PROJECT REPORT

BTECH 3rd Year

ANALOG CIRCUITS

Course: EE301



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Submitted By:-

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AIM: To design beta multiplier, cascode current mirror and cascode amplifier in Itspice and magic.

CALCULATIONS:

→ For 180nm:

Let the assumed current, $I_d = 10\mu\text{A}$ and unity gain frequency, $f_u = 3\text{MHz}$

Required gain =
$$20V/V$$

$$f_{u} = \frac{1}{2 \times \pi \times R_{out} \times C}$$

$$R_{out} = \frac{1}{2 \times \pi \times f_{u} \times C}$$

$$R_{out} = \frac{1}{2 \times \pi \times 3M \times 1p}$$

$$R_{out} = 53051.6476\Omega$$

$$A_{v} = g_{m} \times R_{out} \Rightarrow g_{m} = \frac{A_{v}}{R_{out}} = \frac{20}{53051.6476}$$

$$a_{v} = \sqrt{2 \times 1 \times 2} \times C \times \frac{W}{R_{out}} = \sqrt{2 \times 100} \times C$$

$$\begin{split} A_v &= g_m \times R_{out} \quad \Rightarrow g_m = \frac{A_v}{R_{out}} = \frac{20}{53051.6476} \qquad \Rightarrow g_m = 3.14 \times 10^{-4} \\ g_m &= \sqrt{2 \times I_d \times u_n \times C_{ox} \times \frac{W}{L}} = \sqrt{2 \times 10 \mu \times 270 \mu \times \frac{W}{L}} \\ 314.159 &= 18.277 \sqrt{\frac{W}{L}} \\ \bullet \left(\frac{W}{L}\right) &= 18.277 \end{split}$$

 V_g , $V_{s'}$, V_{thp} be the gate voltage of 1st pmos in cascode amplifier,

$$\Rightarrow V_g = V_{bias1}$$

From cascode current mirror, $V_{higs1} = 1.08V$

$$V_s = 1.8V$$
 , $V_{thp} = 0.3906$

$$I_d = 0.5 \times u_p \times C_{ox} \times \frac{W}{L} \times (V_{gs} - V_{thp})^2$$

$$10\mu = 0.5 \times 45\mu \times \frac{W}{L} \times 0.1085 \implies \frac{W}{L} = 4.096$$
• $(\frac{W}{L})_{n} = 4.096$

→ For 22nm:

Let the assumed current, $I_d = 8\mu A$ and unity gain frequency, $f_u = 1 MHz$

Required gain = 20V/V

$$\begin{split} \boldsymbol{f}_{u} &= \frac{1}{2 \times \pi \times R_{out} \times C} \\ \boldsymbol{R}_{out} &= \frac{1}{2 \times \pi \times f_{u} \times C} \\ \boldsymbol{R}_{out} &= \frac{1}{2 \times \pi \times 1M \times 1p} \\ \boldsymbol{R}_{out} &= 159154.94 \Omega \end{split}$$

$$\begin{split} A_v &= g_m \times R_{out} \quad \Rightarrow g_m = \frac{A_v}{R_{out}} = \frac{20}{159154.94} \qquad \Rightarrow g_m = 12 \times 10^{-5} \\ g_m &= \sqrt{2 \times I_d \times u_n \times C_{ox} \times \frac{W}{L}} \quad \Rightarrow 12 \times 10^{-5} = \sqrt{2 \times 8\mu \times 120\mu \times \frac{W}{L}} \\ 120 &= 43.8178 \sqrt{\frac{W}{L}} \\ \bullet \left(\frac{W}{L}\right)_n &= 7.5 \end{split}$$

 V_g , V_{s} , V_{thp} be the gate voltage of 1st pmos in cascode amplifier, $\Rightarrow V_g = V_{bias1}$

From cascode current mirror, $V_{hias1} = 0.2481V$

$$V_s = 0.8V$$
, $V_{thp} = 0.44$
 $I_d = 0.5 \times u_p \times C_{ox} \times \frac{W}{L} \times (V_{gs} - V_{thp})^2$
 $4\mu = 0.5 \times 55\mu \times \frac{W}{L} \times 0.012544 \implies \frac{W}{L} = 11.59554$

$$\bullet \left(\frac{W}{L}\right)_p = 11.59554$$

INPUTS OF CASCODE AMPLIFIER

→ For 180nm

For nmos to be in saturation region,

$$V_{ds} \ge V_{gs} - V_{thn}$$

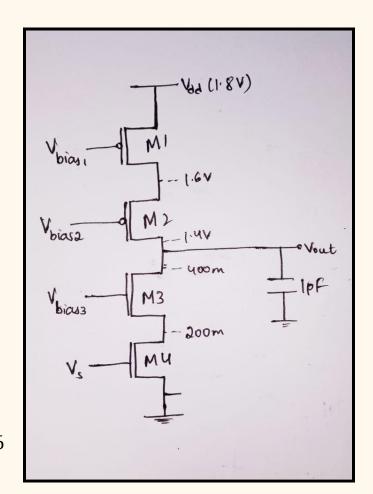
Let us assume $V_{dsat} = 200m$

- For M4, $200m \ge V_s - 0.5$, $\Rightarrow V_s \le 0.7$
- For M3, $200m \ge V_{bias3} - 0.2 - 0.5$ $V_{bias3} \le 0.7$

For pmos to be in saturation region,

$$V_{ds} \le V_{gs} - V_{thp}$$

- For M2, $-200m \le V_{bias2} - 1.6 + 0.3906$ $V_{bias2} \ge 1.0094$
- For M1, $-200m \le V_{bias1} - 1.8 + 0.3906$ $V_{bias1} \ge 1.2094$



Spice Values:

•
$$V_{bias1} = 1.08V$$

•
$$V_{bias2} = 941.2 \text{mV}$$

•
$$V_{bias3} = 649.62 \text{mV}$$

• V_s taken is 500m

→ For 22nm

For nmos to be in saturation region,

$$V_{ds} \ge V_{gs} - V_{thn}$$

Let us assume $V_{dsat} = 200m$

- For M4, $200m \ge V_s - 0.5$, $\Rightarrow V_s \le 0.7$
- For M3, $200m \ge V_{bias3} - 0.2 - 0.5$ $V_{bias3} \le 0.7$

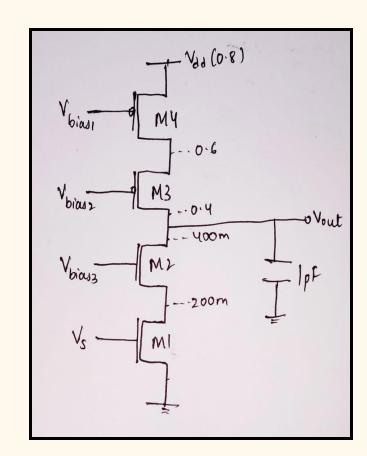
For pmos to be in saturation region,

$$V_{ds} \leq V_{gs} - V_{thp}$$

- For M2, $-200m \le V_{bias2} - 0.6 + 0.46$ $V_{bias2} \ge -0.06$
- For M1, $-200m \le V_{bias1} - 0.8 + 0.3906$ $V_{bias1} \ge 0.14$

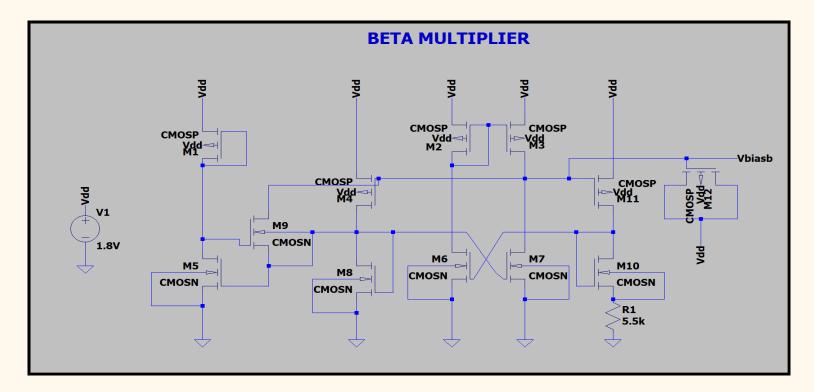
Spice Values:

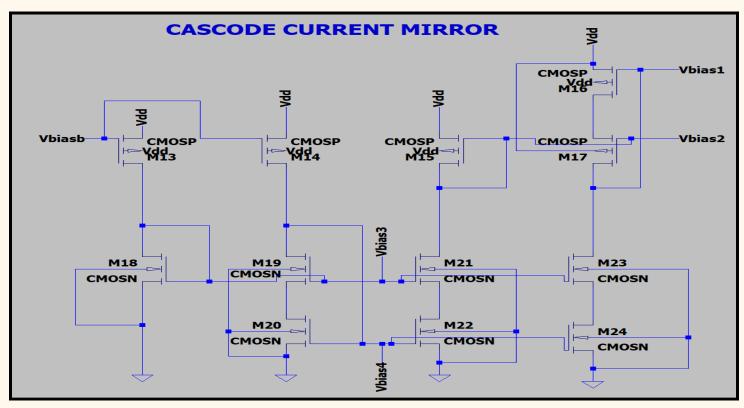
•
$$V_{bias1} = 248.126 \text{mV}$$

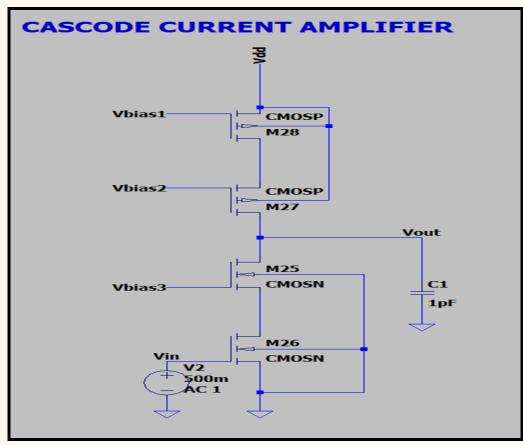


- $V_{bias2} = 150.5 \text{mV}$
- $V_{bias3} = 556.60 \text{mV}$
- V_s taken is 600m

SCHEMATIC







LAYOUT

Cascode Current Mirror

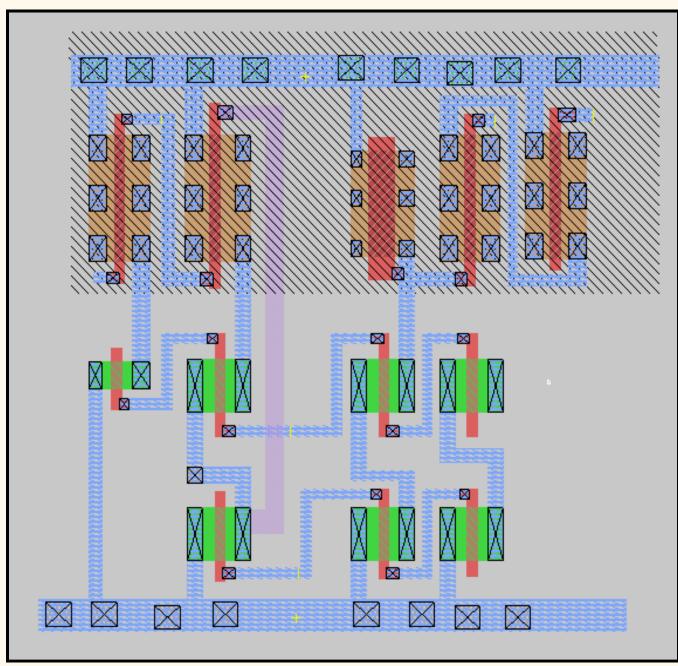


Fig: Cascode Current Mirror Layout

Cascode Amplifier

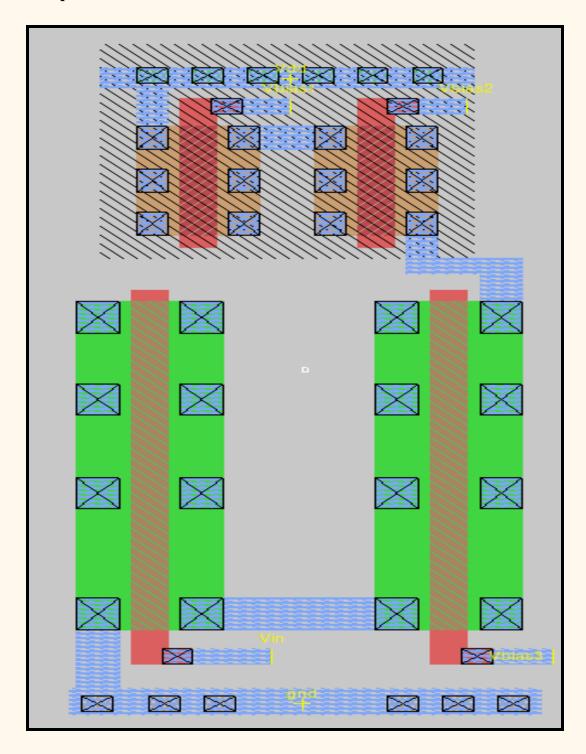


Fig: Cascode Amplifier

OBSERVATIONS:

Ltspice Plots:-

For180nm:

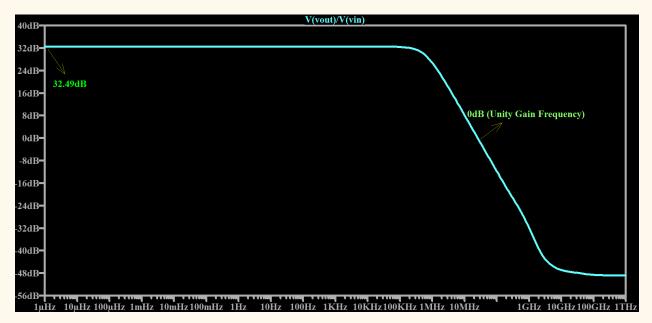


Fig: Frequency Response



Fig: Vbias Values

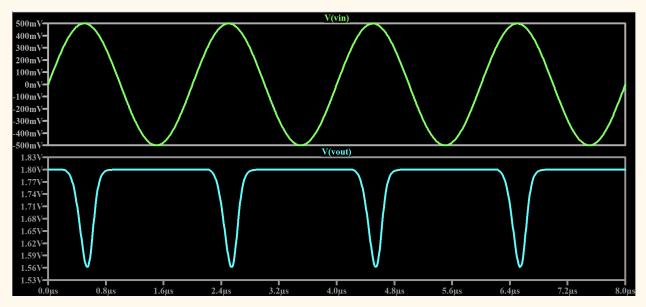


Fig: Sine Input

For 22nm:

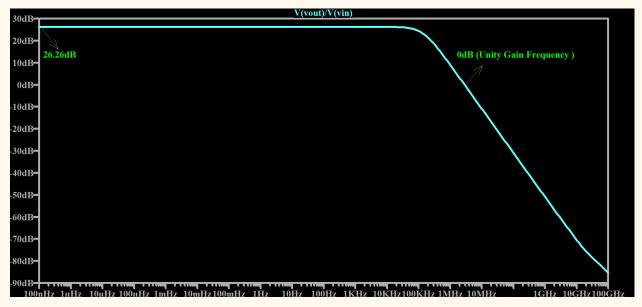


Fig: Frequency Response

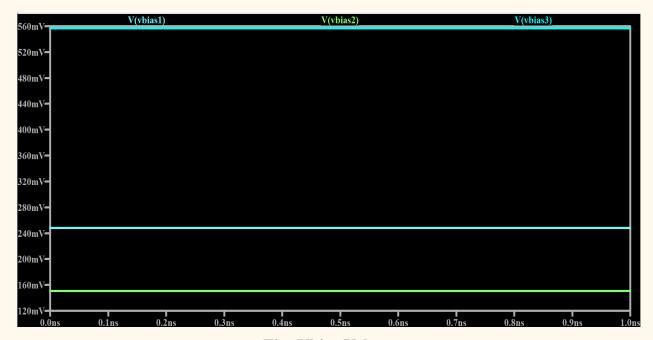


Fig: Vbias Values

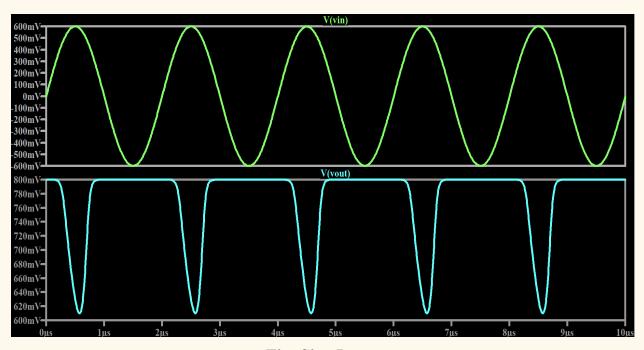


Fig: Sine Input

TABLES:

Technology File		Assumed Values		Spice Values			
	Unity Gain Frequency	Current (microamps)	Unity Gain Frequency	Current (microamps)	Gain (dB)		
180nm	10MHz	10	25MHz	8.92	32.49		
22nm	1MHz	4	2.78MHz	5.84	26.26		

Technology File	Calculated Values			Spice Values		
	gm	$\frac{W}{L}$ nmos	$\frac{W}{L}_{pmos}$	gm	$\frac{W}{L}$ nmos	$\frac{W}{L}_{pmos}$
180nm	3.14e-04	18.277	4.096	1.7e-04	15	5
22nm	12e-05	7.5	11.59	4.59e-05	5	9.39

REQUIRED SPECIFICATIONS:

- Required gain is 20V/V = 20log(20) = 26.02dB, hence simulated gain should be atleast 26.02dB. Gain is 32.49dB and 26.26dB for 180nm and 22nm respectively.
- Power dissipation \leq 5mW. From simulated data 16µW and 4µW for 180nm and 22nm respectively.
- Unity Gain Frequency must be greater than 500KHz. It is 25MHz and 2.78MHz for 180nm and 22nm respectively.
- Frequency response must be a low pass filter. Hence required specifications are satisfied.

CONCLUSION: Beta Multiplier, Cascode Current Mirror and Cascode Amplifier are simulated in Itspice and magic software. Practical calculations are almost appropriate to Itspice values. Different analyses are made and understood. It's also visible from the observation tables that the assumed, calculated and spice values of different parameters are approximately in the same ranges, which verifies that the simulations and practical calculations are almost matched with each other.