ Z = P - 2R = 1 - 2 \times \frac{1}{2} = 0 \end{cases} \\ K_3 \begin{cases} R = N_+ - N_- = \frac{1}{2} - 1 = -\frac{1}{2} \text{ (不稳定)} \\ Z = P - 2R = 1 - 2 \times (-\frac{1}{2}) = 2 \end{cases} \end{cases}$$



§ 5.4.3 对数稳定判据 (5)

特别注意问题

1. 当 $[s]$ 平面虚轴上有开环极点时，奈氏路径要从其右边绕出半径为无穷小的圆弧； $[G]$ 平面对应要补充大圆弧
2. $R=N/2$ 的最小单位为二分之一
3.
$$Z \begin{cases} > 0 & \text{闭环系统不稳定} \\ = 0 & \text{闭环系统稳定} \\ < 0 & \text{有误!} \end{cases}$$

§ 5.5.4 具有延时环节控制系统的稳定性分析

开环传递函数

$$G(s)H(s) = \frac{K \prod_{\mu=1}^m (\tau_{\mu}s + 1)}{s^v \prod_{i=1}^{n-v} (T_i s + 1)} \cdot e^{-\tau s} = G_1(s)H_1(s) \cdot e^{-\tau s}$$

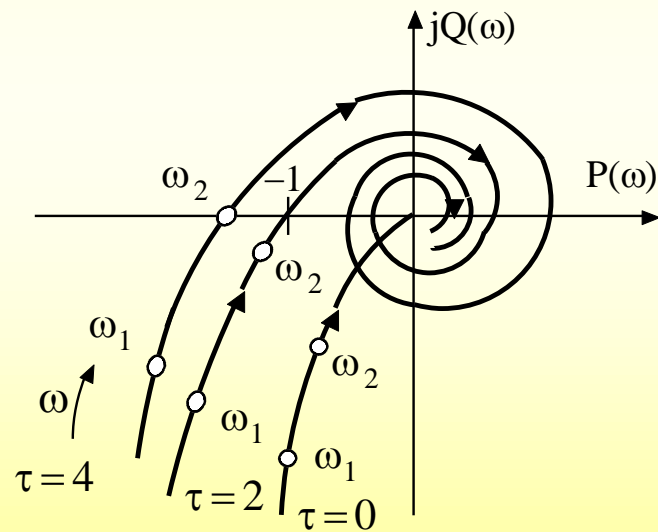
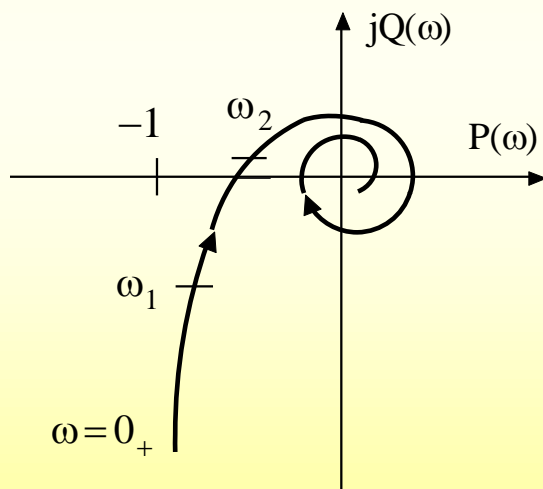
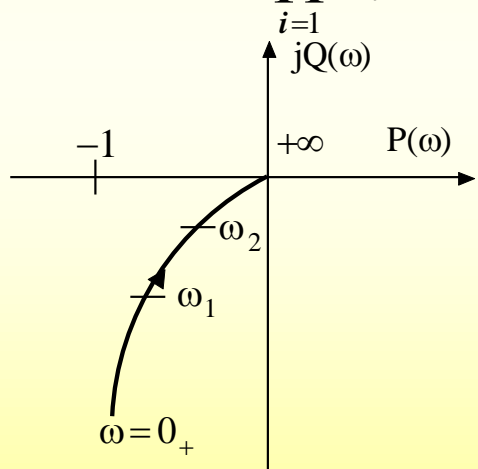
$$G_1(s)H_1(s) = \frac{K \prod_{\mu=1}^m (\tau_{\mu}s + 1)}{s^v \prod_{i=1}^{n-v} (T_i s + 1)}$$

开环频率特性

$$G(j\omega)H(j\omega) = G_1(j\omega)H_1(j\omega) \cdot e^{-j\tau\omega}$$

$$A(j\omega) = |G(j\omega)H(j\omega)| = |G_1(j\omega)H_1(j\omega)|$$

$$\varphi(\omega) = \angle[G_1(j\omega)H_1(j\omega)] - \tau\omega$$



幅频特性与不含延时环节时相同，相频特性滞后 $\tau\omega$ 弧度，不利于稳定。

§ 5.5 稳定裕度 (1)

系统动态性能



稳定程度

稳定边界

稳定程度

时域 (t)

虚轴

阻尼比 ξ

频域 (ω)

$(-1, j0)$

到 $(-1, j0)$ 的距离

稳定裕度

(开环频率指标)

§ 5.5 稳定裕度 (2)

§ 5.5.1 稳定裕度的定义

截止频率 ω_c $|G(j\omega_c)| = 1$

相角裕度 γ $\gamma = 180^\circ + \angle G(j\omega_c)$

相角交界频率 ω_g $\angle G(j\omega_g) = -180^\circ$

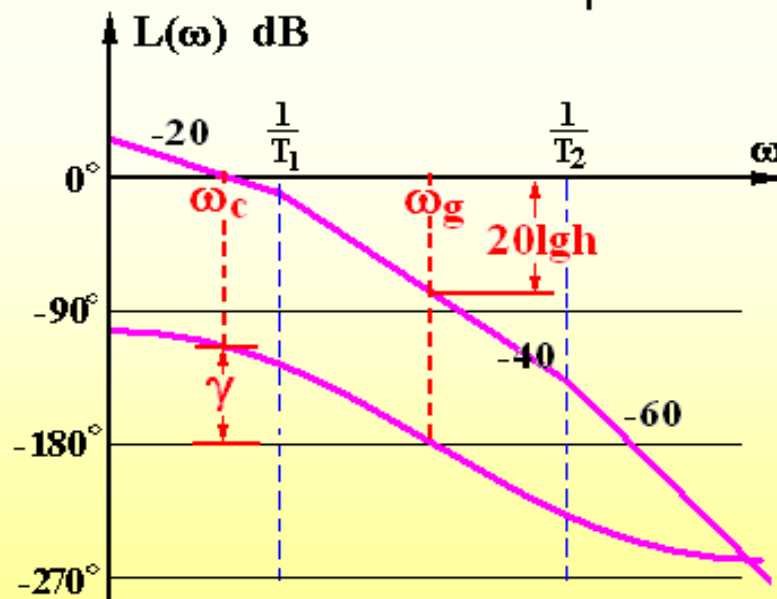
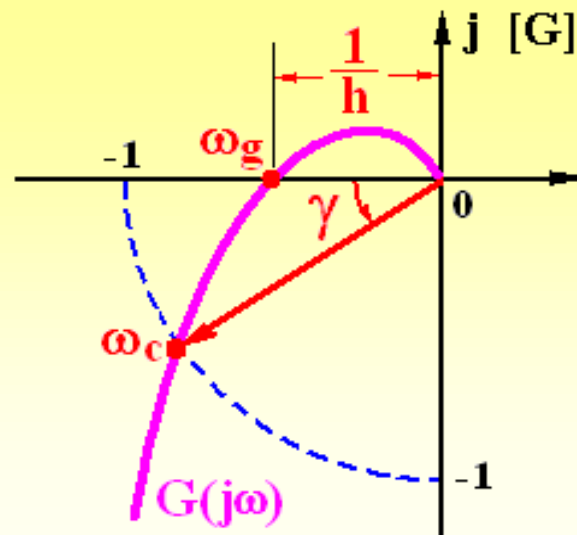
幅值裕度 h $h = \frac{1}{|G(j\omega_g)|}$

γ, h 的几何意义

γ, h 的物理意义

$\begin{cases} \gamma \\ h \end{cases}$ 系统在 $\begin{cases} \text{相角} \\ \text{幅值} \end{cases}$ 方面的稳定储备量

一般要求 $\begin{cases} \gamma > 40^\circ \\ h > 2(6dB) \end{cases}$



§ 5.5 稳定裕度 (3)

§ 5.5.2 稳定裕度的计算

例1 $G(s) = \frac{5}{s(\frac{s}{2} + 1)(\frac{s}{10} + 1)} = \frac{100}{s(s+2)(s+10)}$, 求 γ , h 。

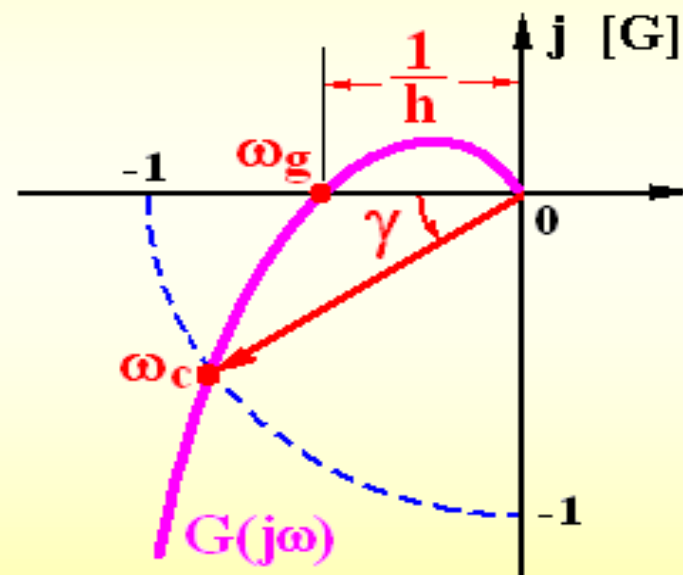
解法I: 由幅相曲线求 γ , h 。

$$(1) \text{ 令 } |G(j\omega_c)| = 1 = \frac{100}{\omega_c \sqrt{\omega_c^2 + 2^2} \sqrt{\omega_c^2 + 10^2}}$$

$$\omega_c^2 [\omega_c^4 + 104\omega_c^2 + 400] = 1000$$

试根得 $\omega_c = 2.9$

$$\begin{aligned} \gamma &= 180^\circ + \angle G(j\omega_c) = 180^\circ + \varphi(2.9) \\ &= 180^\circ - 90^\circ - \arctan \frac{2.9}{2} - \arctan \frac{2.9}{10} \\ &= 90^\circ - 55.4^\circ - 16.1^\circ = 18.5^\circ \end{aligned}$$



§ 5.5 稳定裕度 (4)

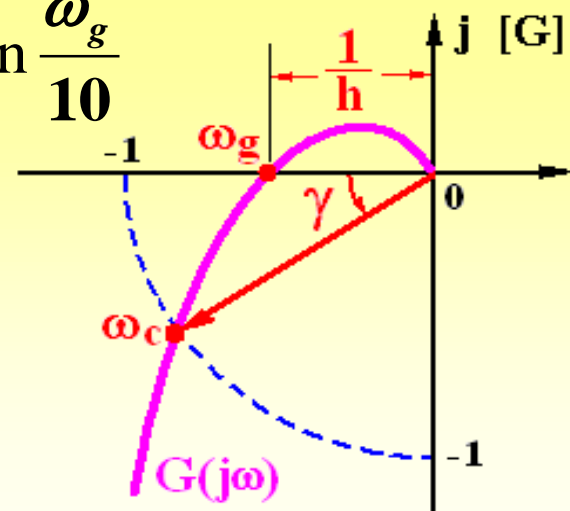
$$G(s) = \frac{5}{s(\frac{s}{2} + 1)(\frac{s}{10} + 1)} = \frac{100}{s(s+2)(s+10)}$$

$$(2) \text{ 令 } \varphi(\omega_g) = -180^\circ = -90^\circ - \arctan \frac{\omega_g}{2} - \arctan \frac{\omega_g}{10}$$

$$\arctan \frac{\omega_g}{2} + \arctan \frac{\omega_g}{10} = 90^\circ$$

$$\frac{\frac{\omega_g}{2} + \frac{\omega_g}{10}}{1 - \frac{\omega_g^2}{20}} = \tan 90^\circ \Rightarrow \begin{aligned} \omega_g^2 &= 20 \\ \omega_g &= 4.47 \end{aligned}$$

$$h = \frac{1}{|G(j\omega_g)|} = \frac{\omega_g \sqrt{\omega_g^2 + 2^2} \sqrt{\omega_g^2 + 10^2}}{100} \Big|_{\omega_g=4.47} = 2.4 \quad (7.6 \text{ dB})$$



或将 $G(j\omega)$ 分解为实部、虚部形式

$$G(j\omega) = \frac{100}{j\omega(2+j\omega)(10+j\omega)} = \frac{-1200\omega - j100(20 - \omega^2)}{\omega(4 + \omega^2)(100 + \omega^2)} = G_X + jG_Y$$

$$\text{Im}[G(j\omega)] = G_Y = 0 \Rightarrow \omega_g = \sqrt{20} = 4.47$$

$$\text{代入实部 } G_X(\omega_g) = -0.4167$$

$$h = \frac{1}{|G(j\omega_g)|} = \frac{1}{0.4167} = 2.4$$

§ 5.5 稳定裕度 (5)

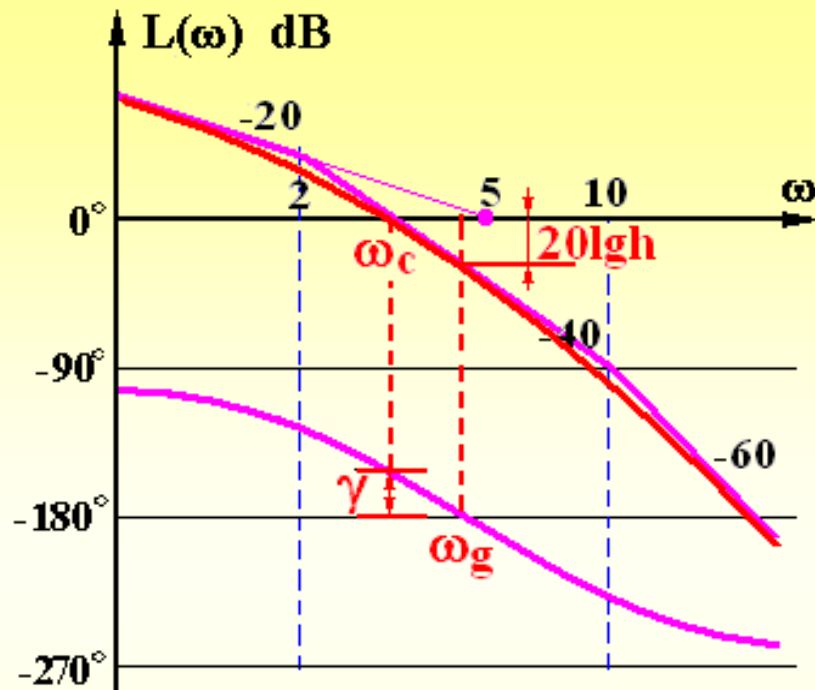
解法II: 由Bode图求 γ , h 。

$$G(s) = \frac{5}{s(\frac{s}{2} + 1)(\frac{s}{10} + 1)}$$

$$\text{由 } L(\omega): |G(j\omega_c)| = 1 = \frac{5}{\omega_c \cdot \frac{\omega_c}{2} \cdot 1} = \frac{10}{\omega_c^2}$$

$$\text{得 } \omega_c = \sqrt{10} = 3.16 > 2.9$$

$$\begin{aligned} \gamma &= 180^\circ + \angle G(j\omega_c) = 180^\circ + \varphi(3.16) \\ &= 180^\circ - 90^\circ - \arctan \frac{3.16}{2} - \arctan \frac{3.16}{10} \\ &= 90^\circ - 57.67^\circ - 17.541^\circ = 14.8^\circ < 18.5^\circ \end{aligned}$$



$$\begin{aligned} \omega_g &= \sqrt{20} = 4.47 \\ h &= \frac{1}{|G(j4.47)|} \\ &= \frac{1}{0.4167} = 2.4 \end{aligned}$$

§ 5.5 稳定裕度 (6)

例2 $G(s) = \frac{6(\frac{s}{2.5} + 1)}{s(\frac{s}{2} + 1)(\frac{s}{5} + 1)(\frac{s}{12.5} + 1)}$, 求 γ , h 。

解. 作 $L(\omega)$ 求 ω_c

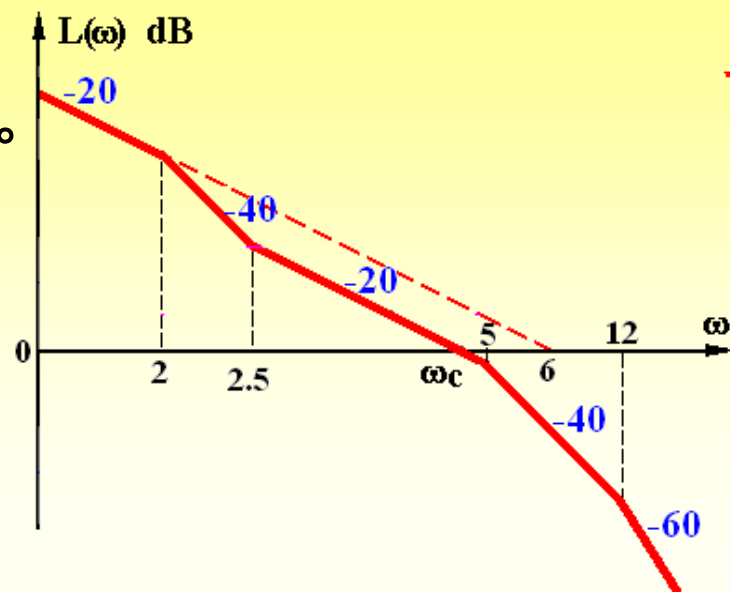
法I: $\frac{6}{\omega_c} = \frac{2.5}{2} \quad \omega_c = \frac{6 \times 2}{2.5} = 4.8$

法II: $G(j\omega_c) = 1 = \frac{6 \times \frac{\omega_c}{2.5}}{\omega_c \cdot \frac{\omega_c}{2} \cdot 1 \cdot 1} = \frac{6 \times 2}{2.5\omega_c} \quad \omega_c = \frac{6 \times 2}{2.5} = 4.8$

$$\gamma = 180^\circ + \angle G(j\omega_c)$$

$$= 180^\circ + \arctan \frac{4.8}{2.5} - 90^\circ - \arctan \frac{4.8}{2} - \arctan \frac{4.8}{5} - \arctan \frac{4.8}{12.5}$$

$$= 180^\circ + 62.5^\circ - 90^\circ - 67.4^\circ - 43.8^\circ - 21^\circ = 20.3^\circ$$



§ 5.5 稳定裕度

$$G(s) = \frac{6(\frac{s}{2.5} + 1)}{s(\frac{s}{2} + 1)(\frac{s}{5} + 1)(\frac{s}{12.5} + 1)} = \frac{300(s + 2.5)}{s(s + 2)(s + 5)(s + 12.5)}$$

求 ω_g $\varphi(\omega_g) = \arctan \frac{\omega_g}{2.5} - 90^\circ - \arctan \frac{\omega_g}{2} - \arctan \frac{\omega_g}{5} - \arctan \frac{\omega_g}{12.5} = -180^\circ$

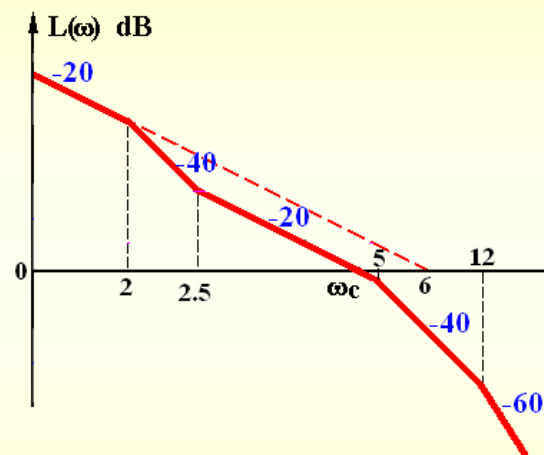
$$\arctan \frac{\omega_g}{12.5} + \arctan \frac{\omega_g}{5} + \arctan \frac{\omega_g}{2} - \arctan \frac{\omega_g}{2.5} = 90^\circ$$

$$\arctan \left[\frac{\frac{\omega_g}{12.5} + \frac{\omega_g}{5}}{1 - \frac{\omega_g^2}{12.5 \times 5}} \right] + \arctan \left[\frac{\frac{\omega_g}{2} - \frac{\omega_g}{2.5}}{1 + \frac{\omega_g^2}{2 \times 2.5}} \right] = 90^\circ$$

$$\arctan \frac{[A] + [B]}{1 - [A] \cdot [B]} = 90^\circ \Rightarrow [A] \cdot [B] = 1$$

整理得 $\omega_g^4 - 49.75\omega_g^2 - 312.5 = 0$ 解出 $\omega_g = 7.4 \text{ (rad/s)}$

$$h = \frac{1}{|G(j\omega_g)|} = \frac{\omega_g \sqrt{\omega_g^2 + 2^2} \sqrt{\omega_g^2 + 5^2} \sqrt{\omega_g^2 + 12.5^2}}{300 \cdot \sqrt{\omega_g^2 + 2.5^2}} = 3.135$$



课程小结

稳定裕度的**概念**

(开环频率指标)

稳定裕度的**定义**

$$\left\{ \begin{array}{ll} \text{截止频率 } \omega_c & |G(j\omega_c)| = 1 \\ \text{相角裕度 } \gamma & \gamma = 180^\circ + \angle G(j\omega_c) \\ \text{相角交界频率 } \omega_g & \angle G(j\omega_g) = -180^\circ \\ \text{幅值裕度 } h & h = \frac{1}{|G(j\omega_g)|} \end{array} \right.$$

稳定裕度的**意义**

$$\left\{ \begin{array}{l} \gamma, h \text{ 的几何意义} \\ \gamma, h \text{ 的物理意义} \end{array} \right.$$

稳定裕度**计算方法**

$$\left\{ \begin{array}{ll} L(\omega) \Rightarrow \omega_c \Rightarrow \gamma = 180^\circ + \varphi(\omega_c) \\ \varphi(\omega) = -180^\circ \Rightarrow \omega_g \Rightarrow h = \frac{1}{|G(j\omega_g)|} \end{array} \right.$$

§ 5.6 利用开环频率特性分析系统的性能 (1)

三频段理论

1. $L(\omega)$ 低频段 \Leftrightarrow 系统稳态误差 e_{ss}

$$G_0(s) = \frac{K}{s^v} \begin{cases} 20\lg|G_0| = 20\lg K - v \cdot 20\lg \omega \\ \angle G_0 = -v \cdot 90^\circ \end{cases}$$

2. $L(\omega)$ 中频段 \Leftrightarrow 系统动态性能 ($\sigma\%$, t_s)

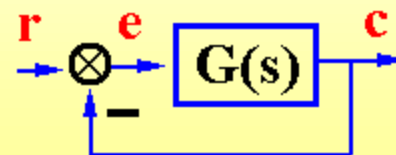
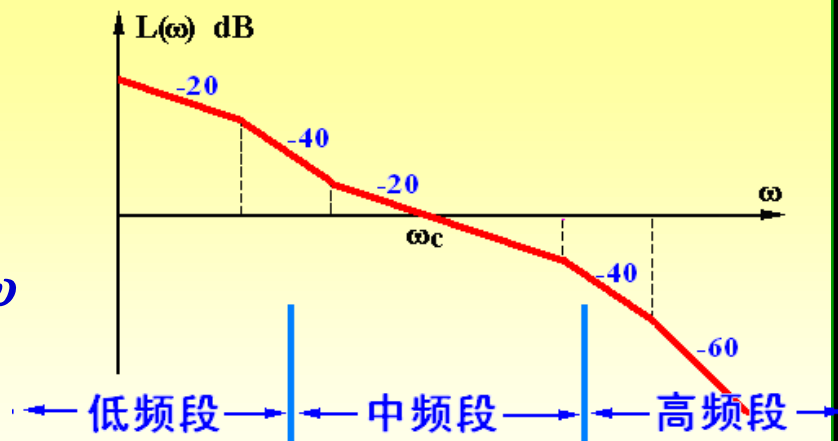
最小相位系统 $L(\omega)$ 曲线斜率与 $\varphi(\omega)$ 的对应关系

-20dB/dec	-90°	$\gamma = 90^\circ$
-40dB/dec	-180°	$\gamma = 0^\circ$
-60dB/dec	-270°	$\gamma = -90^\circ$

希望 $L(\omega)$ 以 -20dB/dec 斜率穿越 0dB 线, 并保持较宽的频段

3. $L(\omega)$ 高频段 \Leftrightarrow 系统抗高频噪声能力

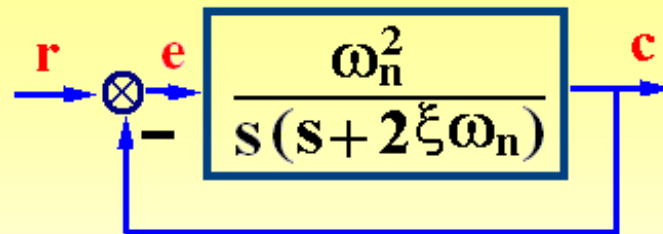
$$\Phi(s) = \frac{G(s)}{1+G(s)} \xrightarrow{|G(s)| \ll 1} |\Phi(s)| \approx |G(s)| \ll 1$$



§ 5.6 利用开环频率特性分析系统的性能 (2)

(1) 二阶系统

$$G(s) = \frac{K}{s(Ts + 1)} = \frac{\omega_n^2}{s(s + 2\xi\omega_n)} \begin{cases} K = \omega_n^2 / 2\xi \\ v = 1 \\ T = \frac{1}{2\xi\omega_n} \end{cases}$$



$$\begin{cases} |G(j\omega)| = \frac{\omega_n^2}{\omega \sqrt{\omega^2 + (2\xi\omega_n)^2}} \\ \angle G(j\omega) = -90^\circ - \arctan \frac{\omega}{2\xi\omega_n} \end{cases}$$

$$\Phi(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$|G(j\omega_c)| = \frac{\omega_n^2}{\omega_c \sqrt{\omega_c^2 + (2\xi\omega_n)^2}} = 1$$

$$\omega_c^2 [\omega_c^2 + 4\xi^2 \omega_n^2] - \omega_n^4 = \omega_c^4 + 4\xi^2 \omega_n^2 \omega_c^2 - \omega_n^4 = 0$$

$$\omega_c = \sqrt{\sqrt{4\xi^4 + 1} - 2\xi^2} \cdot \omega_n$$

$$\gamma = 180^\circ + \varphi(\omega_c) = 90^\circ - \arctan \frac{\omega_c}{2\xi\omega_n} = \arctan \frac{2\xi\omega_n}{\omega_c}$$

§ 5.6 利用开环频率特性分析系统的性能 (3)

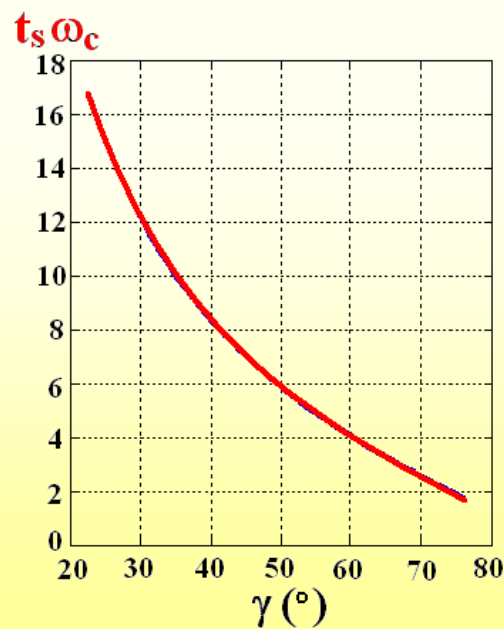
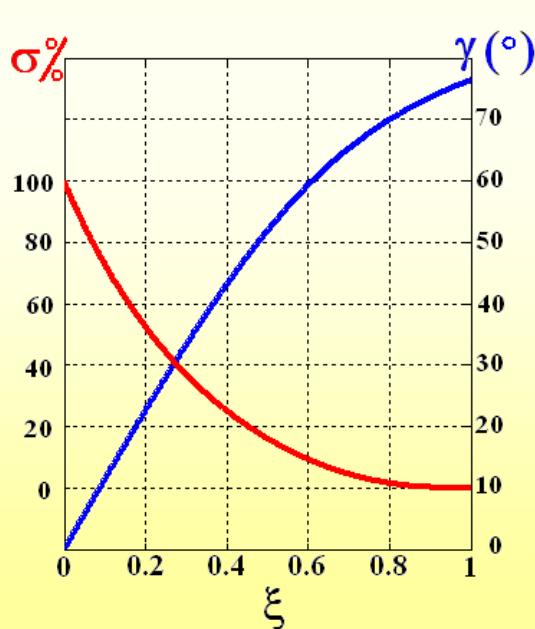
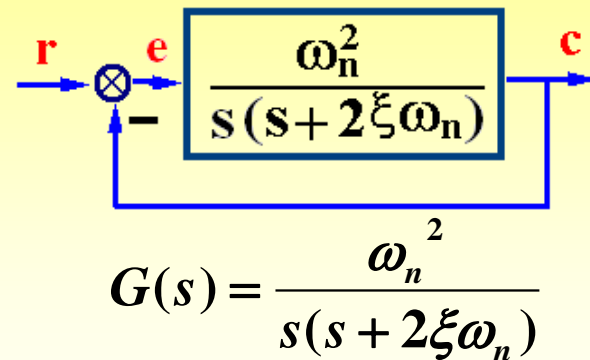
$$\gamma = 180^\circ + \varphi(\omega_c) = 90^\circ - \arctan \frac{\omega_c}{2\xi\omega_n} = \arctan \frac{2\xi\omega_n}{\omega_c}$$

$$\omega_c = \sqrt{\sqrt{4\xi^4 + 1} - 2\xi^2} \cdot \omega_n$$

$$\left. \begin{aligned} \gamma &= \arctan \frac{2\xi}{\sqrt{\sqrt{4\xi^4 + 1} - 2\xi^2}} \\ \sigma\% &= e^{-\pi\xi/\sqrt{1-\xi^2}} \end{aligned} \right\} \gamma \Leftrightarrow \xi \Leftrightarrow \sigma\%$$

$$\text{取 } t_s = \frac{3.5}{\xi\omega_n}$$

$$\begin{aligned} t_s\omega_c &= \frac{3.5}{\xi} \sqrt{\sqrt{4\xi^4 + 1} - 2\xi^2} \\ &= 7 \cdot \frac{\sqrt{\sqrt{4\xi^4 + 1} - 2\xi^2}}{2\xi} = \frac{7}{\tan \gamma} \end{aligned}$$



§ 5.6 利用开环频率特性分析系统的性能 (4)

例 1 已知系统结构图, 求 ω_c , 并确定 $\sigma\%$, t_s 。

解. 绘制 $L(\omega)$ 曲线

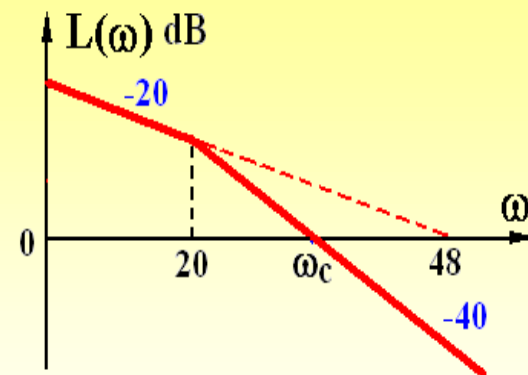
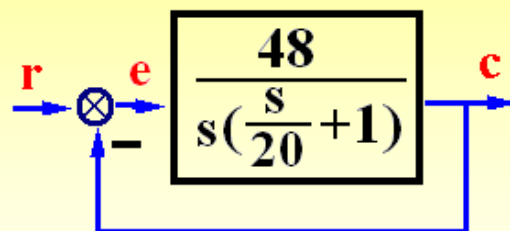
$$\omega_c = \sqrt{20 \times 48} = 31$$

$$\gamma = 180^\circ - 90^\circ - \arctan \frac{31}{20} \\ = 90^\circ - 57.2^\circ = 32.8^\circ$$

查图或根据公式计算:

$$\sigma\% \stackrel{\gamma=32.8^\circ}{\underset{\xi=0.29}{=}} 37\%$$

$$t_s = \frac{7}{\omega_c \cdot \tan \gamma} \\ = \frac{7}{31 \times \tan 32.8^\circ} \\ = 0.35$$



按时域方法:

$$G(s) = \frac{48}{s(s/20 + 1)} = \frac{48 \times 20}{s(s + 20)}$$

$$\Phi(s) = \frac{G(s)}{1 + G(s)} = \frac{960}{s^2 + 20s + 960}$$

$$\sigma\% = e^{-\xi\pi/\sqrt{1-\xi^2}} = 35.3\% \quad \begin{cases} \omega_n = \sqrt{960} = 31 \\ \xi = \frac{20}{2 \times 31} = 0.3226 \end{cases}$$

$$t_s = \frac{3.5}{\xi \omega_n} = \frac{3.5}{10} = 0.35$$

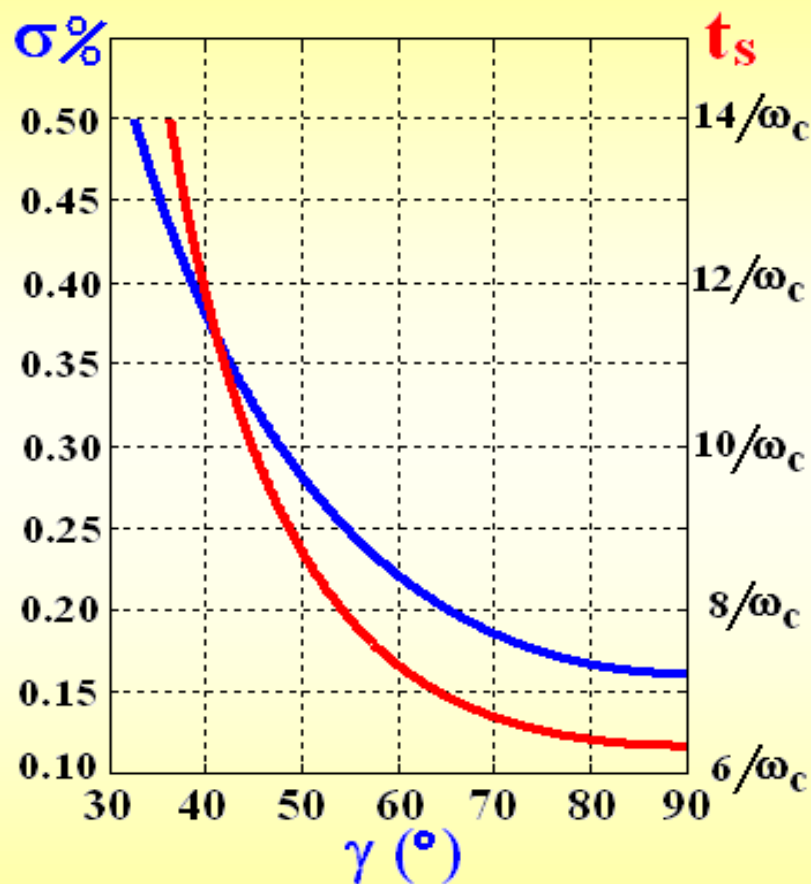
§ 5.6 利用开环频率特性分析系统的性能 (5)

(2) 高阶系统 (开环频率指标与系统时域性能指标之间的关系)

近似公式:

$$\begin{cases} \sigma\% = \left[0.16 + 0.4 \left(\frac{1}{\sin \gamma} - 1 \right) \right] \times 100\% \\ t_s = \frac{\pi}{\omega_c} \left[2 + 1.5 \left(\frac{1}{\sin \gamma} - 1 \right) + 2.5 \left(\frac{1}{\sin \gamma} - 1 \right)^2 \right] \end{cases}$$

$$(35^\circ \leq \gamma \leq 90^\circ)$$

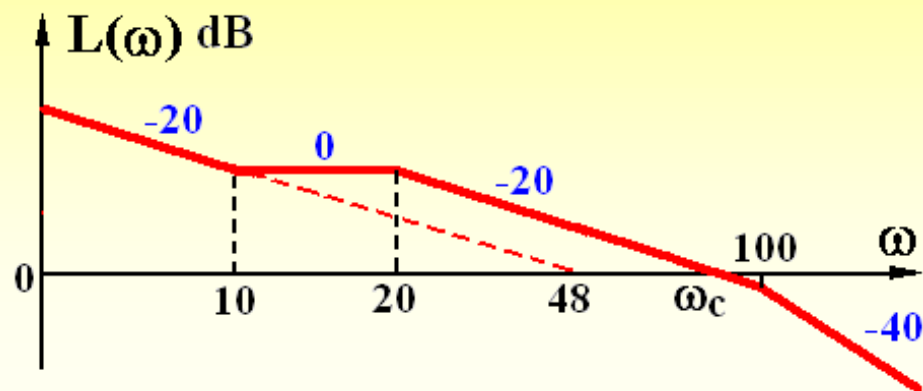


§ 5.6 利用开环频率特性分析系统的性能 (6)

例2 已知单位反馈系统 $G(s)$, 求 ω_c , γ ; 确定 $\sigma\%$, t_s 。

$$G(s) = \frac{48(\frac{s}{10} + 1)}{s(\frac{s}{20} + 1)(\frac{s}{100} + 1)}$$

解. 绘制 $L(\omega)$ 曲线



$$\frac{\omega_c}{48} = \frac{20}{10} \quad \omega_c = 48 \times 2 = 96$$

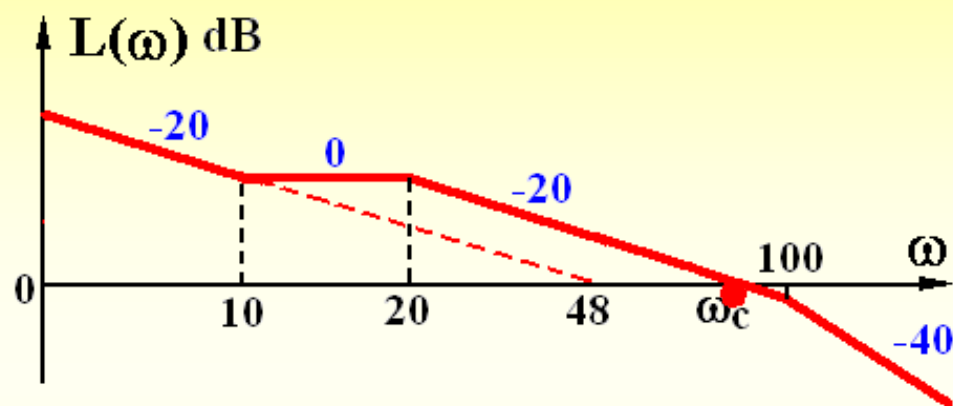
$$\begin{aligned} \gamma &= 180^\circ + \varphi(\omega_c) = 180^\circ + \arctan \frac{96}{10} - 90^\circ - \arctan \frac{96}{20} - \arctan \frac{96}{100} \\ &= 180^\circ + 84^\circ - 90^\circ - 78.2^\circ - 43.8^\circ = 52.1^\circ \end{aligned}$$

查图或基于近似公式

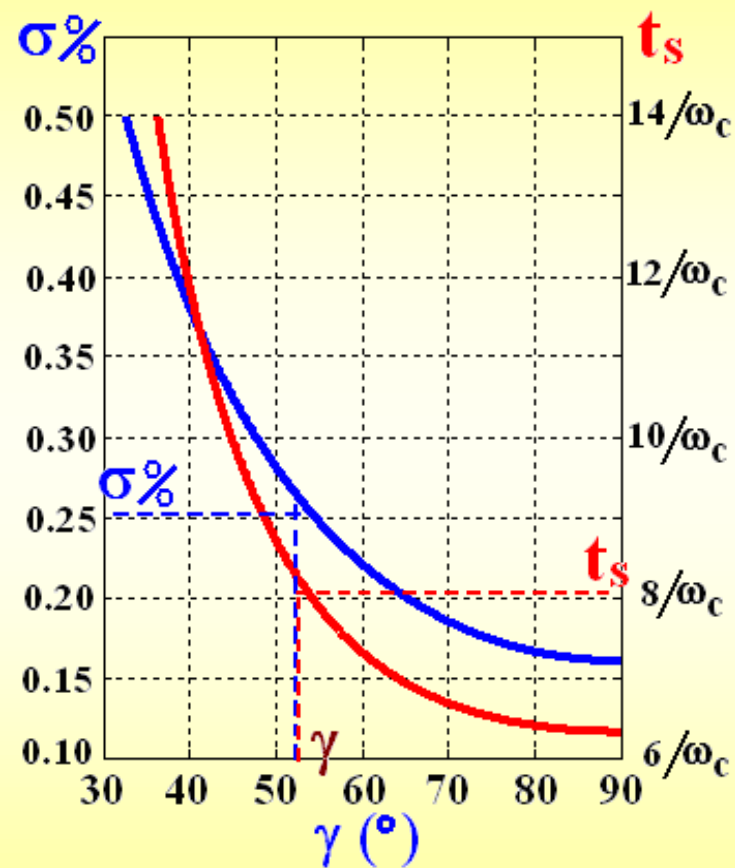
$$\left\{ \begin{array}{l} \sigma\% \stackrel{\gamma=52.1^\circ}{=} 27\% \\ t_s = \frac{8}{\omega_c} = \frac{8}{96} = 0.0833 \end{array} \right.$$

§ 5.6 利用开环频率特性分析系统的性能 (7)

用频域法估算高阶系统动态性能



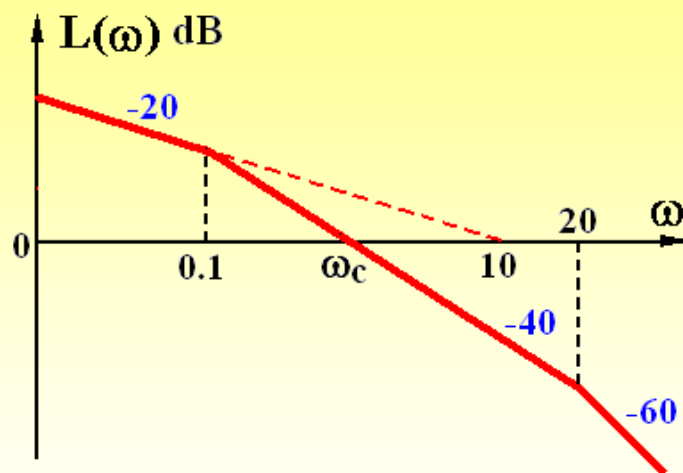
$$L(\omega) \Rightarrow \omega_c \Rightarrow \gamma \Rightarrow \sigma\%$$
$$\omega_c \Rightarrow t_s = \frac{a}{\omega_c}$$



§ 5.6 利用开环频率特性分析系统的性能 (8)

例3 已知最小相位系统 $L(\omega)$ 如图所示, 试确定

- (1) 开环传递函数 $G(s)$;
- (2) 由 γ 确定系统的稳定性;
- (3) 将 $L(\omega)$ 右移10倍频, 讨论对系统的影响。



解. (1)
$$G(s) = \frac{10}{s(\frac{s}{0.1} + 1)(\frac{s}{20} + 1)}$$

(2)
$$\omega_c = \sqrt{0.1 \times 10} = 1$$

$$\gamma = 180^\circ - 90^\circ - \arctan \frac{1}{0.1} - \arctan \frac{1}{20}$$

$$= 90^\circ - 84.3^\circ - 2.86^\circ = 2.8^\circ > 0 \text{ 稳定}$$

$L(\omega)$ 右移后 $\begin{cases} \gamma \text{ 不变} \rightarrow \sigma\% \text{ 不变} \\ \omega_c \text{ 增大} \rightarrow t_s \text{ 减小} \end{cases}$

(3) 将 $L(\omega)$ 右移10倍频后有

$$G(s) = \frac{100}{s(\frac{s}{1} + 1)(\frac{s}{200} + 1)}$$

$$\omega_c = \sqrt{1 \times 100} = 10$$

$$\gamma = 180^\circ - 90^\circ - \arctan \frac{10}{1} - \arctan \frac{10}{200}$$

$$= 90^\circ - 84.3^\circ - 2.86^\circ = 2.8^\circ$$

§ 5.6 利用开环频率特性分析系统的性能 (9)

三频段理论

	频段	对应性能	希望形状
$L(\omega)$	低频段	$\left\{ \begin{array}{l} \text{开环增益 } K \\ \text{系统型别 } \nu \end{array} \right.$ 稳态误差 e_{ss}	陡, 高
	中频段	$\left\{ \begin{array}{l} \text{截止频率 } \omega_c \\ \text{相角裕度 } \gamma \end{array} \right.$ 动态性能 $\left\{ \begin{array}{l} \sigma \% \\ t_s \end{array} \right.$	缓, 宽
	高频段	系统抗高频干扰的能力	低, 陡

三频段理论并没有提供设计系统的具体步骤,
但给出了调整系统结构,改善系统性能的原则和方向

§ 5.6 利用开环频率特性分析系统的性能 (10)

关于三频段理论的说明：

- ① 各频段分界线没有明确的划分标准；
- ② 与无线电学科中的“低”、“中”、“高”
频概念不同；
- ③ 不能用是否以-20dB/dec过0dB线作为判定闭环系统是否稳定的标准；
- ④ 只适用于单位反馈的最小相位系统。

§ 5.7 利用闭环频率特性分析系统的性能 (1)

研究闭环频率特性的必要性

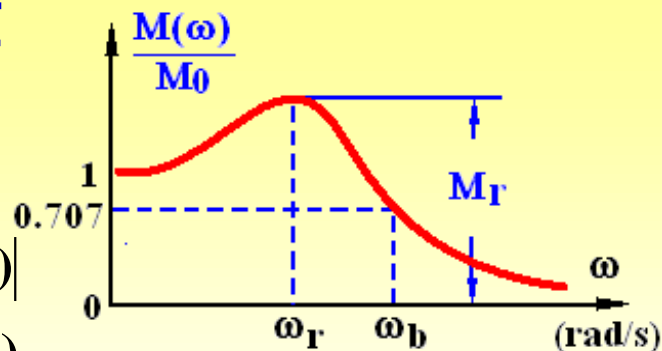
- (1) 闭环频率特性的一些特征量在实际工程中应用十分广泛；
- (2) 通过实验方法很容易得到系统的闭环频率特性；
- (3) 通过闭环频率特性可以估算系统的性能指标。

§ 5.7 利用闭环频率特性分析系统的性能 (2)

§ 5.7.1 闭环频率特性及几个特征量

单位反馈系统开环传递函数: $G(s)$

$$\Phi(j\omega) = \frac{G(j\omega)}{1+G(j\omega)} = M(\omega) \cdot e^{j\phi(\omega)} \quad \begin{cases} M(\omega) = |\Phi(j\omega)| \\ \phi(\omega) = \angle \Phi(j\omega) \end{cases}$$



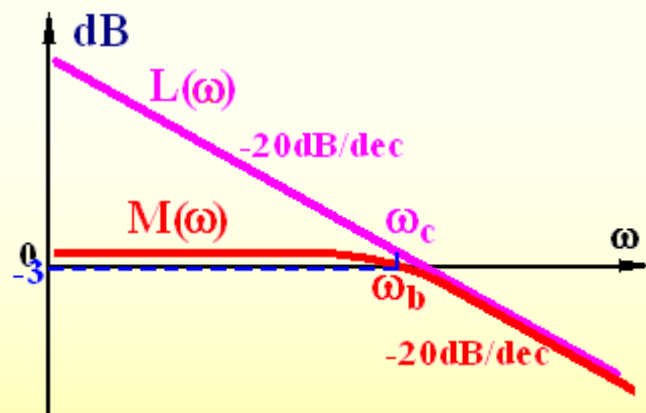
闭环频率特性

(1) 零频值 $M_0 = M(0)$

(2) $\begin{cases} \text{谐振频率 } \omega_r \\ \text{谐振峰值 } M_r \end{cases}$ 对二阶欠阻尼系统 $\begin{cases} \omega_r = \omega_n \sqrt{1-2\xi^2} \\ M_r = \frac{1}{2\xi \sqrt{1-\xi^2}} \end{cases}$

(3) 带宽频率 ω_b

$M(\omega)$ 下降到 $0.707 M_0$ 对应的频率值 ω_b



对一阶系统: $\begin{cases} G(s) = \frac{1}{Ts} & \omega_c = 1/T \\ \Phi(s) = \frac{1}{Ts+1} & \omega_b = 1/T \end{cases} \quad t_s = 3T = \frac{3}{\omega_c} = \frac{3}{\omega_b}$

§ 5.7 利用闭环频率特性分析系统的性能 (3)

§ 5.7.2 闭环频域指标与时域指标的关系

(1) 二阶系统 $\Phi(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$

$$M_0 = M(0) = 1$$

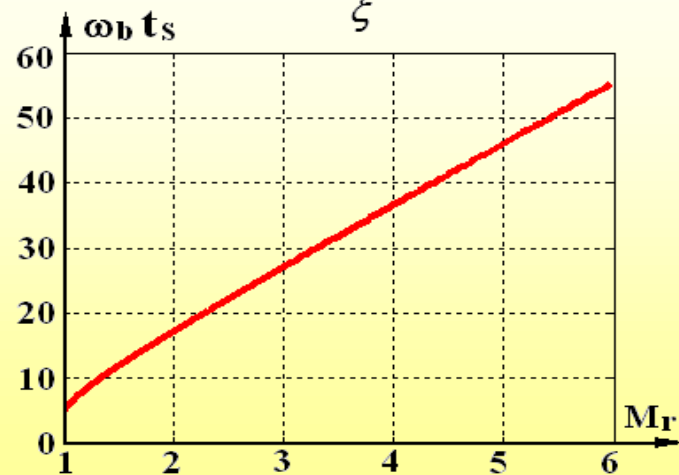
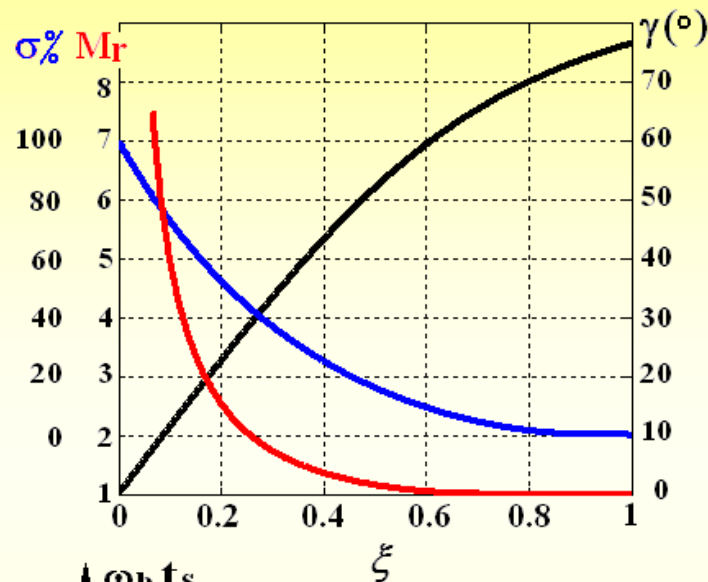
$$\begin{cases} \omega_r = \omega_n \sqrt{1 - 2\xi^2} \\ M_r = \frac{1}{2\xi\sqrt{1 - \xi^2}} \end{cases} \quad (0 \leq \xi \leq 0.707)$$

$$M(\omega_b) = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega_b^2)^2 + (2\xi\omega_n\omega_b)^2}} = 0.707$$

$$\omega_b = \omega_n \sqrt{1 - 2\xi^2 + \sqrt{2 - 4\xi^2 + 4\xi^4}}$$

$$t_s = 3.5 / \xi \omega_n$$

$$\omega_b t_s = \frac{3.5}{\xi} \sqrt{1 - 2\xi^2 + \sqrt{2 - 4\xi^2 + 4\xi^4}}$$



§ 5.7 利用闭环频率特性分析系统的性能 (4)

例1 实验测得某闭环系统的对数幅频特性如图所示, 试确定系统的动态性能 ($\sigma\%$, t_s)。

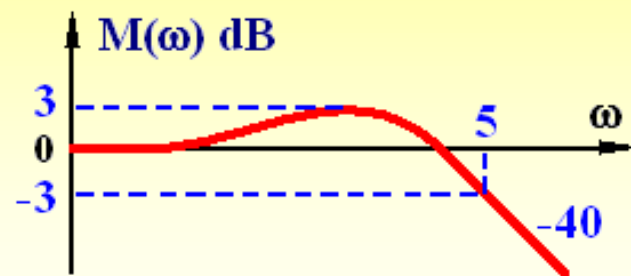
解. 依图, 可以确定是欠阻尼二阶系统

$$20\lg M_r = 3 \text{ dB}$$

$$\begin{cases} M_r = 10^{\frac{3}{20}} = 1.4125 \\ \omega_b = 5 \end{cases}$$

$$\begin{aligned} \xi &= 0.4 & \sigma\% &= 25\% \\ t_s \cdot \omega_b &= 9 & t_s &= 9/5 = 1.8 \end{aligned}$$

由
$$\begin{cases} M_r = \frac{1}{2\xi\sqrt{1-\xi^2}} \\ \omega_b = \omega_n \sqrt{1-2\xi^2 + \sqrt{2-4\xi^2 + 4\xi^4}} \end{cases} \begin{cases} \text{解出 } \xi, \omega_n \\ \Phi(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} \\ \text{可确定 } \sigma\%, t_s \end{cases}$$



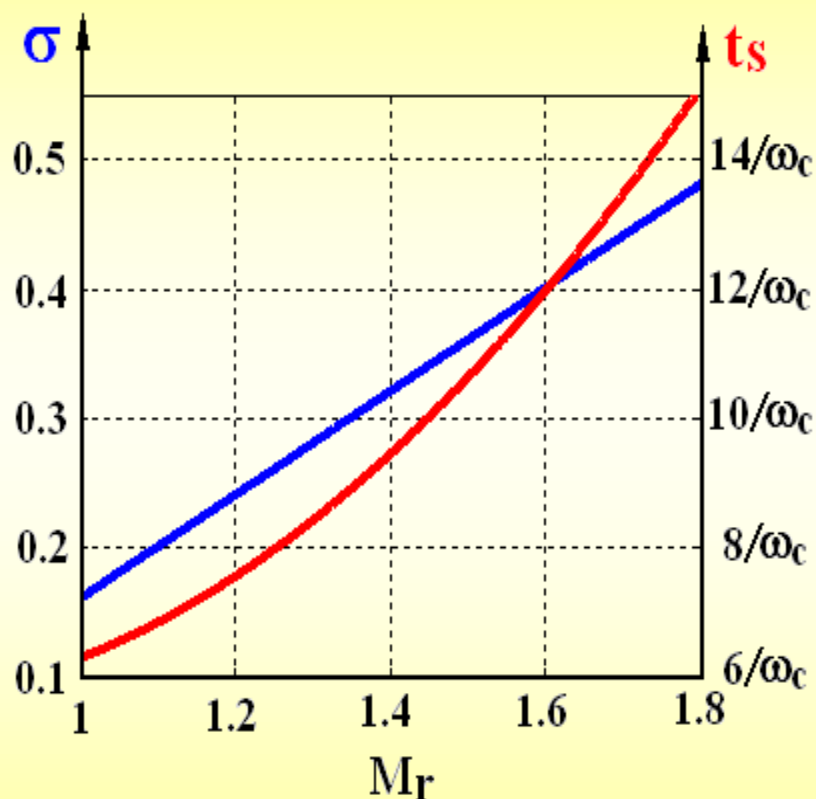
§ 5.7 利用闭环频率特性分析系统的性能 (5)

(2) 高阶系统

$$\sigma\% = [0.16 + 0.4(M_r - 1)] \times 100\%$$

$$t_s = \frac{\pi}{\omega_b} \left[2 + 1.5(M_r - 1) + 2.5(M_r - 1)^2 \right]$$

$$(1 \leq M_r \leq 1.8)$$



§ 5.7 利用闭环频率特性分析系统的性能 (6)

例4 一台记录仪的传递函数为 $\Phi(s) = \frac{1}{Ts + 1}$, 要求在5Hz以内时, 记录仪的振幅误差不大于被测信号的10%, 试确定记录仪应有的带宽 $\omega_b = ?$

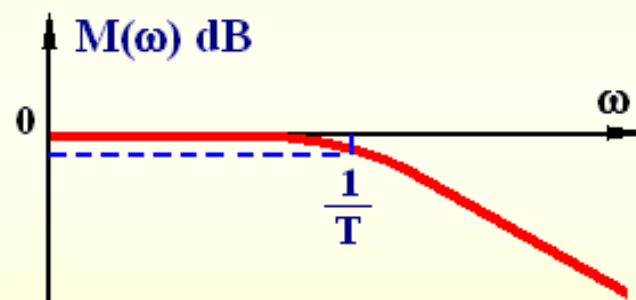
解. 依题意, 当 $\omega = 5 \times 2\pi = 10\pi$ (rad/s) 时

$$\text{要求 } \left| \frac{1}{1 + jT\omega} \right| = \frac{1}{\sqrt{1 + T^2\omega^2}} \geq 0.9$$

$$\text{即 } T^2\omega^2 + 1 \leq \frac{1}{0.9^2}$$

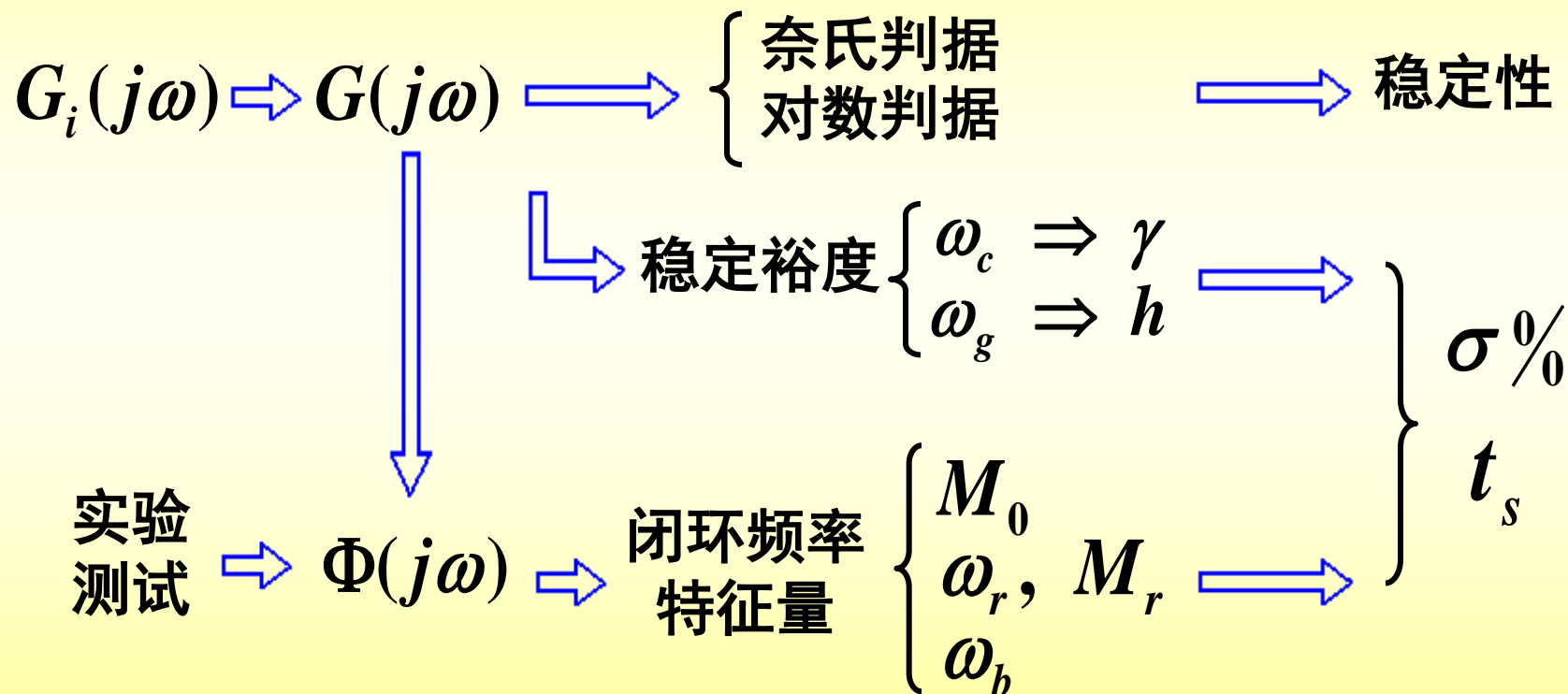
$$T \leq \frac{1}{\omega} \sqrt{\frac{1}{0.9^2} - 1} \Big|_{\omega=10\pi} = 0.0154$$

$$\omega_b = \frac{1}{T} \geq \frac{1}{0.0154} = 64.833 \text{ (rad/s)}$$



课程小结

用频域分析方法估算系统的动态性能



闭环频率特性曲线的绘制(1)

用向量法求闭环频率特性

$$G(s) = \frac{K}{s(T_1s + 1)(T_2s + 1)}$$

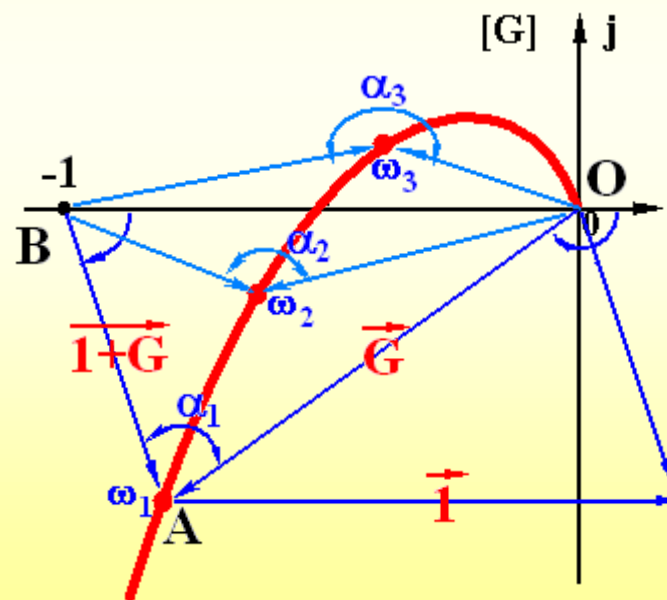
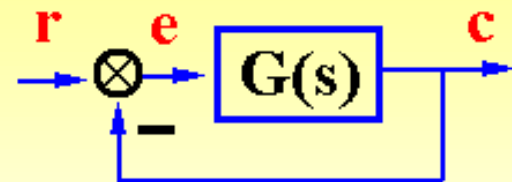
$$\Phi(j\omega) = \frac{G(j\omega)}{1 + G(j\omega)} = M(\omega) \cdot e^{j\phi(\omega)} \quad \begin{cases} M(\omega) = |\Phi(j\omega)| \\ \phi(\omega) = \angle \Phi(j\omega) \end{cases}$$

$$G(j\omega) = \overrightarrow{OA}$$

$$1 + G(j\omega) = \overrightarrow{BA}$$

$$\Phi(j\omega) = \frac{\overrightarrow{OA}}{\overrightarrow{BA}} \left\{ \angle \overrightarrow{OA} - \angle \overrightarrow{BA} \right\}$$

$$\begin{cases} M(\omega) = \left| \frac{\overrightarrow{OA}}{\overrightarrow{BA}} \right| \\ \phi(\omega) = \angle \overrightarrow{OA} - \angle \overrightarrow{BA} = \alpha \end{cases}$$



闭环频率特性曲线的绘制 (2)

等M圆 等N圆图

等M圆 — $|\Phi(\omega)| = \frac{OA}{BA}$ 为常数的轨迹

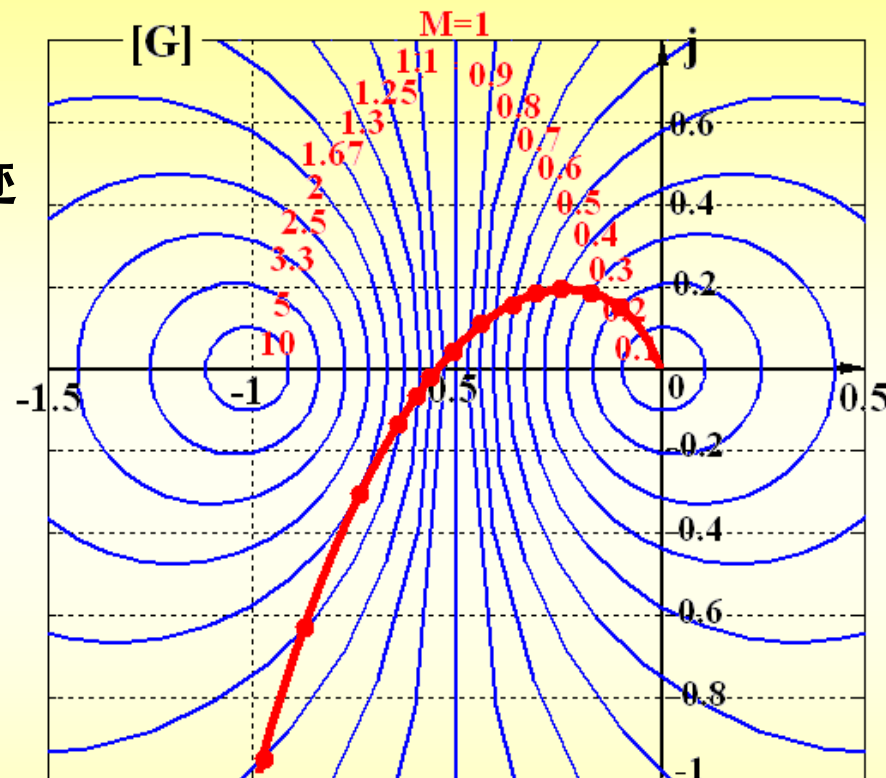
设 $G(j\omega) = X + jY$

$\Phi(j\omega) = M(\omega) \angle \alpha(\omega)$

$$|\Phi| = M(\omega) = \left| \frac{G}{1+G} \right| = \left| \frac{X + jY}{1 + X + jY} \right|$$

$$= \frac{\sqrt{X^2 + Y^2}}{\sqrt{(X+1)^2 + Y^2}} = M(\omega)$$

整理得 $\left(X - \frac{M^2}{1-M^2} \right)^2 + Y^2 = \left(\frac{M}{1-M^2} \right)^2$ — 等M圆方程



闭环频率特性曲线的绘制 (3)

等N圆 — $\angle OAB = \alpha$ 为常数的轨迹

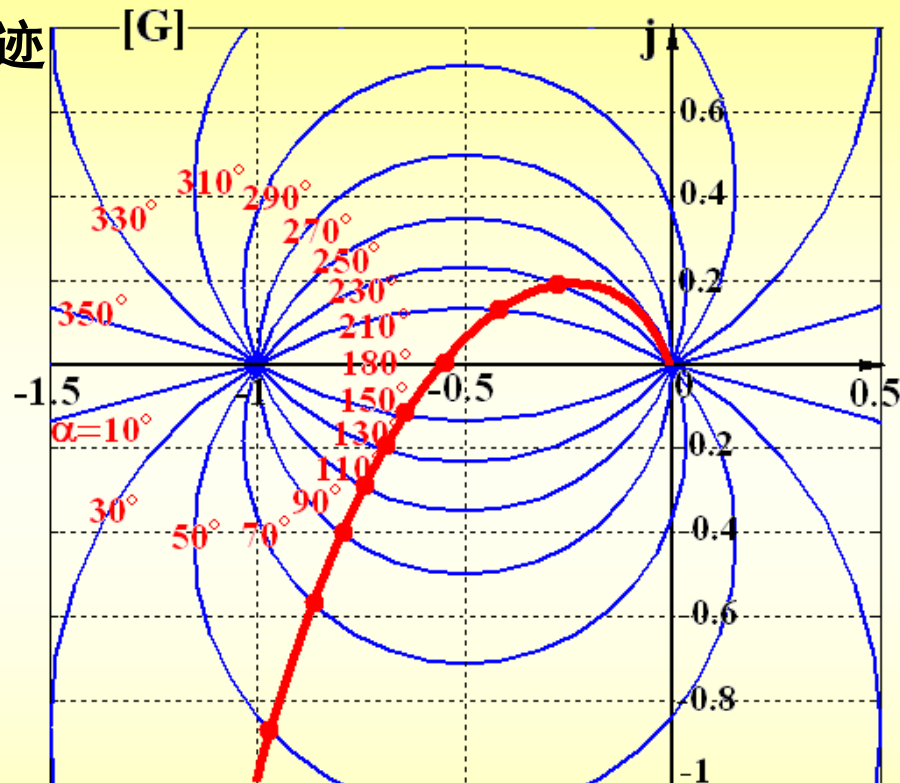
设 $G(j\omega) = X + jY$

$$\Phi(j\omega) = \frac{G}{1+G} = \frac{X + jY}{1 + X + jY}$$
$$= \frac{X^2 + X + Y^2 + jY}{(X+1)^2 + Y^2}$$

$$\angle \Phi(\omega) = \arctan \frac{Y}{X^2 + X + Y^2} = \alpha$$

$$\tan \alpha = N(\omega) = \frac{Y}{X^2 + X + Y^2}$$

整理得 $\left(X + \frac{1}{2}\right)^2 + \left(Y - \frac{1}{2N}\right)^2 = \frac{N^2 + 1}{4N^2}$ — 等N圆方程



例1 已知 $G(s) = \frac{11.7}{s(\frac{s}{10} + 1)(\frac{s}{20} + 1)}$
求 $\Phi(j\omega)$

ω rad/s	1	3	5	9	11.7	20
$L(\omega)$ dB	21.3	11.5	6.3	-1	-5.2	-14.5
$\varphi(\omega)$ (°)	-99°	-115°	-130°	-157°	-170°	-198°
$M(\omega)$ dB	0.1	0.67	2.2	6.9	1.5	-12.8
$\alpha(\omega)$ (°)	-5°	-14°	-28°	-95°	-158°	-202°
$M(\omega)$	1.01	1.08	1.29	2.21	1.19	0.23

