

SO<sub>2</sub> oxidation input data from Example 8-10, H. S. Fogler, "Elements of Chemical Reaction Engineering," 2nd ed., Prentice-Hall (1992):

The feed gas is 7900 lb-mol/h of 11% SO<sub>2</sub>, 10% O<sub>2</sub>, and 79% inert which is mostly N<sub>2</sub>. The simulation accounts for gas pressure drop down the adiabatic bed and the changing heat capacity of the gas as conversion changes.

$$-r_{SO_2} = k \sqrt{\frac{P_{SO_2}}{P_{SO_3}}} \left[ P_{O_2} - \left( \frac{P_{SO_3}}{K_P P_{SO_2}} \right)^2 \right]$$

$$k = \exp \left[ \frac{-176008}{T} - 110.1 \ln(T) + 912.8 \right]$$

$$K_P = \exp \left[ \frac{42311}{RT} - 11.24 \right]$$

where  $k$  has units (lb-mol SO<sub>2</sub>/lb-catalyst/s/atm),  $K_P$  has units (atm<sup>-1/2</sup>), and  $T$  has units (°R). This rate can be used above a conversion of SO<sub>2</sub> of 5% and larger. Below that conversion, assume the rate is equal to the rate at 5% conversion.

$$\Delta H_R(800^\circ \text{F}) = -42471 \text{ Btu/lb-mol-SO}_2$$

diameter of spherical catalyst pellets = 0.015 ft

bed void fraction = 0.45

bulk density of catalyst bed = 33.8 lb/ft<sup>3</sup>