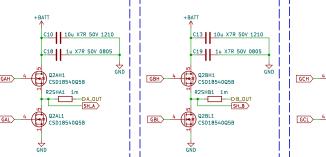
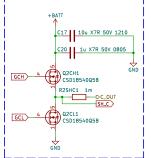




PHASE B HALF-BRIDGE

PHASE C HALF-BRIDGE





CURRENT SENSE RESISTORS

-> P_SENSE = I^2 * R = 50^2 * 1 / 1000 = 2.5 W -> V_SENSE = IR = +- 50 * 1 / 1000 = +- 50 mV

Therefore with the TMC6200-TA's 5 V/V gain setting: -> V_SENSE_OUT = +- 50 mV * 5 V/V = +- 0.25 V

With $V_REF = 1.65 \text{ V}$, we get V_OUT in the range [1.4 V, 1.9

The STM32's internal OPAMP gain can the be programmed with a gain of 4 to get [0.65, 2.65]. It is done this way to supporta wider range of currents.

For example if your motor's max current is 10A, we get 50mV drop across R_SH, to give an initial range of +- 0.05V (ideal range would be +- 1.6V) and we can use an internal opamp gain of 32 to get +- 1.6V.

Note gain options: 1, 2, 4, 8, 16, 32, 64. This means that sensing can be optimised for currents between 1A and 100A

CSD18543Q3A MOSFET INFO:

Product Summary					
T _A = 25°C		TYPICAL VALUE		UNIT	
V _{DS}	Drain-to-Source Voltage	60		V	
Q,	Gate Charge Total (10 V)	41		nC	
Q _{pd}	Gate Charge Gate-to-Drain	6.7		nC	
R _{DS(on)}	Drain-to-Source On Resistance	V _{GS} = 4.5 V	2.6	mΩ	
		V _{GS} = 10 V	1.8		
V	Throchold Voltago	1.0		W	

T _A = 25°C		VALUE	UNIT	
V _{DS}	Drain-to-Source Voltage	60	V	
V _{GS}	Gate-to-Source Voltage	±20	V	
l _D	Continuous Drain Current (Package Limited)	100		
	Continuous Drain Current (Silicon Limited), T _C = 25°C	205	A	
	Continuous Drain Current(1)	29		
I _{DM}	Pulsed Drain Current, T _A = 25°C ⁽²⁾	400	A	
PD	Power Dissipation ⁽¹⁾	3.8	w	
	Power Dissipation, T _C = 25°C	188		
T _J , T _{stg}	Operating Junction, Storage Temperature	-55 to 175	*C	
E _{AS}	Avalanche Energy, Single Pulse I _D = 80 A, L = 0.1 mH, R _G = 25 Ω	320	mJ	

- Typical R_{BJA} = 40°C/W on a 1-in², 2-oz Cu pad on a 0.06-in thick FR4 PCB.
- (2) Max R_{RJC} = 0.8°C/W, pulse duration \leq 100 μ s, duty cycle \leq

MOSFET DECOUPLING

C = (1 * dt) / dV = (50A * 10ns) / 0.2 V = 2.5 uF I use 10uF + 1uf MLCCs close to each MOSFET for a total of 11uF per MOSFET for some margin

This calculation uses the rise time (dt) and the allowable voltage drop on the decoupling cap (dV) to calculate the required capacitance of the cap

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