Section 16.7 Stokes' Theorem Recall that for a v.f. F = < M, N > on the plane we have div  $F = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} = \left( \frac{\text{measures compression}}{\text{or expansion at } (x, y)} \right)$ curl  $F = \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} = \left( \begin{array}{c} \text{measures counterclockwise} \\ \text{circulation at } (x, y) \end{array} \right)$ 

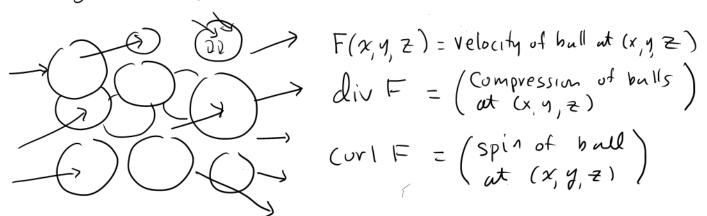
Now lets adapt all this to 3-D. Let F = < M, N, P > and think of it as representing the velocity of a fluid or gas flowing in space.

Divergence div F =  $\frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z} = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right) \cdot \left\langle M, N, P \right\rangle = \nabla \cdot F$ 

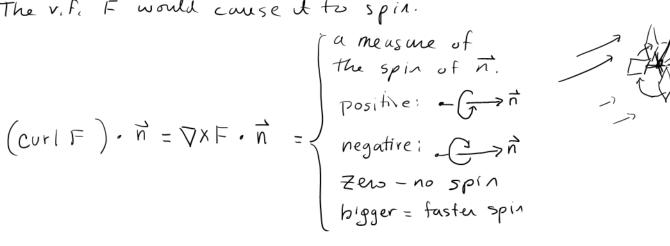
Curl Special notation 
$$\frac{\partial P}{\partial y} - \frac{\partial N}{\partial z} - \frac{\partial N}{\partial z} - \frac{\partial P}{\partial x}$$

$$|Curl F| = \left\langle \frac{\partial P}{\partial y} - \frac{\partial N}{\partial z}, \frac{\partial M}{\partial z} - \frac{\partial P}{\partial x}, \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right\rangle = \left\langle \frac{\partial}{\partial x} - \frac{\partial}{\partial y}, \frac{\partial}{\partial z} - \frac{\partial}{\partial z}, \frac{\partial}{\partial z}, \frac{\partial}{\partial z} - \frac{\partial}{\partial z}, \frac{$$

Imagine V.f. F moving little balls through space As they flow through space, they also may spin.



Given a unit vector in imagine that it has a little puddle wheel at its end. The v.f. F would cause it to spin.

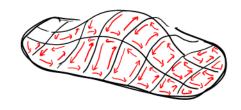


With all this in mind, we can state and understand the main result of this section - Stokes' Theorem.

Stoke's Theorem Suppose F = <M, N, P) is a vector field normal n'and boundary C, a curve r(t) traversel counterclockwise (looking down n). Then: Dr. St = Dr. Tr. Tr. do 7x F. n = > (curl F).7 i.e.  $\begin{pmatrix} \text{circulation} \\ \text{around } \end{pmatrix} = \int \left( \begin{pmatrix} \text{circulation at point} \\ (x, y, \bar{z}) \end{pmatrix} \right) ds$ - "flux of curl"

You can understand this intritively by dividing S up nuto small rectangles

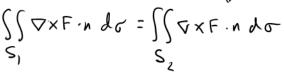
In SS VEIN DE = lim Z VFIN DOK



the contributions to circulation along adjacent rectangles cancel. The only contribution is along the boundary C; it is S F. dr.

Notice that the theorem implies that if surfaces S, and Sz share a common boundary, then becouse both sides equal & F. dr

For instance Suppose S, is top For instance of cone and Sz is side. Then



Notice also what happens if S is a flat surface on the xy-plane  $\Rightarrow \quad \begin{cases} F \cdot T ds = \iint \left( \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dA \end{cases}$ In this case, Stokes theorem reduces to Greens' Theorem. In other words, Stokes theorem is a generalization to Greens The. Example  $F(x,y,z) = \langle y, -x^2, 2z^2 \rangle$ S is the part of 4-x2-y2 above xy-plane Verify that Stokes theorem holds. Left hand side: Buse circle C g F. dr = g F. # # of rudius 2 13 boundary of S  $(\vec{r}_{(t)}) = \langle 2\cos t, 2\sin t, 0 \rangle$  $= \int_{-\infty}^{2\pi} \left(2 \sin t\right) - \left(2 \cos t\right)^{2}, \quad 20^{2} \right) \cdot \left(-2 \sin t\right) = 2 \cos t \cdot 0 dt \left(0 \le t \le 2\pi\right)$  $= \int_{0}^{2\pi} (-4\sin^{2}t - 8\cos^{3}t) dt = \int_{0}^{2\pi} (-4\cos(2t)) - 8\cos^{2}t \cos t dt$  $= \int_{-2}^{2\pi} -2(1-\cos 2t) - 8(1-\sin^2 t) \cos t \, dt$  \( \text{u} = \sin^2 t \)  $= \int_{1}^{2\pi} (-2 + \cos 2t - 8\cos t + 8(\sin t)\cos t) dt$  $= \left[ -2t + \frac{1}{2} \sin 2t - 8 \sin t + 8 \frac{\sin^3 t}{3} \right]^{2\pi}$ 

 $= \left(-4\pi + \frac{1}{2}\sin 4\pi - 8\sin 2\pi + 8\sin^3 2\pi\right) - \left(-20 + \frac{1}{2}\sin 0 - 8\sin 0 + 8\sin^3 6\right)$ 

Now let's compute the right-hand side. JJ VXF.n do. First,  $\nabla \times F = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ y & -x^2 & 2z^2 \end{vmatrix} = \langle 0, 0, -2x - 1 \rangle \Leftrightarrow \begin{cases} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \end{cases} = \langle 0, 0, -2x - 1 \rangle \Leftrightarrow \begin{cases} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \end{cases}$ Next, we parameterize the surface S as:  $T(u,v) = \left\langle u\cos v, u\sin v, 4 - (u\cos v)^2 - (u\sin v)^2 \right\rangle$   $0 \le u \le 2$ ,  $0 \le v \le 2\pi$   $= \left\langle u\cos v, u\sin v, 4 - u^2 \right\rangle$  $\vec{r}_{u} = \langle \cos v \sin v - 2u \rangle$ TV = <-usinv, ucosv, o >  $\vec{r}_{u} \times \vec{r}_{v} = \begin{vmatrix} \lambda & j & K \\ \cos v & \sin v & -zu \end{vmatrix} = \langle zu^{2} \cos v_{j} - zu^{2} \sin v_{j} & u \rangle$  $|\vec{r}_{u} \times \vec{r}_{v}| = \sqrt{(2u^{2}cosv)^{2} + (-2u^{2}sinv)^{2} + u^{2}} = \sqrt{4u^{4}cos^{2}v + 4u^{4}sin^{2}v + u^{2}}$  $= \sqrt{4u^4(\cos^2v + \sin^2v) + u^2} = \sqrt{4u^4 + u^2} = u\sqrt{4u^2 + 1} /$  $\frac{Now:}{S} = \int_{0}^{\sqrt{n}} \int_{0}^{2} \langle 0,0,-2x-1 \rangle \cdot \frac{\vec{r}_{u} \times \vec{r}_{v}}{|\vec{r}_{u} \times \vec{r}_{v}|} |r_{u} \times r_{v}| dudv$  $=\int\int \langle o_{j}o_{j}-zx-i\rangle\cdot (\vec{r}_{\alpha}\times\vec{r}_{\nu})d\mu d\chi$ = \( \int\_{\inle\int\_{\inlimtillet\int\_{\int\_{\int\_{\inle\inlicle\int\_{\int\_{\intit{\int\_{\intit{\inli\tink\tinnet\inlinle\inli\inli\tinn{\inli\inli\inli\tint\_{\inlint\_{\inlii}\inlinlinlint\_{\inlint\_{\inliinle\inlint\_{\inlinlint\_{\inlinlinlinlintilinlinlintille\inliinlinlinlinlint\_{\inlinlii}}}\inliin}\intititi  $= \int_{0}^{2\pi} \int_{0}^{2} \left(-2u^{2} \cos v - u\right) du dv = \int_{0}^{2\pi} \left[-\frac{2}{3}u^{3} \cos v - \frac{u^{2}}{2}\right]_{0}^{2} dv = \int_{0}^{2\pi} \left(-\frac{16}{3} \cos v - 2\right) dv$  $= \left[ -\frac{16}{3} \sin v - 2V \right]_{0}^{2\pi} = \left( -\frac{16}{3} \sin 2\pi - 2(2\pi) \right) - \left( -\frac{16}{3} \sin 0 - 2 \cdot 0 \right) = \left[ -\frac{16}{3} \sin 0 - 2 \cdot 0 \right] = \left[ -\frac{16}{3} \sin 0 - 2 \cdot 0$ Notice we could also integrate over the circular base & get the same answer: SS VXF. nd6 = SS (0,0,-2x-1). (0,0,1) dA (switch to)  $= \iint (-2x-1) dA = \iint (-2x\cos\theta - 1) r dr d\theta = \left[ -4\pi \right]$ 

Besides having many physical applications, Stokes theorem can also help evaluate a line- or surface-integral, if the other side is easier to do.