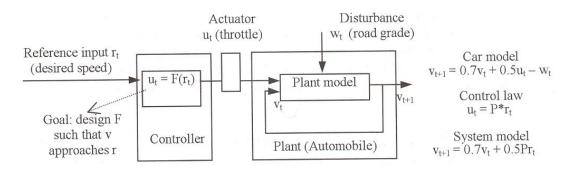
Embedded Systems Design: A Unified Hardware/Software Introduction

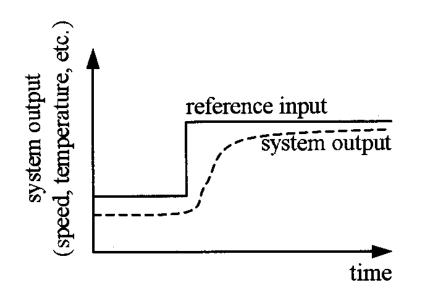
Chapter 9: Control Systems

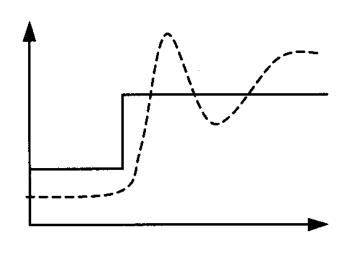
Control System

- Control physical system's output
 - By setting physical system's input
- Tracking
- E.g.
 - Cruise control
 - Thermostat control
 - Disk drive control
 - Aircraft altitude control
- Difficulty due to
 - Disturbance: wind, road, tire, brake; opening/closing door...
 - Human interface: feel good, feel right...



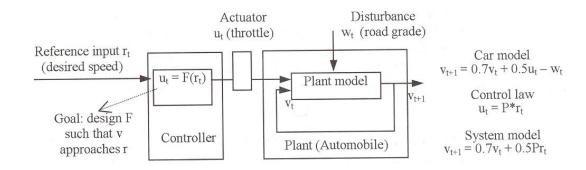
Tracking





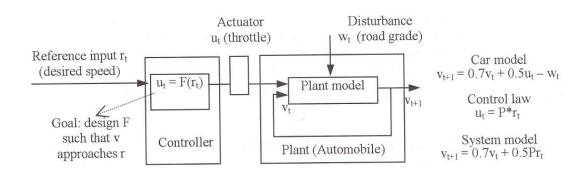
Open-Loop Control Systems

- Plant
 - Physical system to be controlled
 - Car, plane, disk, heater,...
- Actuator
 - Device to control the plant
 - Throttle, wing flap, disk motor,...
- Controller
 - Designed product to control the plant



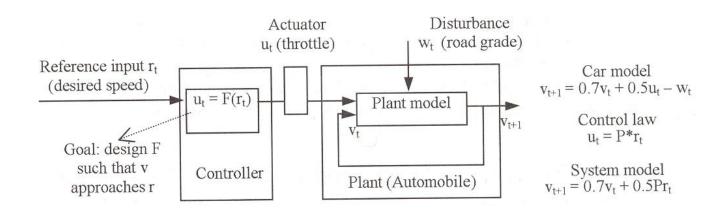
Open-Loop Control Systems

- Output
 - The aspect of the physical system we are interested in
 - Speed, disk location, temperature
- Reference
 - The value we want to see at output
 - Desired speed, desired location, desired temperature
- Disturbance
 - Uncontrollable input to the plant imposed by environment
 - Wind, bumping the disk drive, door opening



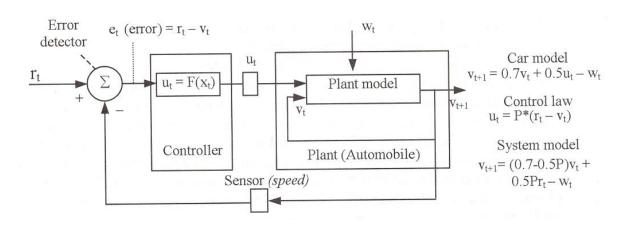
Other Characteristics of open loop

- Feed-forward control
- Delay in actual change of the output
- Controller doesn't know how well thing goes
- Simple
- Best use for predictable systems



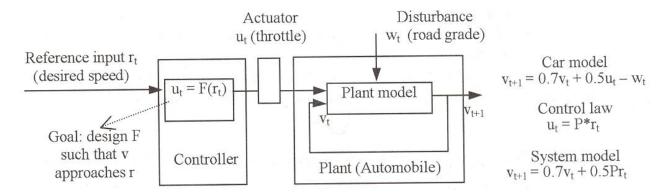
Close Loop Control Systems

- Sensor
 - Measure the plant output
- Error detector
 - Detect Error
- Feedback control systems
- Minimize tracking error



Designing Open Loop Control System

- Develop a model of the plant
- Develop a controller
- Analyze the controller
- Consider Disturbance
- Determine Performance
- Example: Open Loop Cruise Control System

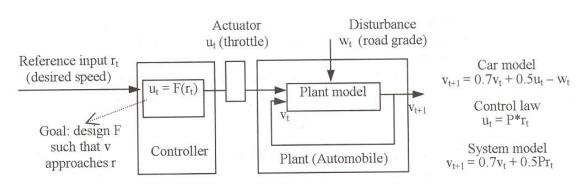


Model of the Plant

- May not be necessary
 - Can be done through experimenting and tuning
- But,
 - Can make it easier to design
 - May be useful for deriving the controller
- Example: throttle that goes from 0 to 45 degree
 - On flat surface at 50 mph, open the throttle to 40 degree
 - Wait 1 "time unit"
 - Measure the speed, let's say 55 mph
 - Then the following equation satisfy the above scenario
 - $v_{t+1}=0.7*v_t+0.5*u_t$
 - 55 = 0.7*50+0.5*40
 - IF the equation holds for all other scenario
 - Then we have a model of the plant

Designing the Controller

- Assuming we want to use a simple linear function
 - $u_t = F(r_t) = P * r_t$
 - r_t is the desired speed
- Linear proportional controller
- $v_{t+1}=0.7*v_t+0.5*u_t=0.7*v_t+0.5P*r_t$
- Let $v_{t+1}=v_t$ at steady state = v_{ss}
- $v_{ss} = 0.7 * v_{ss} + 0.5 P * r_t$
- At steady state, we want $v_{ss}=r_t$
- P=0.6
 - I.e. $u_t = 0.6 * r_t$



Analyzing the Controller

- Let $v_0 = 20$ mph, $r_0 = 50$ mph
- $v_{t+1}=0.7*v_t+0.5(0.6)*r_t=0.7*v_t+0.3*50=0.7*v_t+15$
- Throttle position is 0.6*50=30 degree

v_{t}
20.00
29.00
35.30
39.71
42.80
44.96
46.47
47.53
48.27
48.79
49.15
49.41
49.58

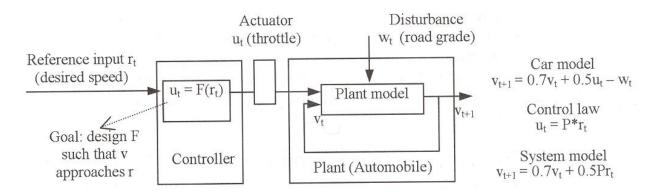
Considering the Disturbance

- Assume road grade can affect the speed
 - From -5mph to +5 mph
 - $-v_{t+1}=0.7*v_t+10$
 - $-v_{t+1}=0.7*v_t+20$

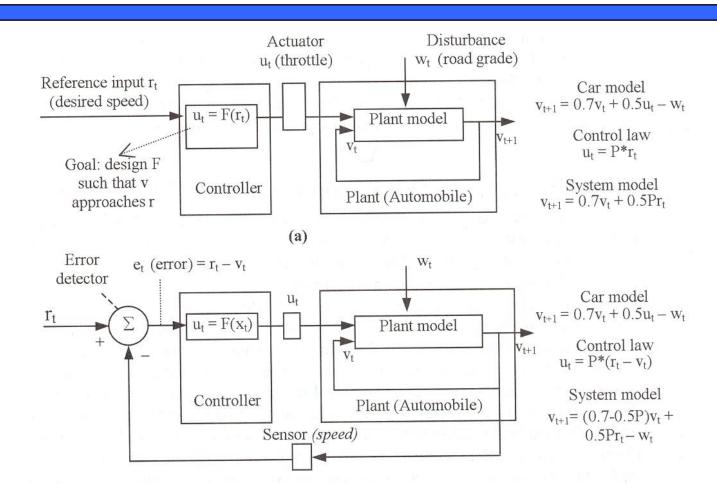
Time (t)	\mathbf{v}_{t}	v_t for $w = +5$	v_t for $w = -5$
0	20.00	20.00	20.00
1	29.00	24.00	34.00
2	35.30	26.80	43.80
3	39.71	28.76	50.66
4	42.80	30.13	55.46
5	44,96	31.09	58.82
6	46.47	31.76	61.18
7	47.53	32.24	62.82
8	48.27	32.56	63.98
9	48.79	32.80	64.78
10	49.15	32.96	65.35
11	49.41	33.07	65.74
12	49.58	33.15	66.02

Determining Performance

- $V_{t+1}=0.7*v_t+0.5P*r_0-w_0$
- $v_1 = 0.7 * v_0 + 0.5 P * r_0 w_0$
- $v_2=0.7*(0.7*v_0+0.5P*r_0-w_0) +0.5P*r_0-w_0=0.7*0.7*v_0+(0.7+1.0)*0.5P*r_0-(0.7+1.0)w_0$
- $v^{t}=0.7^{t*}v_{0}+(0.7^{t-1}+0.7^{t-2}+...+0.7+1.0)(0.5P*r_{0}-w_{0})$
- Coefficient of v_t determines rate of decay of v₀
 - >1 or <-1, v_t will grow without bound
 - <0, v_t will oscillate



Designing Close Loop Control System

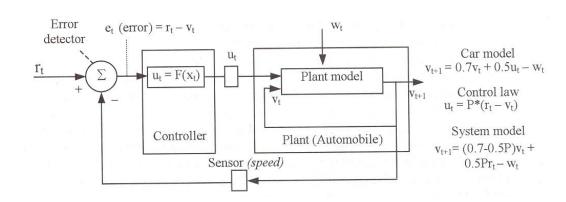


Stability

- $u_t = P * (r_t v_t)$
- $v_{t+1} = 0.7v_t + 0.5u_t w_t = 0.7v_t + 0.5P*(r_t v_t) w_t$ = $(0.7 - 0.5P)*v_t + 0.5P*r_t - w_t$
- $v^{t}=(0.7-0.5P)^{t*}v_{0}+((0.7-0.5P)^{t-1}+(0.7-0.5P)^{t-2}+...+0.7-0.5P+1.0)(0.5P*r_{0}-w_{0})$
- Stability constraint (I.e. convergence) requires

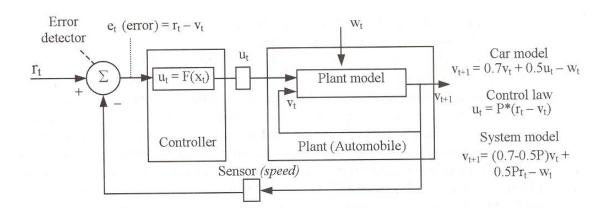
$$|0.7-0.5P| < 1$$

- -1 < 0.7 0.5P < 1
- -0.6 < P < 3.4



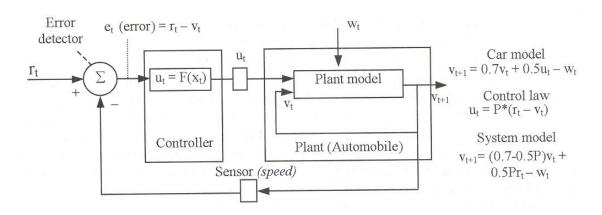
Reducing effect of v₀

- $u_t = P * (r_t v_t)$
- $v_{t+1} = 0.7v_t + 0.5u_t w_t = 0.7v_t + 0.5P*(r_t v_t) w_t$ = $(0.7 - 0.5P)*v_t + 0.5P*r_t - w_t$
- $v^{t}=(0.7-0.5P)^{t*}v_{0}+((0.7-0.5P)^{t-1}+(0.7-0.5P)^{t-2}+...+0.7-0.5P+1.0)(0.5P*r_{0}-w_{0})$
- To reduce the effect of initial condition
 - 0.7-0.5P as small as possible
 - P=1.4



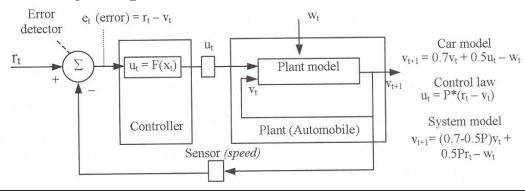
Avoid Oscillation

- $u_t = P * (r_t v_t)$
- $v_{t+1} = 0.7v_t + 0.5u_t w_t = 0.7v_t + 0.5P*(r_t v_t) w_t$ = $(0.7 - 0.5P)*v_t + 0.5P*r_t - w_t$
- $v^{t}=(0.7-0.5P)^{t*}v_{0}+((0.7-0.5P)^{t-1}+(0.7-0.5P)^{t-2}+...+0.7-0.5P+1.0)(0.5P*r_{0}-w_{0})$
- To avoid oscillation
 - -0.7-0.5P>=0
 - P <= 1.4



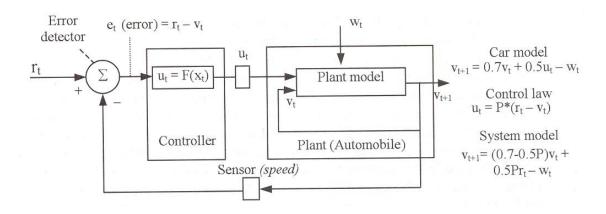
Perfect Tracking

- $u_t = P * (r_t v_t)$
- $v_{t+1} = 0.7v_t + 0.5u_t w_t = 0.7v_t + 0.5P*(r_t v_t) w_t$ = $(0.7 - 0.5P)*v_t + 0.5P*r_t - w_t$
- v_{ss} =(0.7-0.5P)* v_{ss} +0.5P* r_0 - w_0 (1-0.7+0.5P) v_{ss} =0.5P* r_0 - w_0 v_{ss} =(0.5P/(0.3+0.5P)) * r_0 - (1.0/(0.3+0.5P)) * w_0
- To make v_{ss} as close to r_0 as possible
 - P should be as large as possible



Close-Loop Design

- $u_t = P * (r_t v_t)$
- Finally, setting P=3.3
 - Stable, track well, some oscillation
 - $u_t = 3.3 * (r_t v_t)$



Analyze the controller

- $v_0=20$ mph, $r_0=50$ mph, w=0
- $v_{t+1} = 0.7v_t + 0.5P*(r_t v_t) w$ = $0.7v_t + 0.5*3.3*(50 - v_t)$
- $u_t = P * (r_t v_t)$ = 3.3 * (50- v_t)
- But u_t range from 0-45
- Controller saturates

Time	v_{t}	u _t
0	20.00	99.00
1	63.50	-44.55
2	22.18	91.82
3	61.43	-37.73
4	24.14	85.34
5	59.57	-31.58
6	25.91	79.50
7	57.89	-26.02
8	27.51	74.22
9	56.37	-21.01
10	28.95	69.46
45	44.53	18.06
46	40.20	32.34
47	44.31	18.78
48	40.41	31.66
49	44.11	19.42
50	40.59	31.05
SS	42.31	25.38

Analyze the controller

- $v_0=20 \text{ mph}, r_0=50 \text{ mph}, w=0$
- $v_{t+1} = 0.7v_t + 0.5*u_t$
- $u_t = 3.3 * (50-v_t)$
 - Saturate at 0, 45
- Oscillation!
 - "feel bad"

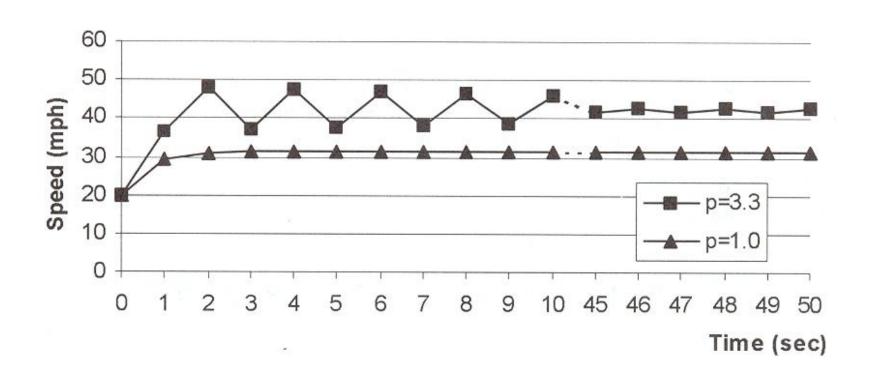
Time	v_{t}	u_t	v_{t}	u_t
0	20.00	99.00	20.00	45.00
1	63.50	-44.55	36.50	44.55
2	22.18	91.82	47.83	7.18
3	61.43	-37.73	37.07	42.68
4	24.14	85.34	47.29	8.95
5	59.57	-31.58	37.58	40.99
6	25.91	79.50	46.80	10.55
7	57.89	-26.02	38.04	39.47
8	27.51	74.22	46.36	12.00
9	56.37	-21.01	38.45	38.10
10	28.95	69.46	45.97	13.31
45	44.53	18.06	41.70	27.39
46	40.20	32.34	42.89	23.48
47	44.31	18.78	41.76	27.20
48	40.41	31.66	42.83	23.66
49	44.11	19.42	41.81	27.02
50	40.59	31.05	42.78	23.83
SS	42.31	25.38	42.31	25.38

Analyze the controller

- Set P=1.0 to void oscillation
 - Terrible SS performance

Time	v_t	u_t	\mathbf{v}_{t}	u_t	v_t	u_t
0	20.00	99.00	20.00	45.00	20.00	30.00
1	63.50	-44.55	36.50	44.55	29.00	21.00
2	22.18	91.82	47.83	7.18	30.80	19.20
3	61.43	-37.73	37.07	42.68	31.16	18.84
4	24.14	85.34	47.29	8.95	31.23	18.77
5	59.57	-31.58	37.58	40.99	31.25	18.75
6	25.91	79.50	46.80	10.55	31.25	18.75
7	57.89	-26.02	38.04	39.47	31.25	18.75
8	27.51	74.22	46.36	12.00	31.25	18.75
9	56.37	-21.01	38.45	38.10	31.25	18.75
10	28.95	69.46	45.97	13.31	31.25	18.75
45	44.53	18.06	41.70	27.39	31.25	18.75
46	40.20	32.34	42.89	23.48	31.25	18.75
47	44.31	18.78	41.76	27.20	31.25	18.75
48	40.41	31.66	42.83	23.66	31.25	18.75
49	44.11	19.42	41.81	27.02	31.25	18.75
50	40.59	31.05	42.78	23.83	31.25	18.75
SS	42.31	25.38	42.31	25.38	31.25	18.75

Analyzing the Controller



Minimize the effect of disturbance

- $v_{t+1} = 0.7v_t + 0.5*3.3*(r_t v_t) w = -5 \text{ or } +5$
- 39.74
 - Close to 42.31
 - Better than
 - 33
 - 66
- Cost
 - SS error
 - oscillation

	, .			
Time	v_{t}	u_t	v_{t}	\mathbf{u}_{t}
0	20.00	45.00	20.00	45.00
1	31.50	45.00	41.50	28.05
2	39.55	34.49	48.08	6.35
3	39.93	33.24	41.83	26.97
4	39.57	34.42	47.76	7.38
5	39.91	33.30	42.13	25.99
6	39.59	34.37	47.48	8.31
7	39.89	33.35	42.39	25.10
8	39.60	34.32	47.23	9.15
9	39.88	33.40	42.63	24.30
10	39.62	34.27	47.00	9.91
45	39.76	33.78	44.52	18.09
46	39.72	33.91	45.21	15.82
47	39.76	33.78	44.55	17.97
48	39.73	33.91	45.17	15.92
49	39.76	33.79	44.58	17.87
50	39.73	33.90	45.14	16.02
SS	39.74	33.85	44.87	16.92

General Control System

Objective

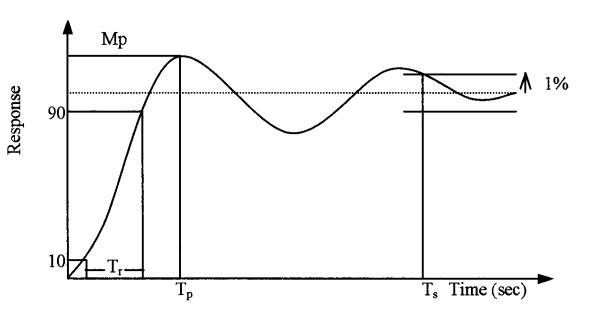
- Causing output to track a reference even in the presence of
 - Measurement noise
 - Model error
 - Disturbances

Metrics

- Stability
 - Output remains bounded
- Performance
 - How well an output tracks the reference
- Disturbance rejection
- Robustness
 - Ability to tolerate modeling error of the plant

Performance (generally speaking)

- Rise time
 - Time it takes form10% to 90%
- Peak time
- Overshoot
 - Percentage by which Peak exceed final value
- Settling time
 - Time it takes to reach 1% of final value

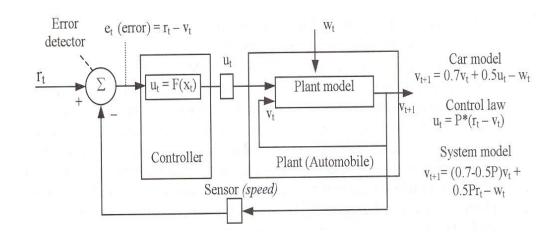


Plant modeling is difficult

- May need to be done first
- Plant is usually on continuous time
 - Not discrete time
 - E.g. car speed continuously react to throttle position, not at discrete interval
 - Sampling period must be chosen carefully
 - To make sure "nothing interesting" happen in between
 - I.e. small enough
- Plant is usually non-linear
 - E.g. shock absorber response may need to be 8th order differential
- Iterative development of the plant model and controller
 - Have a plant model that is "good enough"

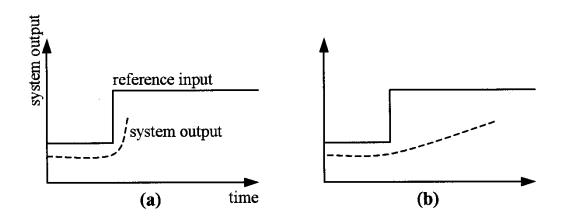
Controller Design: P

- Proportional controller
 - A controller that multiplies the tracking error by a constant
 - $\mathbf{u}_{t} = \mathbf{P} * (\mathbf{r}_{t} \mathbf{v}_{t})$
 - Close loop model with a linear plant
 - E.g. $v_{t+1} = (0.7 0.5P) * v_t + 0.5P * r_t w_t$
- P affects
 - Transient response
 - Stability, oscillation
 - Steady state tacking
 - As large as possible
 - Disturbance rejection
 - As large as possible



Controller Design: PD

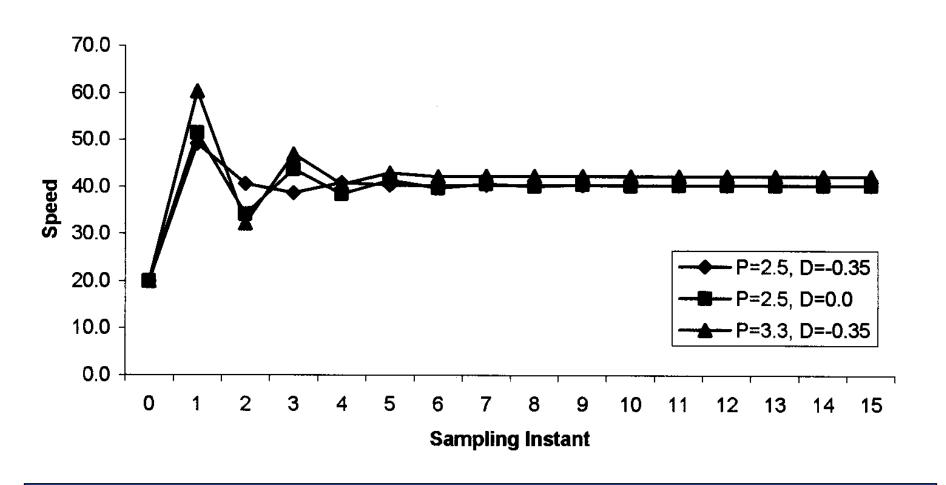
- Proportional and Derivative control
 - $u_t = P * (r_t v_t) + D * ((r_t v_t) (r_{t-1} v_{t-1})) = P * e_t + D * (e_t e_{t-1})$
- Consider the size of error over time
- Intuitively
 - Want to "push" more if the error is not reducing fast enough
 - Want to "push" less if the error is reducing really fast



PD Controller

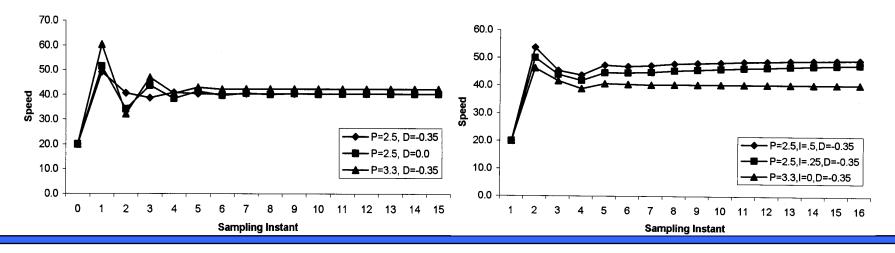
- Need to keep track of error derivative
- E.g. Cruise controller example
 - $-v_{t+1} = 0.7v_t + 0.5u_t w_t$
 - Let $u_t = P * e_t + D * (e_t-e_{t-1}), e_t=r_t-v_t$
 - $v_{t+1} = 0.7v_t + 0.5*(P*(r_t-v_t)+D*((r_t-v_t)-(r_{t-1}-v_{t-1})))-w_t$
 - $v_{t+1} = (0.7 0.5*(P+D))*v_t + 0.5D*v_{t-1} + 0.5*(P+D)*r_t 0.5D*r_{t-1} w_t$
 - Assume reference input and distribunce are constant, the steady-state speed is
 - $V_{ss} = (0.5P/(1-0.7+0.5P)) * r$
 - Does not depend on D!!!
- P can be set for best tracking and disturbance control
- Then D set to control oscillation/overshoot/rate of convergence

PD Control Example



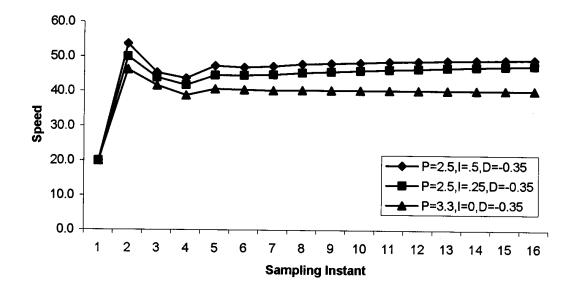
PI Control

- Proportional plus integral control
 - $u_t = P^*e_t + I^*(e_0 + e_1 + ... + e_t)$
- Sum up error over time
 - Ensure reaching desired output, eventually
 - v_{ss} will not be reached until $e_{ss}=0$
- Use P to control disturbance
- Use I to ensure steady state convergence and convergence rate



PID Controller

- Combine Proportional, integral, and derivative control
 - $\quad u_t \!\!=\!\! P^* e_t \!\!+\!\! I^* (e_0 \!\!+\!\! e_1 \!\!+\! \dots \!\!+\!\! e_t) \!\!+\!\! D^* (e_t \!\!-\!\! e_{t\text{-}1})$
- Available off-the shelf



Software Coding

- Main function loops forever, during each iteration
 - Read plant output sensor
 - May require A2D
 - Read current desired reference input
 - Call PidUpdate, to determine actuator value
 - Set actuator value
 - May require D2A

```
void main()
{
    double sensor_value, actuator_value, error_current;
    PID_DATA pid_data;
    PidInitialize(&pid_data);
    while (1) {
        sensor_value = SensorGetValue();
        reference_value = ReferenceGetValue();
        actuator_value =
            PidUpdate(&pid_data,sensor_value,reference_value);
        ActuatorSetValue(actuator_value);
    }
}
```

Software Coding (continue)

- Pgain, Dgain, Igain are constants
- sensor_value_previous
 - For D control
- error_sum
 - For I control

```
typedef struct PID_DATA {
    double Pgain, Dgain, Igain;
    double sensor_value_previous; // find the derivative
    double error_sum; // cumulative error
}
```

Computation

• $u_t = P^*e_t + I^*(e_0 + e_1 + ... + e_t) + D^*(e_t - e_{t-1})$ double PidUpdate(PID_DATA *pid_data, double sensor_value, double reference value) double Pterm, Iterm, Dterm; double error, difference; error = reference value - sensor value; Pterm = pid data->Pgain * error; /* proportional term*/ pid data->error sum += error; /* current + cumulative*/ // the integral term Iterm = pid data->Igain * pid data->error sum; difference = pid data->sensor value previous sensor value; // update for next iteration pid data->sensor value previous = sensor value; // the derivative term Dterm = pid data->Dgain * difference; return (Pterm + Iterm + Dterm);

PID tuning

- Analytically deriving P, I, D may not be possible
 - E.g. plant not is not available, or to costly to obtain
- Ad hoc method for getting "reasonable" P, I, D
 - Start with a small P, I=D=0
 - Increase D, until seeing oscillation
 - Reduce D a bit
 - Increase P, until seeing oscillation
 - Reduce D a bit
 - Increase I, until seeing oscillation
- Iterate until can change anything without excessive oscillation

Practical Issues with Computer-Based Control

- Quantization
- Overflow
- Aliasing
- Computation Delay

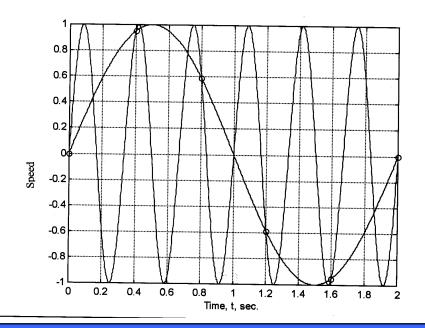
Quantization & Overflow

Quantization

- Can't store 0.36 as 4-bit fractional number
- Can only store 0.75, 0.59, 0.25, 0.00, -0.25, -050,-0.75, -1.00
- Choose 0.25
 - Result in quantization error of 0.11
- Sources of quantization error
 - Operations, e.g. 0.50*0.25=0.125
 - Can use more bits until input/output to the environment/memory
 - A2D converters
- Overflow
 - Can't store 0.75+0.50 = 1.25 as 4-bit fractional number
- Solutions:
 - Use fix-point representation/operations carefully
 - Time-consuming
 - Use floating-point co-processor
 - Costly

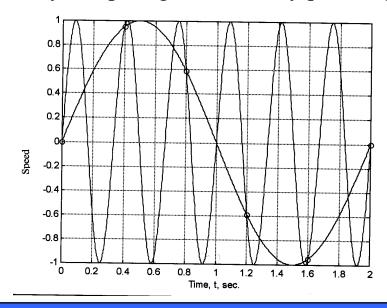
Aliasing

- Quantization/overflow
 - Due to discrete nature of computer data
- Aliasing
 - Due to discrete nature of sampling



Aliasing Example

- Sampling at 2.5 Hz, period of 0.4, the following are indistinguishable
 - $y(t)=1.0*\sin(6\pi t)$, frequency 3 Hz
 - $y(t)=1.0*\sin(\pi t)$, frequency of 0.5 Hz
- In fact, with sampling frequency of 2.5 Hz
 - Can only correctly sample signal below Nyquist frequency 2.5/2 = 1.25 Hz



Computation Delay

- Inherent delay in processing
 - Actuation occurs later than expected
- Need to characterize implementation delay to make sure it is negligible
- Hardware delay is usually easy to characterize
 - Synchronous design
- Software delay is harder to predict
 - Should organize code carefully so delay is predictable and minimized
 - Write software with predictable timing behavior (be like hardware)
 - Time Trigger Architecture
 - Synchronous Software Language

Benefit of Computer Control

- Cost!!!
 - Expensive to make analog control immune to
 - Age, temperature, manufacturing error
 - Computer control replace complex analog hardware with complex code
- Programmability!!!
 - Computer Control can be "upgraded"
 - Change in control mode, gain, are easy to do
 - Computer Control can be adaptive to change in plant
 - Due to age, temperature, ...etc
 - "future-proof"
 - Easily adapt to change in standards,..etc