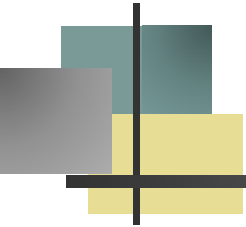




# Chapter 4 Part II

## Time-Dependent Failure Models



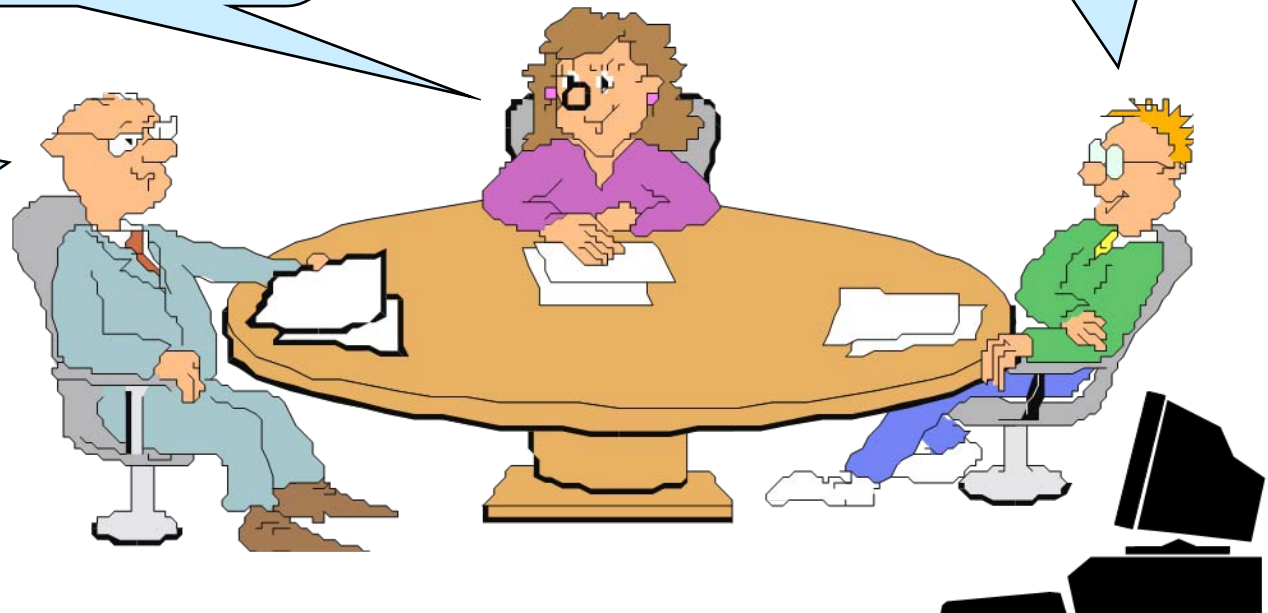
The Normal Distribution  
LogNormal Distribution  
Gamma Distribution

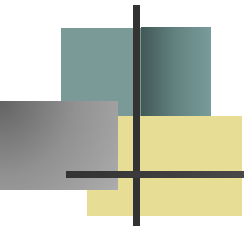
# The Normal Distribution

I understand that the lecture will return to normal.

Ok, But what's a normal deviate?

I really liked those Weibull's





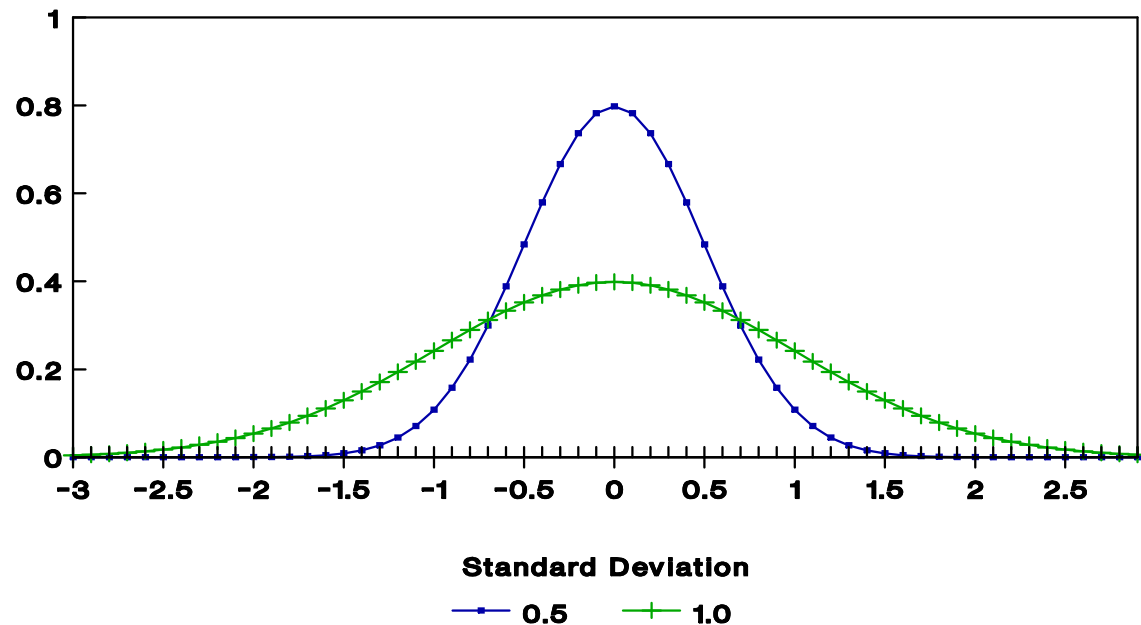
# The Normal Probability Density Function

$$f(t) = \frac{1}{\sqrt{2\pi} \sigma} e^{-\frac{1}{2} \frac{(t-\mu)^2}{\sigma^2}}, -\infty < t < \infty$$

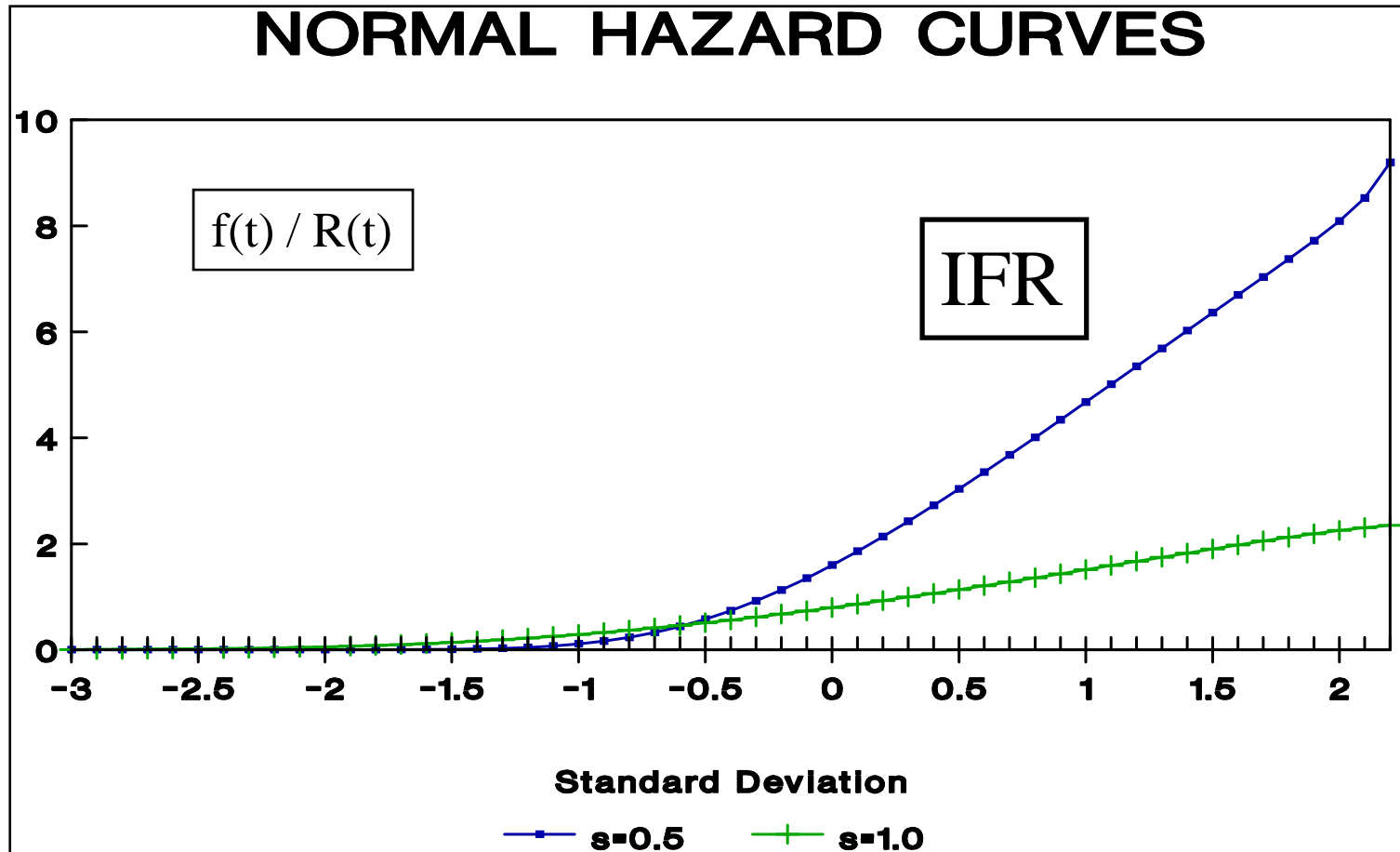
## NORMAL PDF CURVES

$$MTTF = \mu$$

$$Std Dev = \sigma$$



# Normal Hazard Rate Function

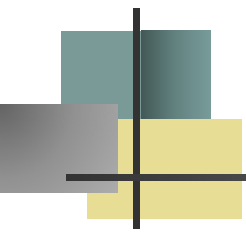


# Normal Distribution - Applications

- Tool failures
- Brake lining wear
- Tire tread wear



It's the additive effect of temperature variation, material wear, friction, and other random stresses over time, isn't it?.



# Finding Normal Cumulative Probabilities

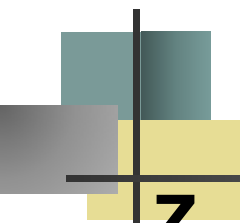
If  $T$  is normally distributed, then let  $z = \frac{T - \mu}{\sigma}$

Then  $z$  has a normal distribution with a mean of 0 and a standard deviation of 1. The PDF for  $z$  is given by

Its cumulative distribution is then given by  $\phi(z) = \frac{1}{\sqrt{2\pi}} e^{-\frac{z^2}{2}}$

$$\Pr\{Z \leq z\} = \Phi(z) = \int_{-\infty}^z \phi(z') dz'$$

*$z$  is the standardized normal deviate*

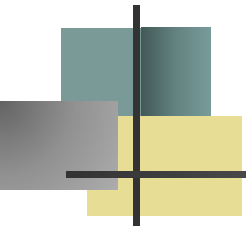


# Normal Probability Tables

<b>Z</b>	<b><math>\Phi(Z)</math></b>	<b><math>1-\Phi(Z)</math></b>
-0.55000	0.29116	0.70884
-0.54000	0.29460	0.70540
-0.53000	0.29806	0.70194
-0.52000	0.30153	0.69847
-0.51000	0.30503	0.69497
-0.50000	0.30854	0.69146
-0.49000	0.31207	0.68793
-0.48000	0.31561	0.68439
-0.47000	0.31918	0.68082
-0.46000	0.32276	0.67724
-0.45000	0.32636	0.67364
-0.44000	0.32997	0.67003

$\Pr\{Z < -.5\} = .30854$

$\Pr\{Z > -.46\} = .67724$

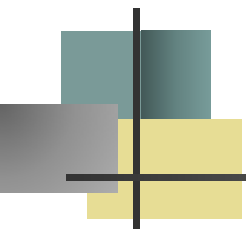


# Normal Reliability Function

$$R(t) = \int_t^{\infty} \frac{1}{\sqrt{2\pi} \sigma} e^{-\frac{(t-\mu)^2}{2\sigma^2}} dt'$$

$$\begin{aligned} R(t) &= \Pr\{T \geq t\} = \Pr\left\{\frac{T - \mu}{\sigma} \geq \frac{t - \mu}{\sigma}\right\} \\ &= \Pr\left\{z \geq \frac{t - \mu}{\sigma}\right\} = 1 - \Phi\left(\frac{t - \mu}{\sigma}\right) \end{aligned}$$





## Example Problem - Normal

The time to failure of a fan belt is normally distributed with a MTTF = 220 (in hundreds of vehicle miles) and a standard deviation of 40 (in hundreds of vehicle miles).

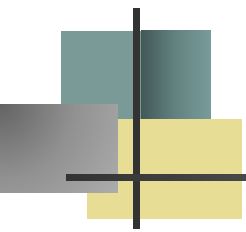
$$R(100) = 1 - \Phi[(100-220)/40] = 1 - \Phi(-3) = .99865$$

$$R(200) = 1 - \Phi[(200-220)/40] = 1 - \Phi(-.5) = .69146$$

$$R(300) = 1 - \Phi[(300-220)/40] = 1 - \Phi(2) = .02275$$

$$R(100|200) = R(300) / R(200) = .02275 / .69146 = .0329$$

note: both the median and mode = MTTF = 22,000 miles



## Normal Example problem - design life

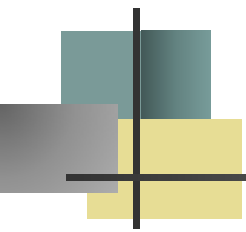
A new fan belt is developed from a higher grade of material. It has a time to failure distribution which is normal with a mean of 35,000 vehicle miles and a standard deviation of 7,000 vehicle miles. Find its designed life if a .97 reliability is desired.

$$R(t) = 1 - \Phi[(t - 350)/70] = .97; \text{ find } t !$$

From the normal table,  $1 - \Phi(-1.88) = .96995$

$$\text{Therefore; } (t - 350) / 70 = -1.88$$

$$\text{and } t_{.97} = 350 - 1.88 (70) = 218.4 \text{ or } 21,840 \text{ vehicle miles}$$

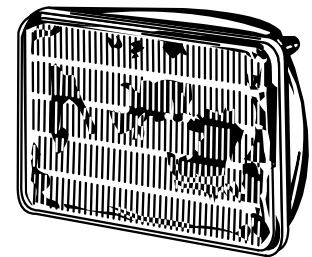


# Student Exercise - Normal

The operating hours until failure of a halogen headlamp is normally distributed with a mean of 1200 hr. and a standard deviation of 450 hr.

Find:

- The 5 year reliability if normal driving results in the use of the headlamp an average of .2 hr. a day.
- The .90 design life in years.





## Student exercise - solution

a.  $t = .2 \text{ hr./da.} \times 365 \text{ da./yr.} \times 5 \text{ yr.} = 365 \text{ hr.}$

$$\begin{aligned} R(365) &= 1 - F[(365 - 1200)/450] \\ &= 1 - F[-1.86] = .96856 \end{aligned}$$

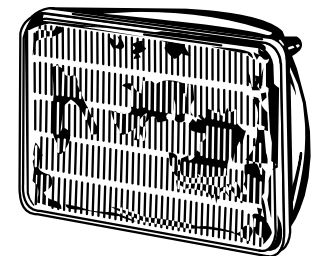
b.  $R(t_{.90}) = .90$

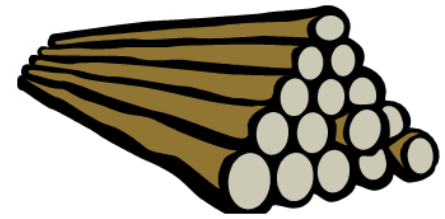
or  $1 - F[(t_{.90} - 1200)/450] = .90$

$$(t_{.90} - 1200) / 450 = -1.28$$

$$t_{.90} = 1200 - 1.28(450) = 624 \text{ hr.}$$

or  $t_{.90} = 624 / (.2 \times 365) = 8.5 \text{ yr.}$





some normal logs

## The Lognormal Failure Process

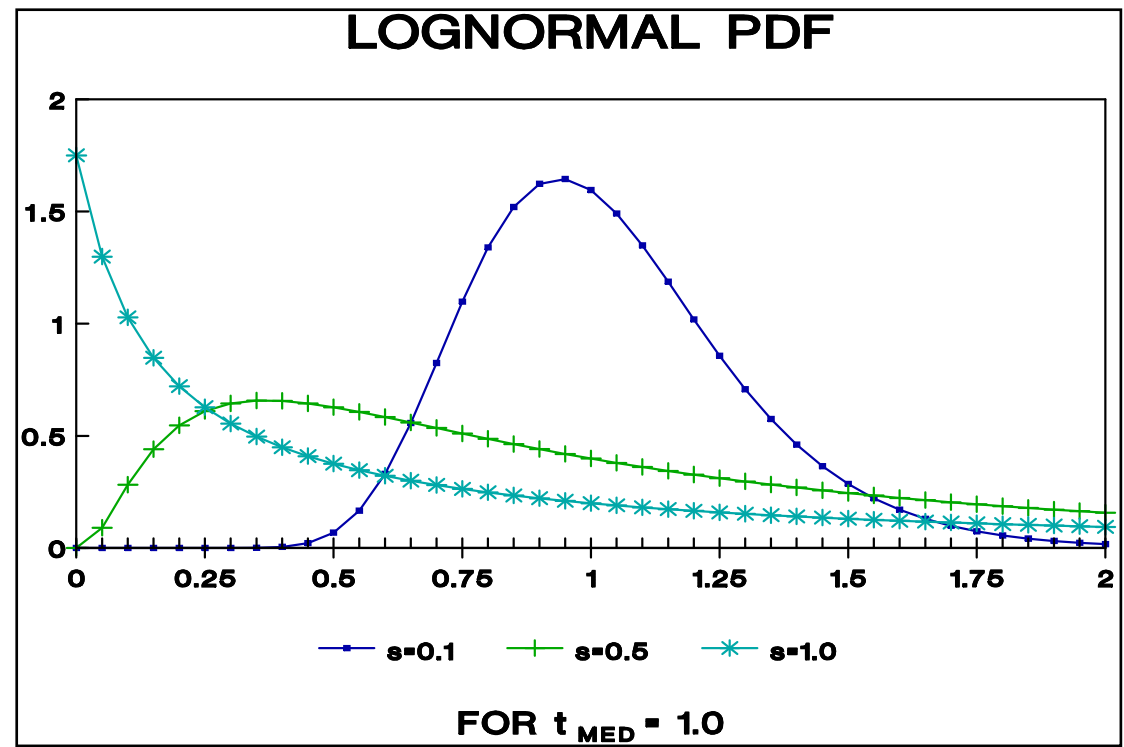
Let  $T$  = a random variable, the time to failure. If  $T$  has a lognormal distribution, then the logarithm of  $T$  has a normal distribution.



# Lognormal Density Function

$$f(t) = \frac{1}{\sqrt{2\pi}s t} e^{-\frac{1}{2s^2} \left( \ln \frac{t}{t_{MED}} \right)^2} ; t \geq 0$$

$t_{med}$  = median time  
to failure  
 $s$  = shape parameter

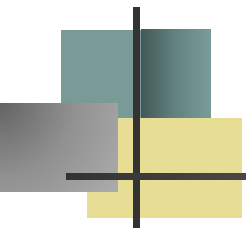




# Lognormal/Normal Relationship

Given T is a lognormal random variable, then

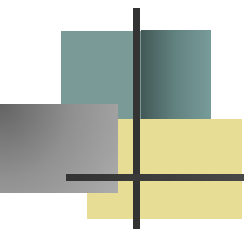
	<u>T</u>	<u>Log T</u>
Distribution	Lognormal	Normal
Mean	$t_{\text{med}} e^{s^2 / 2}$	$\ln t_{\text{med}}$
Variance	$t_{\text{med}}^2 e^{s^2} [e^{s^2} - 1]$	$s^2$
Mode	$t_{\text{mode}} = \frac{t_{\text{med}}}{e^{s^2}}$	$\ln t_{\text{med}}$



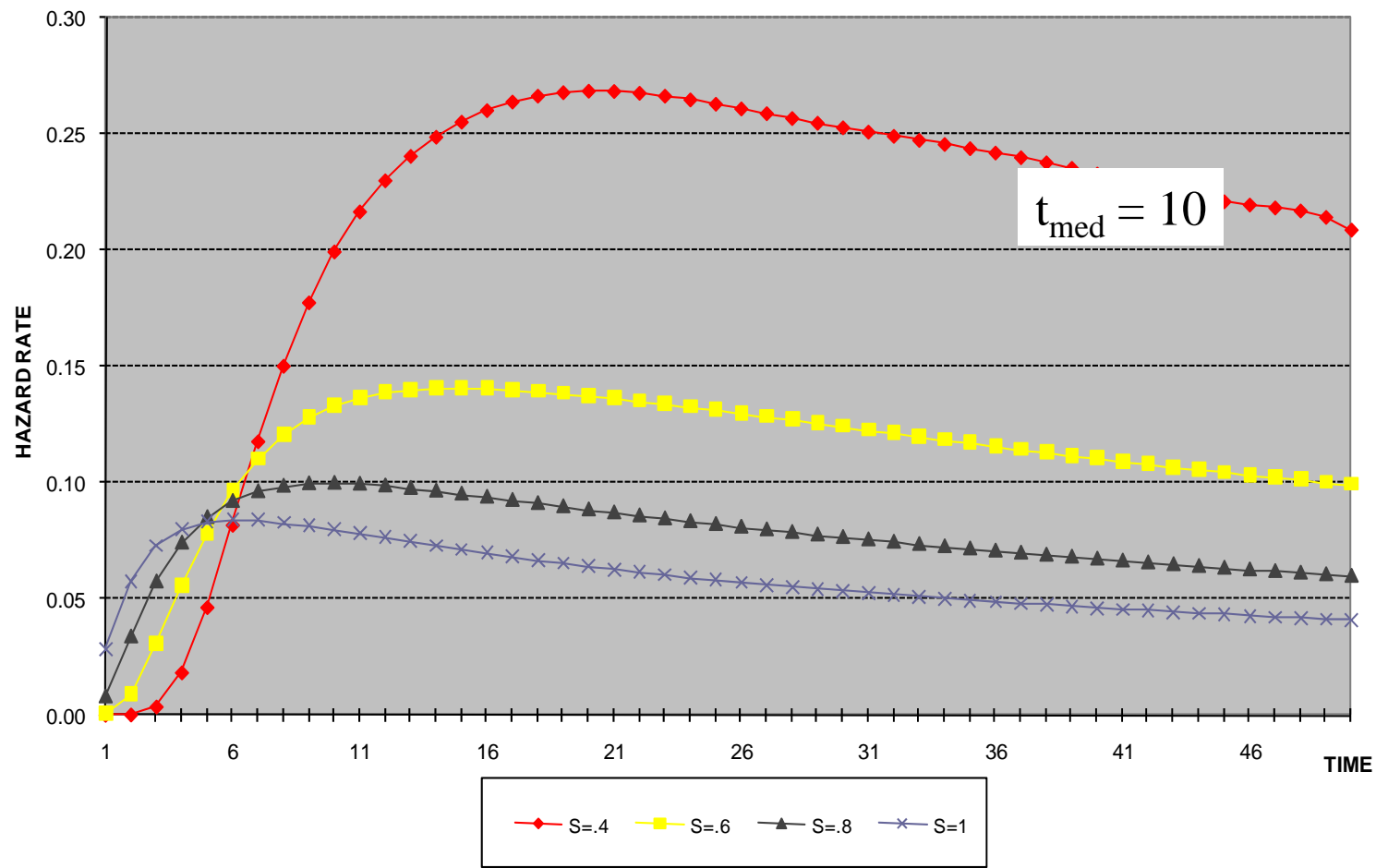
# Lognormal Failure & Reliability Distribution

$$\begin{aligned} F(t) &= P\{T \leq t\} = P\{\ln T \leq \ln t\} \\ &= P\left\{\frac{\ln T - \ln t_{MED}}{s} \leq \frac{\ln t - \ln t_{MED}}{s}\right\} \\ &= P\left\{z \leq \frac{1}{s} \ln \frac{t}{t_{MED}}\right\} = \Phi\left(\frac{1}{s} \ln \frac{t}{t_{MED}}\right) \\ R(t) &= 1 - \Phi\left(\frac{1}{s} \ln \frac{t}{t_{MED}}\right) \end{aligned}$$





# Lognormal Hazard Rate Function

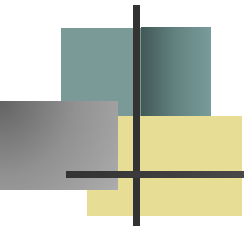




# Lognormal Hazard Rate Function

s	1.0	.8	.6	.4
Mode	3.7	5.3	7.0	8.5
MTTF	16.5	13.8	12.0	10.8
Max $\lambda(t)$	7	10	16	20

$$t_{\text{med}} = 10$$



# Design Life

$$1 - \Phi\left(\frac{1}{s} \ln \frac{t_R}{t_{med}}\right) = R$$

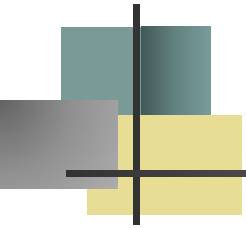
$$\Phi\left(\frac{1}{s} \ln \frac{t_R}{t_{med}}\right) = 1 - R$$

Find  $z_{1-R}$  such that:

$$\Phi(z_{1-R}) = 1 - R$$

$$\frac{1}{s} \ln \frac{t_R}{t_{med}} = z_{1-R}$$

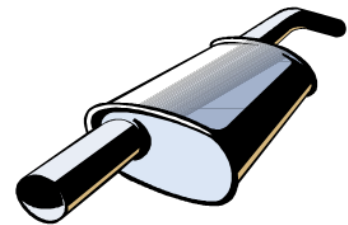
$$t_R = t_{med} e^{s z_{1-R}}$$



# Lognormal Example

The failure distribution of an exhaust system is lognormal with  $t_{\text{med}} = 50,000$  vehicle miles and  $s = .8$ . Therefore:

- a.  $\text{MTTF} = 50,000 e^{.64/2} = 68,856$  mi.
- b.  $t_{\text{mode}} = 50,000 / e^{.64} = 26,640$  mi.
- c.  $\text{variance} = 50,000^2 e^{.64} [e^{.64} - 1]$  and the standard deviation = 65,195 mi.



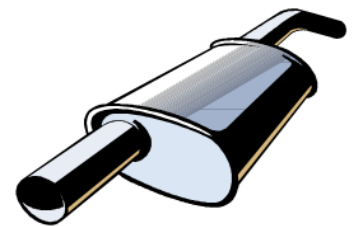


## Lognormal Example (continued)

$$R(10,000) = 1 - \Phi\left(\frac{1}{.8} \ln \frac{10,000}{50,000}\right) = 1 - \Phi(-2.01) = .9779$$

$$R(20,000) = 1 - \Phi\left(\frac{1}{.8} \ln \frac{20,000}{50,000}\right) = 1 - \Phi(-1.15) = .8749$$

$$R(10,000 | 10,000) = R(20,000) / R(10,000) = .8749 / .9770 = .8955$$





## Example (continued)

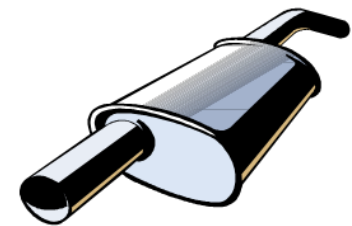
Find the design life corresponding to a 90 percent reliability.

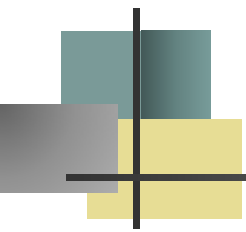
$$R(t_{.9}) = 1 - \Phi\left(\frac{1}{.8} \ln \frac{t_{.9}}{50,000}\right) = .90$$

from the normal probability tables:

$$\left(\frac{1}{.8} \ln \frac{t_{.9}}{50,000}\right) = -1.285$$

$$\text{or } t_{.9} = 50,000 e^{-1.285(.8)} = 17,886 \text{ mi.}$$



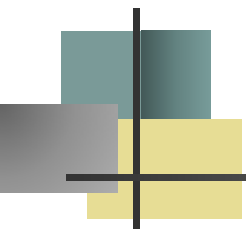


## Class Exercise - Lognormal

Reliability testing of the new 1.6 liter automotive engine has resulted in a time to failure distribution which is lognormal with  $t_{\text{med}} = 100,000$  mi. and  $s = .70$ . Find:

- a.  $R(36,000 \text{ mi.})$
- b. MTTF and Std. Dev.
- c.  $R(100,000|36,000)$
- d.  $t_{.95}$



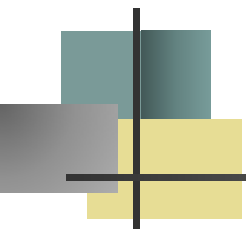


## Class Exercise - solution

- a.  $R(36,000) = 1 - \Phi[(1/.7)\ln(36,000/100,000)]$   
 $= 1 - \Phi[-1.46] = .92786$
- b.  $MTTF = 100,000 e^{.49/2} = 127,762$  mi.  
 $Var = 100,000^2 e^{.49} [e^{.49} - 1] = 1.032 \times 10^{10}$   
 $Std Dev = 101,594$  mi.
- c.  $R(64,000|36,000)$   
 $= R(100,000)/R(36,000)$   
 $= 5. / .92786 = .539$







## Class Exercise - solution

d.  $R(t_{.95}) = .95$

$$1 - \Phi[ (1/.7) \ln(t_{.95} / 100,000) ] = .95$$

$$(1/.7) \ln(t_{.95} / 100,000) = -1.645$$

$$t_{.95} = 100,000 e^{-1.645 \times .7} = 31,616 \text{ mi.}$$

general approach:

$$t_R = t_{\text{med}} e^{z \times s}$$





# The Gamma Distribution

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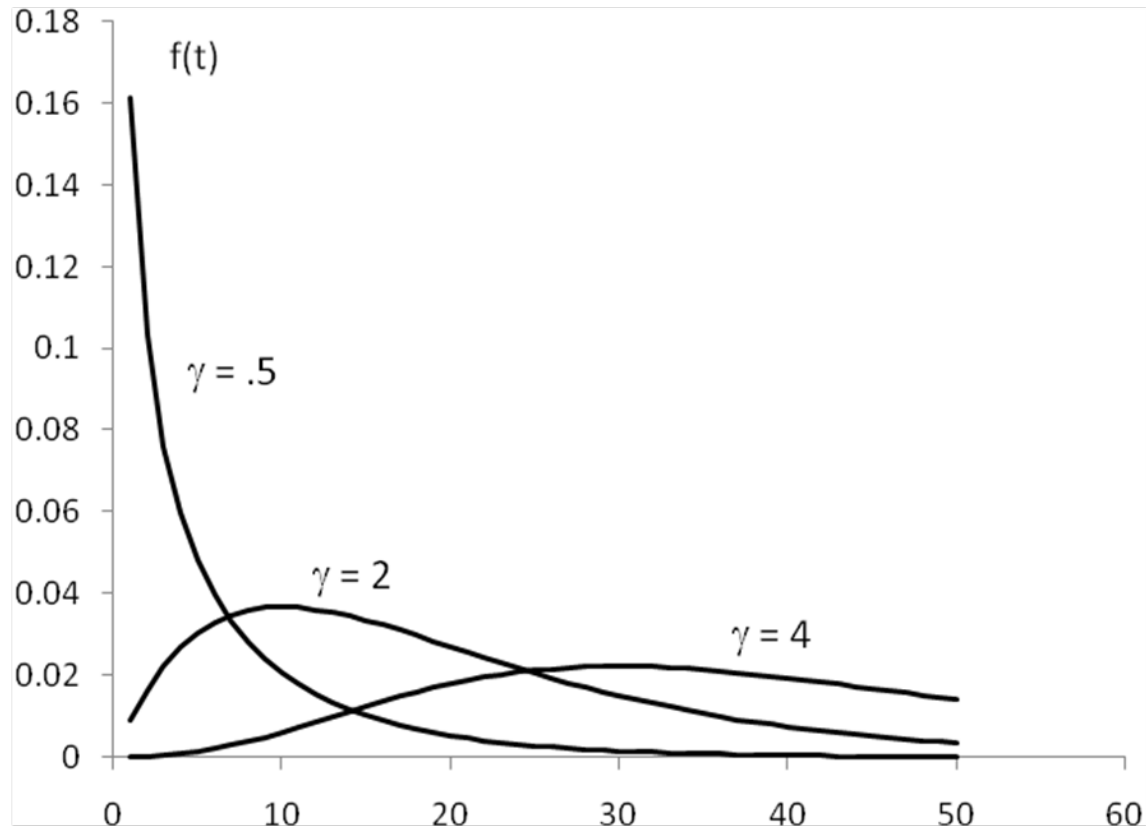
$$f(t) = \frac{t^{\gamma-1} e^{-t/\alpha}}{\alpha^\gamma \Gamma(\gamma)} \quad \text{for } \gamma, \alpha > 0 \text{ and } t \geq 0$$

$\gamma$  - shape parameter

$\alpha$  - scale parameter

When  $\gamma = 1$ , the resulting distribution is exponential with a mean equal to  $\alpha$ .

# The Density Function Graphed





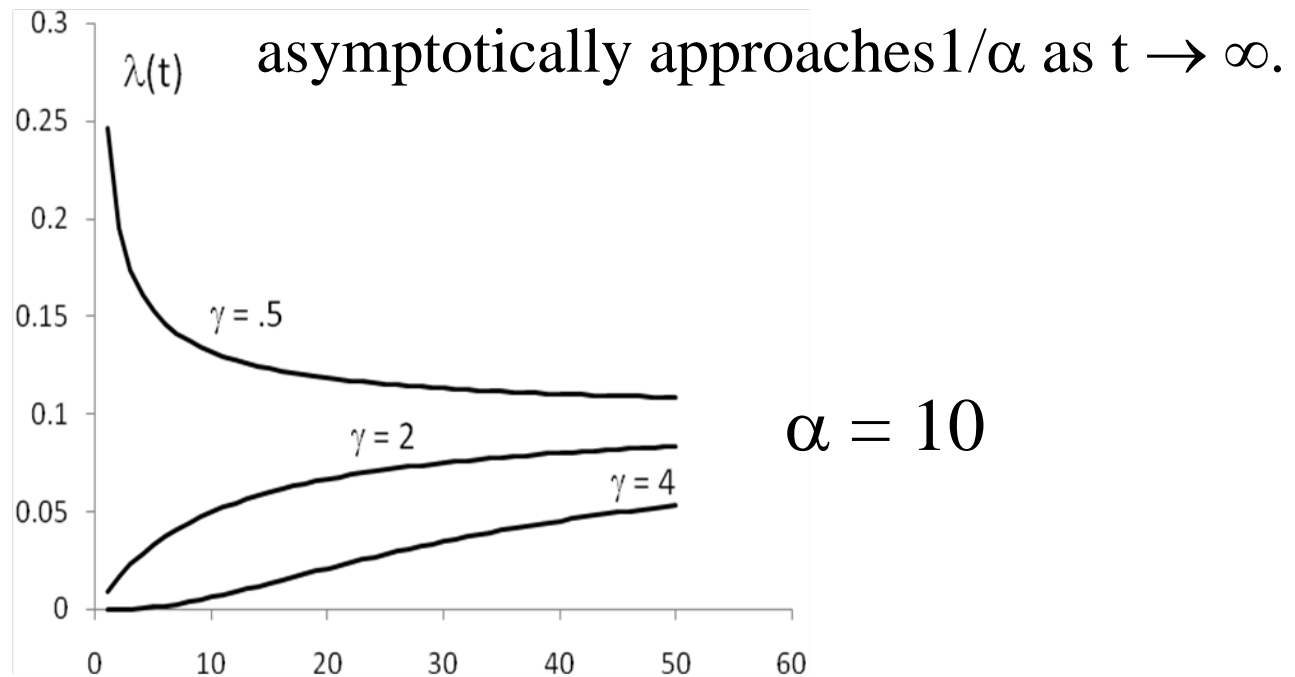
# The Reliability Function

$$F(t) = \int_0^t \frac{t'^{\gamma-1} e^{-t'/\alpha}}{\alpha^\gamma \Gamma(\gamma)} dt' = \frac{1}{\Gamma(\gamma)} \int_0^{t/\alpha} y^{\gamma-1} e^{-y} dy = \frac{I\left(\frac{t}{\alpha}, \gamma\right)}{\Gamma(\gamma)}$$

where  $y = t' / \alpha$  and  $I\left(\frac{t}{\alpha}, \gamma\right) = \int_0^{t/\alpha} y^{\gamma-1} e^{-y} dy$

$$\text{Therefore } R(t) = 1 - \frac{I\left(\frac{t}{\alpha}, \gamma\right)}{\Gamma(\gamma)}$$

# The Hazard Rate Function



Shape parameter	Hazard rate function
$0 < \gamma < 1$	DFR
$\gamma = 1$	CFR
$\gamma > 1$	IFR



# Distribution Characteristics

---

$$MTTF = \gamma\alpha$$

$$\sigma^2 = \gamma\alpha^2$$

$$t_{\text{mode}} = \begin{cases} \alpha(\gamma - 1) & \text{for } \gamma > 1 \\ 0 & \text{otherwise} \end{cases}$$



## EXAMPLE 4.11

---

Failures of a critical machine part due to cyclical vibration has a gamma distribution with a shape parameter of 2.3 and a scale parameter of 2,000 operating hours. Then

$$\text{MTTF} = \gamma\alpha = (2.3)(2,000) = 4600 \text{ hr}$$

$$\sigma = \sqrt{\gamma\alpha^2} = \sqrt{(2.3)(2,000)^2} = 3033.15 \text{ hr}$$

$$t_{\text{mode}} = \alpha(\gamma - 1) = 2,000(2.3 - 1) = 2,600 \text{ hr}$$

Using the Excel Chapter 4 template for the gamma distribution the median is found to be 3,953.25 hr and  $R(1000) = .9463$

# Summary

## Reliability

## MTTF

Exponential

$$R(t) = e^{-\lambda t}$$

$$1 / \lambda$$

Weibull

$$R(t) = e^{-\left(\frac{t}{\theta}\right)^B}$$

$$\theta \Gamma\left(1 + \frac{1}{\beta}\right)$$

Min Extreme Value

$$R(t) = \exp\left[-e^{\frac{(t-\mu)}{\alpha}}\right]$$

$$\mu - .577215665\alpha$$

Normal

$$R(t) = 1 - \Phi\left(\frac{t - \mu}{\sigma}\right)$$

$$\mu$$

Lognormal

$$R(t) = 1 - \Phi\left(\frac{1}{s} \ln \frac{t}{t_{med}}\right)$$

$$t_{med} e^{s^2/2}$$

Gamma

$$R(t) = 1 - \frac{I\left(\frac{t}{\alpha}, \gamma\right)}{\Gamma(\gamma)}$$

$$\alpha \gamma$$





# That's all folks!

I cannot wait to work the Chapter 4 problems and to start reading Chapter 5!

