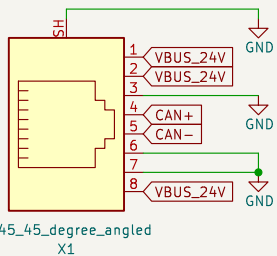
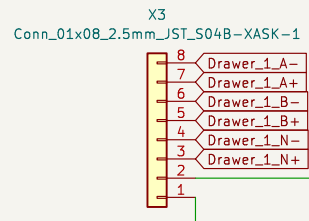


Input

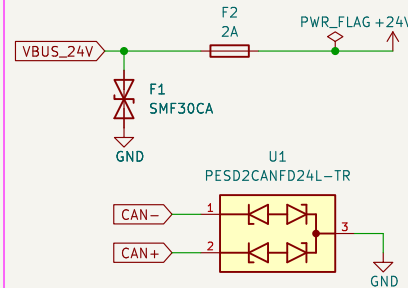
CAN and Power Input



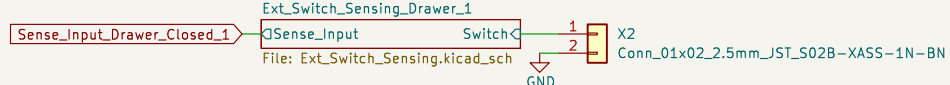
Drawer Encoder Sensor Input



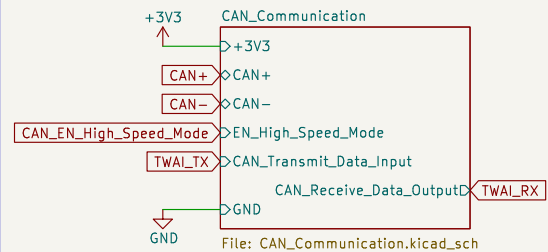
Input protection



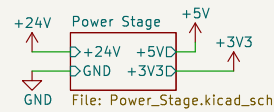
Drawer Closed Sensor Input



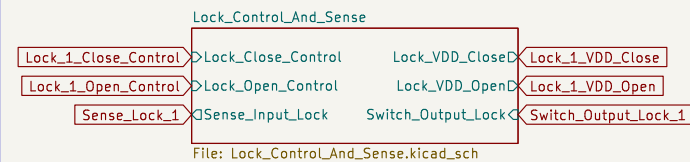
CAN Communication



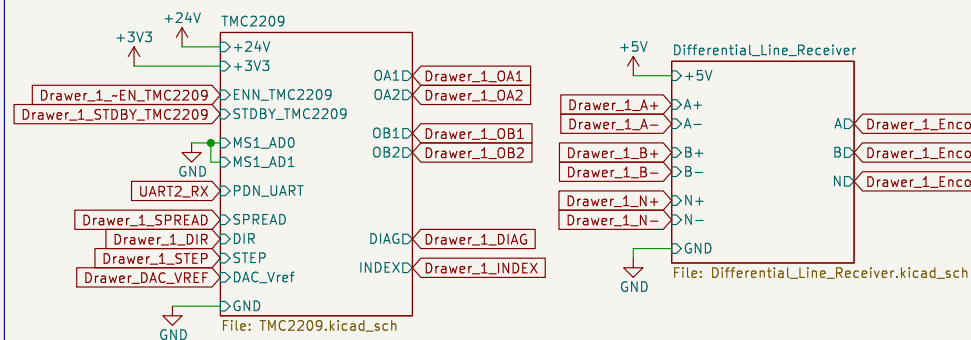
Power Stage



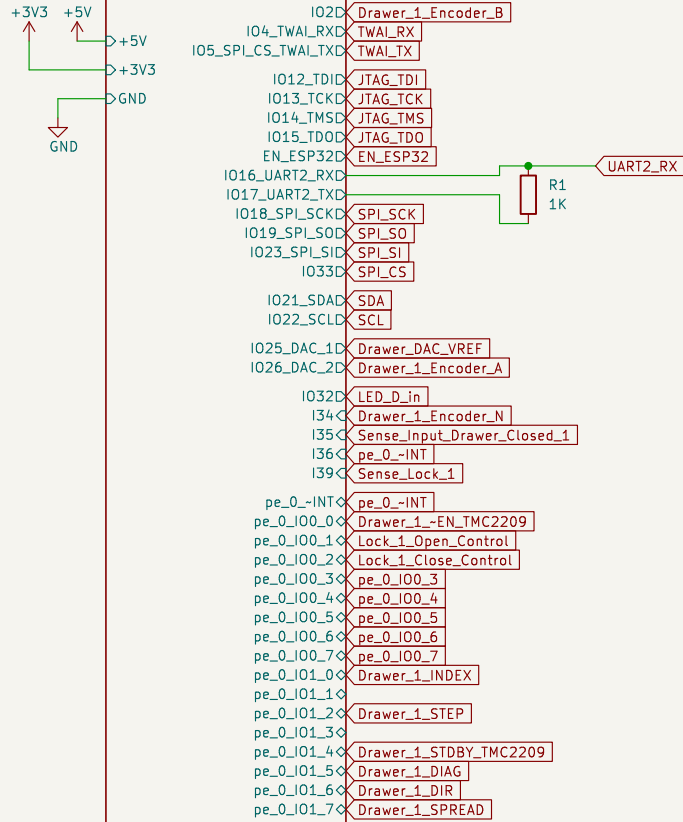
Lock Control and Sense



Electrical Drawer with Encoder

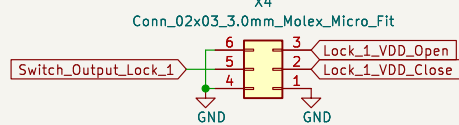


ESP32

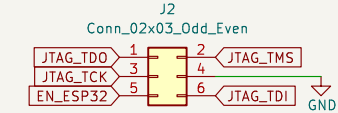


Output

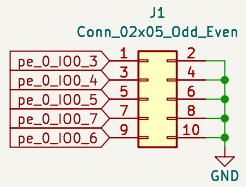
Locks



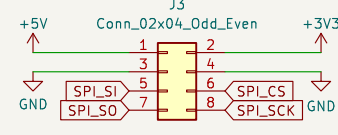
JTAG Debugging



Spare Port Expander pins



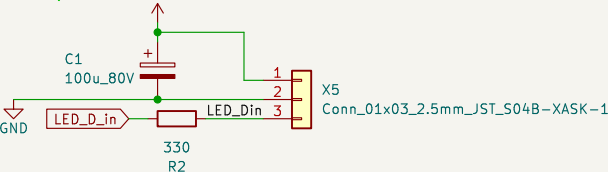
SPI



Electrical Drawer



LED Output



Mounting Holes

M3



M2 for cable ties



Sheet: /
File: Drawer_Controller_v4_hotfix.kicad_sch

Title:

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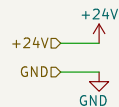
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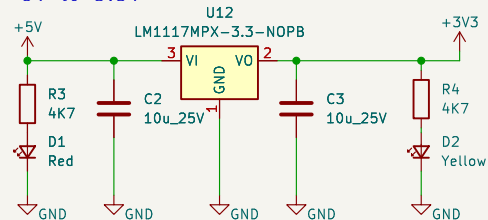
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Id: 1/12

Input



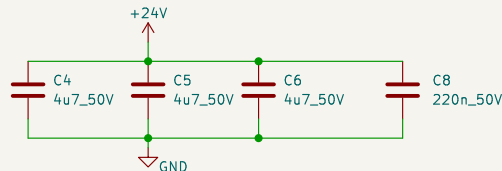
5V to 3.3V



24V to 5V

Input Capacitor

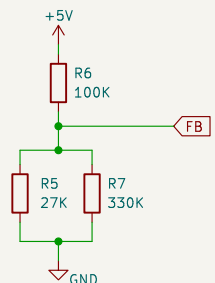
A minimum of 10 μF of ceramic capacitance is required on the input of the LMR33630. This must be rated for at least the maximum input voltage that the application requires; preferably twice the maximum input voltage. This capacitance can be increased to help reduce input voltage ripple and maintain the input voltage during load transients. In addition, a small case size, 220-nF ceramic capacitor must be used at the input, as close as possible to the regulator. This provides a high frequency bypass for the control circuits internal to the device. For this example a 4.7- μF , 50-V, X7R (or better like COG) ceramic capacitor is chosen. The 220 nF must also be rated at 50 V with an X7R or COG dielectric. Please mind that the small capacitor should have a smaller footprint to have smaller ESL. <https://www.signalintegrityjournal.com/articles/1509-the-myth-of-three-capacitor-values>



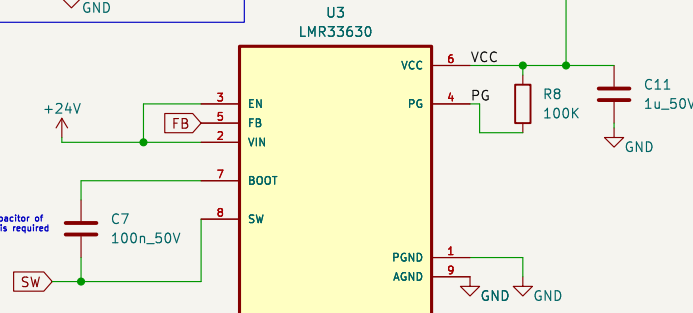
Reference Voltage

Output Voltage Set-Point:
 $R1 = R2 / (V_{\text{Out}}/1V) - 1$
 $R1 = 100k / (5V - 1V) = 25k$

Please mind:
R2 is recommended to be app. 100k Ω
For R1 = 24.9k is chosen as recommended in the datasheet.
 $27k || 330k = 27k * 330k / (27k + 330k) = 24,958$



A high-quality ceramic capacitor of 100 nF and at least 10 V is required



Output Filter

Inductor Selection

The parameters for selecting the inductor are the inductance and saturation current. The inductance is based on the desired peak-to-peak ripple current and is normally chosen to be in the range of 20% to 40% of the maximum output current. Experience shows that the best value for inductor ripple current is 30% of the maximum load current. Note that when selecting the ripple current for applications with much smaller maximum load than the maximum available from the device, the maximum device current should be used. Equation 4 can be used to determine the value of inductance. The constant K is the percentage of inductor current ripple. For this example, K = 0.3 was chosen.

$$L = \frac{(V_{\text{IN}} - V_{\text{OUT}}) \times (V_{\text{OUT}} / V_{\text{IN}})}{f_{\text{sw}} \times K \times I_{\text{OUTMax}}} = \frac{(24V - 5V) \times (5V / 24V)}{(400\text{kHz} \times 0.3 \times 2.3A)} = 14.34\mu\text{H}$$

Therefore we take the next available standard inductor value of 15uH.

For this example, a $\Delta V_{\text{OUT}} \leq 250 \text{ mV}$ for an output current step of $\Delta I_{\text{OUT}} = 2 \text{ A}$ is required. Equation 6 gives a minimum value of 52 μF and a maximum ESR of 0.11 Ω . More output capacitance can be used to improve the load transient response.

Ceramic capacitors can easily meet the minimum ESR requirements. In some cases, an aluminum electrolytic capacitor can be used in parallel with the ceramics to help build up the required value of capacitance. In general, use a capacitor of at least 10 V for output voltages of 3.3 V or less and a capacitor of 16 V or more for output voltages of 5 V and above.

For the capacitor we use 4 x 25V 22uF X5R $\pm 10\%$ 1206 Multilayer Ceramic Capacitors MLCC (CL31A226KAHNNNE).

If you check the specifications under <https://product.samsungsem.com/mlcc/cl31a226KAHNNN.do>

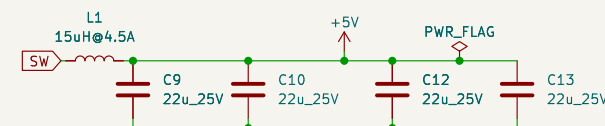
You can find, that the DC Bias at 5V DC is -37.96% of the original capacity, so

$$C_0 = 4 \times 22\mu\text{F} \times 0.62 = 54.56\mu\text{F}$$

To find out the Resr of the capacitor we can check the graph given in the above link and check the ESR value at the self-resonant frequency where the Impedance |Z| is minimal. This is at least what they did with the capacitor they took in the datasheet. The link to the capacitor of the datasheet can be found here: https://product.tdk.com/en/search/capacitor/ceramic/mlcc/info?part_no=C3216X5R0J476M160AC

Following this procedure, the ESR value for ONE CL31A226KAHNNNE is something like:

$$\text{Resr}_{1\text{uc}} = 3.82\text{m}\Omega\text{m} = 0.00382 \text{ Ohm}$$



Sheet: /Power Stage/
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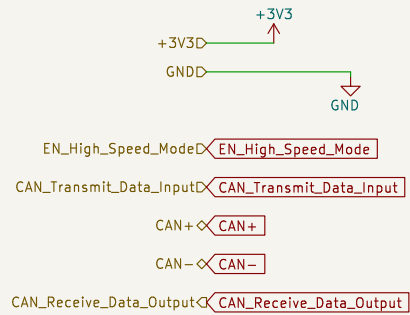
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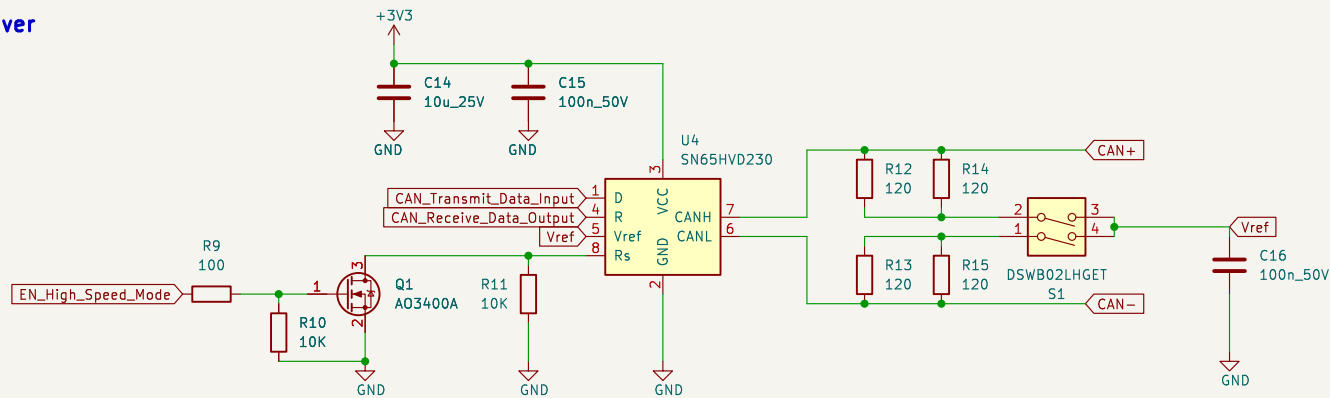
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Input/Output



CAN Transceiver



The RS pin (pin 8) on the SN65HVD230 and SN65HVD231 provides three different modes of operation: high speed mode, slope control mode, and low-power mode. The high speed mode of operation is selected by connecting the RS pin to ground, allowing the transmitter output transistors to switch on and off as fast as possible with no limitation on the rise and fall slopes. The rise and fall slopes can also be adjusted by connecting a resistor in series between the RS pin and ground. The slope will be proportional to the pin's output current. With a resistor value of 10 kΩ the device will have a slew rate of ~15 V/μs, and with a resistor value of 100 kΩ the device will have a slew rate of ~2 V/μs.

Sheet: /CAN_Communication/
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Title:

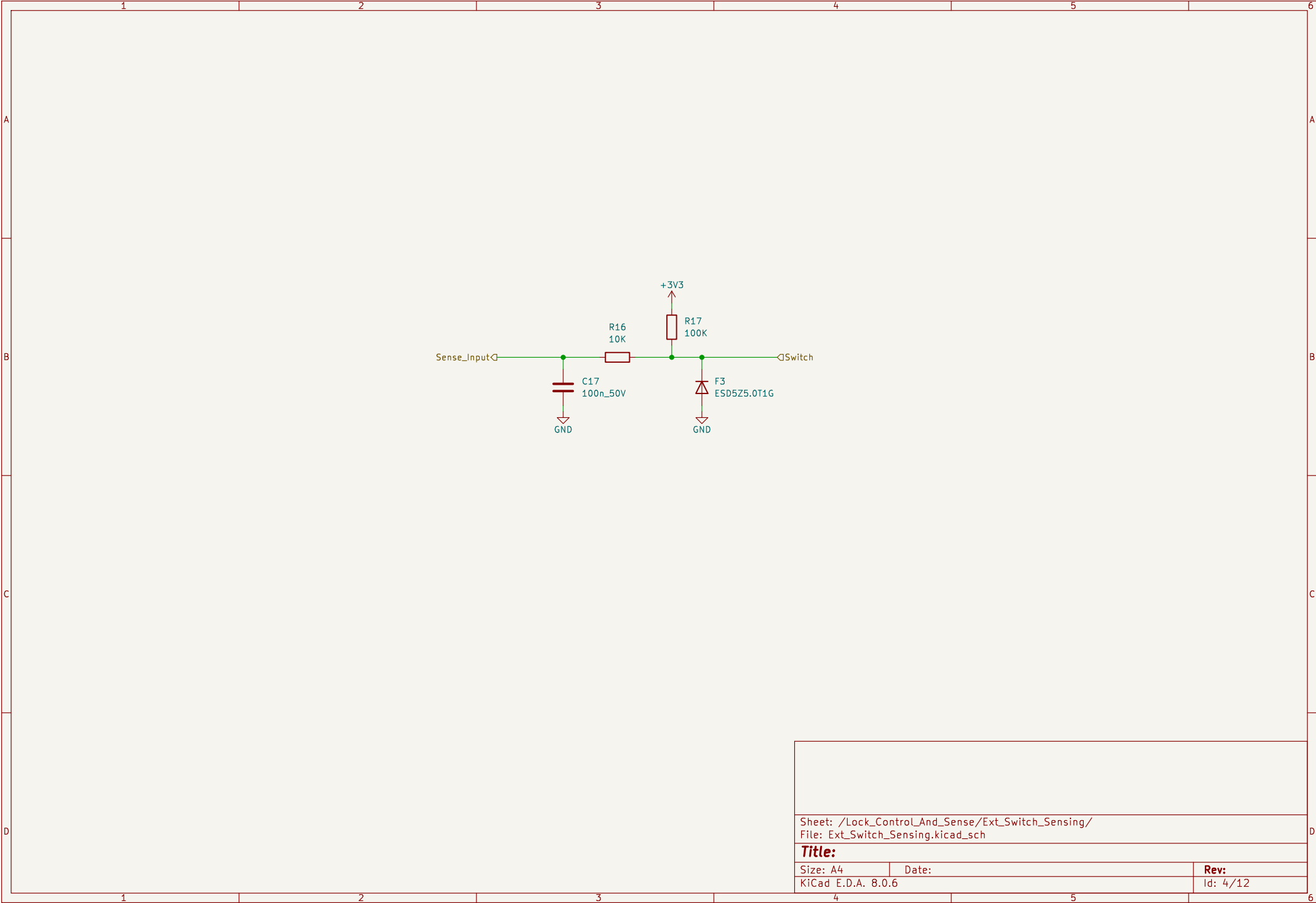
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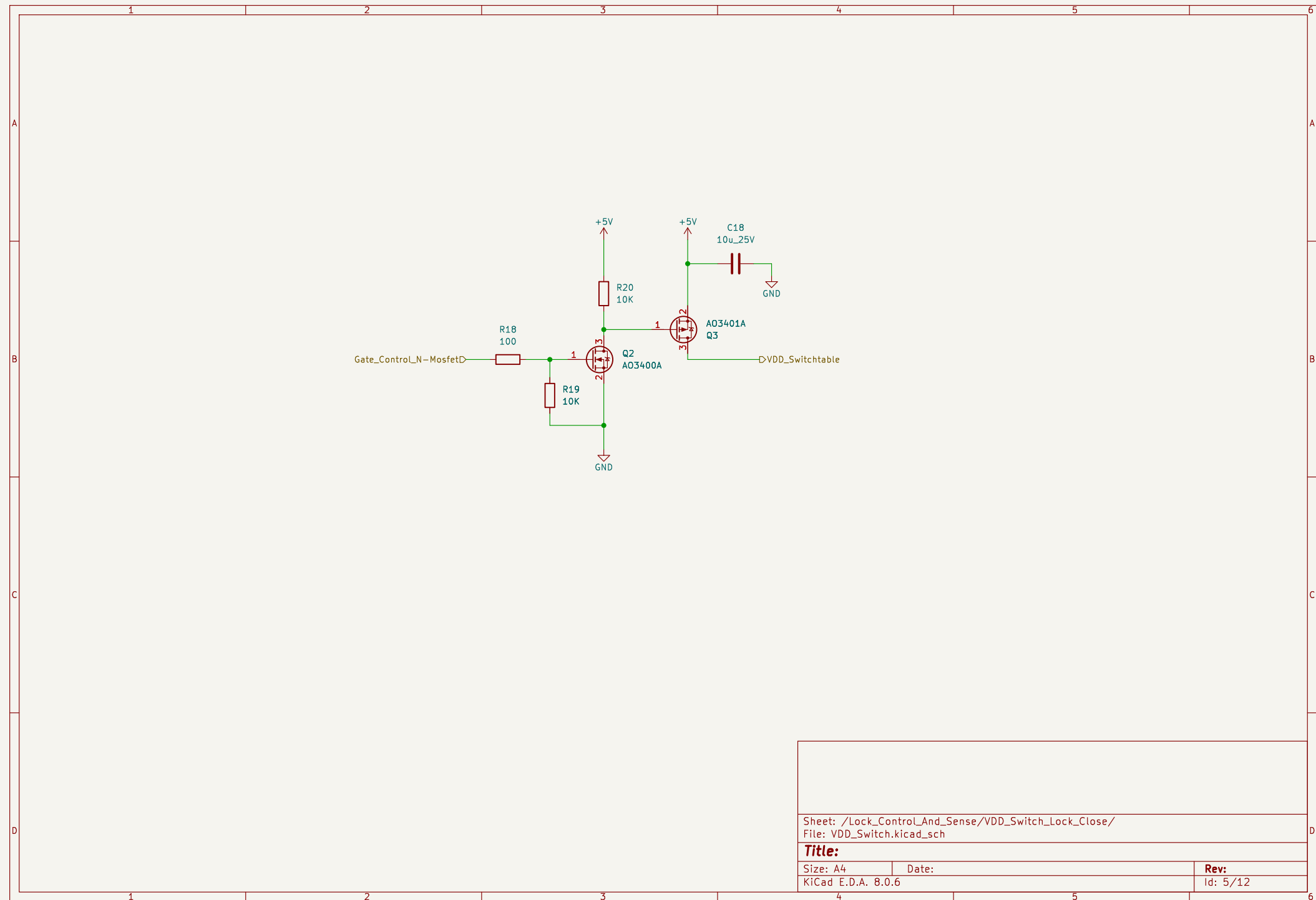
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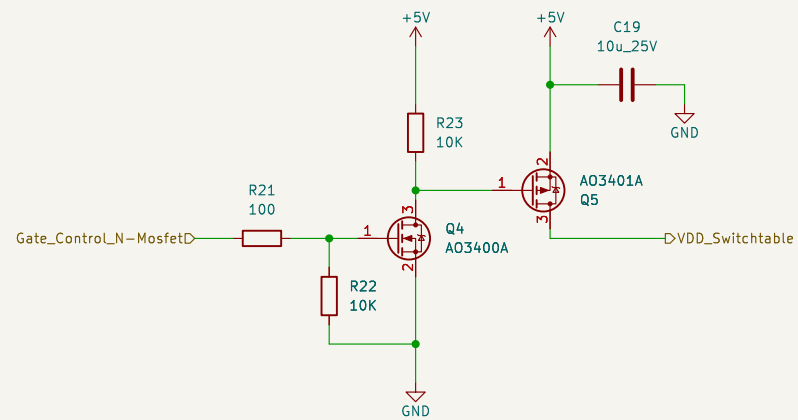
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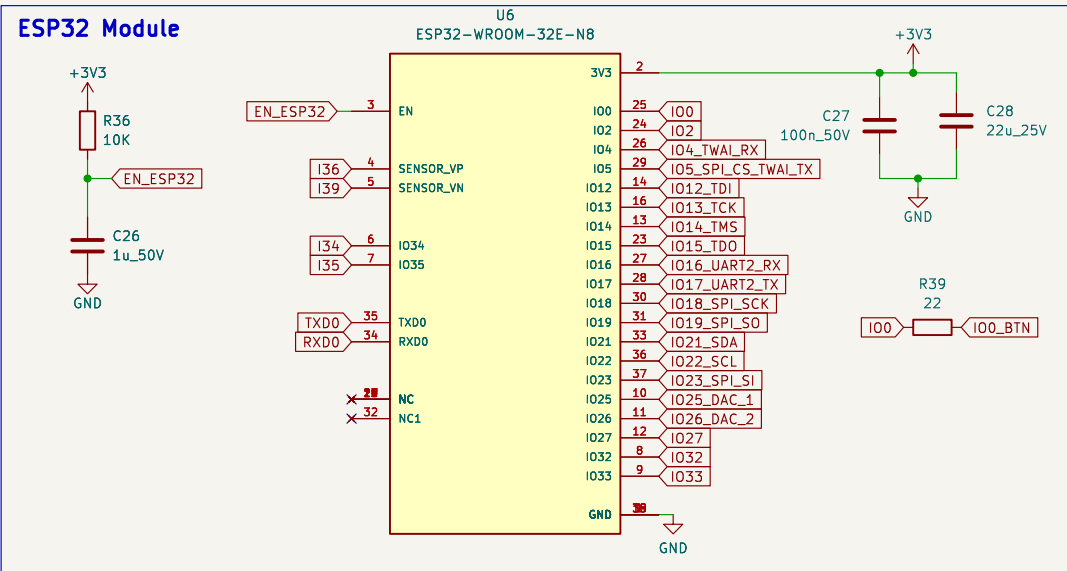
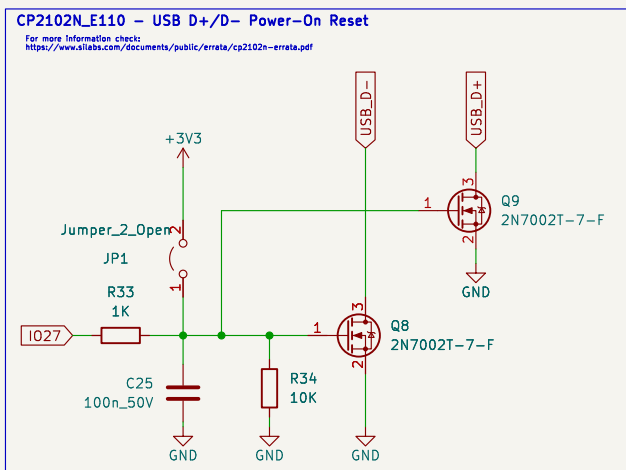
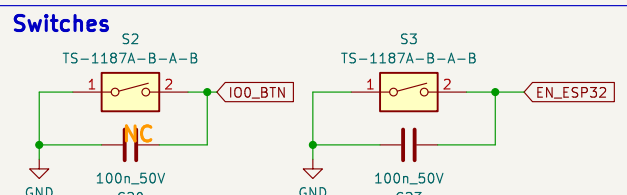
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I2C Pullup Resistor

Application Report:
I2C Bus Pullup
Resistor Calculation

I2C Bus Capacitance:
 - typ. ~10pF per device
 - ~0.08085 pF per cm microstrip (0.18mm width, 0.2104mm above reference plane)

We have 2 devices and ~2.5cm microstrip
 $C_{bus} = 2 * 10\text{pF} + 2.5 * 0.08085\text{pF}$
 $= 22.02 \text{ pF}$

Pullup Resistor for Fast-mode I2C:
 $R_p(\text{max}) = t_r / (0.8473 * C_{bus})$
 $= 300 * 10^{-9} / (0.8473 * 22.02 * 10^{-12})$
 $= 16.08 \text{ k}\Omega$

$R_p(\text{min}) = (V_{cc} - V_{OL}(\text{max})) / I_{OL}$
 $= (5 \text{ V} - 0.4 \text{ V}) / (3 * 10^{-3} \text{ A})$
 $= 1.5 \text{ k}\Omega$

So we can take e.g. 10 kΩ pullup resistor.

Output

I02 → I02
 I04_TWI_RX → I04_TWI_RX
 I05_SPL_CS_TWI_TX → I05_SPL_CS_TWI_TX

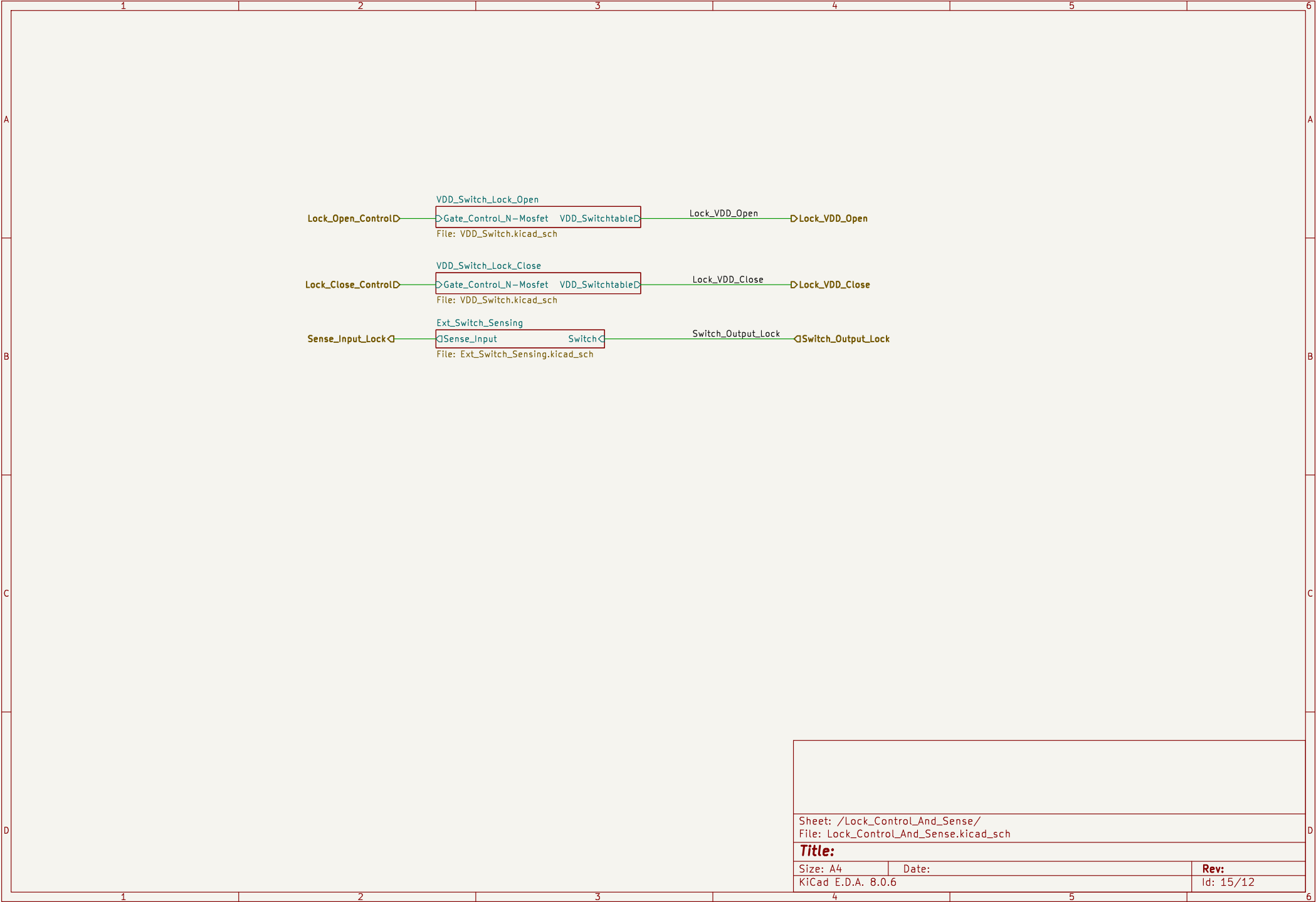
JTAG Debug Interface

I012_TDI → I012_TDI
 I013_TCK → I013_TCK
 I014_TMS → I014_TMS
 I015_TDO → I015_TDO
 EN_ESP32 → EN_ESP32

More information:
[FT232RH Debugging ESP32](#)

I016_UART2_RX → I016_UART2_RX
 I017_UART2_TX → I017_UART2_TX
 I018_SPL_SCK → I018_SPL_SCK
 I019_SPL_SO → I019_SPL_SO

Datasheets & References:
https://www.espressif.com/sites/default/files/documentation/esp32-wroom-32e_esp32-wroom-32ue_datasheet_en.pdf
https://dl.espressif.com/dl/schematics/esp32_devkitc_v4-sch.pdf
https://www.youtube.com/watch?v=5_p0YV-JlfU&t=4185s



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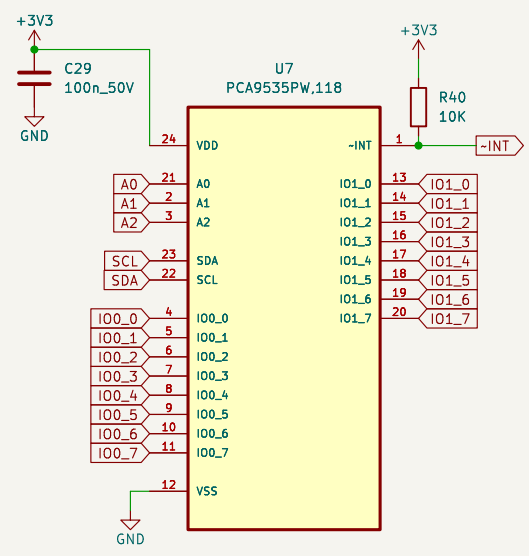
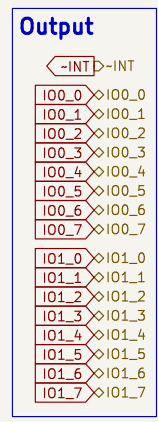
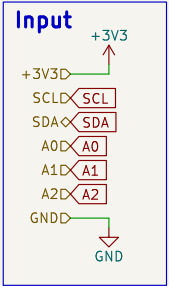
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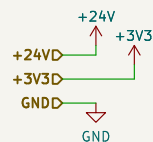
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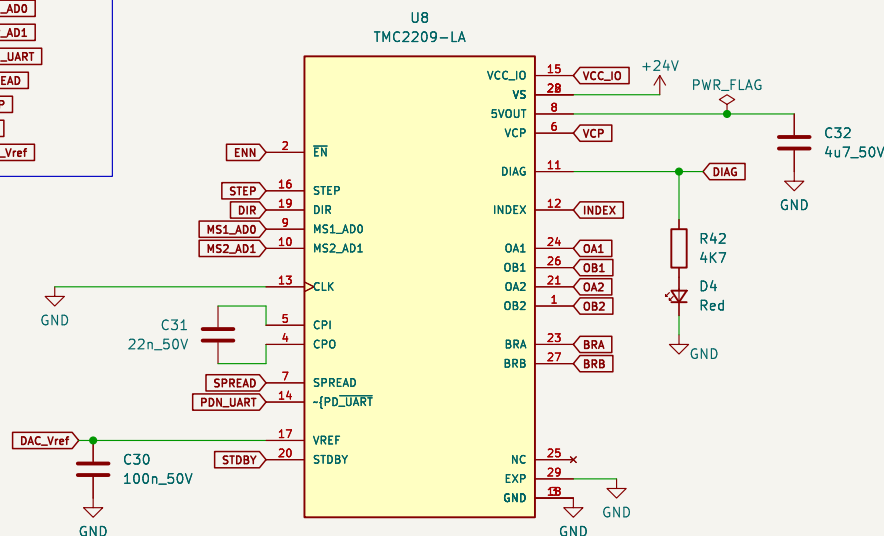
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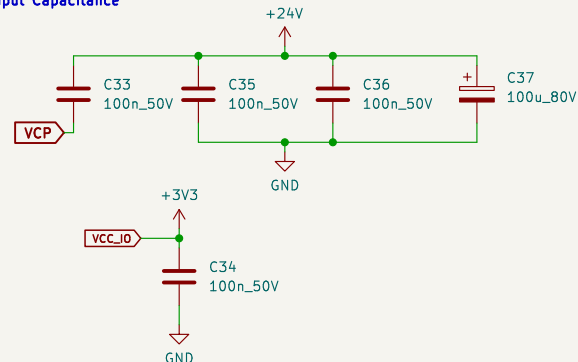
Input



STDBY_TMC2209D<STDBY_TMC2209
 ENN_TMC2209D<ENN_TMC2209
 MS1_AD0D<MS1_AD0
 MS1_AD1D<MS2_AD1
 PDN_UARTD<PDN_UART
 SPREADD<SPREAD
 STEPDD<STEP
 DIRD<DIR
 DAC_VrefD<DAC_Vref



Input Capacitance



Output

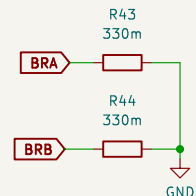
OA1>OA1
 OB1>OB1
 OA2>OA2
 OB2>OB2
 DIAG>DIAG
 INDEX>INDEX

Sense Resistor

Sense resistors should be carefully selected. The full motor current flows through the sense resistors. Due to chopper operation the sense resistors see pulsed current from the MOSFET bridges. Therefore, a low-inductance type such as film or composition resistors is required to prevent voltage spikes causing ringing on the sense voltage inputs leading to unstable measurement results. Also, a low-inductance, low-resistance PCB layout is essential. Any common GND path for the two sense resistors must be avoided, because this would lead to coupling between the two current sense signals. A massive ground plane is best.

The sense resistor needs to be able to conduct the peak motor coil current in motor standstill conditions, unless standby power is reduced. Under normal conditions, the sense resistor conducts less than the coil RMS current, because no current flows through the sense resistor during the slow decay phases. A 0.5W type is sufficient for most applications up to 1.2A RMS current.

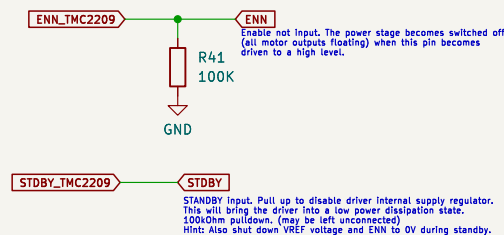
Be sure to use a symmetrical sense resistor layout and short and straight sense resistor traces of identical length. Well matching sense resistors ensure best performance. A compact layout with massive ground plane is best to avoid parasitic resistance effects.



According to the datasheet:
 330mΩ resistor results in 0.66A max motor current

Low Power Standby

Battery powered applications, and mains powered applications conforming to standby energy saving rules, often require a standby operation, where the power-supply remains on, but current draw goes down to a low value. The TMC2209/2226 support standby operation of roughly 2mW (at 12V supply), or <1mW at 5V supply using a dedicated pin STANDBY. Pull up STANDBY to VCC_IO to go to low power standby. VCC_IO may be dropped down to 1.5V during standby. A high level on STANDBY will disable the internal 5V regulator and at the same time switches off all internal units. Prior to going to STANDBY, stop the motor, and allow it to enter standstill current, or switch off the motor completely. When in STANDBY, inputs ENN and VREF have to be driven to a low level, VCC_IO shall remain active. In standby mode, All driver registers are reset to their power-up defaults after leaving standby mode.



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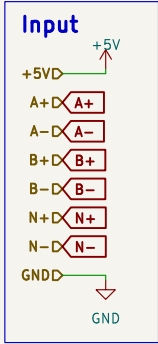
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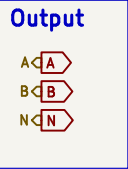
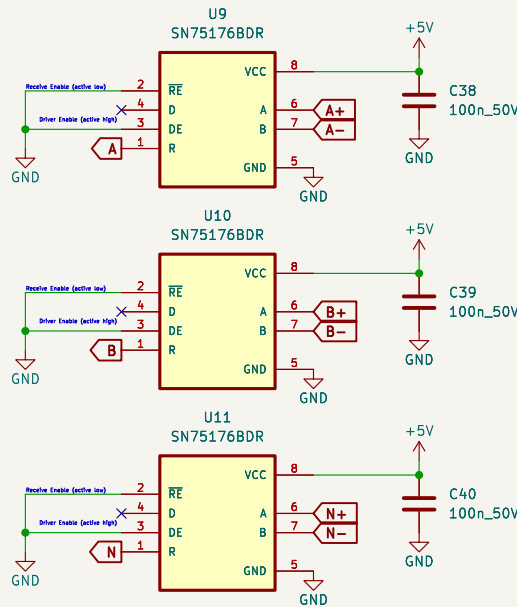
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Differential Line Receiver



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