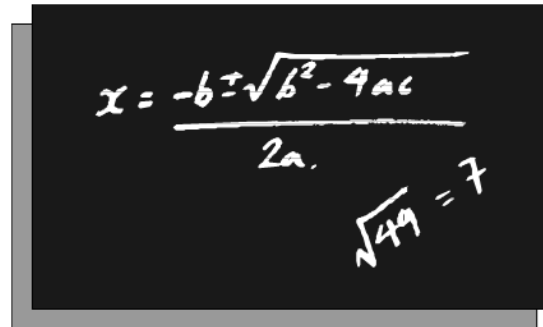


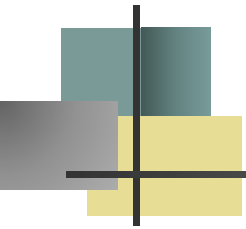


Chapter 2

Basic Reliability Models

The Failure Distribution


$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$
$$\sqrt{49} = 7$$



The Reliability Function

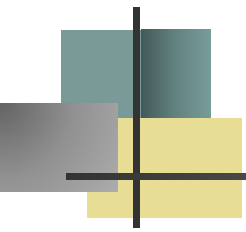
Let T = a random variable, the time to failure of a component

$$R(t) = \Pr\{T \geq t\}$$

where $R(t) \geq 0$, $R(0) = 1$, and

$$\lim_{t \rightarrow \infty} R(t) = 0$$

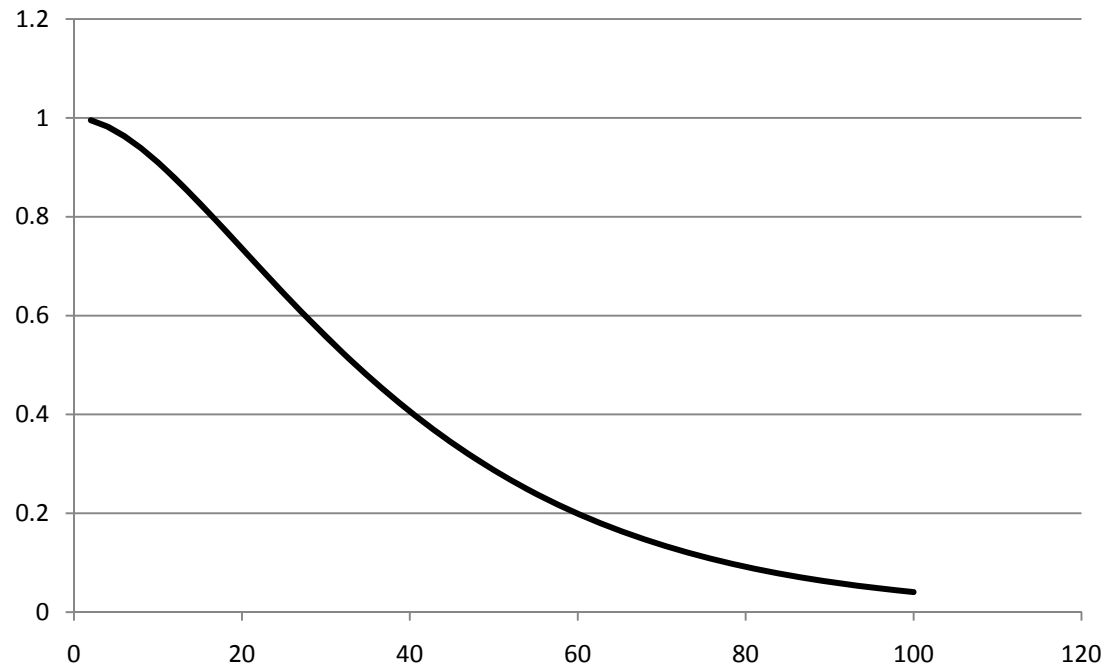
Often called the **SURVIVAL FUNCTION**

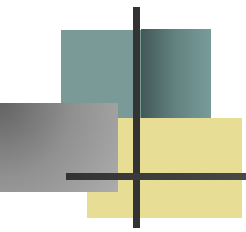


Graph of a Reliability Function

$R(t)$

Probability of surviving





The Cumulative Distribution Function (CDF)

$$F(t) = 1 - R(t) = \Pr \{T < t\}$$

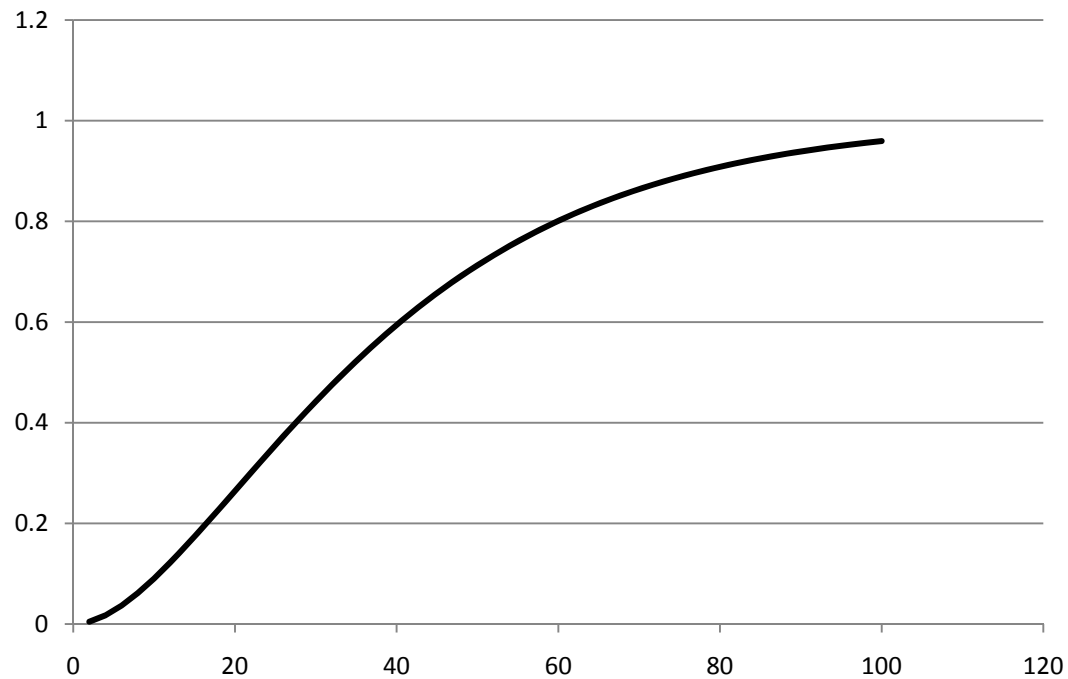
where $F(0) = 0$ and $\lim_{t \rightarrow \infty} F(t) = 1$

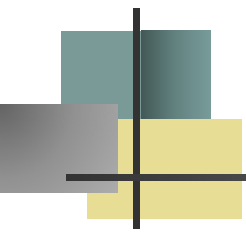


Graph of a CDF

$F(t)$

The probability of a failure





The Density Function (PDF)

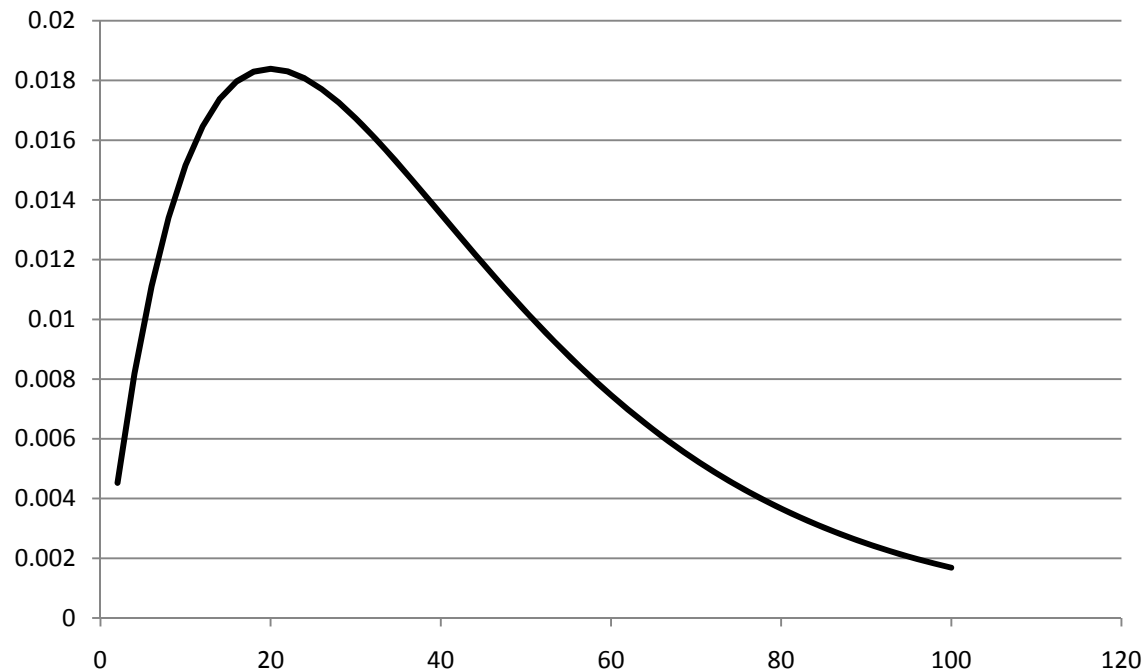
$$f(t) = \frac{d F(t)}{dt} = - \frac{d R(t)}{dt}$$

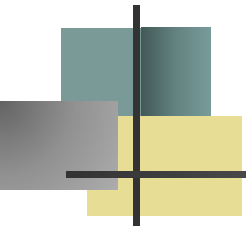
$$f(t) \geq 0 \text{ and } \int_0^{\infty} f(t) dt = 1$$



Graph of a Density Function (PDF)

$f(t)$

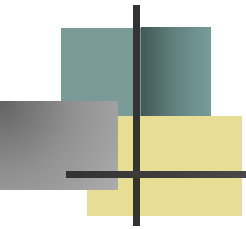




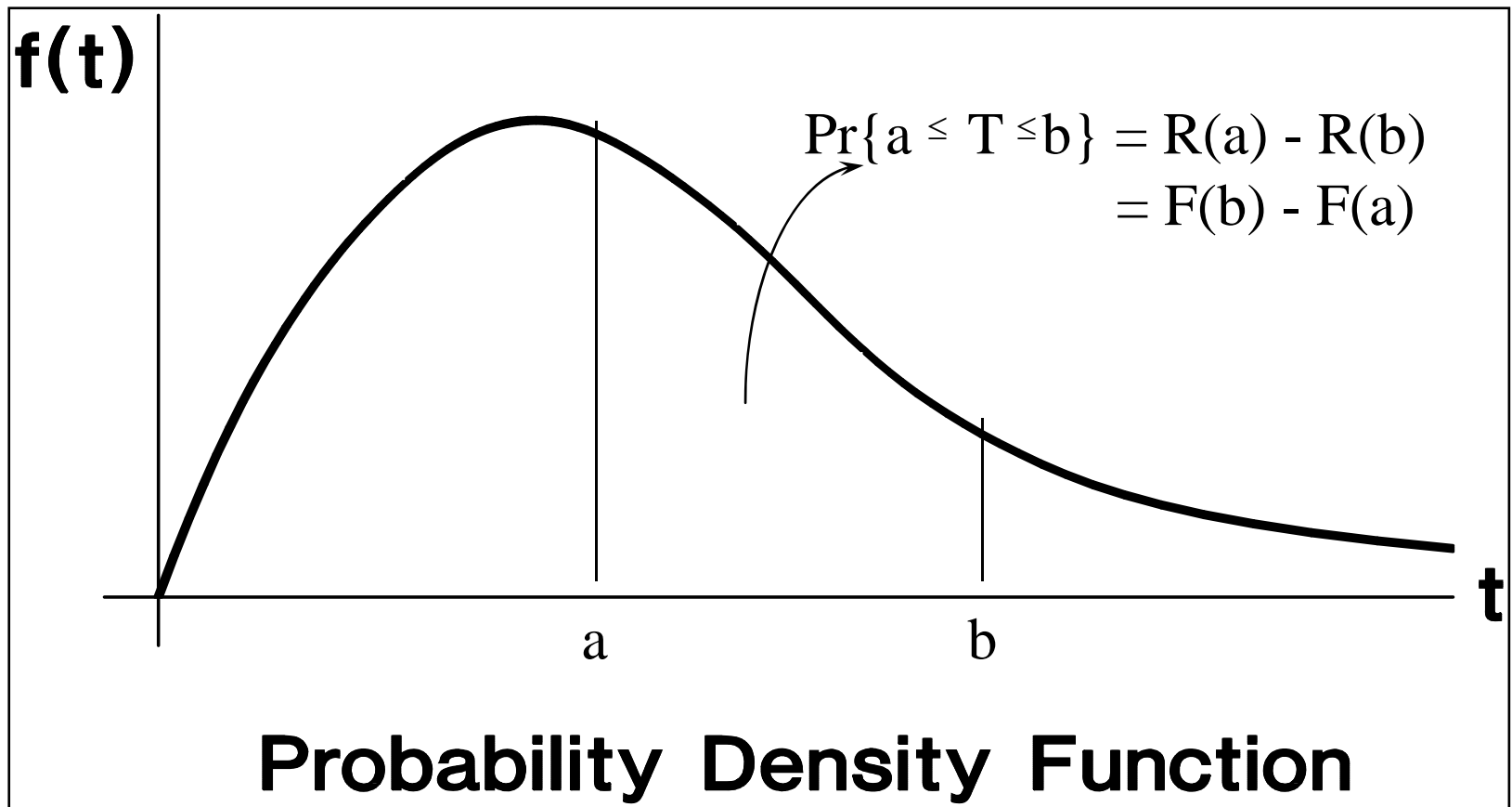
Relationship between PDF and CDF

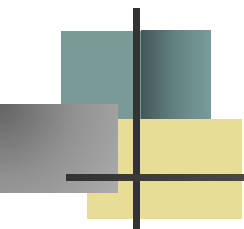
$$F(t) = \int_0^t f(t') dt'$$

$$R(t) = \int_t^{\infty} f(t') dt'$$



Finding Failure Probabilities





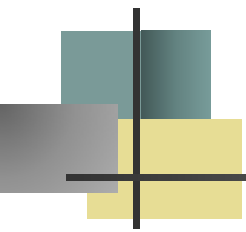
Example

The passive components of a distribution system for natural gas has the following reliability function:

$$R(t) = 1 - \frac{t^2}{100}; \quad 0 \leq t \leq 10 \text{ yrs}$$

- Find:
- a. $R(3 \text{ yrs})$
 - b. The CDF, $F(t)$
 - c. $\Pr\{1 < T < 3\}$
 - d. The density function, $f(t)$





Example - solution

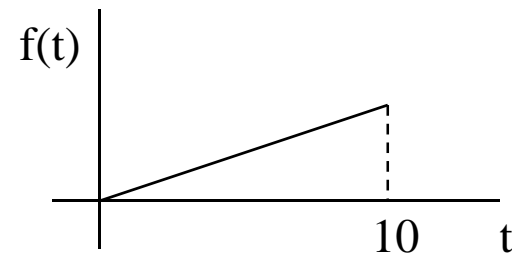
$$a. \quad R(3) = 1 - \frac{3^2}{100} = .91$$

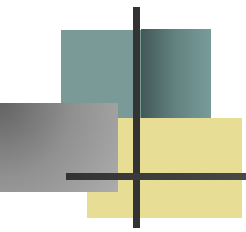
$$R(t) = 1 - \frac{t^2}{100}; \quad 0 \leq t \leq 10 \text{ yrs}$$

$$b. \quad F(t) = 1 - [1 - t^2 / 100] = t^2 / 100$$

$$c. \quad \Pr\{1 < T < 3\} = F(3) - F(1) = .09 - .01 = .08$$

$$d. \quad f(t) = \frac{dF(t)}{dt} = \frac{2t}{100} = \frac{t}{50}; \quad 0 \leq t \leq 10$$

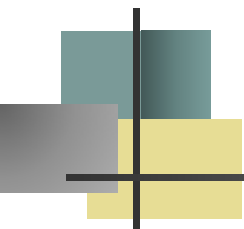




Mean Time to Failure (MTTF)

$$MTTF = \int_0^{\infty} t f(t) dt = \int_0^{\infty} R(t) dt$$

Note alternate notation: $MTTF = E[T]$



Derivation of MTTF (Appendix 2A)

$$MTTF = \int_0^{\infty} t f(t) dt = \int_0^{\infty} -t \frac{dR(t)}{dt} dt$$

Integration by parts:

$$MTTF = -tR(t) \Big|_0^{\infty} + \int_0^{\infty} R(t) dt = \int_0^{\infty} R(t) dt$$

Since

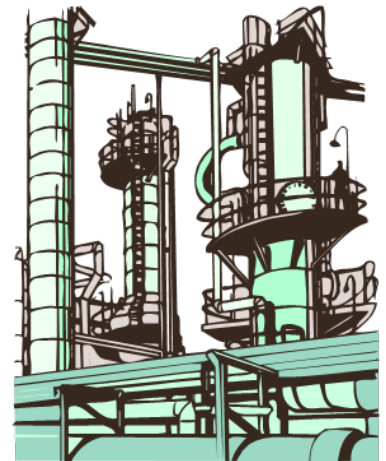
$$-tR(t) \Big|_0^{\infty} = \lim_{t \rightarrow \infty} t R(t) - 0R(0) = \lim_{t \rightarrow \infty} t \exp \left[-\int_0^t \lambda(t') dt' \right] = 0$$



Example - MTTF

For the distribution system, find the MTTF.

$$\begin{aligned} MTTF &= \int_0^{\infty} t f(t) dt = \int_0^{10} t \frac{t}{50} dt \\ &= \frac{t^3}{150} \Big|_0^{10} = \frac{10^3}{150} = \frac{100}{15} = 6 \frac{2}{3} \text{ yr} \end{aligned}$$

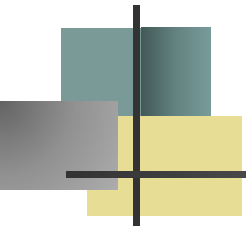




Example - MTTF revisited

For the distribution system, find the MTTF.

$$\begin{aligned} MTTF &= \int_0^{\infty} R(t) dt = \int_0^{10} \left(1 - \frac{t^2}{100}\right) dt \\ &= t - \frac{t^3}{300} \Big|_0^{10} = 10 - \frac{1000}{300} = 6\frac{2}{3} \text{ yr} \end{aligned}$$



Median Time to Failure and Mode

$$R(t_{med}) = .5 = P\{T \geq t_{med}\}$$

$$f(t_{mode}) = \max_{0 \leq t < \infty} f(t)$$

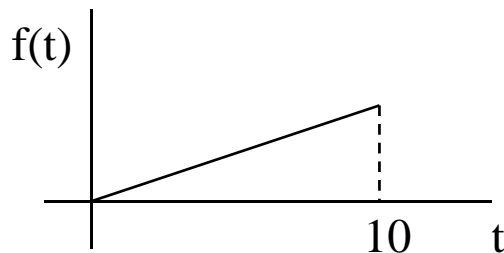


Example - median and mode

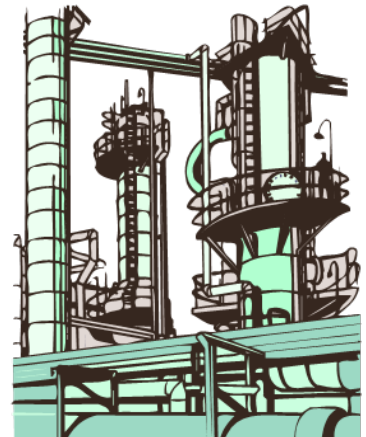
$$R(t) = 1 - t^2 / 100 = .5$$

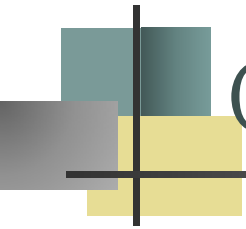
$$t^2 / 100 = .5$$

$$t^2 = 50 \quad \text{or} \quad t_{\text{med}} = 7.07 \text{ yrs}$$

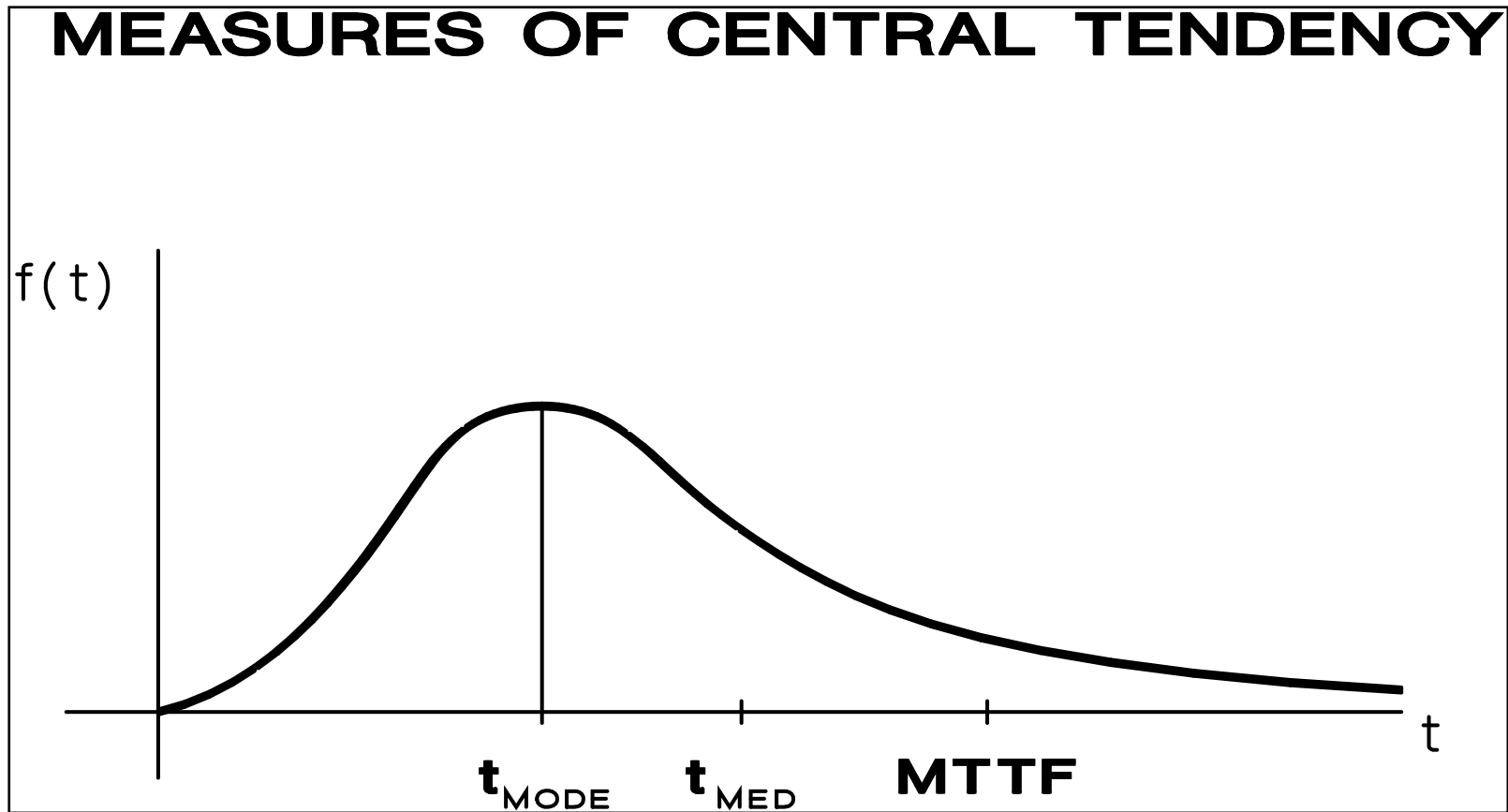


by inspection
 $t_{\text{mode}} = 10 \text{ yrs}$





Comparison of MTTF, Median, & Mode





Design Life



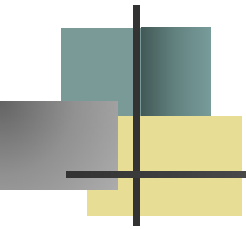
Find t_R such that $R(t_R) = R$

For example:

Find that time, $t_{.99}$ such that $R(t_{.99}) = .99$

Then $t_{.99}$ is the 99 percent design life.

One percent will fail before time $t_{.99}$

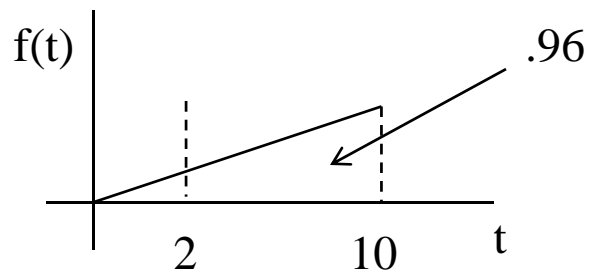


Example – design life

$$R(t) = 1 - t^2 / 100 = .96$$

$$t^2 / 100 = .04$$

$$t^2 = 4 \quad \text{or} \quad t_{.96} = 2 \text{ yrs}$$





Variance & Standard Deviation

definitional form:

$$\sigma^2 = \int_0^{\infty} (t - MTTF)^2 f(t) dt$$

computational form:

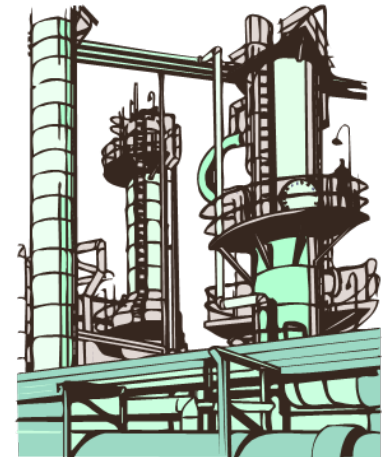
$$\sigma^2 = \int_0^{\infty} t^2 f(t) dt - (MTTF)^2$$

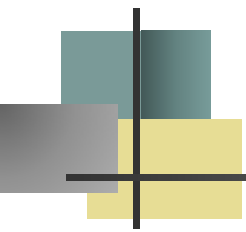


Example - standard deviation

$$\begin{aligned}\sigma^2 &= \int_0^{10} \frac{t^3}{50} dt - \left(6\frac{2}{3}\right)^2 \\ &= \frac{t^4}{200} \Big|_0^{10} - \left(6\frac{2}{3}\right)^2 = \frac{10,000}{200} - 44.444 = 5.55\end{aligned}$$

$$\text{or } \sigma = \sqrt{5.55} = 2.36 \text{ yr.}$$





Hazard Rate Function

$$P(A | B) = \frac{P(A \cap B)}{P(B)}$$

$$\Pr \{t \leq T \leq t + \Delta t\} = R(t) - R(t + \Delta t)$$

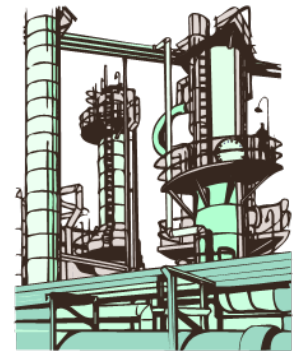
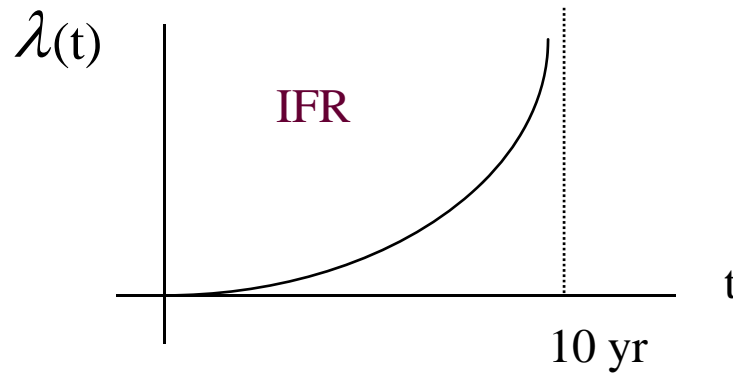
$$\Pr \{t \leq T \leq t + \Delta t | T \geq t\} = \frac{R(t) - R(t + \Delta t)}{R(t)}$$

$$\lambda(t) = \lim_{\Delta t \rightarrow 0} \frac{-[R(t + \Delta t) - R(t)]}{\Delta t} \cdot \frac{1}{R(t)} = \frac{-dR(t)}{dt} \cdot \frac{1}{R(t)} = \frac{f(t)}{R(t)}$$



Example - hazard rate function

$$\lambda(t) = \frac{t / 50}{1 - t^2 / 100} = \frac{t / 50}{\frac{100 - t^2}{100}} = \frac{2t}{100 - t^2}$$



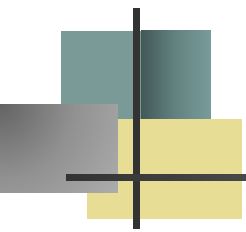
Derivation of R(t) from the Hazard Rate Function

$$\lambda(t) = - \frac{d R(t)}{d t} \frac{1}{R(t)}$$

$$\lambda(t)dt = - \frac{d R(t)}{R(t)} \rightarrow \int_0^t \lambda(t')dt' = - \int_1^{R(t)} \frac{d R(t')}{R(t')}$$

$$-\int_0^t \lambda(t')dt' = \ln R(t)$$

$$R(t) = \exp \left[- \int_0^t \lambda(t')dt' \right]$$



Hazard Rate Function & R(t)

$$R(t) = e^{-\int_0^t \lambda(t') dt'}$$

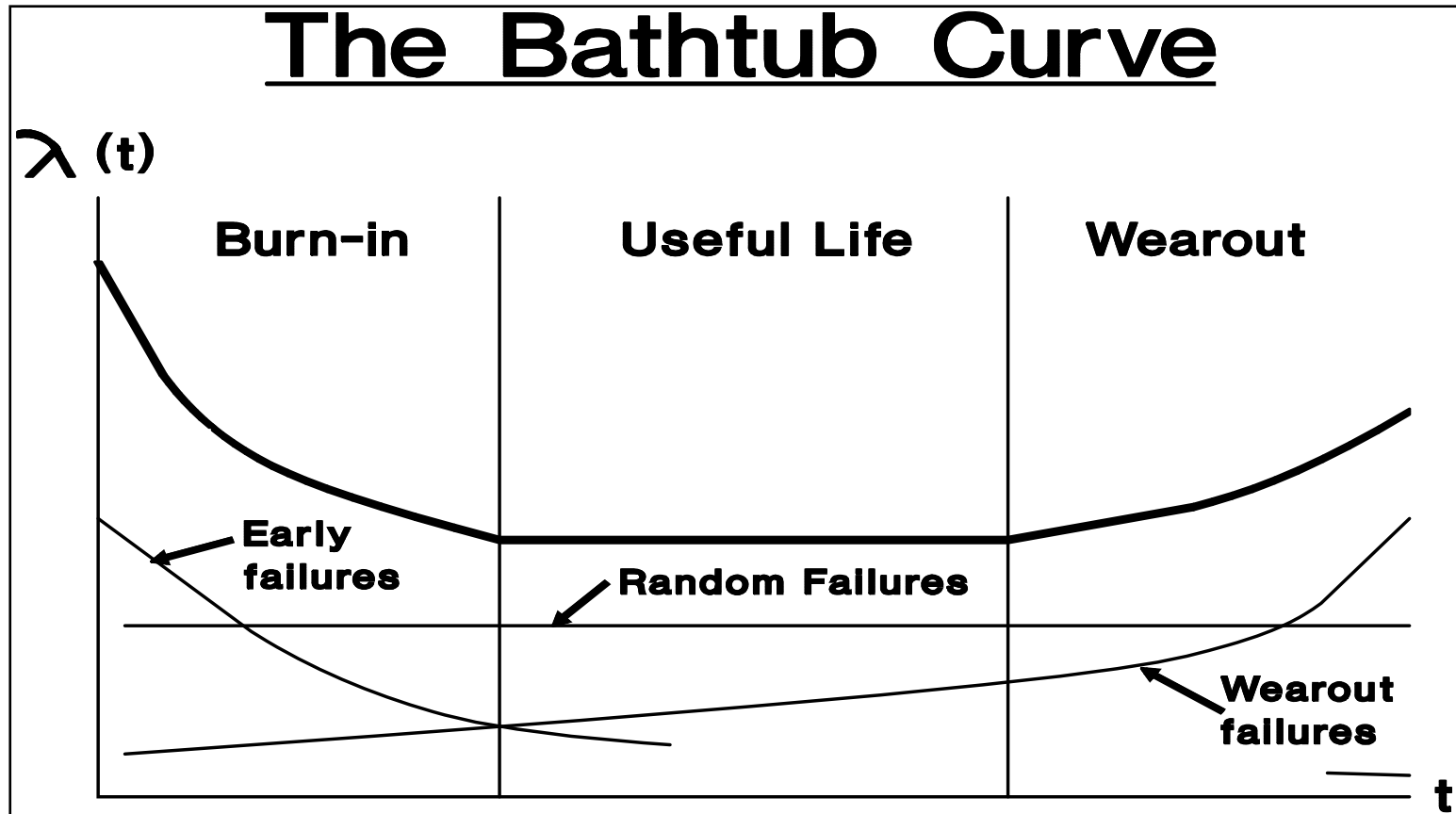
Example:

$$\lambda(t) = .02t, \text{ then}$$

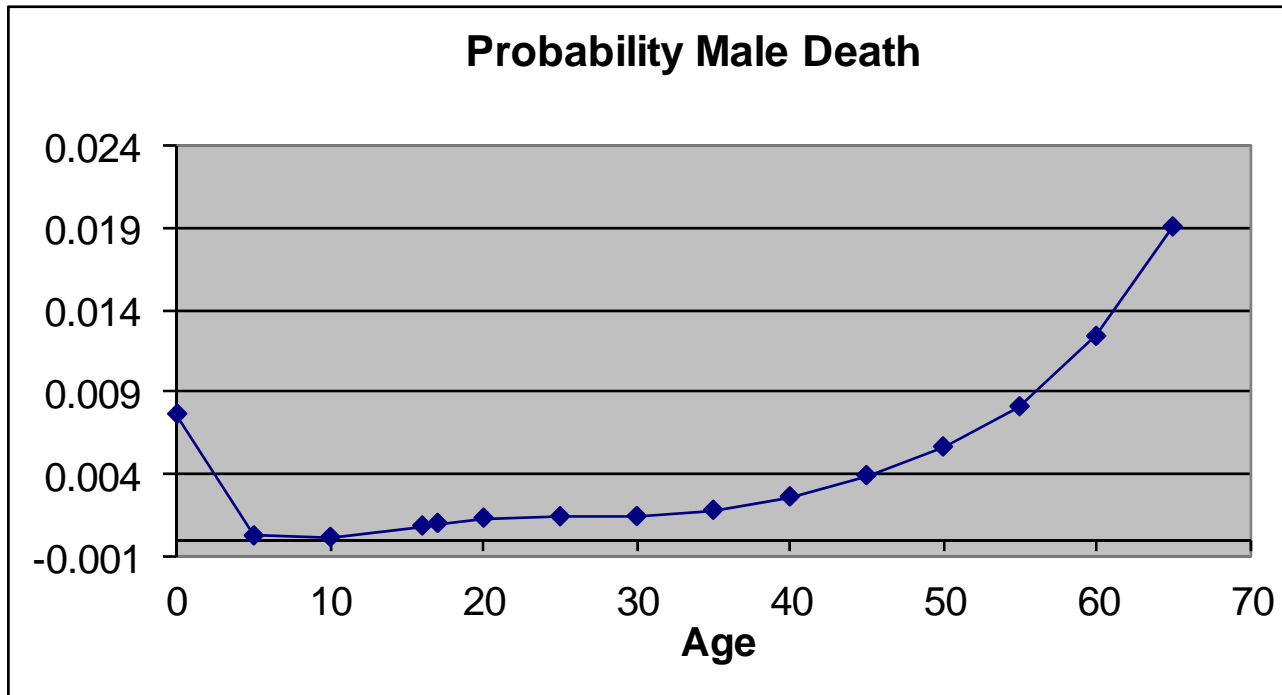
$$R(t) = e^{-\int_0^t .02t' dt'} = e^{-.01t^2}$$



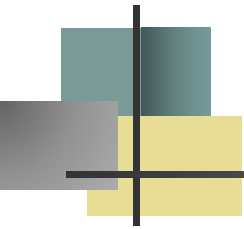
The Bathtub Curve



Human Mortality Curve



age	Male	Female
0	0.007644	0.006275
5	0.000202	0.000152
10	0.00011	0.000113
16	0.00081	0.000375
17	0.000964	0.000423
20	0.00129	0.000456
25	0.001379	0.000499
30	0.001389	0.000628
35	0.00177	0.000953
40	0.002589	0.001514
45	0.003891	0.002264
50	0.005643	0.003227
55	0.008106	0.004884
60	0.012405	0.007732
65	0.019102	0.012199
70	0.029824	0.019312
75	0.046499	0.030582
80	0.073269	0.050396
85	0.120186	0.086443
90	0.192615	0.147616



More on the Bathtub Curve



	Burn-in	Useful Life	Wearout
Characterized by	DFR	CFR	IFR
Caused by	Manufacturing defects Welding flaws, Cracks, Defective parts, Poor quality control, Contamination, Poor workmanship	Environment Random loads Human error "Acts of God" Chance events	Fatigue Corrosion Aging Friction Cyclical loading
Reduced by	Burn-in testing Screening Quality control Acceptance testing	Redundancy Excess strength	Derating Preventive Maint. Parts replacement Technology



Average Failure Rate (AFR)

$$AFR(t_1, t_2) = \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} \lambda(t') dt' = \frac{\ln R(t_1) - \ln R(t_2)}{t_2 - t_1}$$

since:

$$R(t) = e^{-\int_0^t \lambda(t') dt'}$$

Note: $AFR(0, t) = AFR(t) = -\ln R(t) / t$

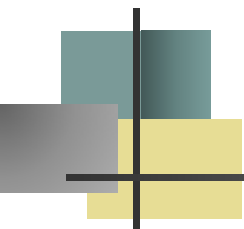


Example - Average Failure Rate

$$AFR(t) = \frac{-\ln\left[1 - \frac{t^2}{100}\right]}{t}$$



$$AFR(5 \text{ yr}) = -\ln [1 - .25] / 5 = .0575 \text{ failures / yr}$$



Conditional Reliability

$$R(t/T_0) = P \{ T > T_0 + t \mid T > T_0 \}$$

Event A



Event B



$$= \frac{P \{ T > T_0 + t \}}{P \{ T > T_0 \}} = \frac{R(T_0 + t)}{R(T_0)}$$



Residual MTTF

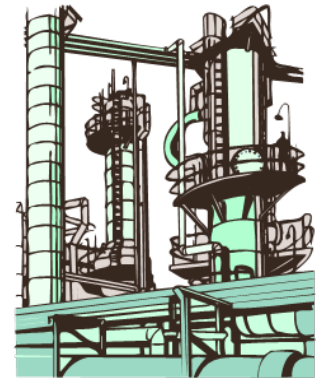
$$\begin{aligned} MTTF(T_0) &= \int_0^{\infty} R(t/T_0) dt = \int_0^{\infty} \frac{R(t+T_0)}{R(T_0)} dt \\ &= \frac{1}{R(T_0)} \int_{T_0}^{\infty} R(t') dt' \end{aligned}$$

where $t' = t + T_0$

Example - conditional reliability

$$\begin{aligned} R(t|1) &= \frac{R(t+1)}{R(1)} = \frac{1 - (t+1)^2 / 100}{1 - (1 / 100)} \\ &= \frac{100 - (t+1)^2}{100(.99)} = 1.01 - (t+1)^2 / 99 \end{aligned}$$

$$R(t) = 1 - \frac{t^2}{100}$$



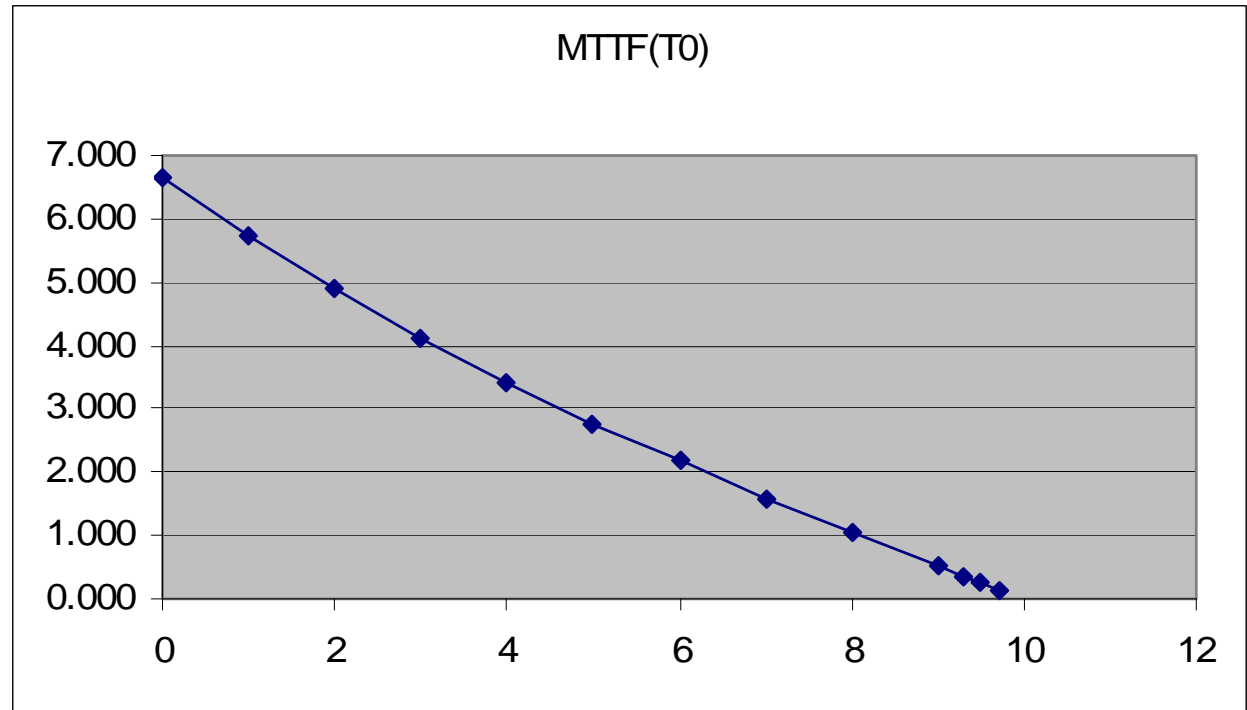
Therefore: $R(5|1) = 1.01 - 36/99 = .646$
where $R(5) = 1 - .25 = .75$

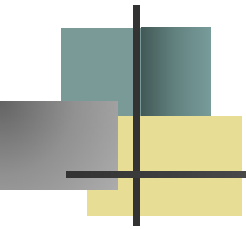
$$MTTF(T_0) = \frac{1}{1 - T_0^2 / 100} \int_{T_0}^{10} 1 - \frac{t^2}{100} dt = \frac{1}{.99} \left[t - \frac{t^3}{300} \right]_{T_0=1}^{10}$$

$$\text{or } MTTF(1) = \frac{1}{.99} \left[10 - \frac{10^3}{300} - 1 + \frac{1}{300} \right] = \frac{5.67}{.99} = 5.72 \text{ yr.}$$

Residual MTTF(T_0)

T_0	MTTF(T_0)
0	6.667
1	5.727
2	4.889
3	4.128
4	3.429
5	2.778
6	2.167
7	1.588
8	1.037
9	0.509
9.5	0.252
9.8	0.100
9.9	0.050





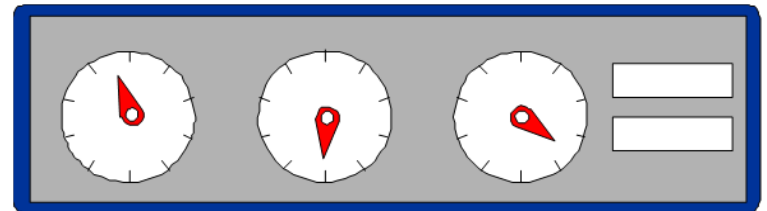
Student Exercise #1

A panel consisting of analog displays has a reliability function given by

$$R(t) = (200-t)/200 \text{ for } 0 < t < 200$$

where t is measured in 1000's of hr. Find:

- a. $R(50,000)$ and $R(12,000)$
- b. $R(50,000 \mid 12,000)$
- c. MTTF
- d. $MTTF(12,000)$





Student #1- solution

a. $R(50) = (200 - 50)/200 = .75$

$$R(12) = (200 - 12)/200 = .94$$

b. $R(50|12) = R(62) / R(12) = (200 - 62) / 200 / .94 = .69 / .94 = .734$

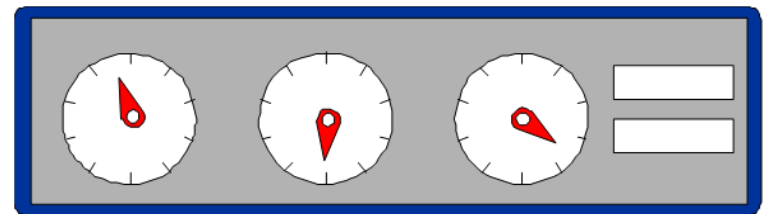
c. $MTTF = \int_0^{200} 1 - t / 200 dt = t - \frac{t^2}{400} \Big|_0^{200} = 200 - \frac{40000}{400} = 100$

d. $MTTF(12) = \frac{1}{.94} \int_{12}^{200} (1 - t / 200) dt = \frac{1}{.94} \left[t - \frac{t^2}{400} \right]_{12}^{200} = 94$



Student Exercise #1 (continued)

- e. What is the shape of the density function?
- f. Is the hazard rate function increasing or decreasing?
- g. Compute the average failure rate over the first 100,000 miles.



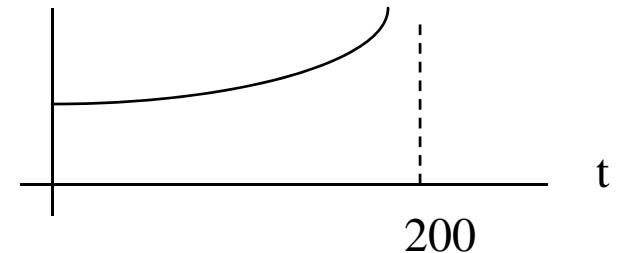


Student Exercise #1-solution

e. $f(t) = -dR(t) / dt$
 $= - d \{ (200-t)/200 \} / dt = 1/200$



$$f. \lambda(t) = \frac{1/200}{(200-t)/200} = \frac{1}{200-t}$$



g. $AFR(100) = - \ln \{ (200-100)/200 \} / 100$
 $= .007 \text{ failures/ } 1000 \text{ mi.}$



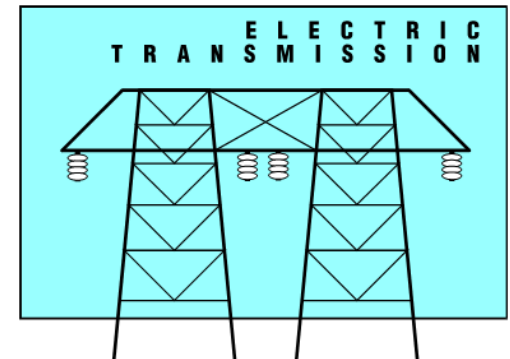
Student Exercise #2

Insulators on a power distribution system have a reliability function with t measured in yr.

$$R(t) = 1 / (1 + .05t) \text{ where } t \geq 0$$

Find:

- a. $F(1 \text{ yr})$ and $R(2)$
- b. $R(2|1)$
- c. The hazard rate function
(optional)
- d. $AFR(3)$





Student Exercise #2 - solution

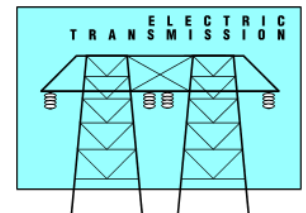
a. $F(1) = \Pr\{T < 1\} = 1 - 1/[1 + .05(1)] = 1 - .9524 = .0476$

$$R(2) = \Pr\{T > 2\} = 1/[1 + .05(2)] = .9091$$

b. $R(2|1) = \Pr\{T > 3 \mid T > 1\} = R(3) / R(1)$
 $= [1 + .05(3)]^{-1} / .9524 = .913$

c. $f(t) = -d [1 + .05t]^{-1} / dt = .05[1 + .05t]^{-2}$
 $\lambda(t) = f(t)/R(t) = .05/[1 + .05t]$ which is DFR

d. $AFR(3) = \{-\ln [1 + .05(3)]^{-1}\} / 3$
 $= -\ln .8696 / 3 = .0466$ failures per year.





Summary - The Four Functions

$f(t)$, the Probability Density Function (PDF)

$F(t)$, the Cumulative Distribution Function (CDF)

$R(t)$, the Reliability Function

$\lambda(t)$, the Hazard Rate Function

