



# Week 3: Wheeled Kinematics

## AMR - Autonomous Mobile Robots

**Paul Furgale**

Margarita Chli, Marco Hutter, Martin Rufli, Davide Scaramuzza, Roland Siegwart

# AMRx Flipped Classroom

- A Matlab exercise is coming later in the class. Download it now!
  - <http://tinyurl.com/amrx-wheels>

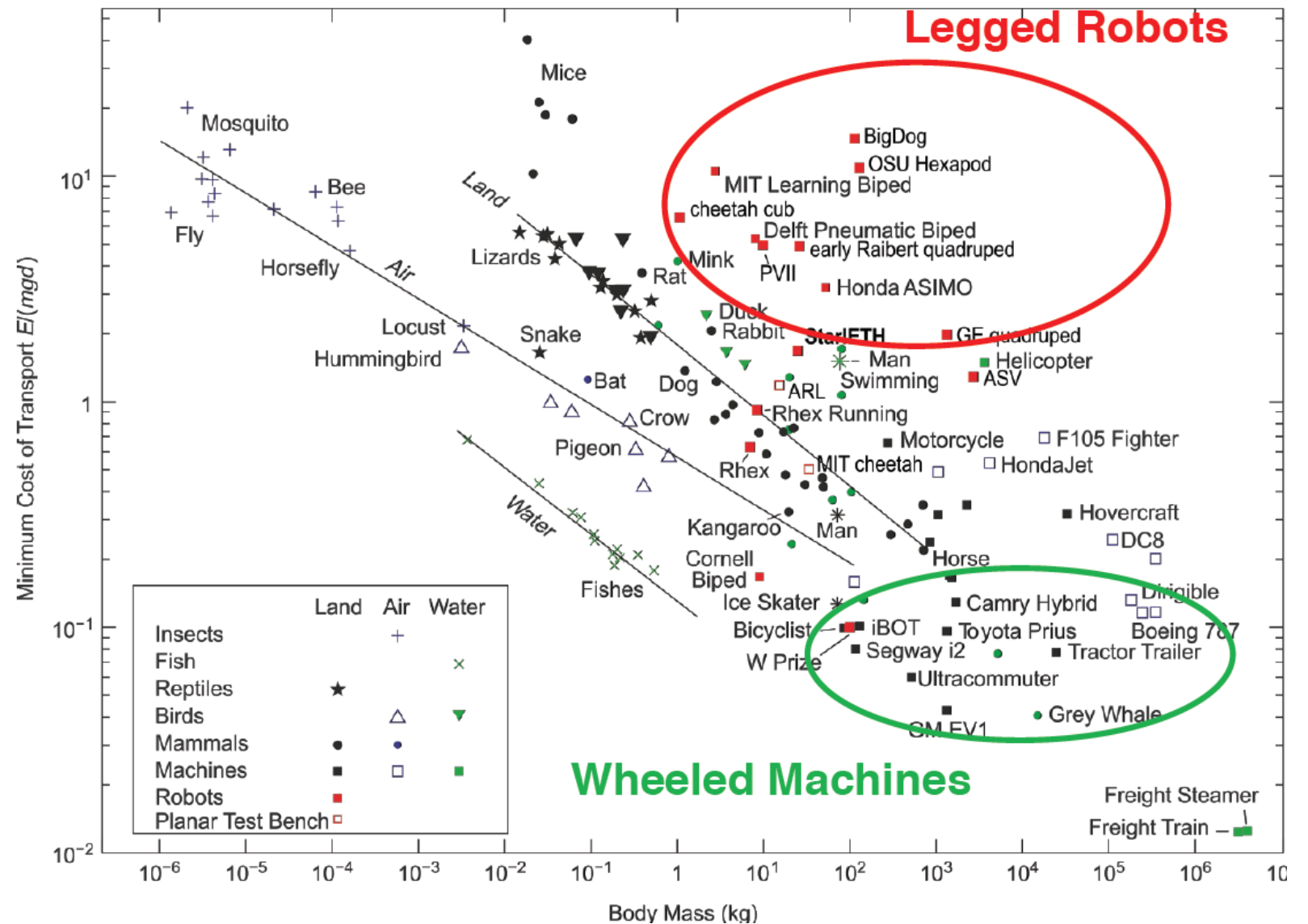
# AMRx

## A review

- Please register in at [edx.org](https://edx.org) and watch the lecture segments
- Please try the problem sets online (they don't count for your grade but they are useful)
- Bring your laptop along for the lectures
  - We may provide short examples or problems for you to work out
  - We may ask for feedback on the worked exercises
- Flipped Classroom
  - You ask us, we try to help
  - No recording of the lecture, no questions are stupid
  - Feel free to interrupt

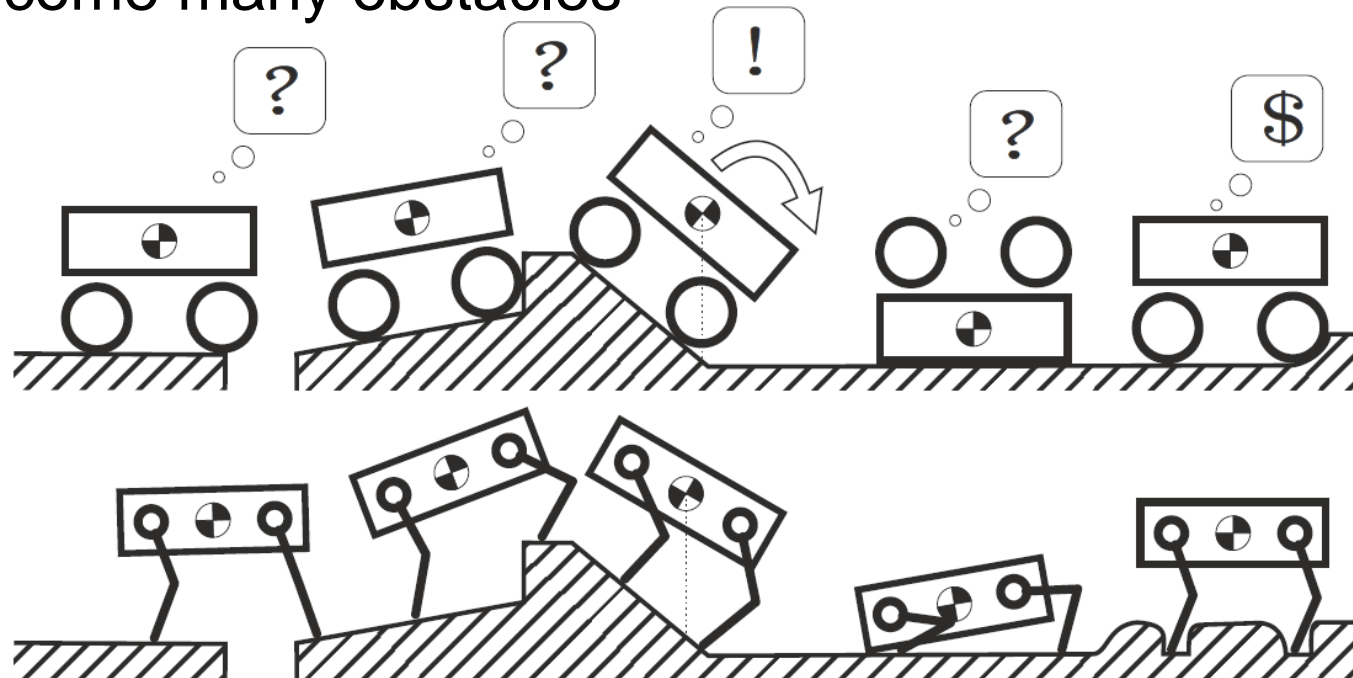
# Why Wheeled Robots?

- + Requires small control action (in comparison to legs)
- + Energetically very efficient



# Why Wheeled Robots?

- + Requires small control action
- + Energetically very efficient
- Unable to overcome many obstacles



# AMRx

## Today's lecture

- Teacher: Paul Furgale, Deputy Director @ ASL



- Review
- Practical problems:
  - Intuition about matrices
  - Computing good steering angles
  - Computing wheel odometry

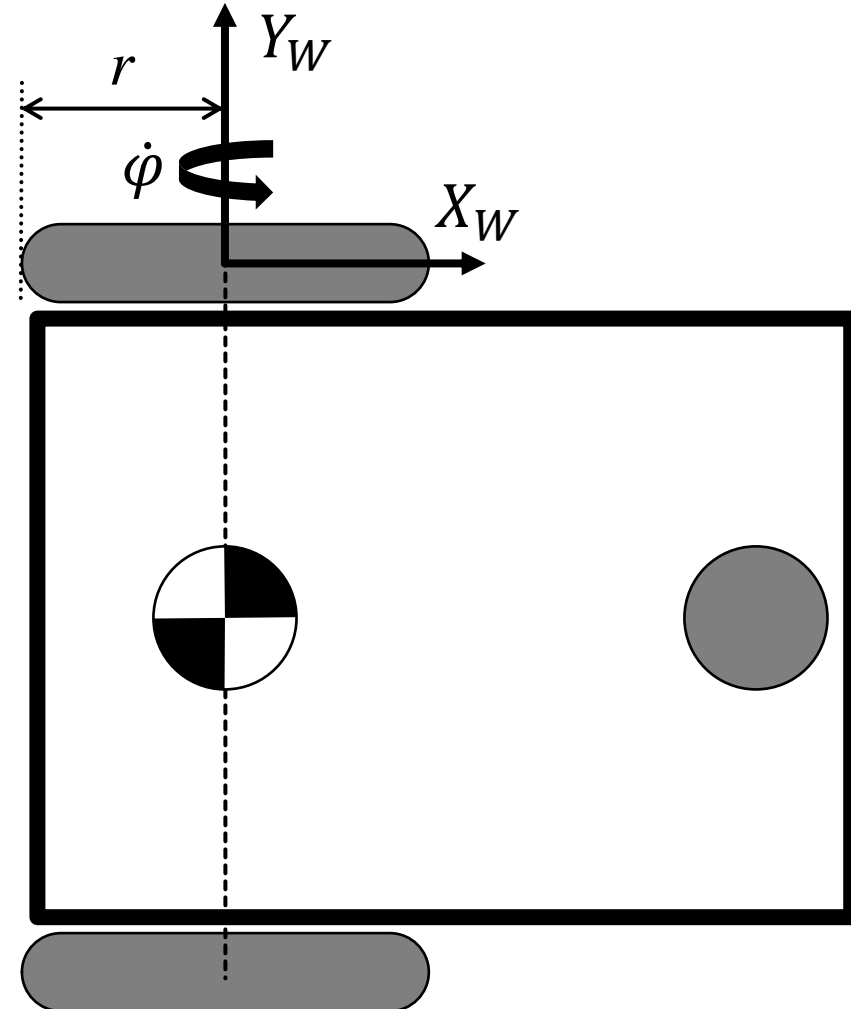
# Wheeled Kinematics

- Not all degrees of freedom of a wheel can be actuated or have encoders
- Wheels can impose **differential constraints** that complicate the computation of kinematics

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} \dot{\phi} r \\ 0 \end{bmatrix}$$

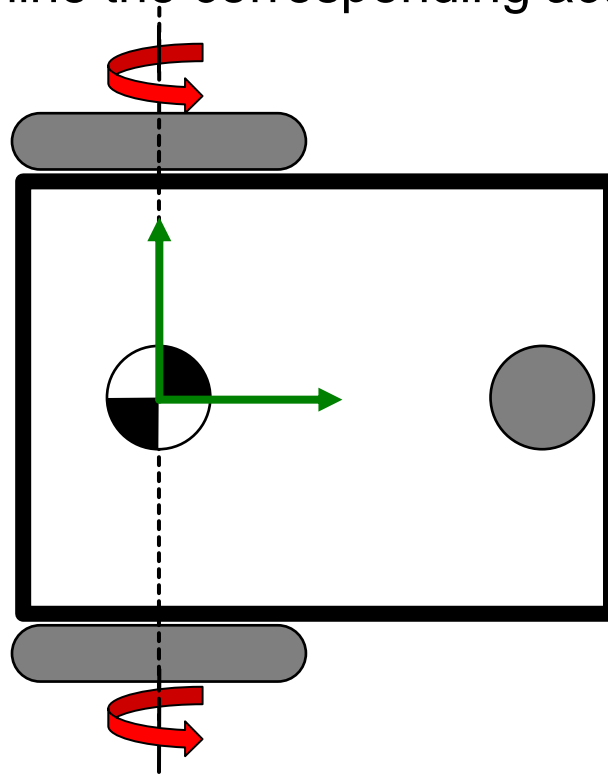
rolling constraint

no-sliding constraint



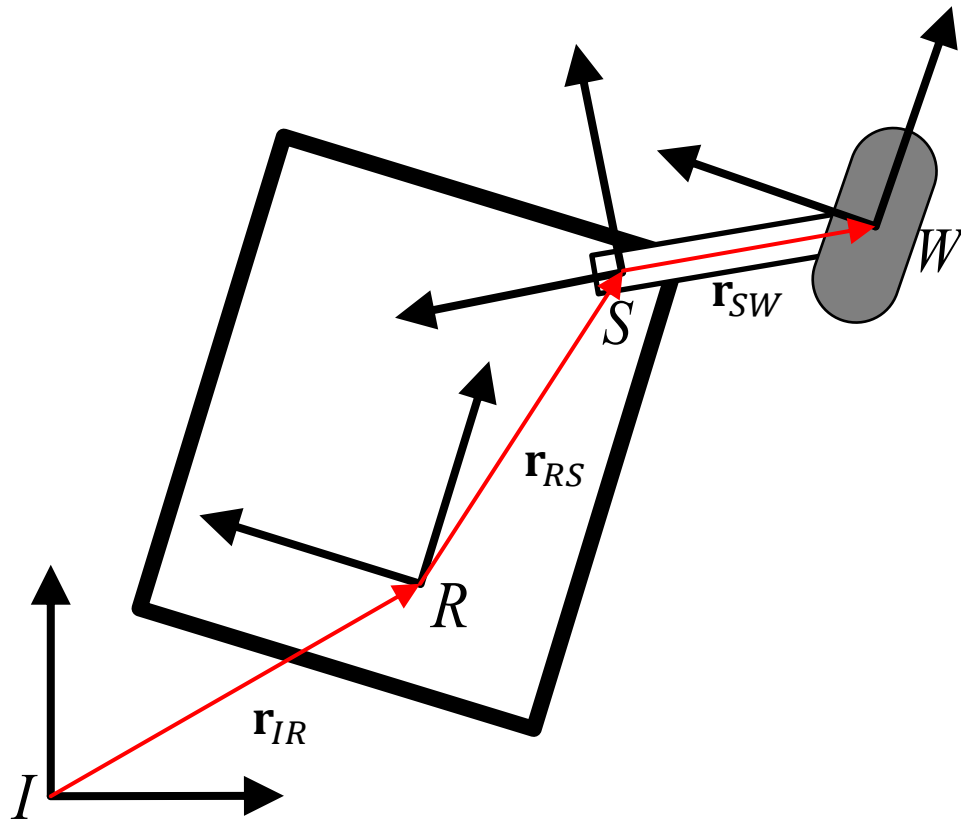
# Differential Kinematics

- Differential forward kinematics
  - Given a set of actuator speeds, determine the corresponding velocity
- **Differential inverse kinematics**
  - Given a desired velocity, determine the corresponding actuator speeds





# Deriving a general wheel equation



$$\mathbf{v}_{IW} = \mathbf{v}_{IR} + \omega_{IR} \times \mathbf{r}_{RS} + \omega_{IR} \times \mathbf{r}_{SW} + \omega_{RS} \times \mathbf{r}_{SW}$$

robot angular velocity

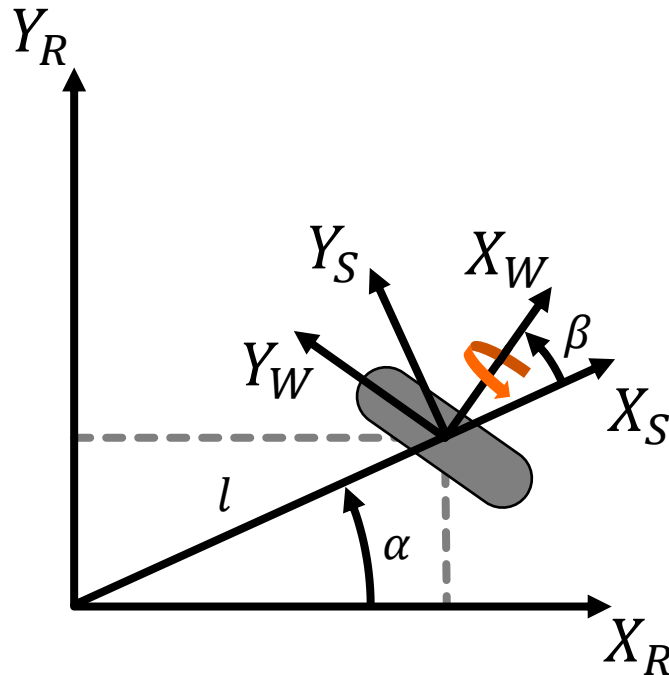
steering rate

robot velocity

steering offset

wheel offset

# Example: Standard wheel



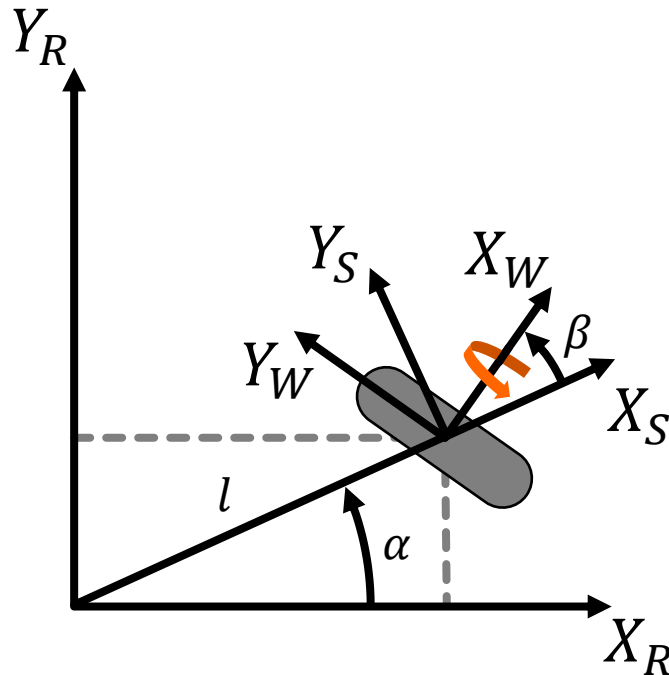
- Rolling constraint

$$[\sin \alpha + \beta \quad -\cos \alpha + \beta \quad -l \cos \beta] R(\theta) \dot{\xi}_I - \dot{\phi} r = 0$$

- No-sliding constraint

$$[\cos \alpha + \beta \quad \sin \alpha + \beta \quad l \sin \beta] R(\theta) \dot{\xi}_I = 0$$

# Example: Standard wheel



- This equation had a mistake in the online lecture. The slides have been updated and we will update the video soon
- No-sliding constraint

$$[\cos \alpha + \beta \quad \sin \alpha + \beta \quad l \sin \beta] R(\theta) \dot{\xi}_I = 0$$

# Differential Kinematics

- Given a wheeled robot, each wheel imposes  $n$  constraints
- Only fixed and steerable standard wheels impose no-sliding constraints
- Suppose a robot has  $n$  wheels of radius  $r_i$ , the individual wheel constraints can be concatenated in matrix form:
  - Rolling constraints

$$J_1(\beta_S)R(\theta)\dot{\xi}_I - J_2\dot{\phi} = 0, \quad J_1(\beta_S) = \begin{bmatrix} J_{1f} \\ J_{1s}(\beta_S) \end{bmatrix}, \quad J_2 = \text{diag}(r_1, \dots, r_N), \quad \dot{\phi} = \begin{bmatrix} \dot{\phi}_1 \\ \vdots \\ \dot{\phi}_N \end{bmatrix}$$

- No-sliding constraints

$$C_1(\beta_S)R(\theta)\dot{\xi}_I = 0, \quad C_1(\beta_S) = \begin{bmatrix} C_{1f} \\ C_{1s}(\beta_S) \end{bmatrix}$$

# Differential Kinematics

- Stacking the rolling and no-sliding constraints gives an expression for the differential kinematics

$$\begin{bmatrix} J_1(\beta_s) \\ C_1(\beta_s) \end{bmatrix} R(\theta) \dot{\xi}_I = \begin{bmatrix} J_2 \\ 0 \end{bmatrix} \dot{\phi}$$

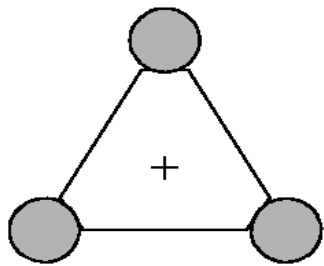
- Solving this equation for  $\dot{\xi}_I$  yields the **forward differential kinematics** equation needed for computing wheel odometry
- Solving this equation for  $\dot{\phi}$  yields the **inverse differential kinematics** equation needed for control

# Degree of Maneuverability

- The Degree of Maneuverability,  $\delta_M$ , combines mobility and steerability

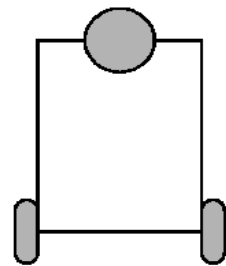
$$\delta_M = \delta_m + \delta_s$$

- Examples



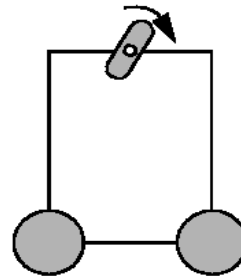
*Omnidirectional*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 3 \\ \delta_s &= 0\end{aligned}$$



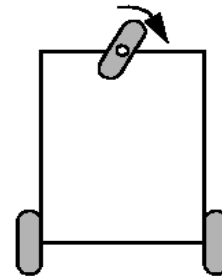
*Differential*

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 2 \\ \delta_s &= 0\end{aligned}$$



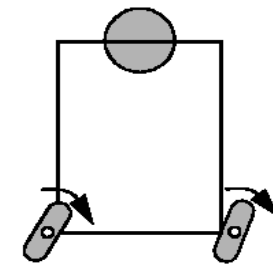
*Omni-Steer*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 2 \\ \delta_s &= 1\end{aligned}$$



*Tricycle*

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 1 \\ \delta_s &= 1\end{aligned}$$

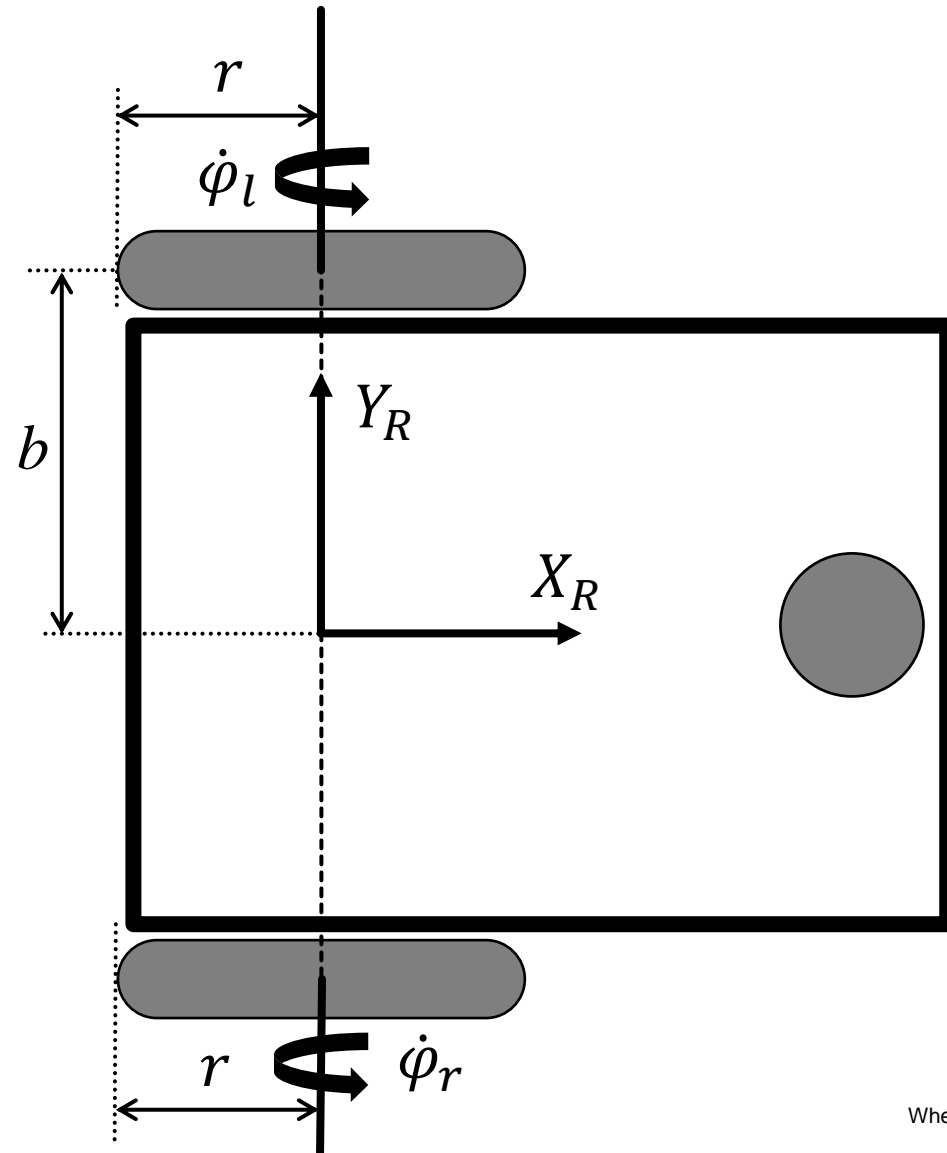


*Two-Steer*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 1 \\ \delta_s &= 2\end{aligned}$$

# Worked Exercise | A Differential Drive Robot

- Two fixed standard wheels
- The robot frame (R) in between the wheels
- Stack the wheel equations for this configuration



# A Differential Drive Robot | Summary

- Degree of Maneuverability

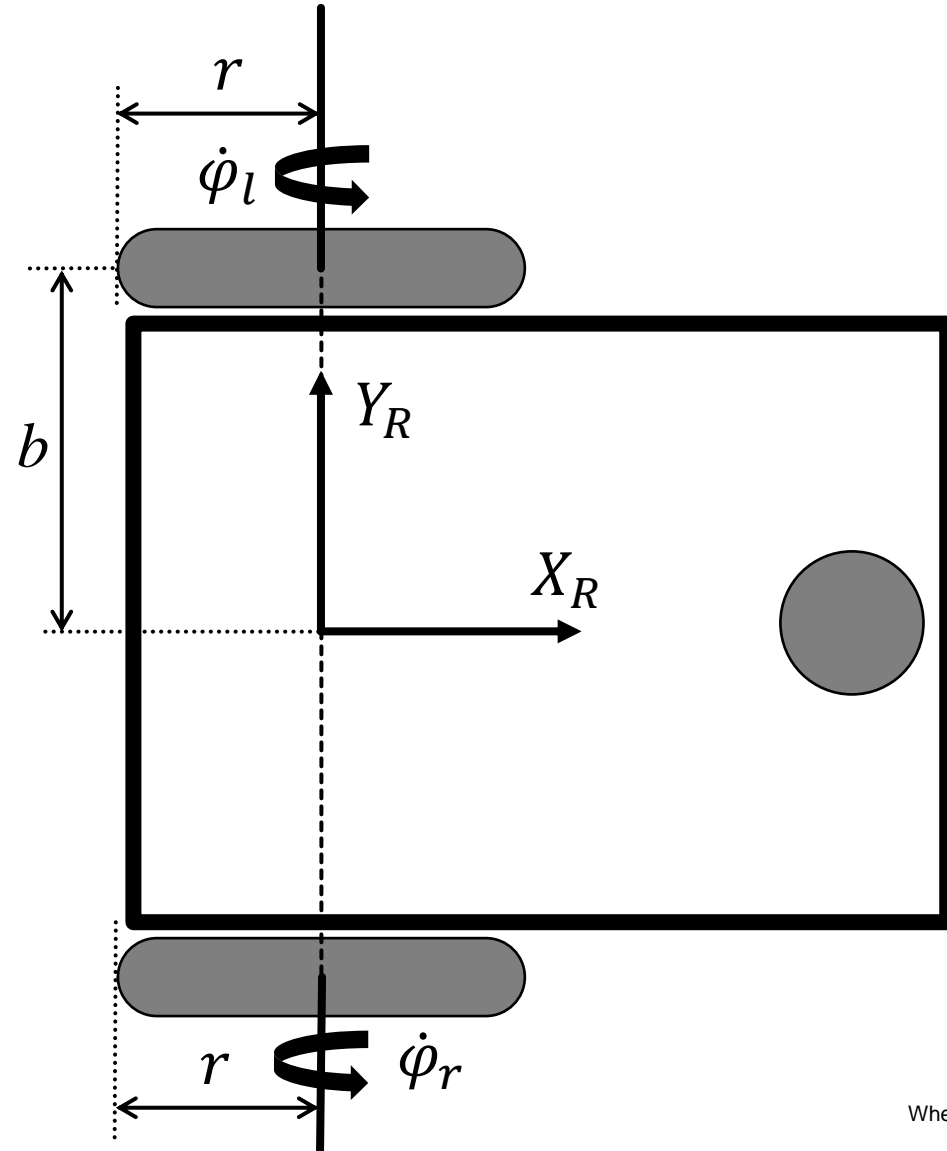
$$\delta_m = 2, \quad \delta_s = 0, \quad \delta_M = 2$$

- Forward differential kinematics

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} r/2 & r/2 \\ 0 & 0 \\ r/2b & -r/2b \end{bmatrix} \begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix}$$

- Inverse differential kinematics

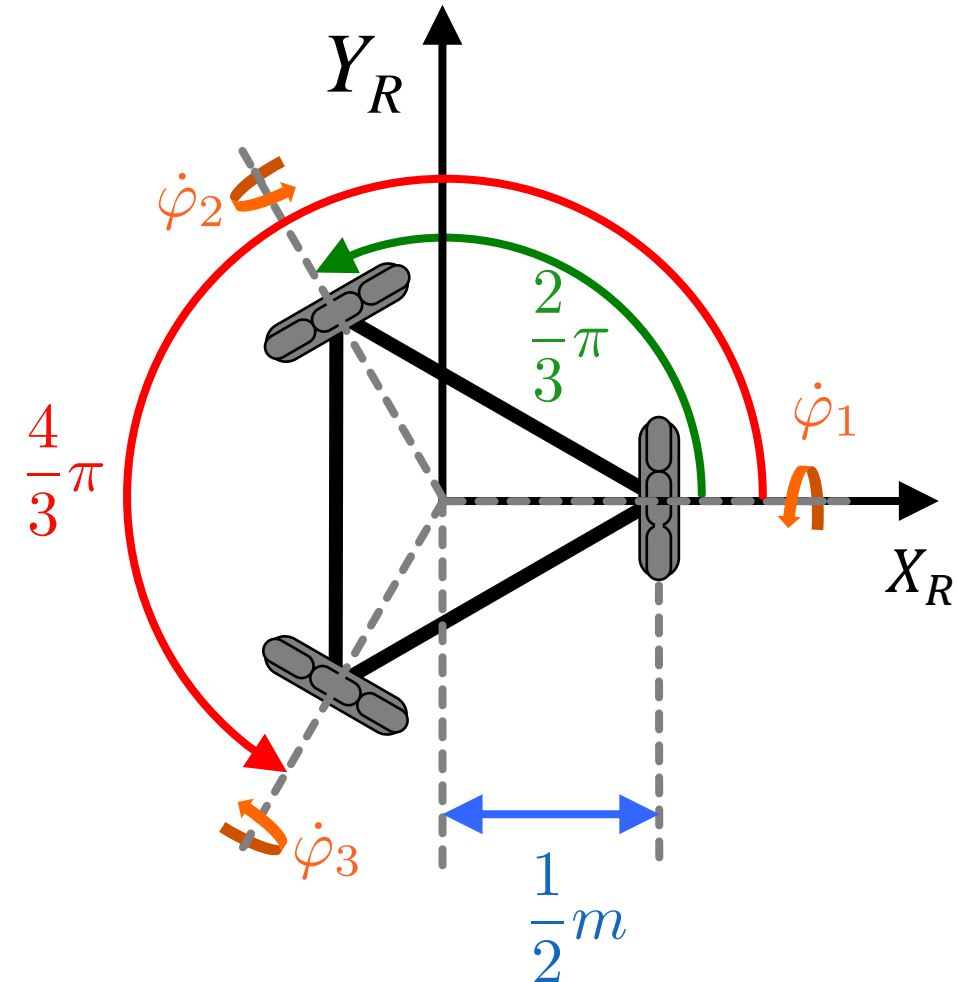
$$\begin{bmatrix} \dot{\phi}_r \\ \dot{\phi}_l \end{bmatrix} = \begin{bmatrix} 1/r & 0 & b/r \\ 1/r & 0 & -b/r \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix}$$



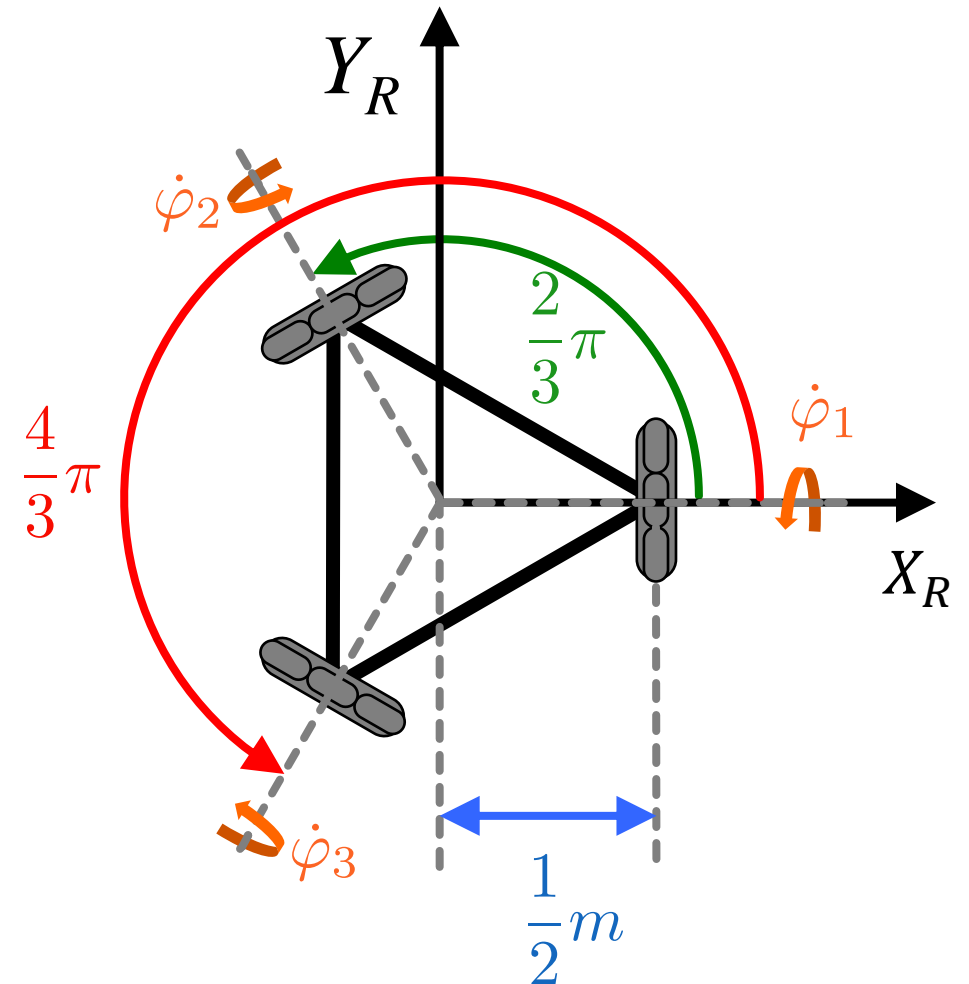
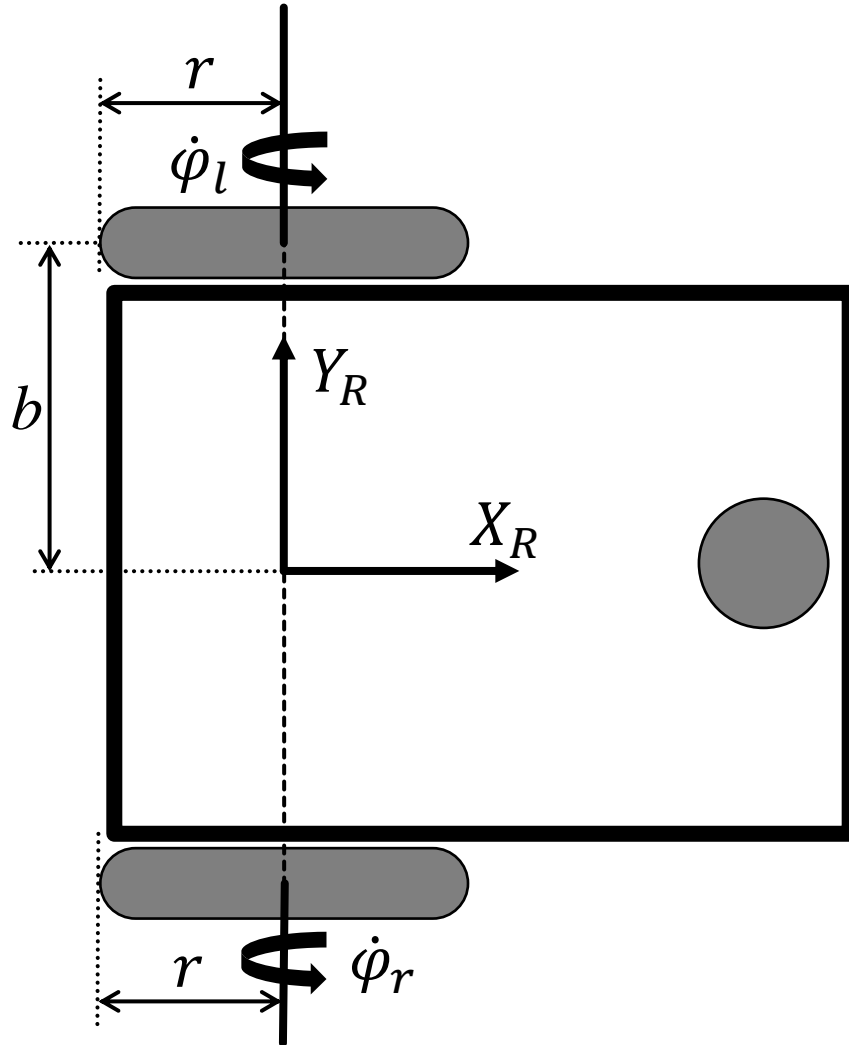


# An Omnidirectional Robot

- This robot was the example in the online problem set.
- Were there any questions about the example?



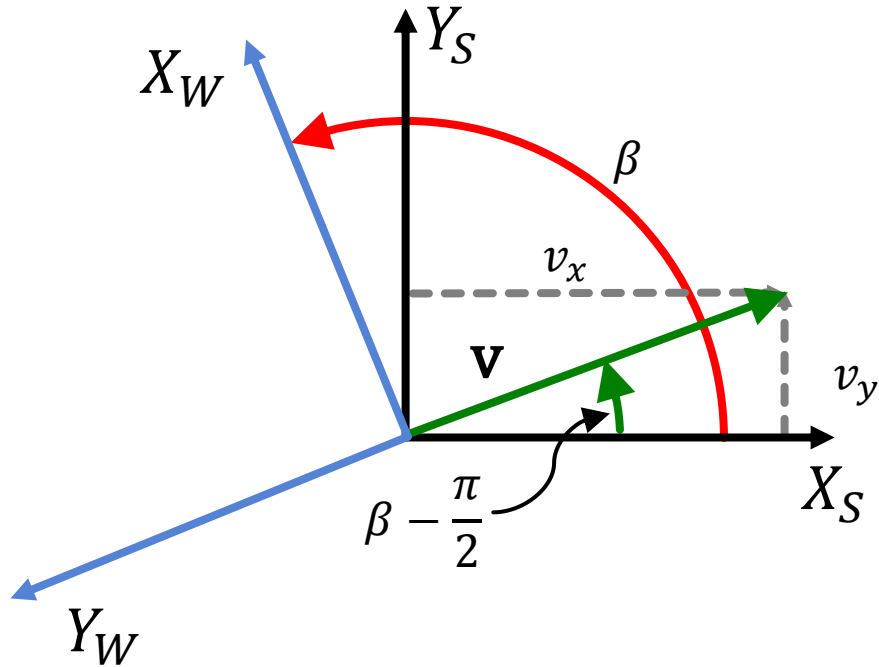
# Simple Robots



# Practical Problems

- Head over to MATLAB and get into groups
- <http://tinyurl.com/amrx-wheels>

# Computing the steering angle



$$\beta = \frac{\pi}{2} + \text{atan}(v_y/v_x)$$

- To compute the steering angle, we must transform the velocity of the vehicle into the steering frame S, then determine the angle,  $\beta$ , that brings the velocity into the negative  $y$  direction in the wheel frame.

# Computing Wheel Odometry

- Given sensed wheel speeds at time  $t$ , we know how to generate a predicted platform velocity:

$$\dot{\xi}_R(t) = \mathbf{F} \dot{\phi}(t)$$

- Recall that

$$\dot{\xi}_R = R(\theta) \dot{\xi}_I$$

- In the inertial frame, the velocity equation is:

$$\dot{\xi}_I(t) = R(-\theta(t)) \mathbf{F} \dot{\phi}(t)$$

# Computing Wheel Odometry

- Assumptions:
  - Timesteps of size  $T$
  - Constant acceleration

$$\dot{\xi}_R(t) = \dot{\xi}_R(t_0) + \frac{t-t_0}{T} (\dot{\xi}_R(t_1) - \dot{\xi}_R(t_0)), \quad t_0 \leq t < t_1$$

- The velocity integration equation:

$$\xi_I(t_k) = \xi_I(t_{k-1}) + \int_{t_{k-1}}^{t_k} \dot{\xi}_I(t) dt$$

# Computing Wheel Odometry

- Assumptions:
  - Timesteps of size  $T$
  - Constant acceleration

$$\dot{\xi}_R(t) = \dot{\xi}_R(t_0) + \frac{t-t_0}{T} (\dot{\xi}_R(t_1) - \dot{\xi}_R(t_0)), \quad t_0 \leq t < t_1$$

- The velocity integration equation:

$$\xi_I(t_k) \approx \xi_I(t_{k-1}) + \frac{T}{2} R(-\theta(t_{k-1})) (\dot{\xi}_R(t_{k-1}) + \dot{\xi}_R(t_k))$$

# Computing Wheel Odometry

- Assumptions:
  - Timesteps of size  $T$
  - Constant acceleration

$$\dot{\xi}_R(t) = \dot{\xi}_R(t_0) + \frac{t-t_0}{T} (\dot{\xi}_R(t_1) - \dot{\xi}_R(t_0)), \quad t_0 \leq t < t_1$$

- The velocity integration equation:

$$\xi_I(t_k) \approx \xi_I(t_{k-1}) + \frac{T}{2} R(-\theta(t_{k-1})) (\mathbf{F}(t_{k-1}) \dot{\phi}(t_{k-1}) + \mathbf{F}(t_k) \dot{\phi}(t_k))$$



# Computing Wheel Odometry

- The velocity integration equation:

$$\xi_I(t_k) \approx \xi_I(t_{k-1}) + \frac{T}{2} R(-\theta(t_{k-1})) (\mathbf{F}(t_{k-1}) \dot{\phi}(t_{k-1}) + \mathbf{F}(t_k) \dot{\phi}(t_k))$$