

# DESIGN REPORT

## Group V8G

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## Name of the Machine

Railway Cart

## Purpose of the Machine

Railway carts are used for the transportation of cargo. This cart is attached to the front of the train, between the winch and the rest of the wagons. We expect all the wagons to move with the velocity at which they are being pulled, but it may not always be the case. (Example- during travel along an inclined plane the wagons move with a velocity greater than the pulling velocity) Therefore, to regulate the velocity of the wagons, the railway cart in question is used.

## Design Objective

To design a safe railway cart that regulates the velocity of the 26 wagons attached to it. It should be done in such a manner that the train can be stopped within 1m @ 2 minutes.

## Broad Design Specifications

- Has 26 wagons of 100 tonnes each attached to it
- Velocity of cart-  $0.125\text{m/s}$
- Stopping distance- 1m
- Wheels and axle- According to Indian railway standards

# Calculation of Design Load

## 1. Braking load

The stopping distance,  $s = 1\text{m}$  and

the velocity of the cart,  $v = 0.125\text{m/s}$

Total mass,  $m = 26 \times 100 \times 1000\text{kg}$

therefore, acceleration,  $a = v^2/2s = 0.00781\text{m/s}^2$  and

**The braking load,  $F = ma = 20300\text{N}$**

## 2. Weight of Cart

- Without dead weight

braking force = frictional force

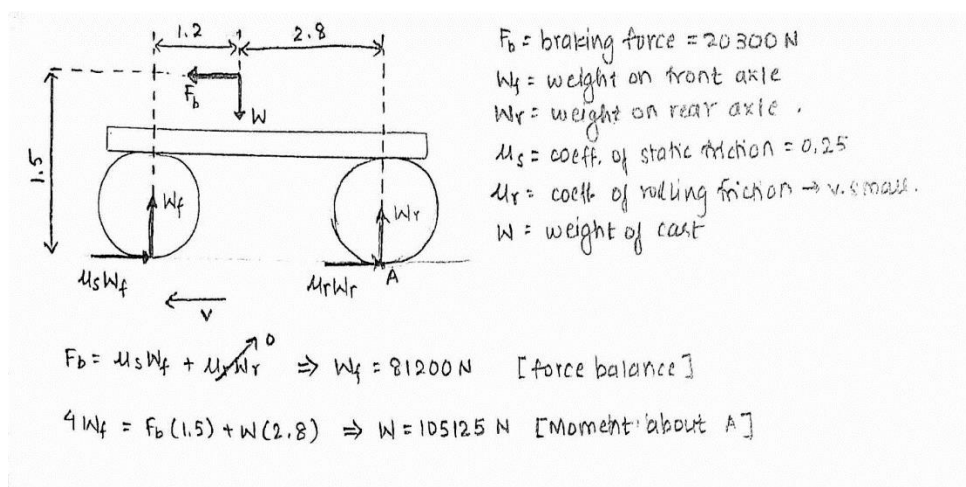
where the coefficient of friction,  $\mu = 0.25$

$20300 = \mu \times (\text{weight of the cart})$

therefore, the weight of the cart,  $W = 81200\text{N}$

- With dead weight

Considering a mass distribution of 7:3 and brake on the front axle and a distance of 4m between the axles of the wheels

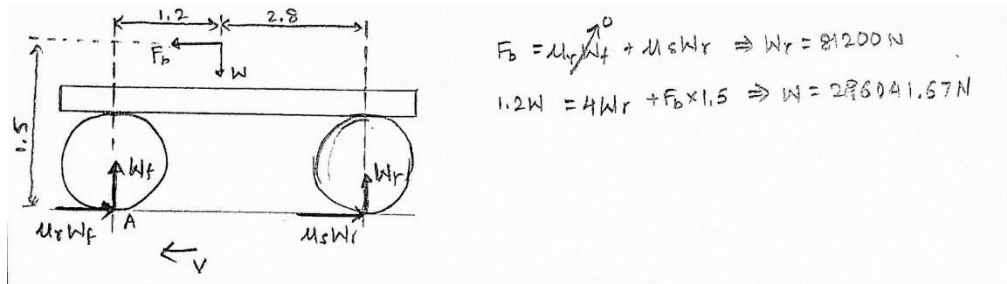


Centre of gravity lies at 1.2m from the front axle  
where coefficient of static friction on the front

wheel,  $\mu(s) = 0.25$

balancing forces (weight on front axle,

$W(f) = 81200\text{N}$ ) and moment about the centre of gravity, we get weight of the cart,  $W = 105125\text{N}$



(Considering 7:3 mass distribution and brake on the rear axle, the weight of the cart comes out to be  $296041.67\text{N}$ . The case where the mass of the cart is less; is chosen.)

**The final weight of the cart is  $W = 105125\text{N}$**

# Design on Machine Elements

## No. of wheels

material of wheels- cast steel ( $E = 215\text{GPa}$ ,  $\nu = 0.265$ )

material of track- rolled steel ( $E = 186\text{GPa}$ ,  $\nu = 0.287$ )

radius of wheel,  $r(w) = 0.5\text{m}$

$S_{yc} = 250\text{MPa}$ ,  $f_{os} = 2$ ,  $P = S_{yc}/f_{os} = 125\text{MPa}$

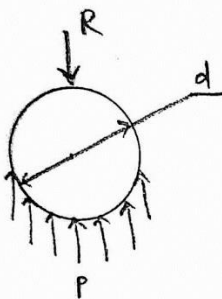
Maximum axle load = 20.32 tonne

Maximum bearing load by wheel,

$F = \text{Maximum axle load}/2 = 10.16 \text{ tonne}$

**Number of wheels = total load/ $F = 4$**

## Bush bearing



$p = \text{Bearing pressure} = 3\text{MPa}$

$R = \text{max. force on one wheel}$

$= W(f)/2 = 40600\text{N}$

$d = \text{diameter of shaft} = 128.5\text{mm}$

Diameter of shaft where bush is to be placed,  $d = 128.5\text{mm}$   
(Indian Railway Standards)

Bearing pressure,  $p = 3\text{MPa}$

Maximum force on one wheel,  $R = W(f)/2 = 40600\text{N}$

using,  $p = R/(l \cdot d)$  we get,

**length of the bush,  $l = 105.32\text{mm}$**

radius of shaft,  $r = d/2 = 64.25\text{mm}$  and  $c/r = 0.001$ ,

therefore  $c = 0.06425\text{mm}$

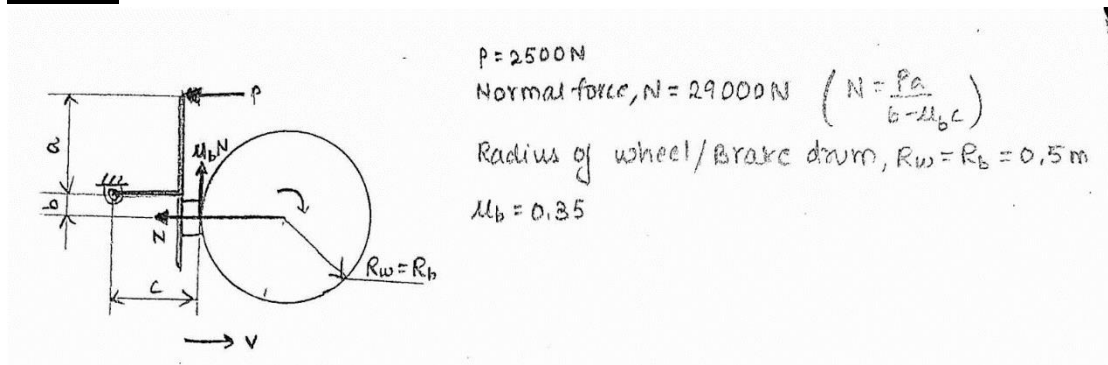
**inner diameter of bush,  $d(i) = d + 2c = 128.6285\text{mm}$**

thickness of bush,  $t = 2.54\text{mm}$

outer diameter of bush,

$$d(o) = d(i) + 2t = 133.7085\text{mm} \sim 134\text{mm}$$

## Brake



Placing the drum brake on the front axle

The brake is self-energizing in nature

weight on each front wheel,  $R = 81600/2 = 40600\text{N}$

coefficient of friction between wheel and track,  $\mu = 0.26$

radius of wheel,  $r(w) = 0.5\text{m}$

Braking torque,  $T = \mu * R * r(w) = 0.25 * 40600 * 0.5 = 5075\text{N}$

$$T = (a * \mu(b) * P * R(b)) / (b - \mu(b) * c)$$

where  **$R(b)$**  i.e radius of brake drum =  **$r(w) = 0.5\text{m}$** ,

**$b = 125\text{mm}$** ,

**$\mu(b)$**  i.e friction coefficient between wheel and  
brake shoe =  **$0.35$** ,

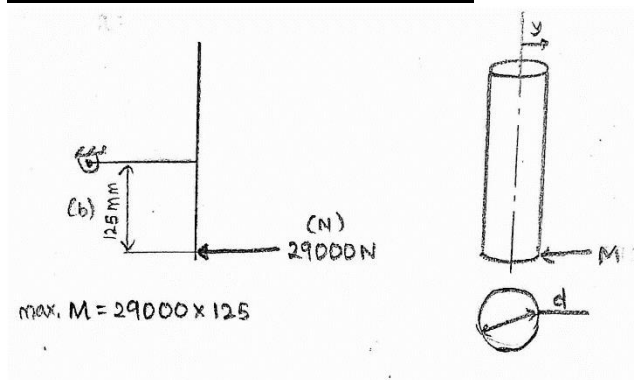
**$P = 2500\text{N}$**

For self-energizing,  $b < \mu(b) * c$  i.e  $c > 125/0.35 = 375\text{mm}$

hence, taking  **$c = 500\text{mm}$** ,

we get  **$a = 580\text{mm}$**

## Brake Lever Dimensions



Material- mild steel

Maximum bending moment on the lever,  $M = N \cdot b$

$$M = 29000 \cdot 125 = 3625000 \text{ Nmm}$$

$$\sigma(\text{permissible}) = 400 / \text{fos} = 400 / 2 = 200 \text{ MPa}$$

$$\sigma = M \cdot y / I$$

for a circular cross section,  $I / y = \pi \cdot D^3 / 64$

$$200 = 3625000 \cdot 64 / \pi \cdot D^3$$

the diameter of the brake lever,  **$D = 71.75 \text{ mm} \sim 72 \text{ mm}$**

## Bolts on axle housing

material- mild steel

$$(\text{Shear Stress, } \tau_{\text{os}}) = S_{yt} / 2 = 400 / 2 = 200 \text{ MPa}$$

Permissible Shear stress,

$$\tau_{\text{os}} = \tau_{\text{os}} / \text{fos} = 200 / 2 = 100 \text{ MPa}$$

$$\text{force on each bolt, } f = 20300 / 2 = 10150 \text{ N}$$

using  $\tau_{\text{os}} = f / \text{area of bolt}$ , we get

$$\text{diameter of bolt, } d(c) = 11.37 \text{ mm} \sim 12 \text{ mm}$$

$$\text{taking thickness of housing} = 3 \cdot d = 36 \text{ mm}$$



### Bolts on axle cap

Material- mild steel ( $S_{yt} = 400\text{MPa}$ )

Permissible tensile stress,

$$\sigma = S_{yt}/f_{os} = 400/2 = 200\text{MPa}$$

$$\text{Axial load} = 0.2 * F = 4060\text{N}$$

$$\text{Axial load on each bolt, } p' = 4060/4 = 1015\text{N}$$

using  $\sigma = p'/\text{area of bolt}$ , we get

**diameter of bolt,  $d' = 2.54\text{mm} \sim 5\text{mm}$**

**length of bolt,  $l' = 1.5d' = 7.5\text{mm}$**

### Cross Section of chassis (Longitudinal beam)

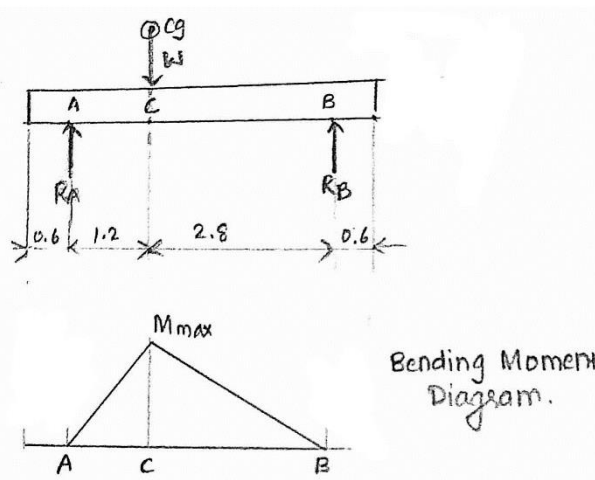
material- mild steel ( $S_{yt} = 400\text{MPa}$ )

Permissible tensile stress,

$$\sigma = S_{yt}/f_{os} = 400/2 = 200\text{MPa}$$

Considering the entire weight of the vehicle ( $W = 105125\text{N}$ ) at the centre of gravity (1.2m from the front axle), and reaction forces  $R_A$ ,  $R_B$  at the front and rear wheel respectively.

Weight on one longitudinal bar =  $W/2 = 52562.5\text{N}$  (in the line of  $C_g$ )



Balancing forces and moment about the centre of gravity, we get

$R_a = 36793.75\text{N}$  and  $R_b = 15768.75\text{N}$

Calculating the maximum bending moment based on the values above,

$$M(\max) = 44152.5\text{Nm}$$

$$\sigma(b) = M/z = 44152500/z$$

We know that pulling force,  $F(p) = 20300\text{N}$

$$\sigma(p) = F(p)/\text{Area} = 20300/A$$

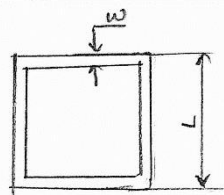
$$\sigma(b) + \sigma(p) = \sigma$$

$$\text{i.e. } 44152500/z + 20300/A = 200 \text{ (where } z \text{ and } A \text{ are in mm)}$$

The I-section beam suitable for the above condition is

**ISLB 250(h=250mm, b=125mm,  $t_f = 8.2\text{mm}$ ,  $t_w = 6.1\text{mm}$ )**

### Cross section of chassis (Lateral beam)



$$L = 250 - 2(8.2) = 233.6\text{ mm}$$

[to have full contact with the  
I-sectional longitudinal beam]

**width of the section,  $w = 8.2\text{mm}$**

### Compression Spring

material- En 10277 (spring steel)

ultimate tensile strength,  $S(ut) = 1200\text{MPa}$

$$\tau = S(ut)/2 = 600\text{MPa}$$

$E = 212\text{ GPa}$ ,  $\nu = 0.29$  at  $20^\circ\text{C}$

$$G = E/(2(1+\nu)) = 82.17\text{ GPa}$$

$$c = D/d = 6;$$

where  $D$  is the mean diameter of the coil and  $d$  is the diameter of the spring

$$k = (4c - 1/4c - 4) + 0.615/c = 1.2525$$

$$\tau = k * (8 * P * c / \pi * d^3)$$

solving for d, we get **d = 25.45mm ~ 26mm**

since D/d = 6, **D = 156mm**

$$\text{deflection} = (8 * P * (D^3) * N) / (G * d^4) = 15\text{mm}$$

solving for number of active coils, N, we get **N = 0.91 ~ 1**

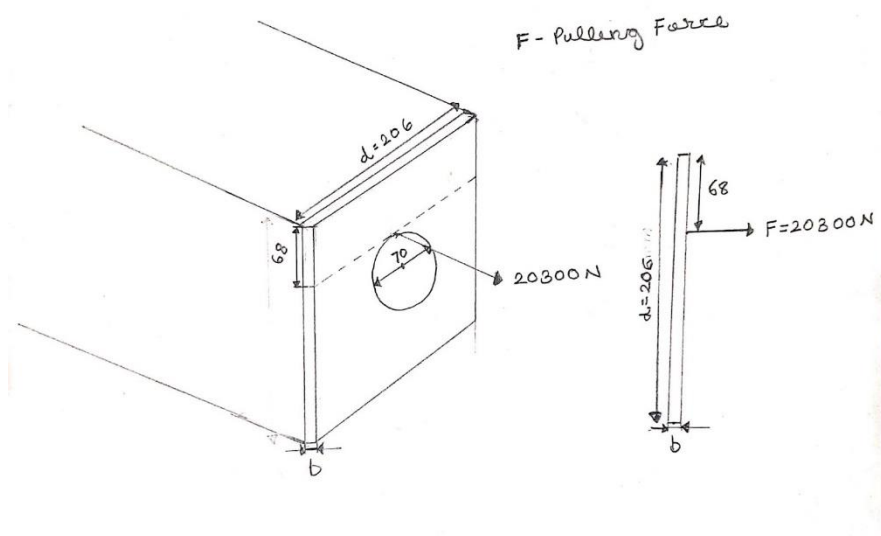
Using square and grounded ends;

so the **total number of coils, N(t) = N + 2 = 3**

Solid length of the spring = N(t) \* D = 78mm

**free length of the spring = 94.5mm**

### Width of box



Material used- mild steel

Ultimate Yield Stress = 400MPa

Tensile strength( $\sigma$ ) = 400/FOS = 400/2 = 200MPa

Pulling force(F)=20300N

Max bending moment(M)=F\*68=20300\*68

**d=206mm**

$$\text{Bending Stress}(\sigma) = M*y/I$$

$$200 = (20300*68*b/2)/(db^3/12)$$

$$\text{width of box}(b) = (20300*68*6/206*200)^{1/2}$$

$$\mathbf{b = 14.17mm \sim 15mm}$$

### Bolts for attaching box with chassis

material- mild steel ( $S_{yt} = 400\text{MPa}$ )

Permissible tensile stress,

$$\sigma = S_{yt}/f_{os} = 400/2 = 200\text{MPa}$$

$$F = 20300\text{N}$$

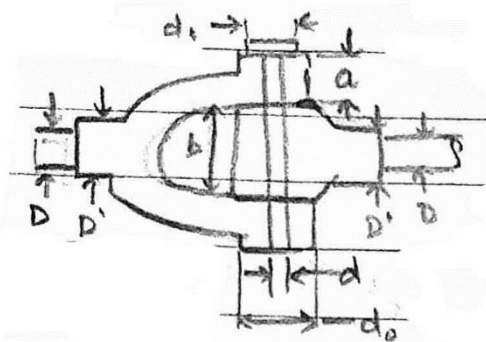
$$\text{Axial load on each bolt, } p' = 20300/2 = 10150\text{N}$$

using  $\sigma = p'/\text{area of bolt}$ , we get

$$\mathbf{\text{diameter of bolt, } d = 8.04\text{mm} \sim 9\text{mm}}$$

$$\mathbf{\text{length of bolt, } l = 35\text{mm}}$$

### Pin joint(Knuckle)



Material used - steel

Ultimate Yield Strength = 400 MPa

Tensile strength =  $400/F.O.S = 400/2 = 200\text{ MPa}$

Shear Strength =  $\sigma/2 = 100\text{ MPa}$

$$\mathbf{D = \sqrt[4]{4p/\pi * \sigma(t)}} = 11.37 \sim 12\text{mm}$$

$$D' = 1.1D = 13.2 \text{ mm}$$

$$a = 0.75D = 9 \text{ mm}$$

$$b = 1.25D = 15 \text{ mm}$$

Diameter of pin,

$$d = \max(\sqrt[3]{(2p/\pi \cdot \tau)}, \sqrt[3]{((32/p\pi \cdot \sigma \cdot (b)) \cdot (p/2)((b/4) + (a/3)))}) \\ = \max(11.37, 15.17)$$

$$d = 15.17 \sim 16 \text{ mm}$$

$$d_o = 2d = 32 \text{ mm},$$

$$d_1 = 1.5d = 24 \text{ mm}$$

$$\sigma'_t = P/b(d_o - d) = 84.58 < \sigma(t),$$

$$\sigma'_c = 84.58 = \tau_1 < \sigma_c, \sigma$$

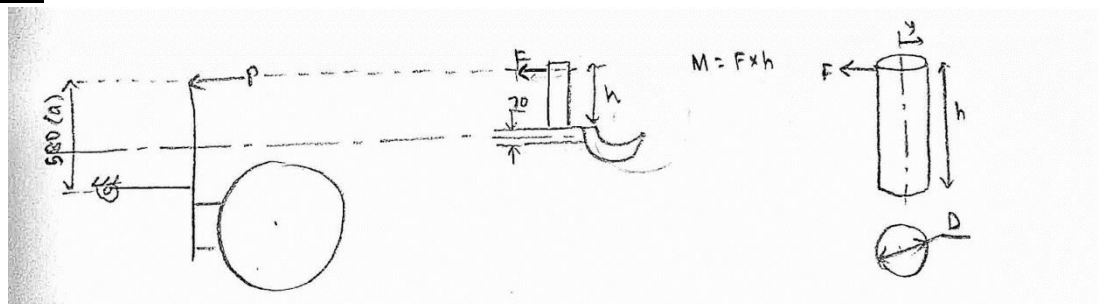
It is a safe design for eye

$$\sigma''_t = P/2a(d_o - d) = 70.48 = \sigma''_c$$

$$= \tau_1 < \sigma_t, \sigma_c,$$

It is a safe design for fork

### Vertical rod



The height of the point of force on the rod from the hook ( $h$ ) must coincide with the height ' $a$ ' of the brake lever,  $h = 441.1 \text{ mm}$

Maximum bending moment on the lever,  $M = F \cdot h$

$$M = 20300 \cdot 441.1 = 8954330 \text{ Nmm}$$

$$\sigma(\text{permissible}) = 400/\text{fos} = 400/2 = 200\text{MPa}$$

$$\sigma = M*y/I$$

$$\text{for a circular cross section, } I/y = \pi*D^3/64$$

$$200 = 8954330*64/\pi*D^3$$

$$\text{the diameter of rod, } D = 96.99\text{mm} \sim 97\text{mm}$$

### Horizontal rod

$$\text{Tensile strength} = 400/\text{F.O.S} = 400/2 = 200 \text{ MPa}$$

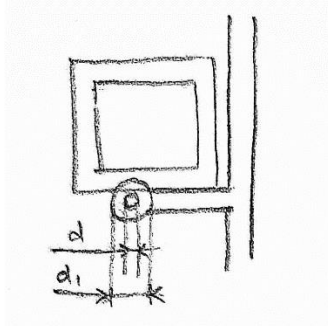
$$\text{Tensile strength} = F/A$$

$$F = 20300\text{N, and } A = (\pi*d^2)/4$$

$$\text{Solving for diameter of rod, } d;$$

$$\text{we get, } d = 11.37\text{mm} \sim 12\text{mm}$$

### Pin joint for brake lever



$$\text{Material -Annealed steel (Syt=520Mpa)}$$

$$\text{Shear strength} = 260 \text{ MPa}$$

$$\tau(\text{permissible}) = 260/2 = 130\text{Mpa}$$

$$\text{Moment, } T = N*b = 29000*125$$

$$\tau = (\pi*(d^3)*T)/16$$

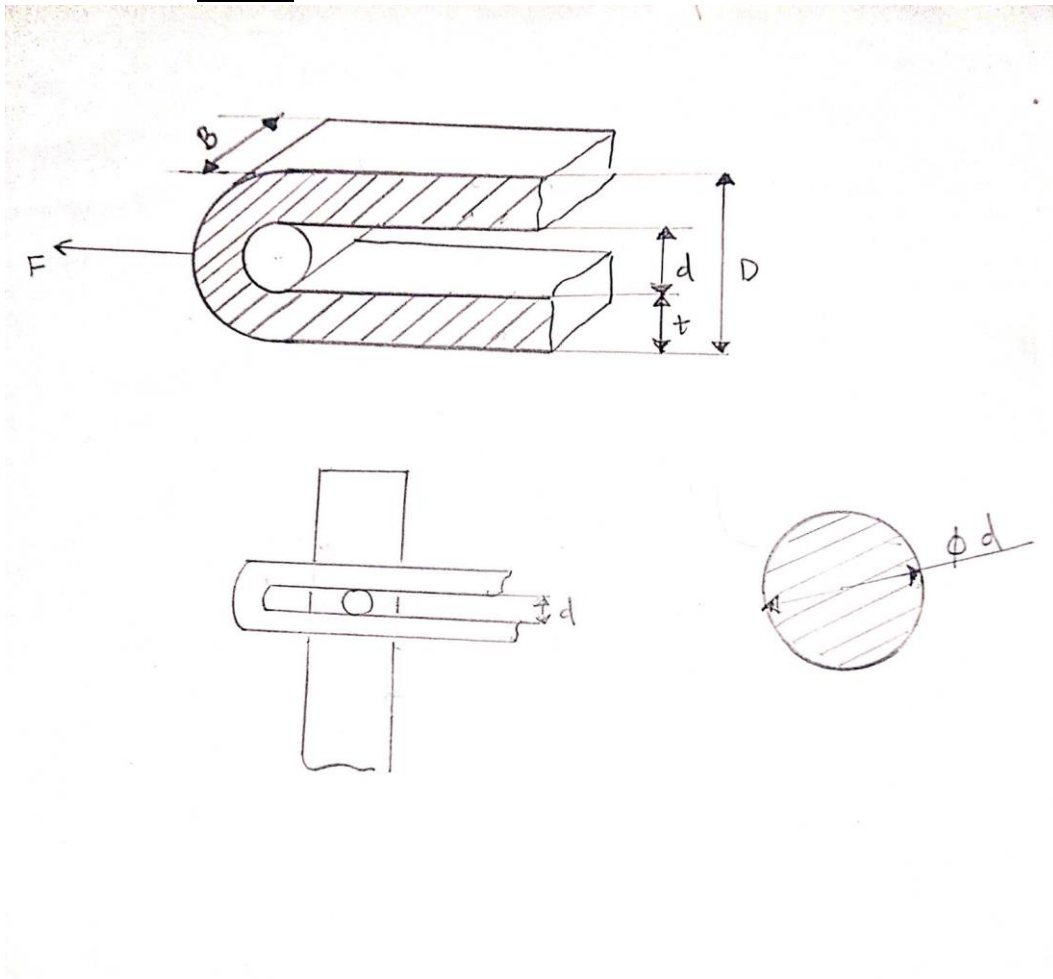
$$\text{solving for diameter, } d; \text{ we get}$$

$$\text{pin diameter, } d = 52\text{mm}$$

$$\text{boss diameter,}$$

$$d(1) = 1.6*d = 81\text{mm}$$

## Brake Handle



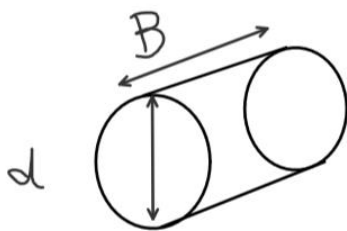
### **Stresses on pin of handle**

$$\text{Area} = \pi d^2 \quad \text{FOS} = 2$$

$$\tau(\text{shear}) = F/A$$

$$200/\text{FOS} = 20300/(\pi d^2/4)$$

$$\mathbf{d = 16.07 \sim 17mm}$$



### **Stresses on slider**

$$\text{Area} = B \times t$$

$$\sigma(\text{compressive})/\text{FOS} = F/A$$

$$400/2 = 20300/B \times t$$

$$t = 16.9 \sim 18 \text{ mm}$$

$$\tau = F(\text{compressive on collar})/\text{Area}$$

$$400/2 = 20300/18 \times B$$

$$B = 5.6 \sim 6 \text{ mm}$$

### Hook

Working Load- 30 tonnes

Weight Each- 46.7 kg



# Specifications of the Machine

**1. Overall Dimensions:**  $(6.45 \times 2.13 \times 1.22) \text{ m}^3$

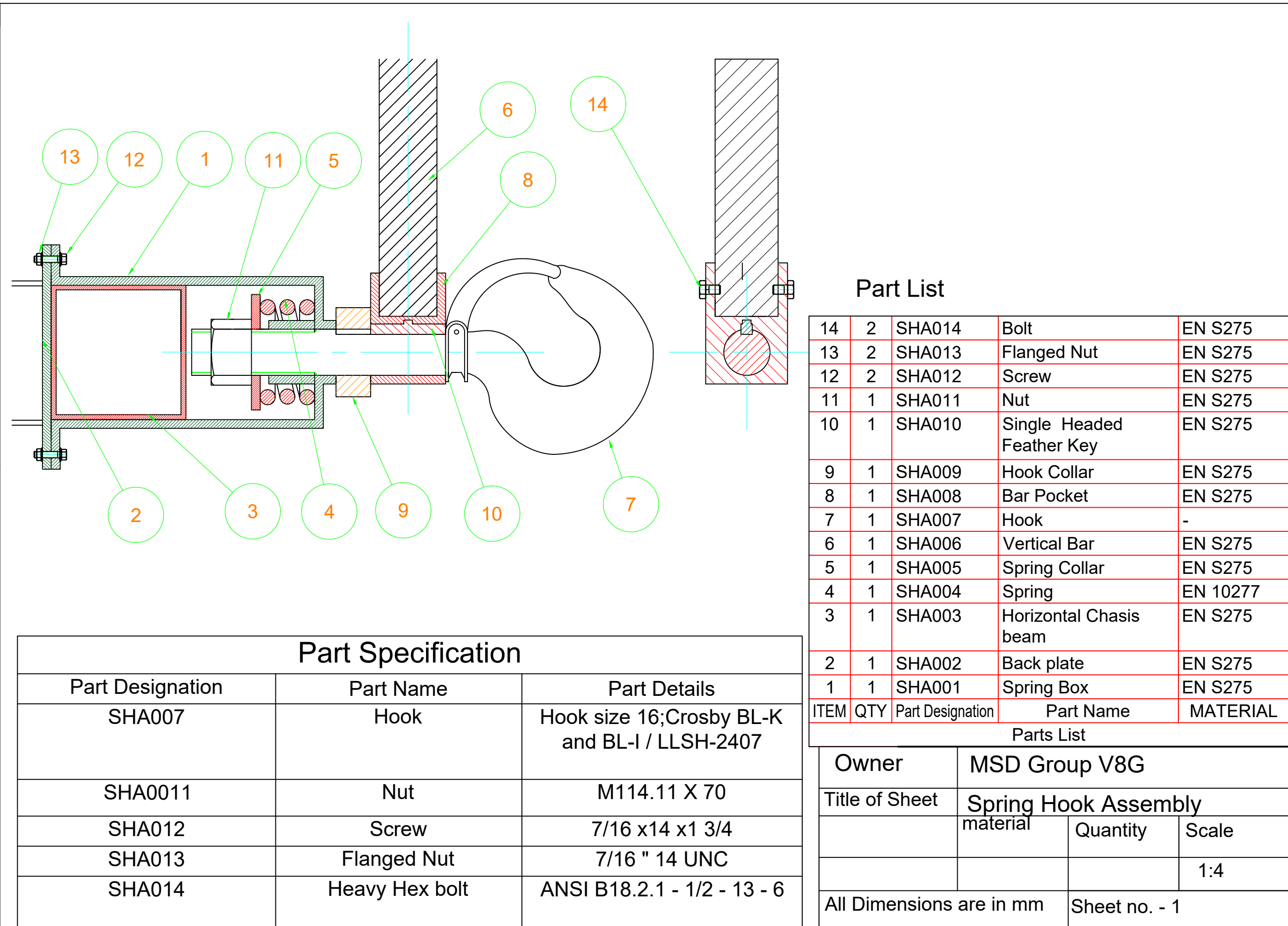
**2. Power Requirement:** 2537.5 W

**3. Operational Specifications:**

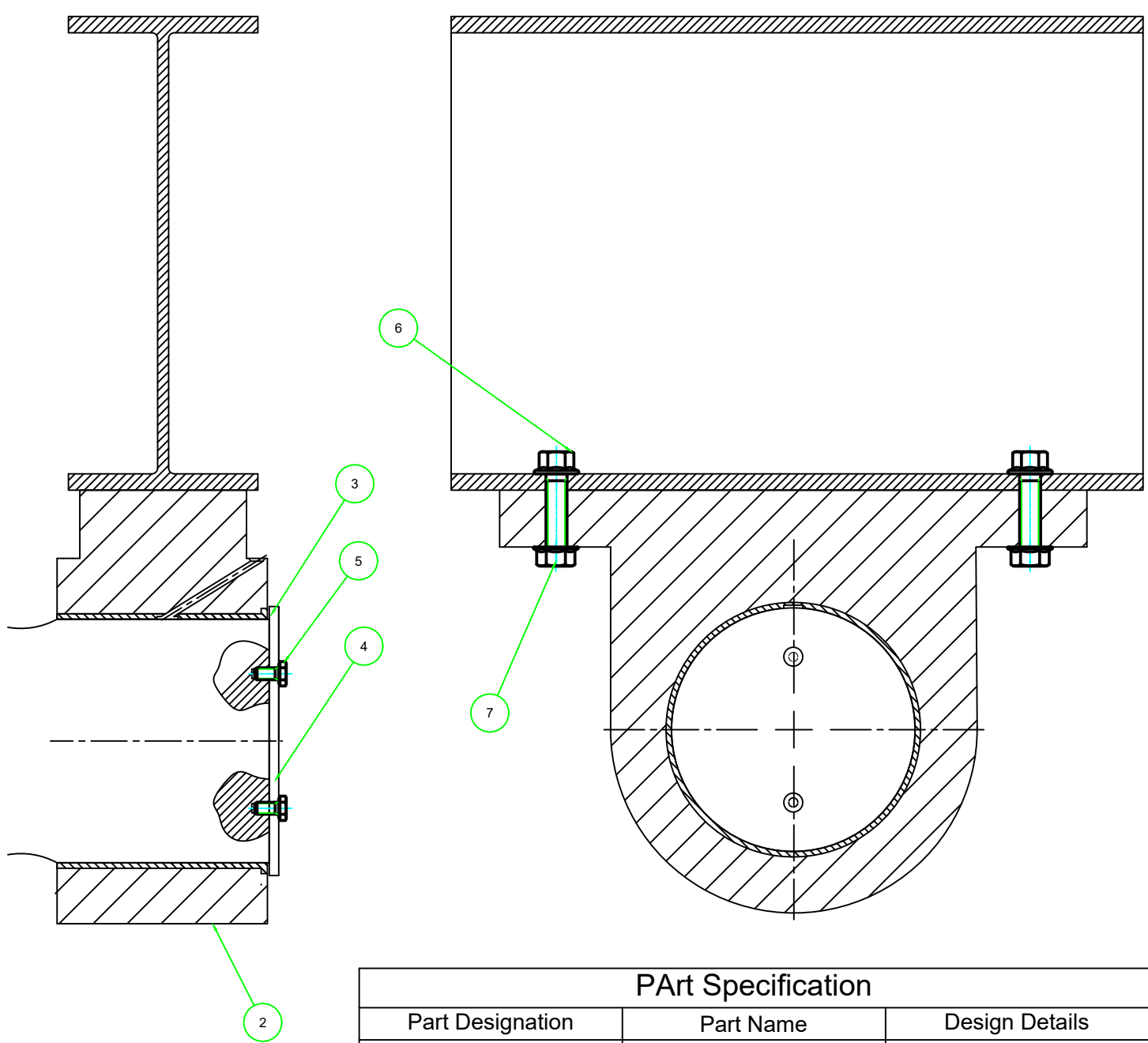
- The cart maintains a velocity of 0.125 m/s
- The stopping distance is 1 m
- The cart is subjected to only linear motion

# SUBASSEMBLY DRAWINGS

## 1.Spring Hook Assembly



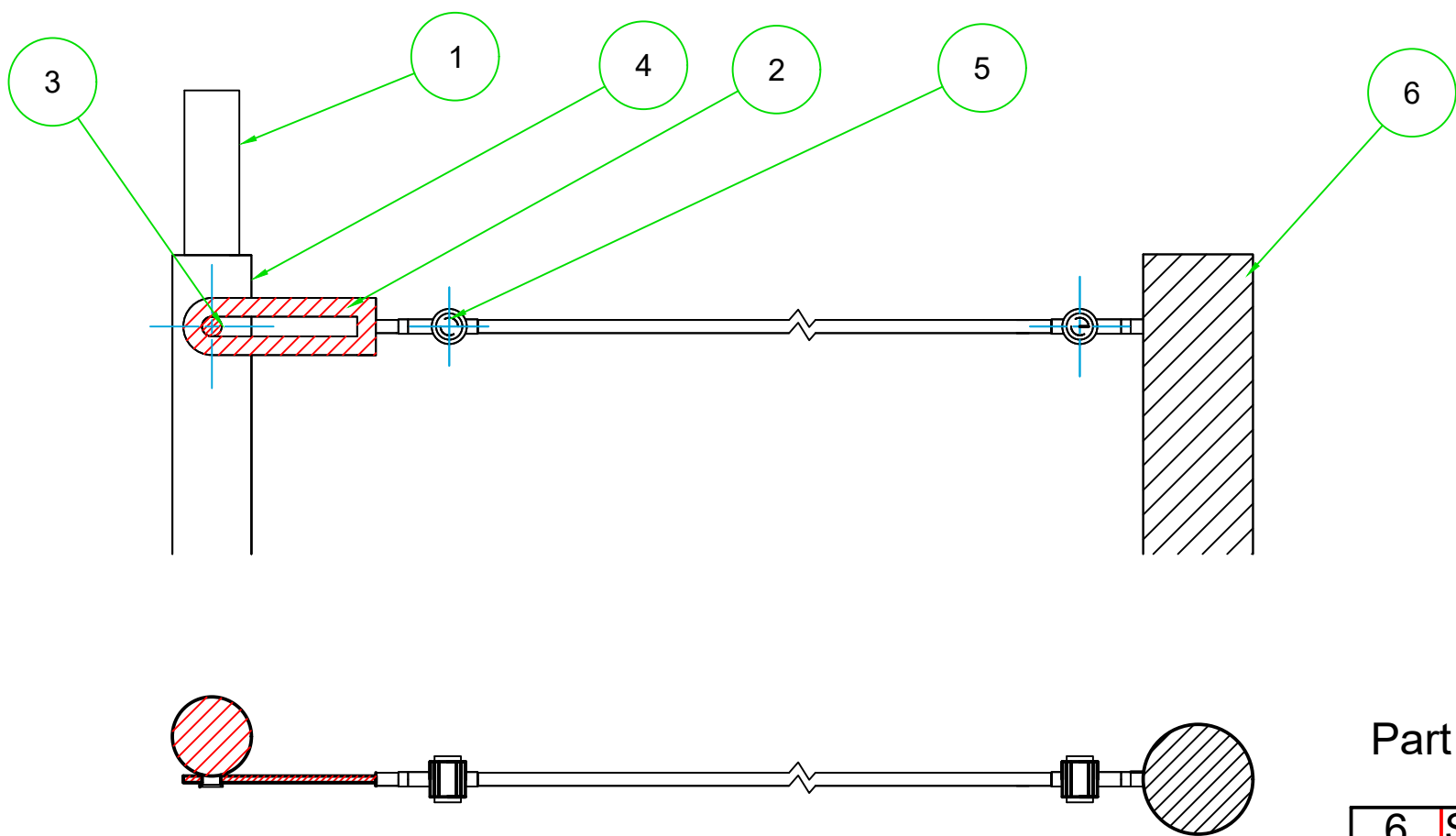
## 2. Bush Housing Assembly



PArT Specification		
Part Designation	Part Name	Design Details
BHA005	Hex Screws	Hex Cap Screw - ANSI B18.2.1 - 1/4 - 20 - 1/2
BHA006	Housing Screws	Hex Flange Screw - Regular Thread - Inch - IFI 111 - 1/2 x 13 x 1 3/4
BHA007	Housing Flange Nut	Hex Flange Nut - UNC - IFI - 1/2 - 13

7	2	BHA007	Housing Flange Nut	EN S275
6	2	BHA006	Housing Screw	EN S275
5	2	BHA005	Hex Screws	EN S275
4	1	BHA004	Axle cap	EN S275
3	1	BHA003	Bush	SAE 841
2	1	BHA002	Bush Housing	EN S275
Item	Qty	Part Designation	Part Name	Material
Owner		MSD Group V6A		
Title of Sheet		Bush Housing Assembly		
		material	Quantity	Scale
				1:1
All Dimensions are in mm			Sheet no. - 2	

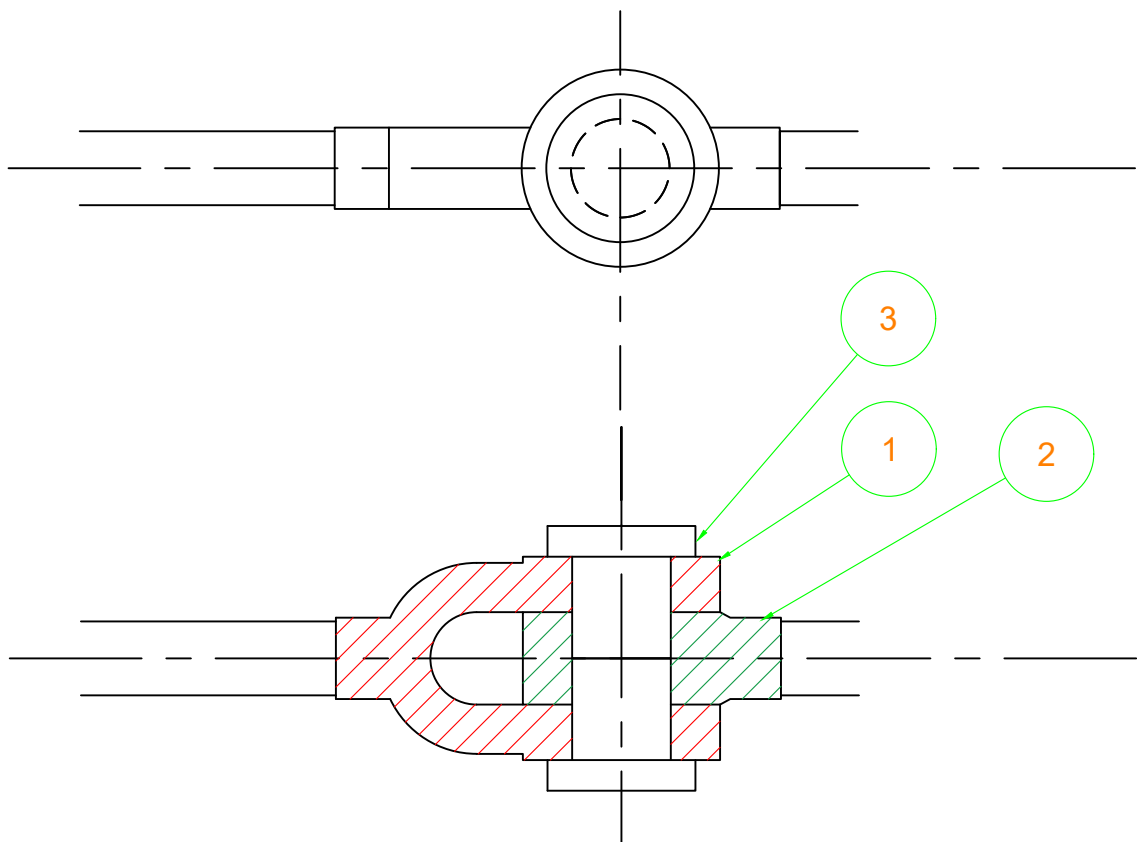
### 3.Slider Knuckle Rod Assembly



Part List

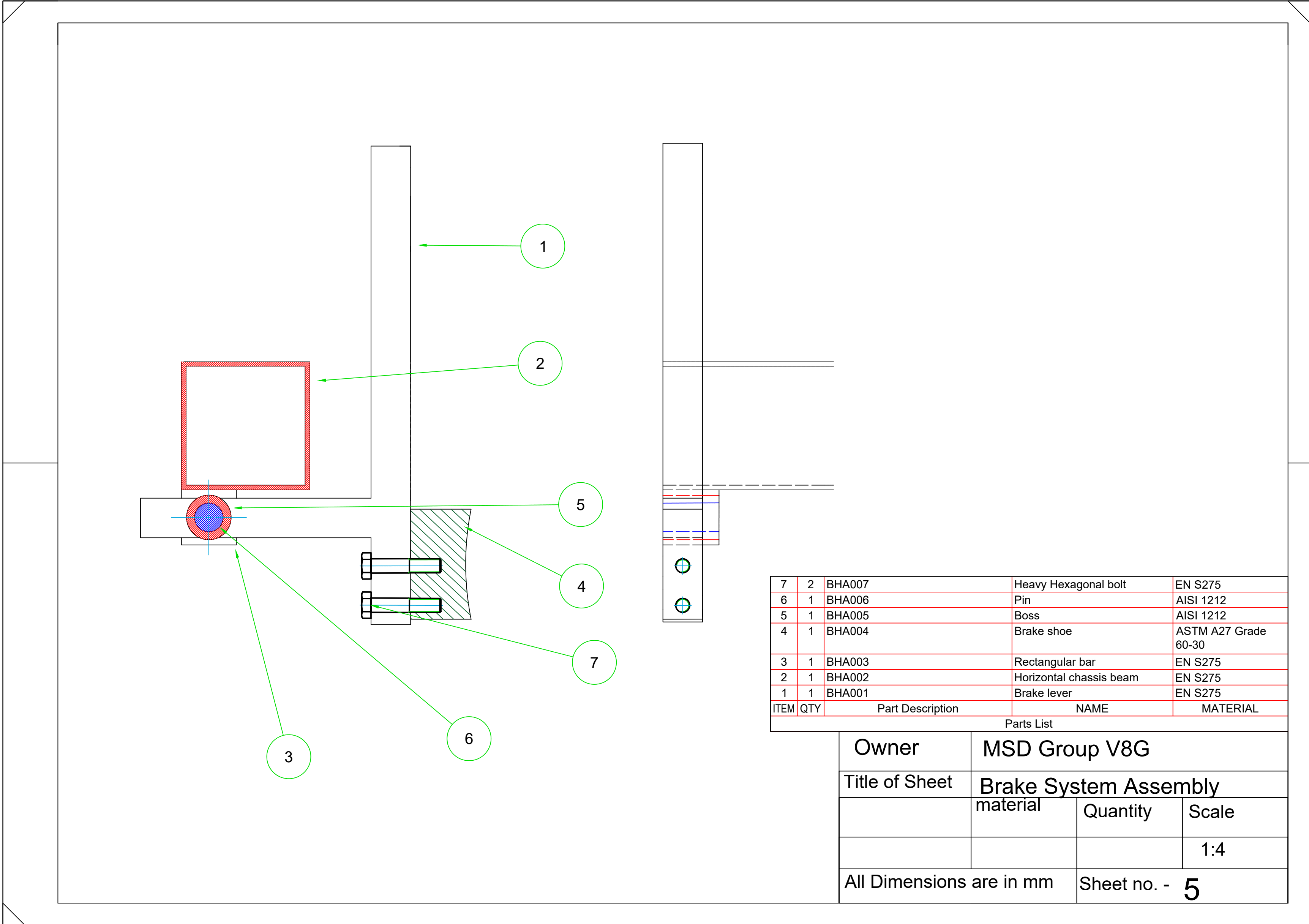
6	SKR006	Vertical Rod	1	EN S275
5	KPA	Knuckle Pin Subassembly	2	ASTM A27 GRADE 60-30
4	SKR004	Main Brake Lever	1	EN S275
3	SKR003	Slider Pin	1	EN S275
2	SKR002	Slider	1	EN S275
1	SKR001	Brake handle	1	EN S275
Item	Part Designation	Part Name	Qty	Material
Owner		MSD Group V8G		
Title of Sheet		Slider Knuckle Rod		
		material	Quantity	Scale
				1:4
All Dimensions are in mm			Sheet no. - 3	

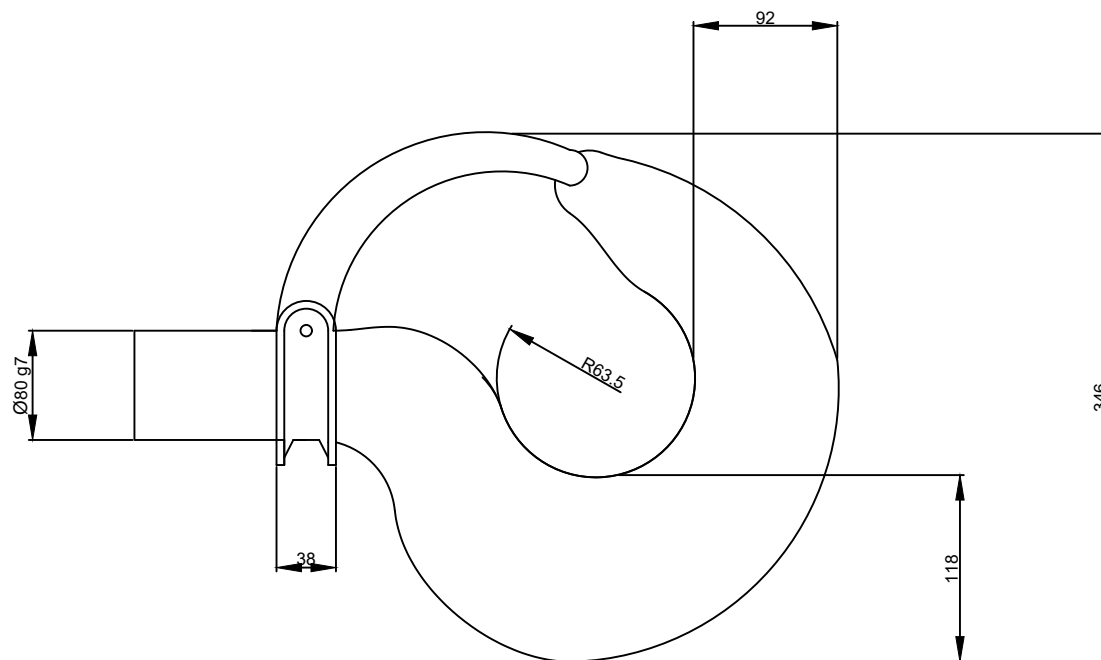
# 4.Knuckle Pin Assembly



3	KPA003	Pin	EN S275	2
2	KPA002	Eye	EN S275	2
1	KPA001	Fork	EN S275	2
ITEM	Part Designation	Part Name	MATERIAL	QTY
Parts List				
Owner		MSD Group V8G		
Title of Sheet		Knuckle Pin Assembly		
		Quantity	Scale	
			1:1	
All Dimensions are in mm      Sheet no. - 4				

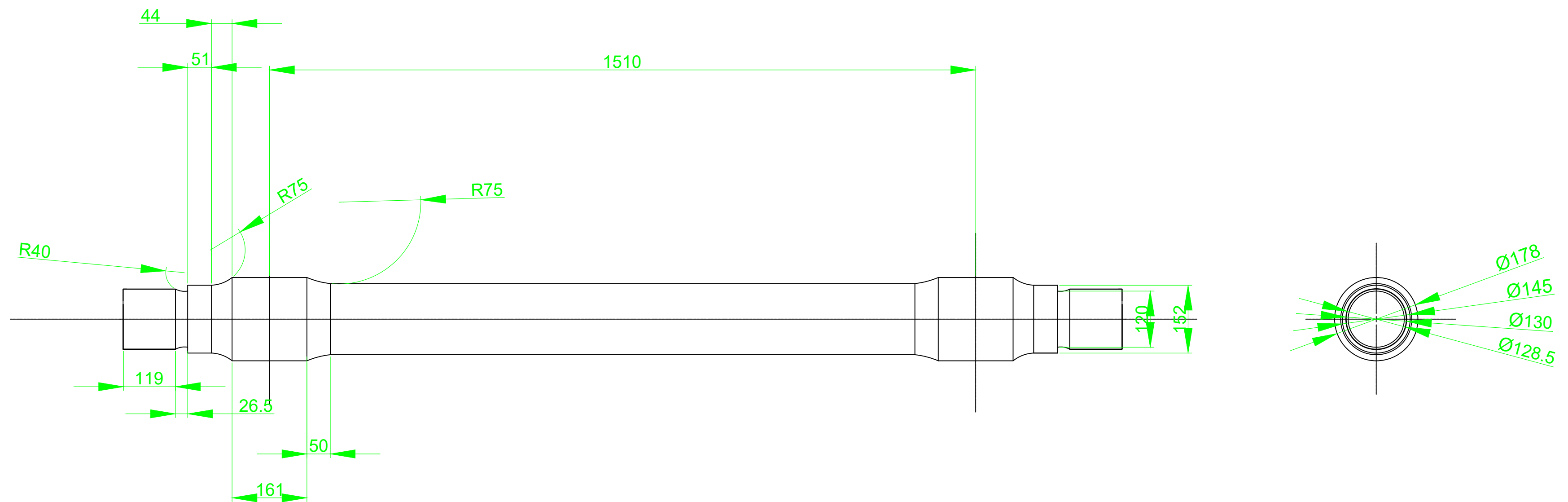
# 5. Brake Assembly





# SHA007

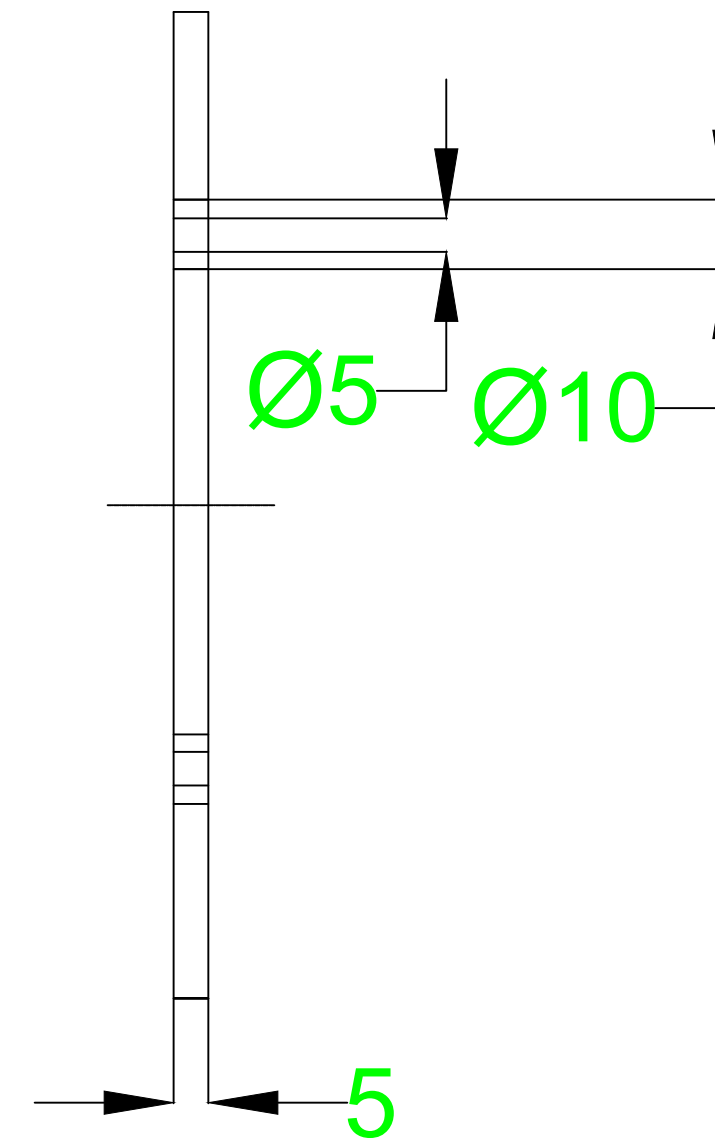
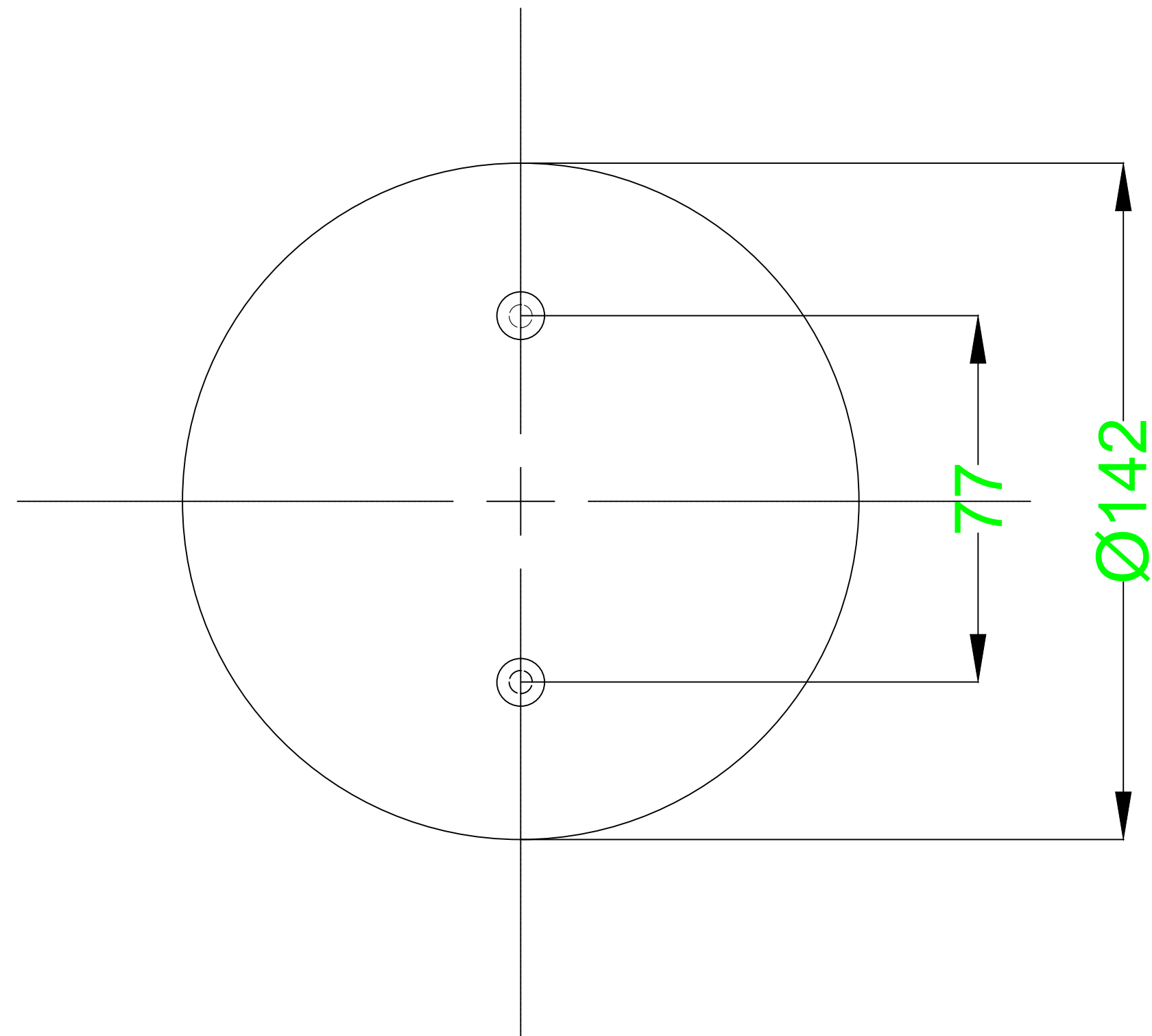
Owner	MSD Group V8G		
Title of Sheet	Hook		
		Quantity	Scale
			1:2
All Dimensions are in mm		Sheet no. - 6	



CWA003

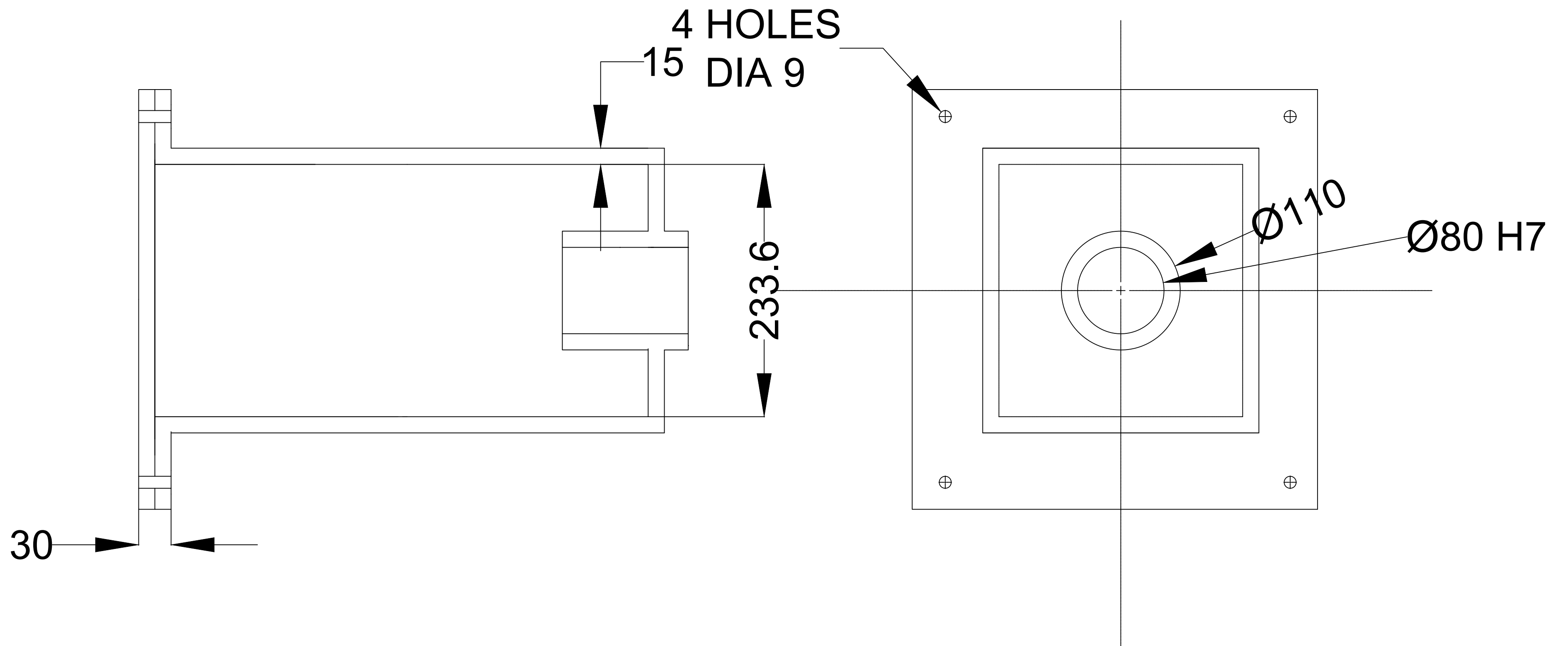
Owner	MSD Group V8G		
Title of Sheet	Axle component drawing		
		Quantity	Scale
			1:6.667
All Dimensions are in mm		Sheet no. - 7	





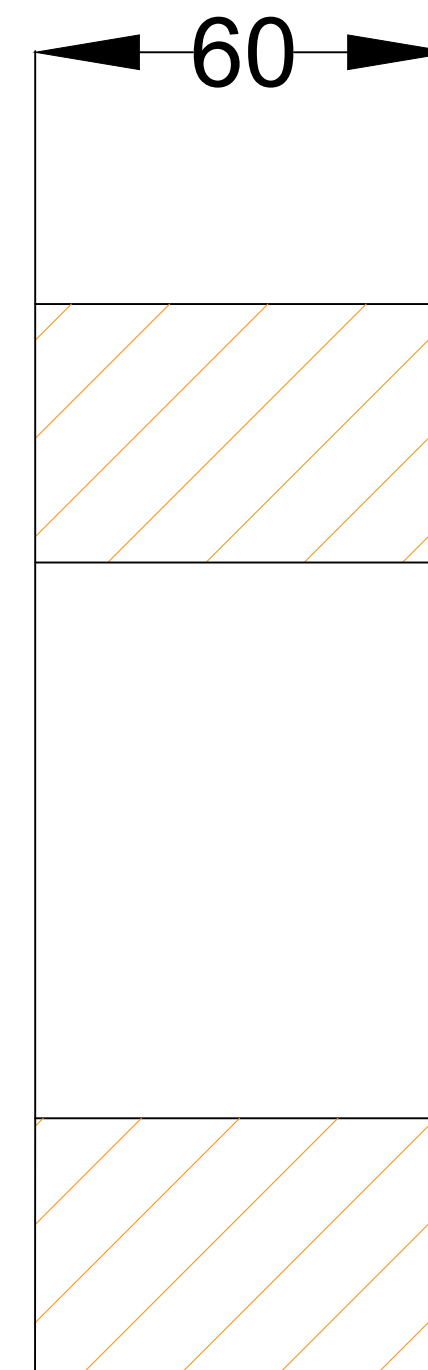
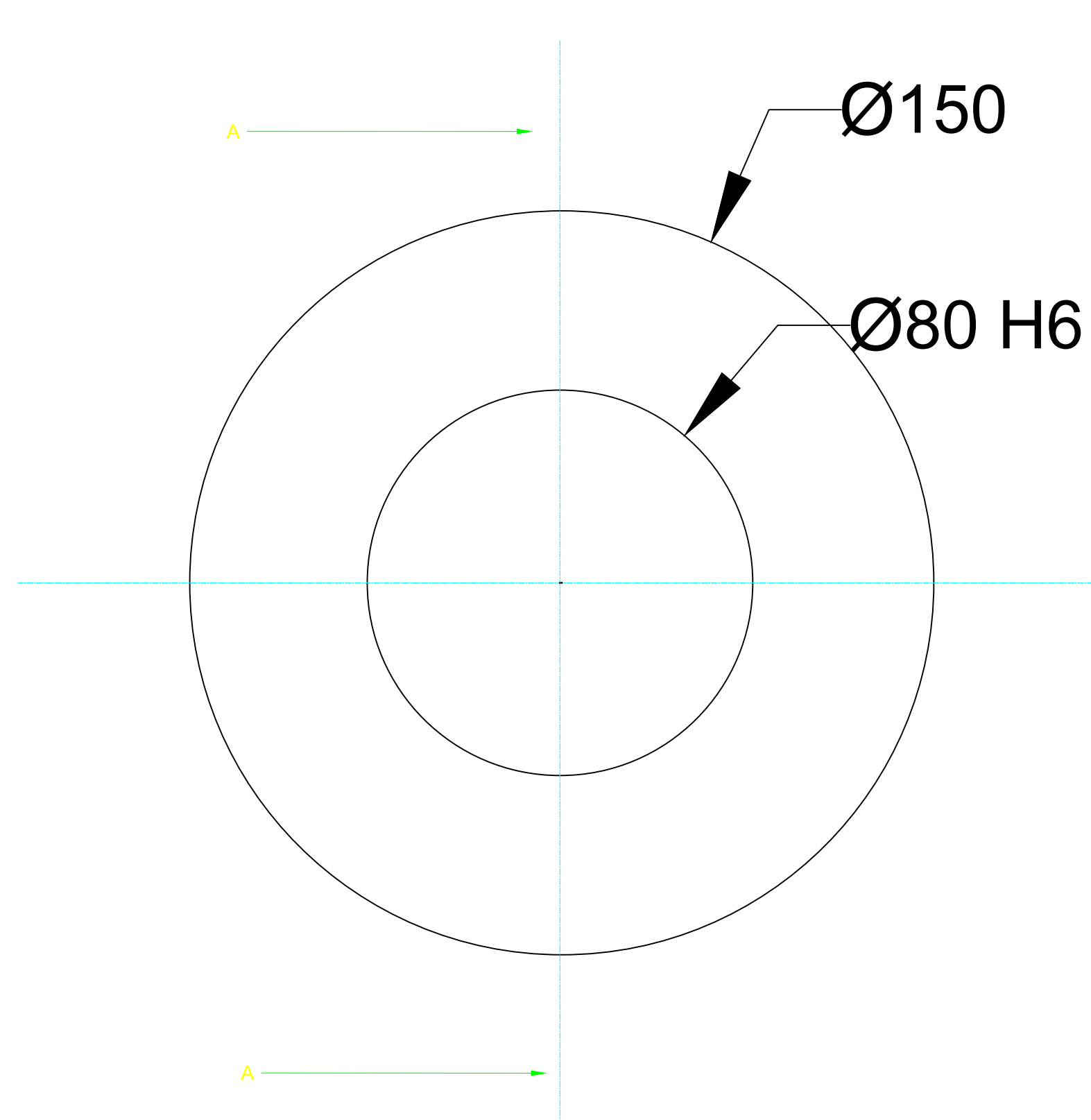
BHC003

Owner	MSD Group V8G		
Title of Sheet	Axle Cap		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 8	



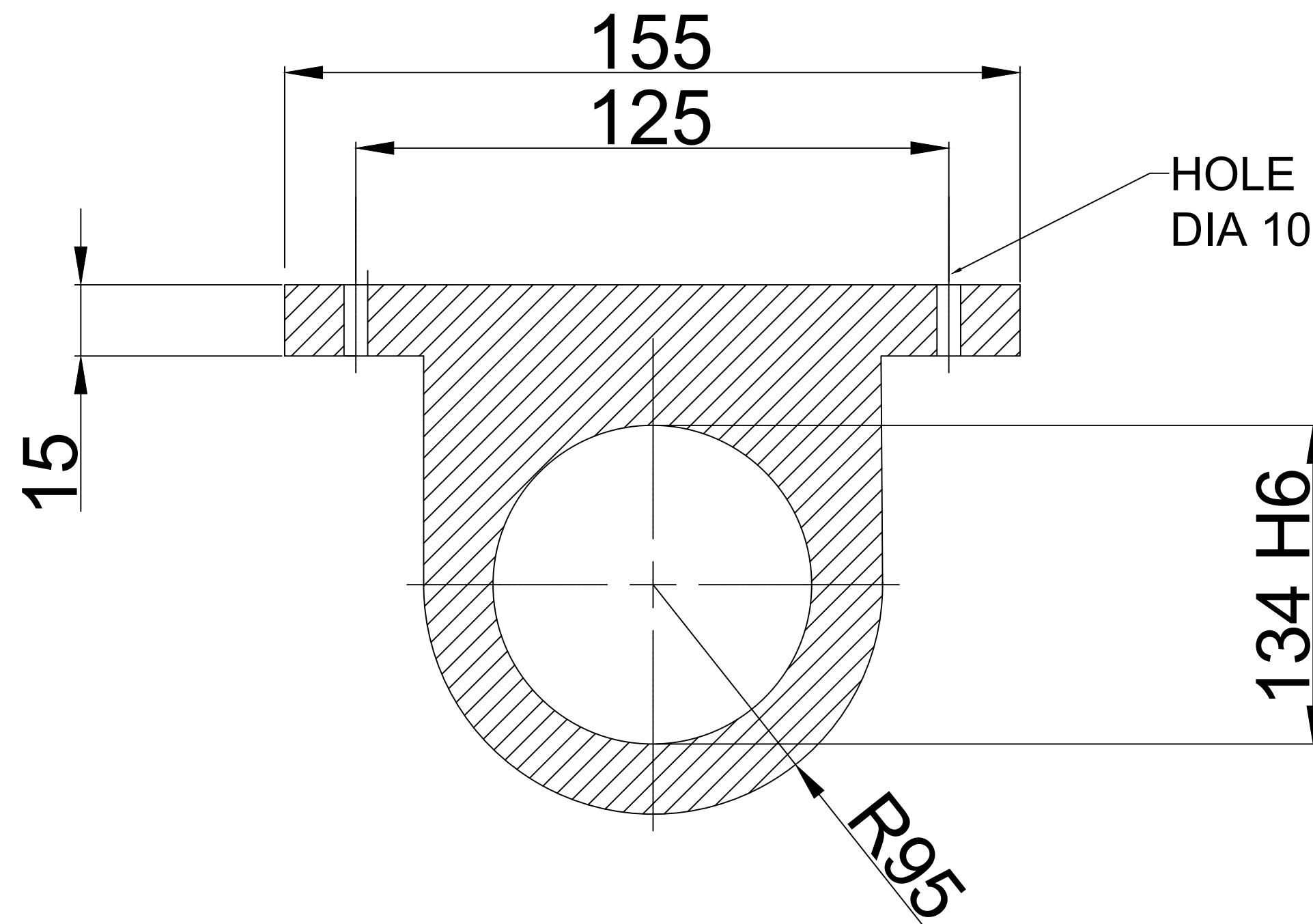
SHA001

Owner	MSD Group V8G		
Title of Sheet	Spring box		
		Quantity	Scale
			1:2
All Dimensions are in mm		Sheet no. - 9	



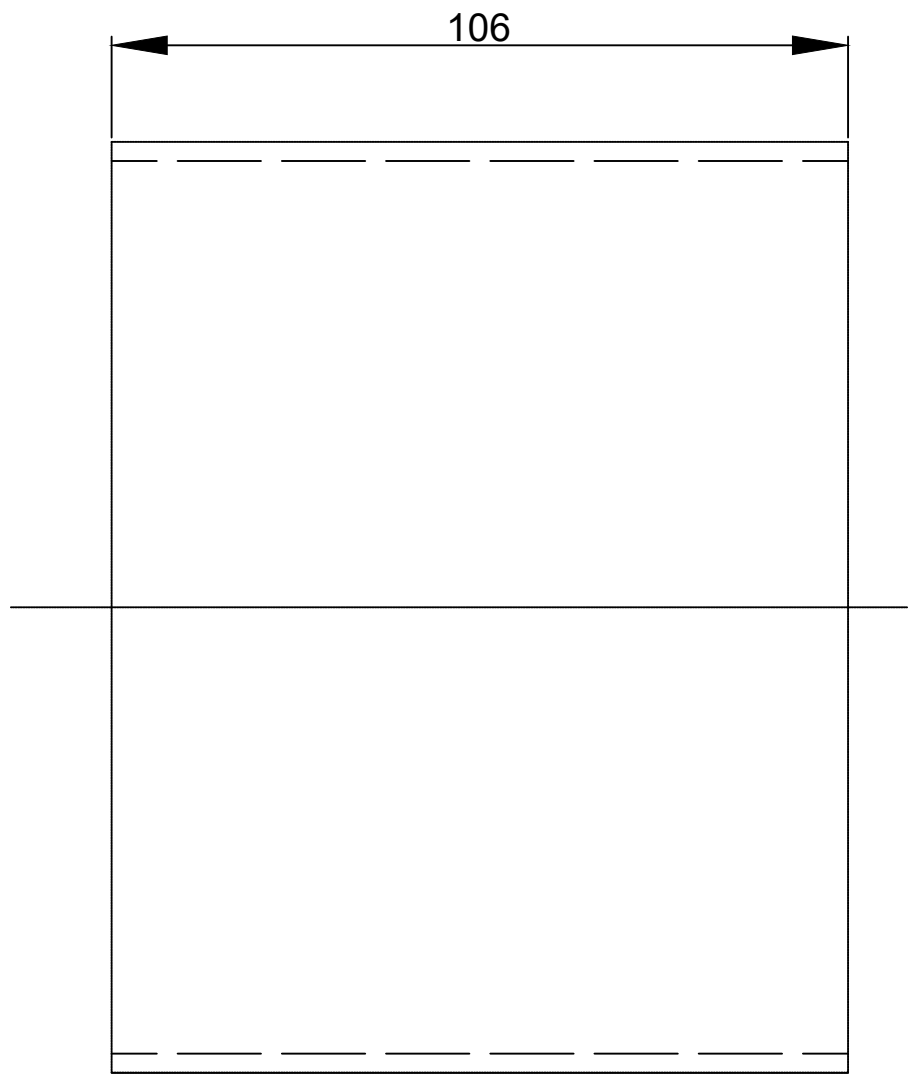
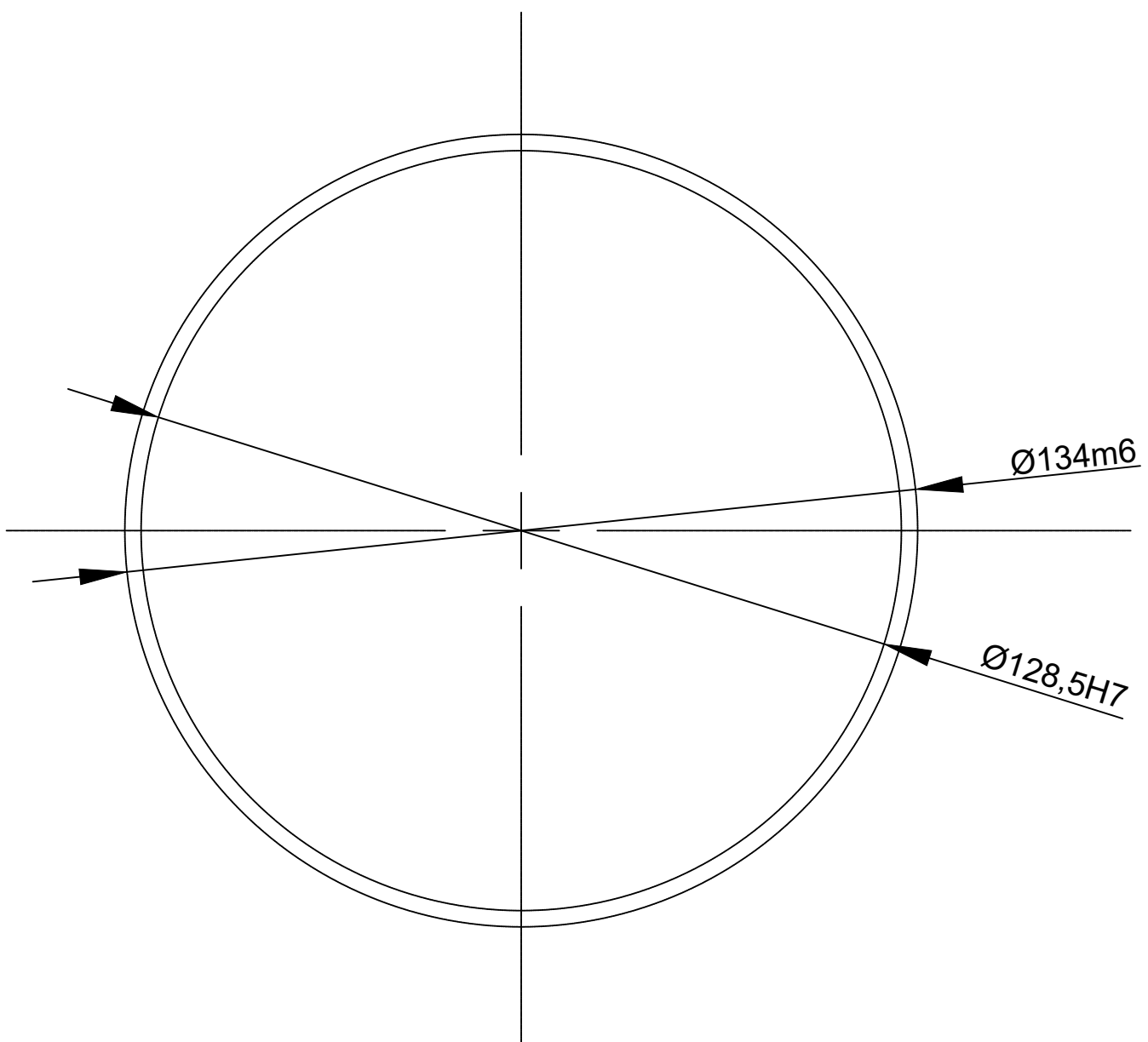
SHA009

Owner	MSD Group V8G		
Title of Sheet	Bar collar		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 10	



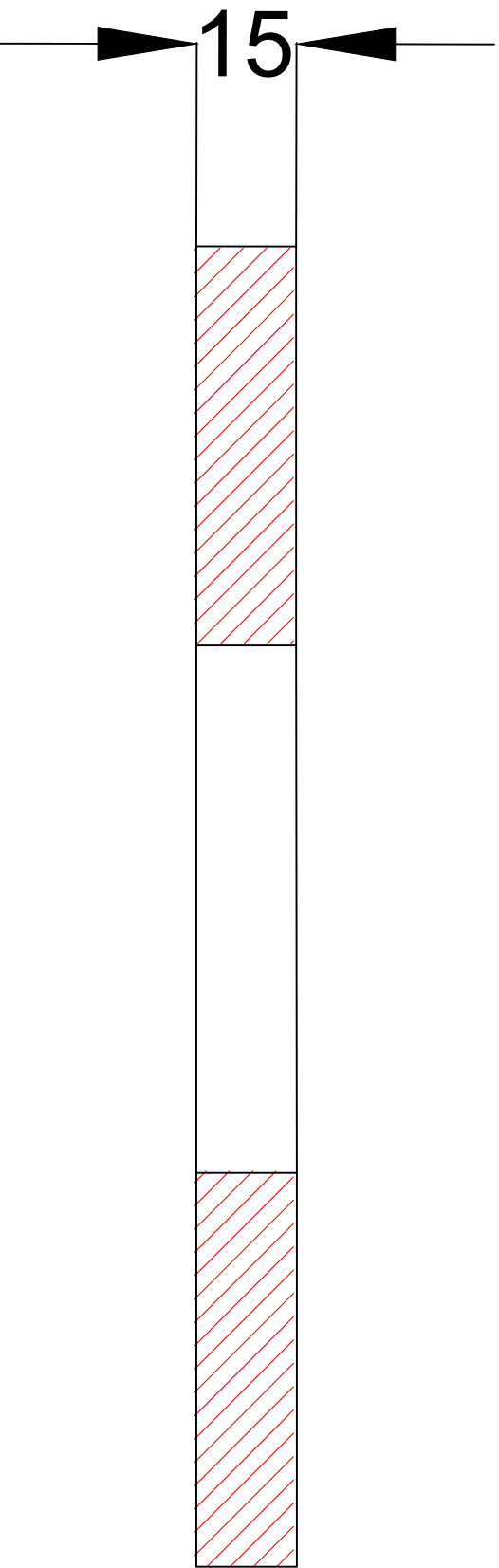
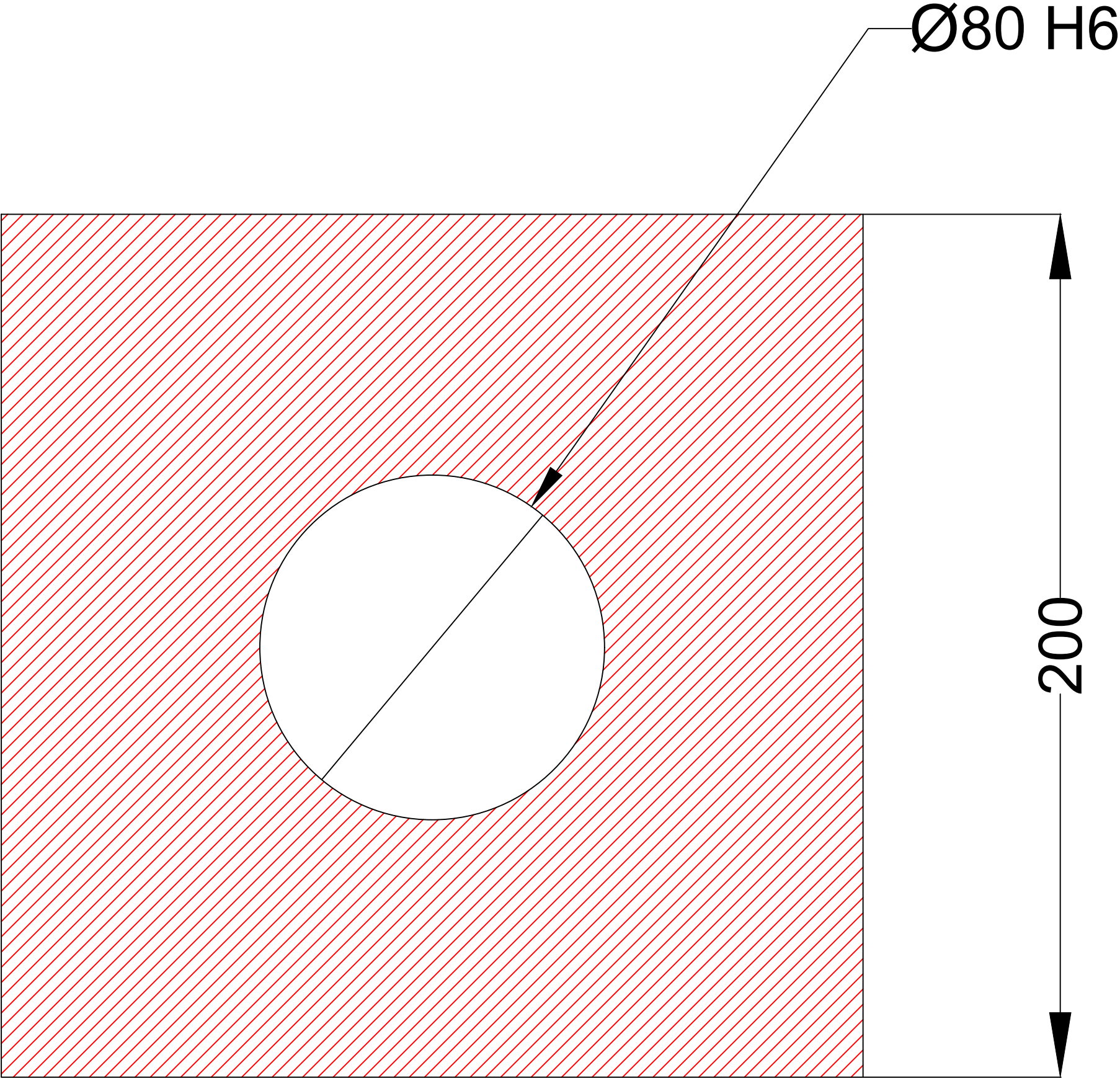
BHC002

Owner	MSD Group V8G		
Title of Sheet	Bush housing		
		Quantity	Scale
			1:2
All Dimensions are in mm		Sheet no. - 5	



BHC001

Owner	MSD Group V8G		
Title of Sheet	Bush		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 5	



SHA005

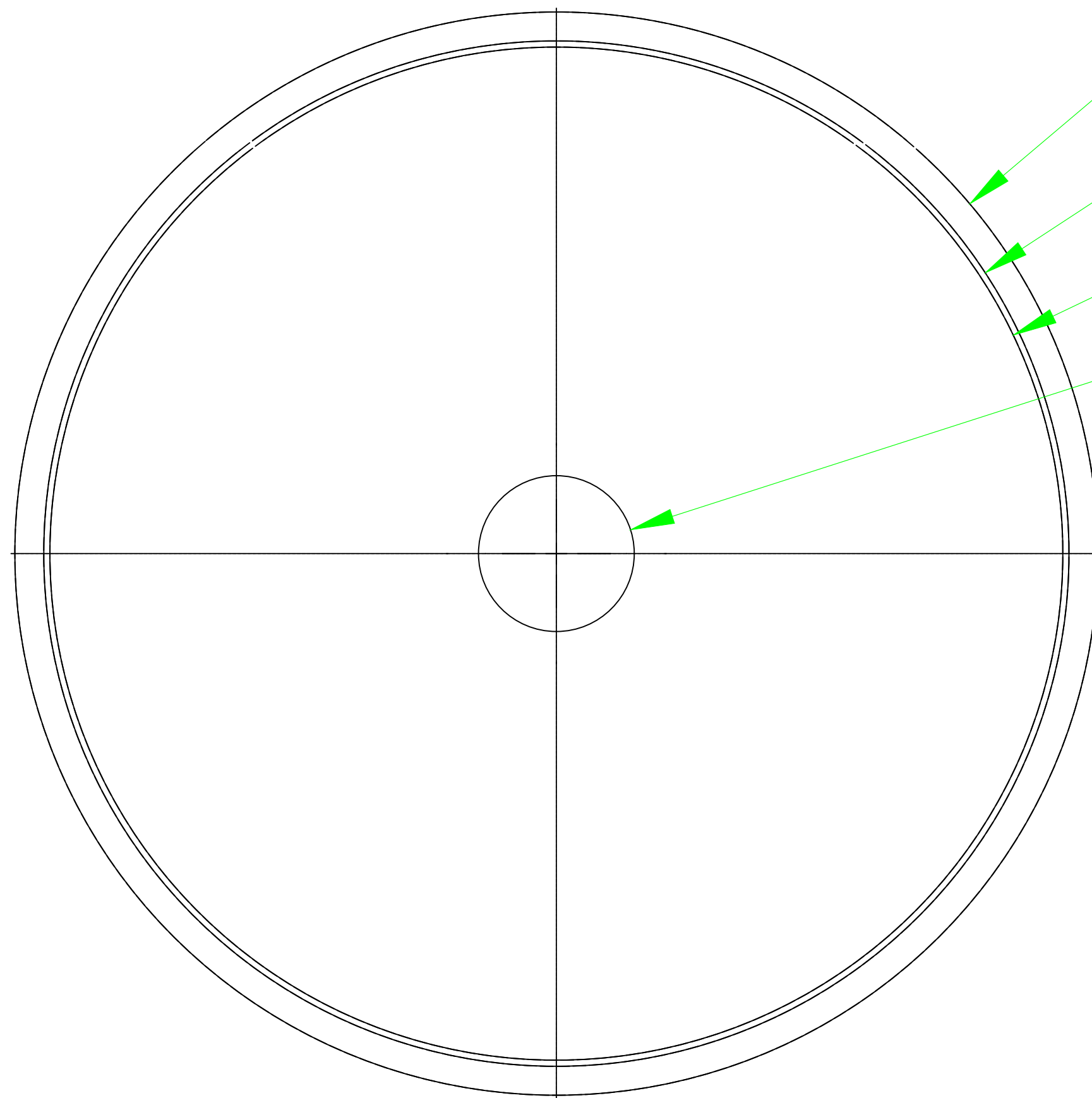
Owner	MSD Group V8G		
Title of Sheet	Collar		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 3	

8.2000

233.6000

CWA002

Owner	MSD Group V8G		
Title of Sheet	Lateral Beam of Chassis		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 5	



Ø1000

Ø934

Ø930

Ø178

R13

R16

120°

40

150

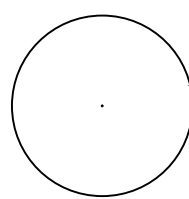
CWA004

Owner	MSD Group V8G		
Title of Sheet	Railway Wheel		
		Quantity	Scale
			1:4
All Dimensions are in mm		Sheet no. - 1	

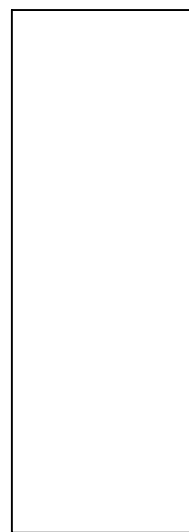


BSA0006

scale= 1:2

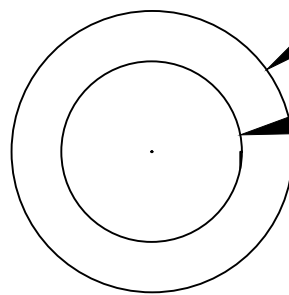


DIA 52 h6



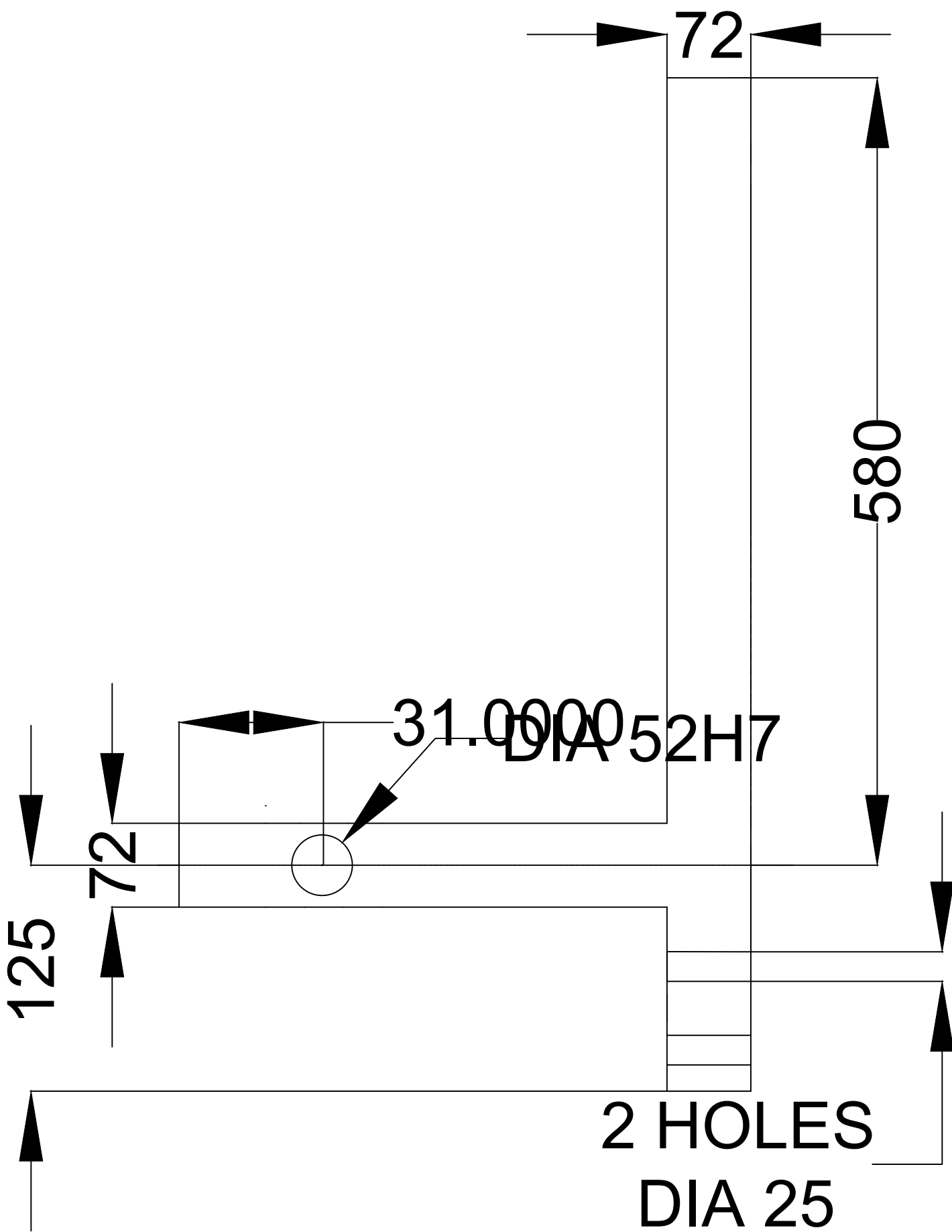
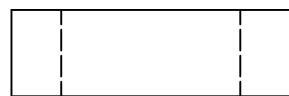
BSA0007

scale= 1:2



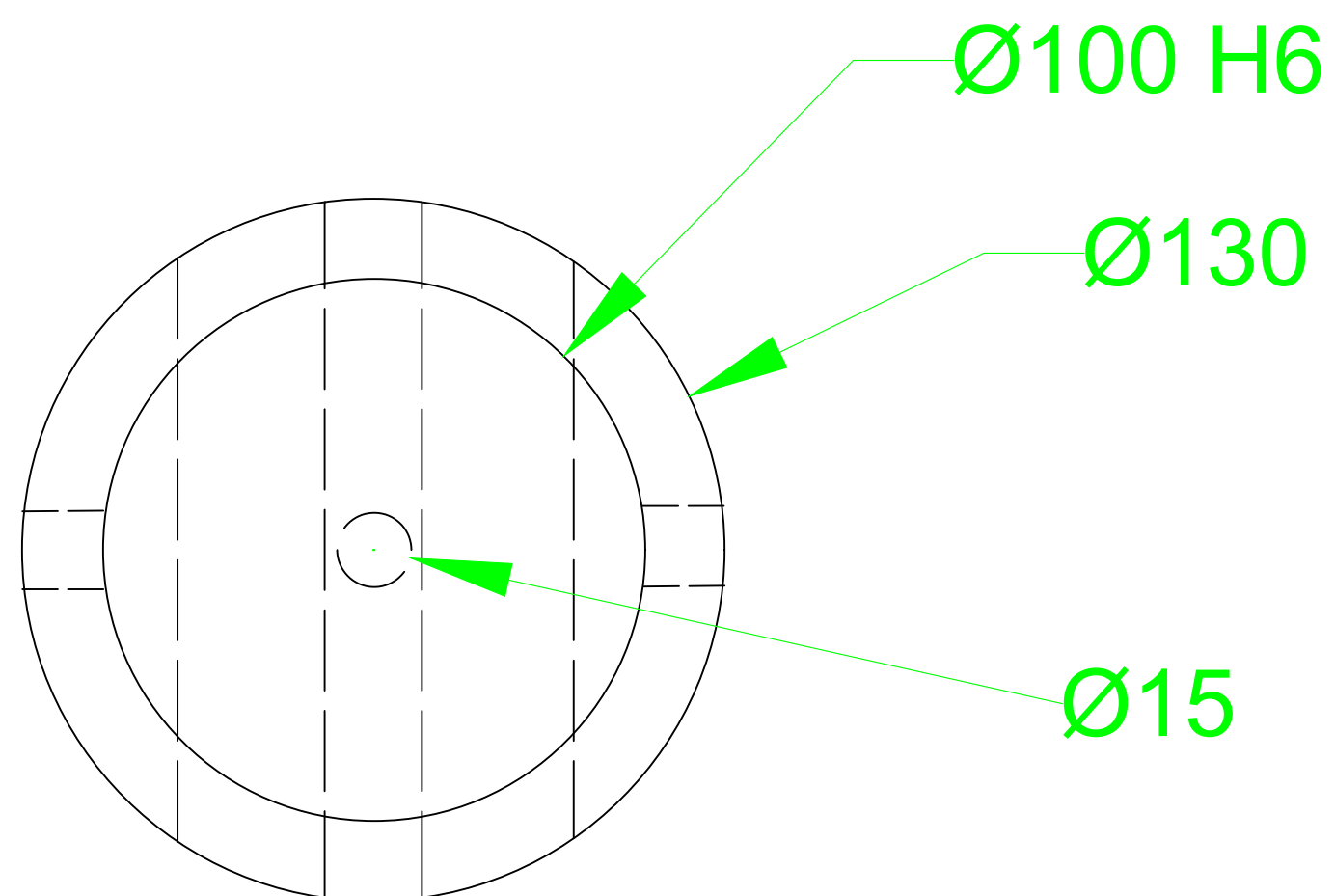
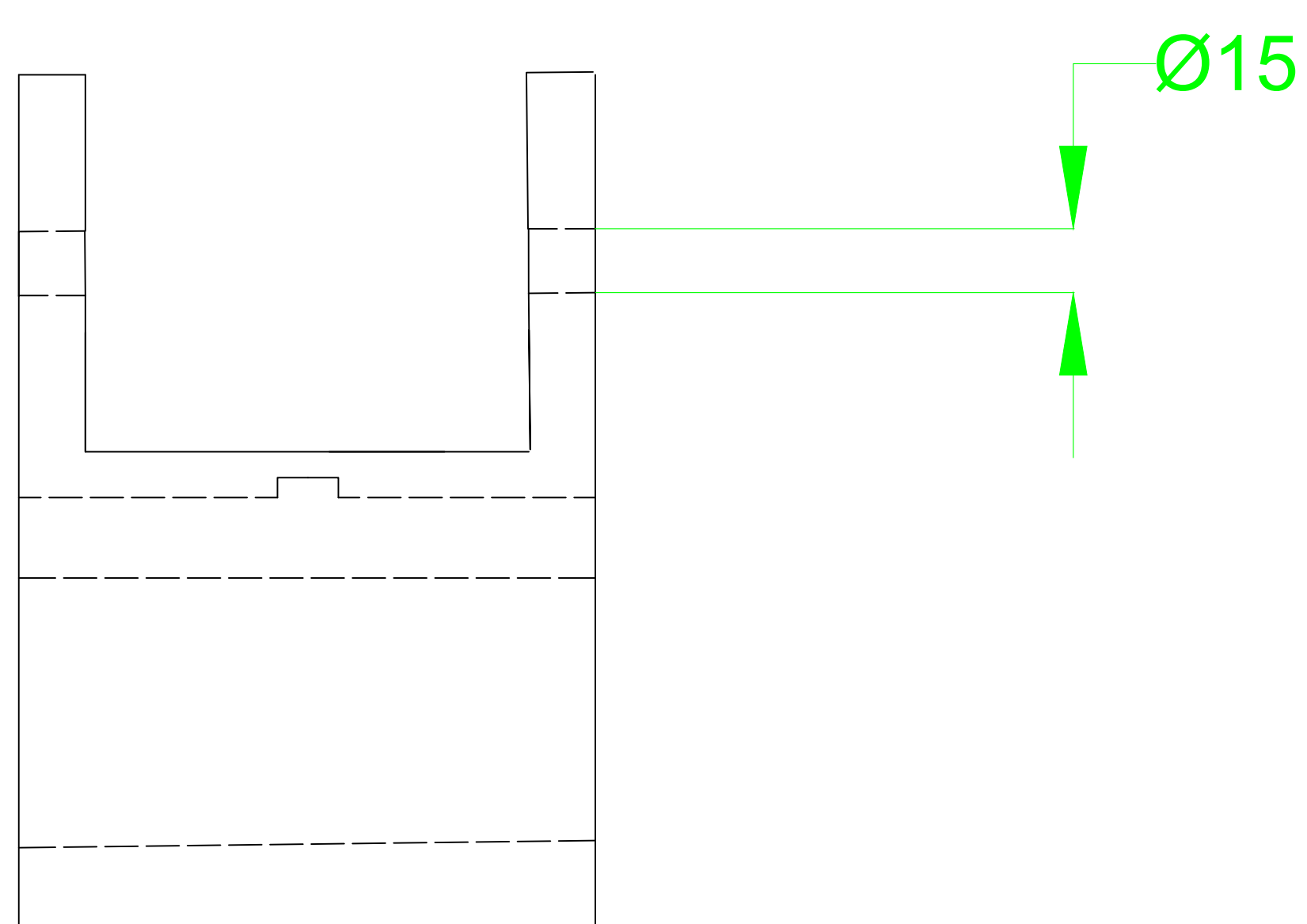
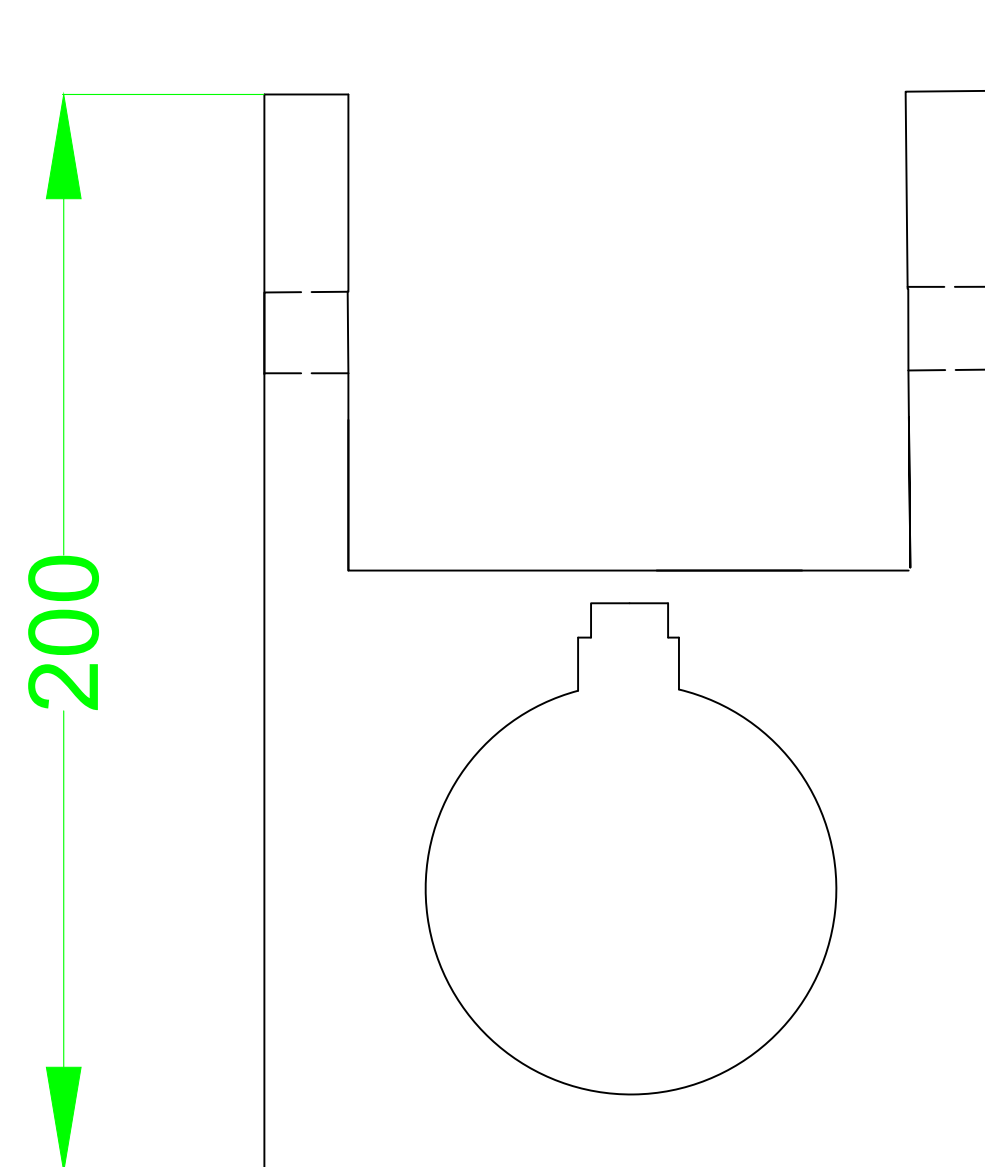
DIA 81

DIA 52 H7

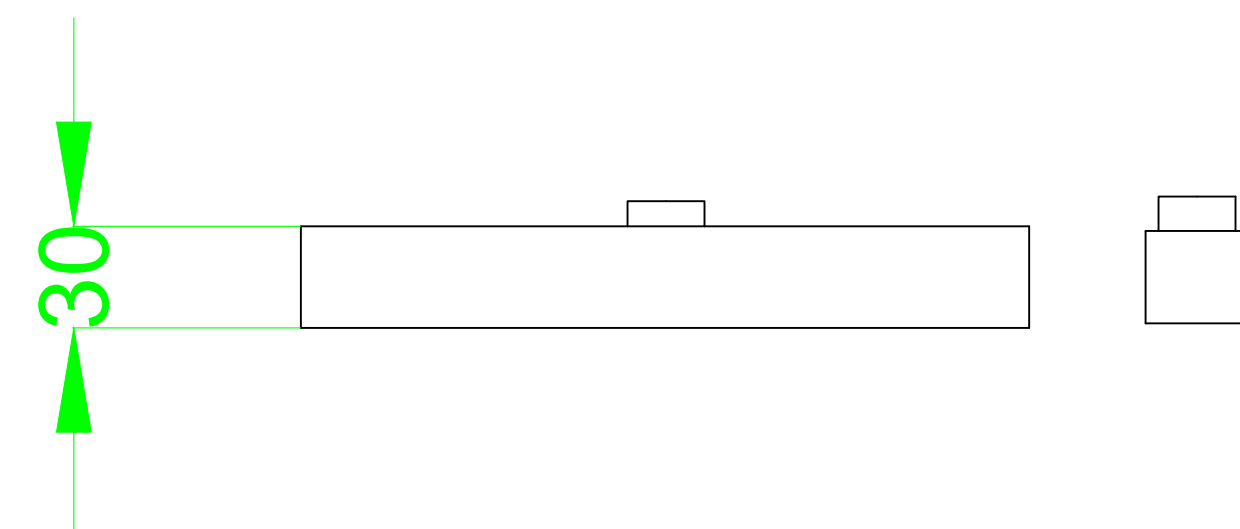


BSA0001

Owner	MSD Group V8G		
Title of Sheet	Brake Lever and pin		
		Quantity	Scale
			1:4
All Dimensions are in mm		Sheet no. - 4	



SHA008

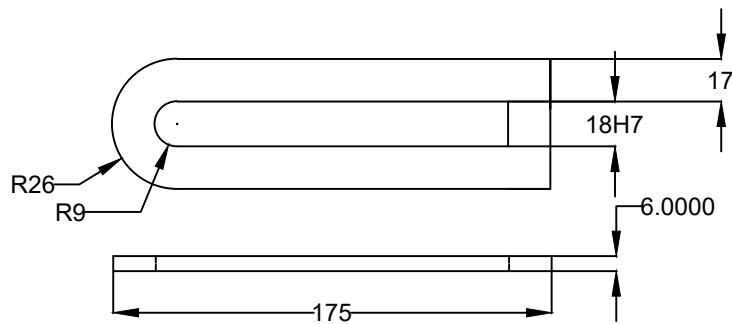
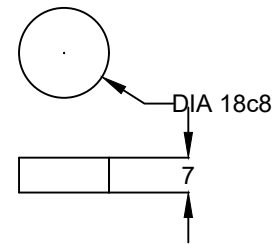


SHA010

Owner	MSD Group V8G		
Title of Sheet	Bar pocket		
	material	Quantity	Scale
			1:4
All Dimensions are in mm		Sheet no. - 2	

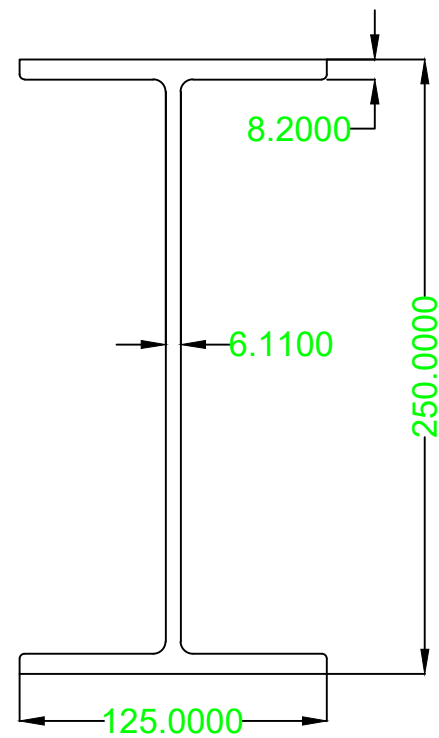
BSA003

scale= 2:1



BSA002

Owner	MSD Group V8G		
Title of Sheet	Slider and slider pin		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 4	

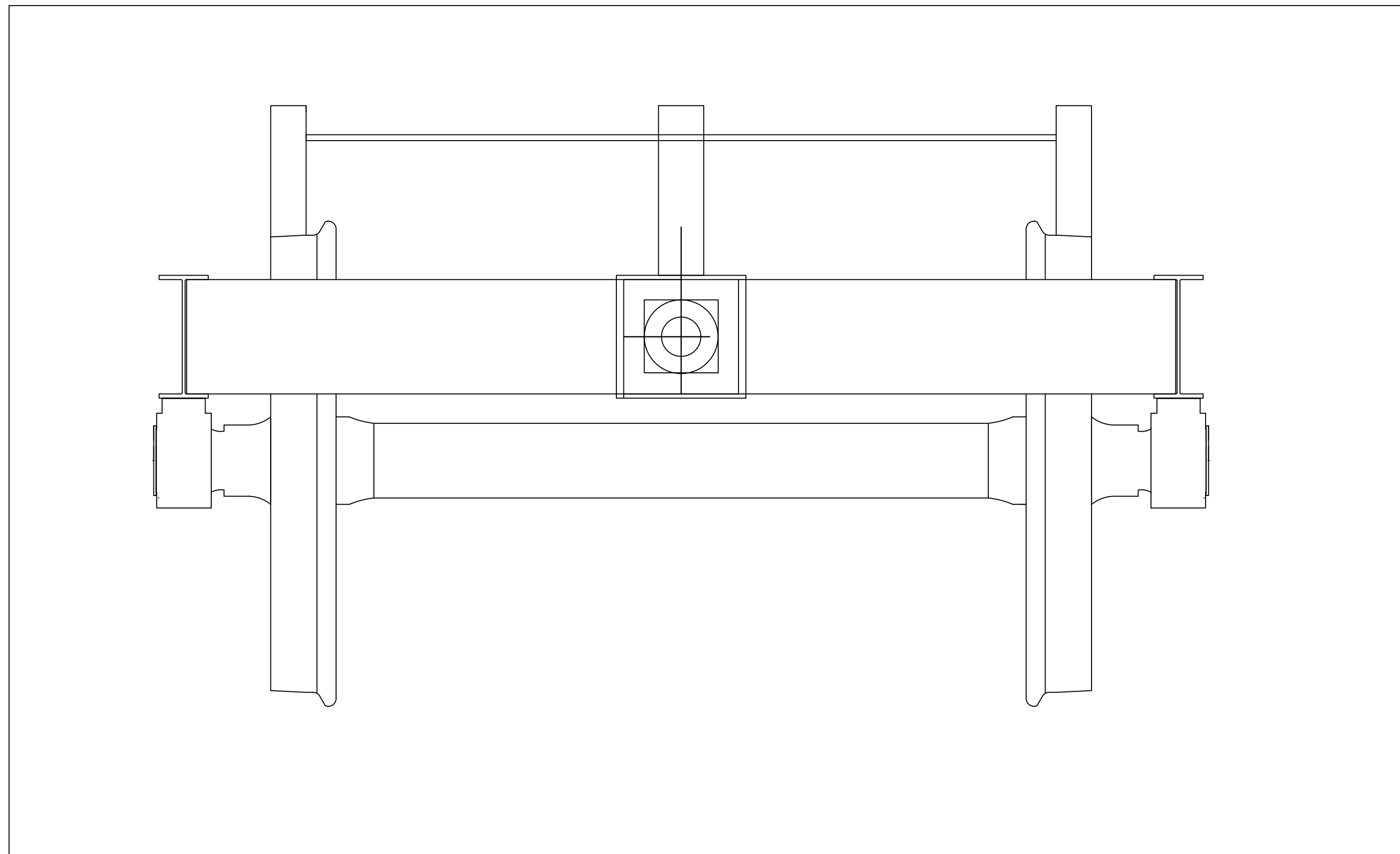


CWA001

Owner	MSD Group V8G		
Title of Sheet	Longitudinal Beam of Chassis		
		Quantity	Scale
			1:1
All Dimensions are in mm		Sheet no. - 4	

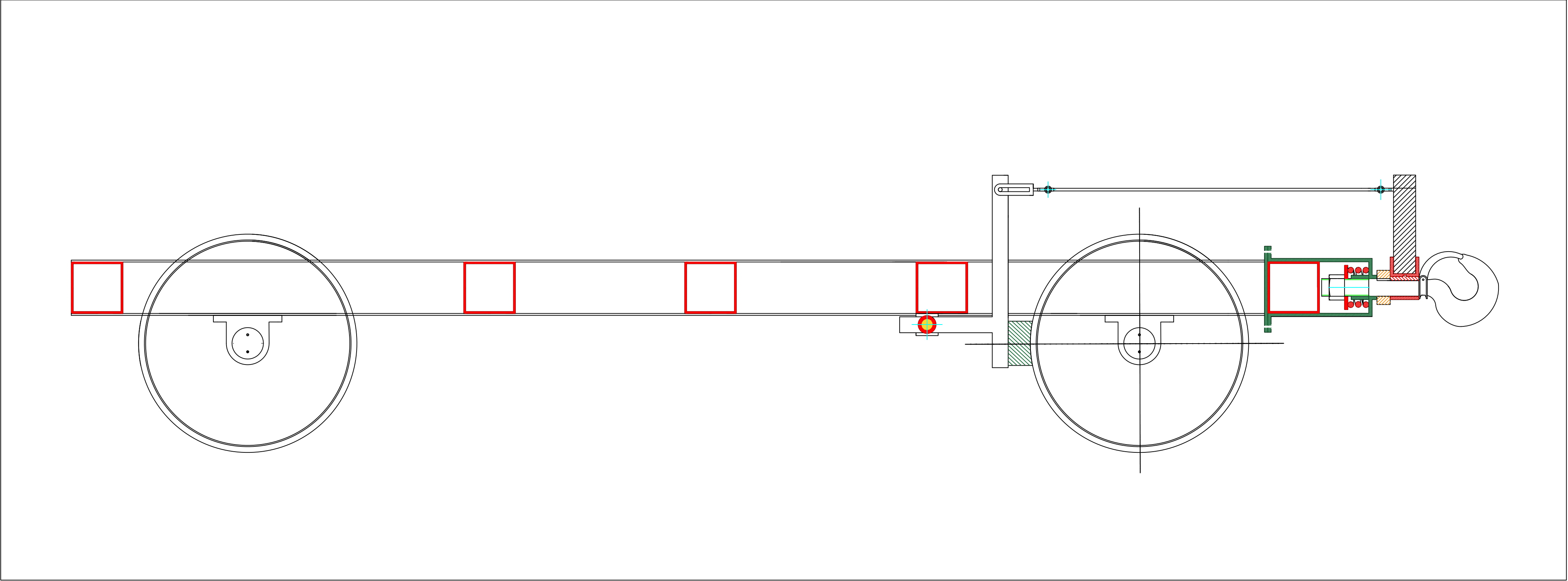
# Final Assembly

*Front View*



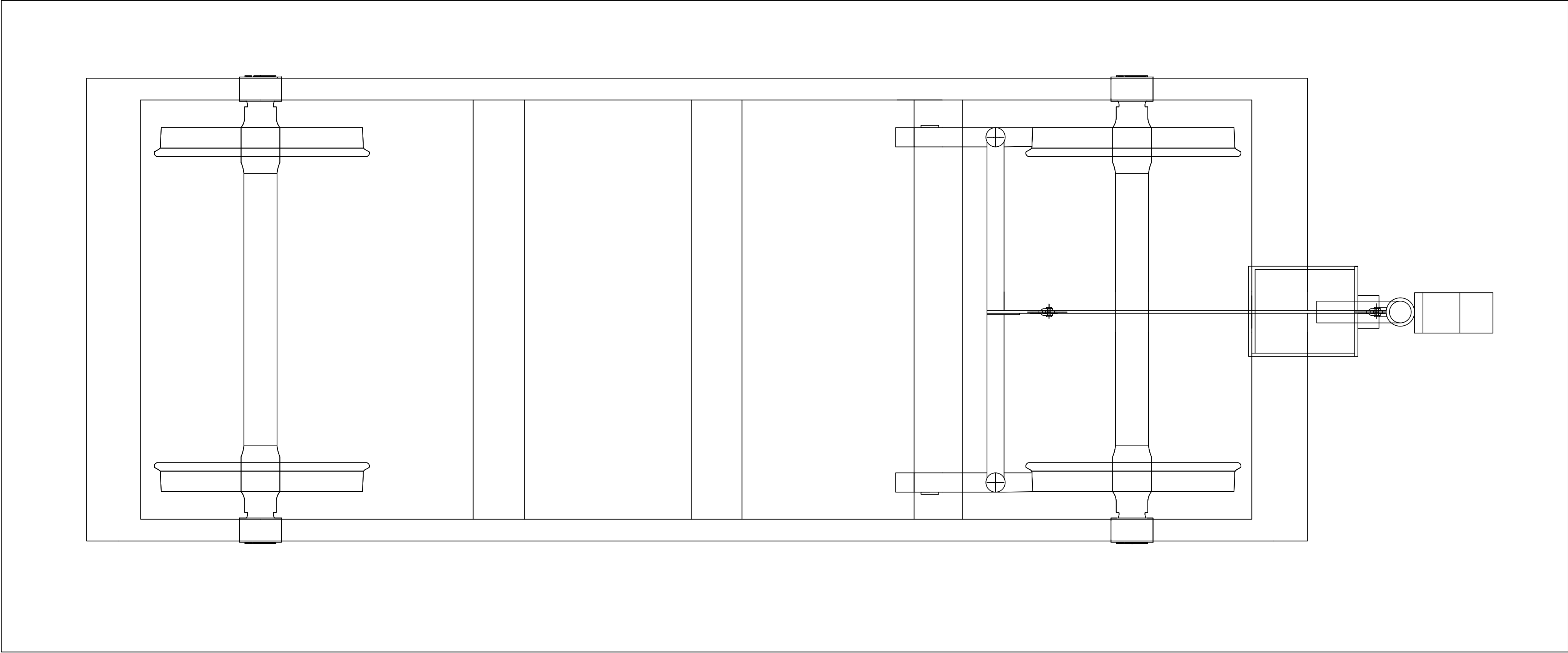
# Final Assembly

Side View



# Final Assembly

Top View



# Specifications of the Machine

**1. Overall Dimensions:**  $(6.45 \times 2.13 \times 1.22) \text{ m}^3$

**2. Power Requirement:** 2537.5 W

**3. Operational Specifications:**

- The cart maintains a velocity of 0.125 m/s
- The stopping distance is 1 m
- The cart is subjected to only linear motion