

# Piano Tuning Method

Zuheng Kang

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## ABSTRACT

*Since the piano string is consider to be a stick rather than a pure ideal string, it contains stiffness and its harmonics will shift in such way that make piano tuning a difficult work. In this work, the method of the optimization algorithm similar to Tunelab®, however, construct and developed all by the author. The algorithm is divided into several models that using various fitting technique to construct model functions, and finally convert to linear regression problem for optimization. Finally, the piano tuning curve is constructed and final tuning frequencies are calculated. In addition, more functions is introduced, such as the different temperament tuning.*

**Keyword:** piano tuning, Tunelab®, inharmonicity, optimization

**Project Location**

Reference [2]

# 1 INTRODUCTION

Piano tuning is a difficult work since the harmonics shift that make the piano hard to tune, and tuning process will be a task to highly reduce the audible cacophonous. There are several factors we need to consider, which the rule of harmony is.

- The cacophonous created by its base frequency and audible harmonics; a good tuning will largely reduce the inharmonic for harmonies (the frequency domain will greatly coincide).
- The inner music scales related pitch; the odd pitch tuning will result in the weird sound when playing music scales.

Other famous related works are:

- Tunelab (closed source; has trial version)
- Keyburn CyberTuner (closed source; no trial version)
- Entropy Piano Tuner (open source) [1]

The first two are similar, which represent the old tuning techniques, and my work mostly focus on this algorithm. Since it is closed source, I guessed their tuning method and create a similar solution, and will be shown in this article.

As for Entropy Piano Tuner, it represent the new way of piano tuning, however I heard its demo of tuning, I found that it contain two major deficiencies:

- It violate the second rule of harmony – inner scales sound weird.
- It only consider the sound which at the certain striking level of piano keys, which result in the optimization of keys are based only on sampling striking level.

In my work, I will guess the algorithm and model it in the similar way of optimization. Besides, I used more accurate model for inharmonicity coefficients.

In this article, the first part is to introduce the background of knowledge for higher level modeling algorithms. The second part is to introduce my piano modeling and tuning optimization method. Finally, the future work will be introduce and followed a conclusion.

## 2 BACKGROUND KNOWLEDGE

### 2.1 Key Names

The left most key name is defined as “A0”, where “A” is the note name, 0 is the scale number. “C” is the starting point of one scale. It only allowed sharp in the note, flat is not allowed in this naming format.

*A0, A#0, B0, C1, C#1, ..., B1, C2, ..., B7, C8*

There are 88 keys for standard piano.

### 2.2 Key Numbers

In the real world, the piano key will labeled with numbers when the piano is open and machine part is shown off.

A0 key is labeled to be 1, and C8 is 88.

However, in my program, A0 key is labeled as 0 for easier calculation, which is defined as  $k$ .

## 2.3 Functions

Frequency ratio to cents function:

$$Fr_{\rightarrow c}(\gamma) = 1200 \log_2(\gamma) \quad (2.1)$$

Where cents is from 12 equal temperament, each half note has 100 point, named cents.

Frequency add cents (pitch) function:

$$F_{+c}(f, c) = f \cdot 2^{\left(\frac{c}{1200}\right)} \quad (3.1)$$

This function returns the frequency that added the pitch (cents)  $c$ .

The ideal frequency for the key  $k$  is:

$$\tilde{f}_k = 440 \cdot 2^{\left(\frac{k-48}{12}\right)} \quad (3.2)$$

Where 440Hz is the international standard pitch for “A4”. Other tuning standard will replace this number, 48 is the key number for “A4”.

## 3 METHOD

### 3.1 Sampling Piano

Before tuning a piano, we need to sample a piano by recording the piano keys sound audios. This process will roughly or precisely measure the inharmonicity of piano strings (which will talk about later), such that we could model the inharmonicity for the target piano.

The sampling is suggested to measure keys “C1”, “C2”, “C3”, “C4”, “C5” (and probably “C6”; user could record more piano keys such as “A1” ~ “A6” for better result). The piano key sound should be recorded in a quiet environment, which allows more accuracy for later frequency analysis.

In my program, I use fully or almost fully sampled piano for research purposes.

### 3.2 Audio Processing

Since the real audio may contains the white space at the start or the end, and the sound length varies. I use this method to process my sampled audio:

- Normalize ( $N(x) = x / \max(x)$ ) the audio file into 1, then, find the peak volume of audio, and start from here.
- Slice these audio pieces into tiny partitions, say 0.1 second is one partition. The maximum number of each partition will be its assumed volume at this time point.
- Select these pieces volume start from some large number to small number – since piano sound is loud from its beginning and decay by the time. Say from 90% to 2% of the sampled sound audio.

### 3.3 Frequency Analysis

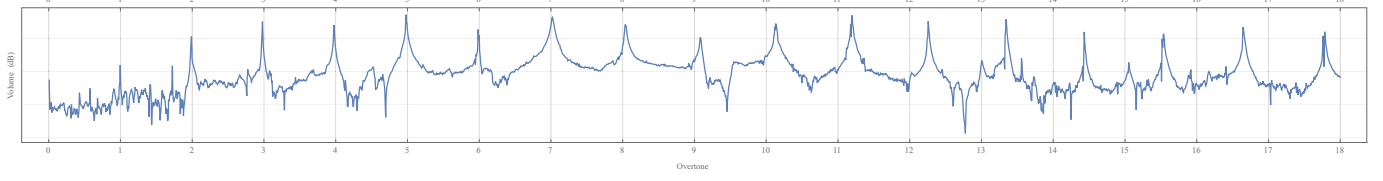


Figure 3-1 “A#0” Key (at Upright Piano Samples) Overtone Plot; Volume at Logarithm Scale

Then, put this audio samples into fourier analysis (FFT algorithm). Then we get the function  $G(\omega) = FFT(S(t))$  where  $S(t)$  is the audio function, and  $G(\omega)$  is the frequency domain function. In our work, the frequency domain is converted to the ratio to its ideal fundamental frequency, thus we can see the Figure 3-1, the peaks will always almost lies in the grid by dividing its ideal frequency.

From Figure 3-1, we can see that the higher overtone (right hand side peaks with larger numbers) shifts higher.

It is a problem to capture all these peaks numbers, since some are not clear: the fundamental frequency (at 1), and some has multiple peaks: at 15 ~ 16.

In my work, I use the frequency *Catchup Method* to get octave values for all these peaks.

### 3.4 Catchup Overtone

From the charactors of these peaks, there are several charactors will be considered:

- From left to right, the gap between two peaks are increasing gradually.
- The largest value of this plot is probably some peak of overtone
- The valid peak should be nearly larger than fundamental frequency position: at 1.
- The peak may be broken into several peaks, we need centralize the targeted position.

From this characteristics, the *Catchup Method* could be built:

- Analyze the frequency samples which roughly larger than 1 (my program is starting from 0.8), get the peak frequency  $f_{k,peak}$  at key number  $k$ .
- Comparing with ideal frequency  $\tilde{f}_k$ . We can then assume that it is  $n = round(f_{k,peak} / \tilde{f}_k)$  harmonics.

Then, we can know its guessed fundamental frequency is  $\hat{f}_k = f_{k,peak} / n$ . Then, this should be the step size for catchup method.

- The catchup method is forward (goes to the right), and the backward (goes to the left). If we are in the forward operation, the next guessed target frequency is  $\hat{f}_{k,peak+1} = f_{k,peak} + f'_k$ , where  $f'_k$  is the assumed gap between two peak at this position. In the first try, we set this number to  $f'_k = \hat{f}_k$ , and this number will be increasing for more right harmonics. Then, we get the around data (in a relatively small area) for guessed target frequency  $\hat{f}_{k,peak+1} \pm \delta$ , we can find its maximum number these data to be the frequency candidate  $\hat{f}_{k,peak+1}^{candidate}$ , then we get the data of smaller surround area  $\hat{f}_{k,peak+1}^{candidate} \pm \delta'$  where  $\delta' \ll \delta$ . Then, we calculate the weighted average for this smaller area, and the result is the actual frequency of this peak

$f_{k,peak+1} = \int_{-\delta'}^{\delta'} \omega \cdot G(\hat{f}_{k,peak+1}^{candidate}) d\omega$ , where  $\omega$  is proportional to frequency. Then, the assumed gap between two peak at this step is updated to be  $f'_k = f_{k,peak+1} - f_{k,peak}$ .

- Iterate this method for forward catchup to get all higher frequencies.
- If the highest peak is not fundamental frequency, we will perform the backward catchup. Since there are less peaks and the overtone shift will be far less than the right, the assumed targeted gap between two peaks is set to be the assumed fundamental frequency  $\hat{f}_k$ .

From this method, we can get a overtone (frequency) list for the key  $k$ . Which is:

$$k \rightarrow \{f_{k,1}, f_{k,2}, \dots\} \quad (3.3)$$

### 3.5 Inharmonicity Model

From reference [1], we assume that the piano string is a bar, which follows the partial differential equation:

$$\ddot{y} \propto -y'' - \varepsilon y'''' \quad (3.4)$$

Where  $y$  is the special position of piano string (bar model). The prime is the derivative to spatial domain, and dots is the derivative to time domain.

Then, use the modal analysis and solved the natural frequencies for this string are:

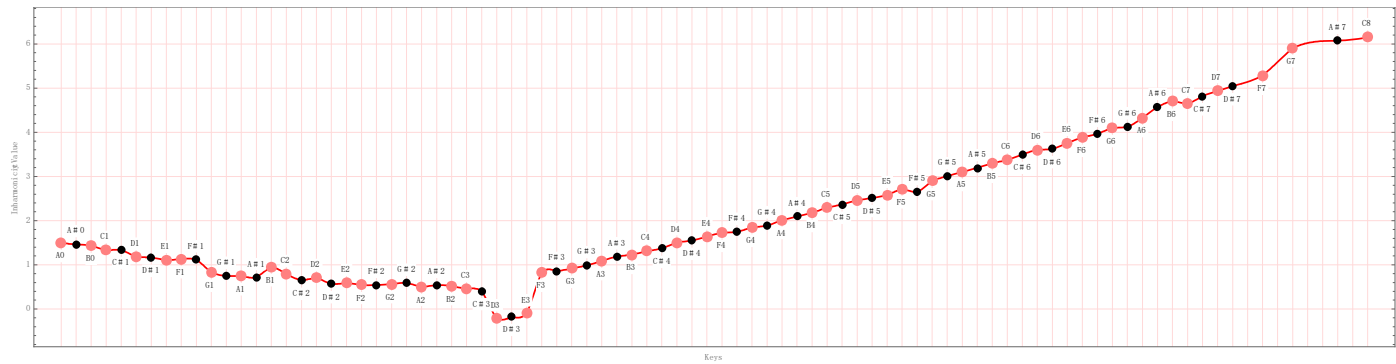
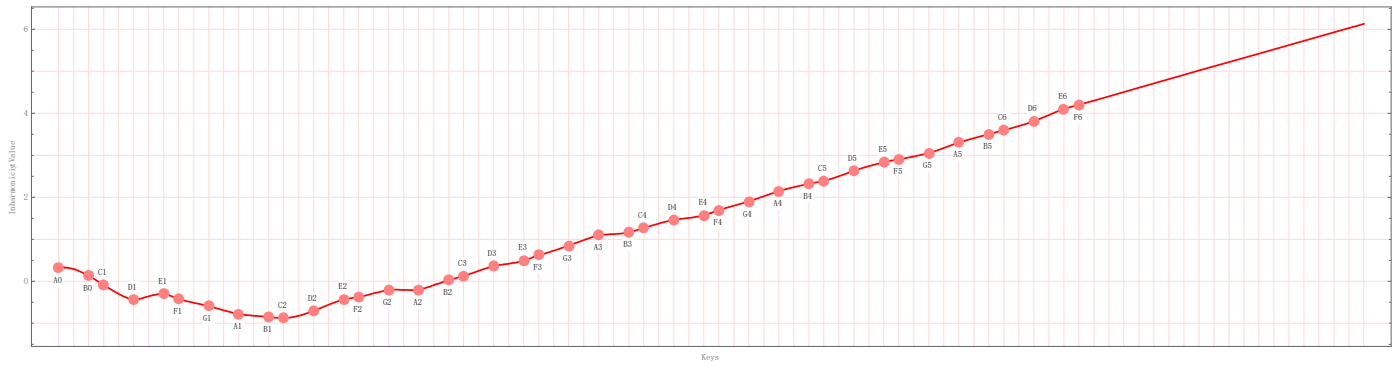
$$f_{k,n} \propto n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \Rightarrow f_{k,n} = A_k \cdot n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \quad (3.5)$$

Here we have two unknown variables.

Then, we use this function to fit all frequency results at Eq.(3.3). Since  $A_k$  value is always almost 1 all the time, we can ignore this number, and focus only on  $B_k$ . However in the optimization process, with parameter  $A_k$  could achieve much better result, although finally its value is almost 1. We set 0 to be the fundamental frequency is that when  $n = 0$  that the equation holds, we will restore this number later.

Then, we can get inharmonicity parameter list  $\{\{k, B_k\}\}$ .

From my observation, the logarithm of this number has some beautiful properties with the data  $\{\{k, \ln(s \cdot B_k)\}\}$ , where  $s$  is a scaling parameter (I set to 10000).



From Figure 3-2 and Figure 3-3, we can clearly see the line is divided into 2 parts.



Figure 3-4 Grand Piano String Arrangement



Figure 3-5 Upright Piano String Arrangement

From Figure 3-4 and Figure 3-5, we can clearly see that the string is divided into two parts, the steel string and copper string (may be covered by silver for highly expensive pianos). The upright piano has more copper strings since the steel string cannot go longer, and the string will become thicker to make the string vibrate slower. From spring vibration formula:

$$\omega = \sqrt{\frac{K}{m}} \quad (3.6)$$

Where  $\omega$  is proportional to frequency,  $m$  is the mass of spring,  $K$  is the stiffness of spring.

When  $m$  increases,  $K$  increase a little bit,  $\omega$  decreases, then frequency decrease.

Since the piano cannot grow longer, it becomes thick and more like a stick rather than an ideal string. For higher notes strings, it is too short, and the thickness becomes relatively larger comparing to its length, thus it is more likely to be a bar.

Thus, from the plot, we can see the inharmonicity increases at two ends, and break at the position of separation of two kinds of strings.

Since grand concert piano is longer, and can have more steel strings, less copper strings, thus the break will become more left side.

The figure of inharmonicity plot also tells us that two separate lines are almost linear. In my model, I used the valid sampled points are modeled with interpolation function, and two edges are modeled with linear function, and the method is shown below.

We get several samples from one line, and fit in a linear form.

Get its slope, and build a line which passes the right end point (since I will not wish to have a break for the interpolation function), and add some samples for edges situation to sample pool.

Similar to the left hand side.

We use interpolation for these samples of sample pool – “Left hand side + samples + right hand side”, which is our final model for inharmonicity model function  $Ih(k)$ .

Thus, we can have the modeled parameter  $B_k$  with:

$$B_k = e^{\frac{Ih(k)}{s}} \quad (3.7)$$

Then, the frequencies  $\tau(k, n)$  will be:

$$\tau(k, n) = f_{k,1} \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \quad (3.8)$$

Where  $f_{k,1}$  is currently unknown but it will be eliminated.

### 3.6 Tuning Curve Optimization Model

Similar to Tunelab, I set the tuning optimization method to separate the lower tones (bass) and higher tones (tenor) into two tuning target optimization method, the separation point  $k_0$  is “C#4/D4”. And the default tuning method for bass is to set 6:3. Since  $6/3=2$  ( $a/b$ ), this frequency ratio is  $\gamma = a/b$ , and its corresponding pitch range is  $Fr_{\rightarrow c}(\gamma)$  which is 1200, and 1200 is an octave, it means the tone say “A0”’s 6<sup>th</sup> harmonics will largely match its octave’s “A1”’s 3<sup>rd</sup> harmonics.

Here pitch is defined by cents.

The error function  $\varepsilon_k$  is defined as:

$$\begin{aligned} \varepsilon_k &= Fr_{\rightarrow c} \left( \frac{\tau(k, a)}{\tau(k + Fr_{\rightarrow c}(a/b), b)} \right) \\ &= Fr_{\rightarrow c} \left( \sqrt{\frac{1 + B_k \cdot a^2}{1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2}} \cdot \frac{a}{b} \right) \end{aligned} \quad (3.9)$$

We can do this for all bass strings.

For tenor strings, the default tuning method is set to 4:1 ( $c/d$ ). But this time we count the higher note as the target to calculate.

$$\varepsilon_k = Fr_{\rightarrow c} \left( \sqrt{\frac{1 + B_{k-Fr_{\rightarrow c}(c/d)} \cdot c^2}{1 + B_k \cdot d^2}} \cdot \frac{c}{d} \right) \quad (3.10)$$

The combined expression is:

$$E(k) = \begin{cases} Fr_{\rightarrow c} \left( \sqrt{\frac{1 + B_k \cdot a^2}{1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2}} \cdot \frac{a}{b} \right) & k \leq k_0 \\ Fr_{\rightarrow c} \left( \sqrt{\frac{1 + B_{k-Fr_{\rightarrow c}(c/d)} \cdot c^2}{1 + B_k \cdot d^2}} \cdot \frac{c}{d} \right) & k > k_0 \end{cases} \quad (3.11)$$



From this equation, we can see  $E(k)$  is only a value for calculation.

From this point, we need a function to largely eliminate these errors. The piano tuning curve  $C(k)$  is introduced.

The cost function for optimization is:

$$J(k) = \sum_k (C(k) - E(k))^2 \quad (3.12)$$

Which minimize the square error of these functions.

Here I use polynomial for easier calculation:

$$C(x) = \sum_{i=1}^n c_i \cdot x^i \quad (3.13)$$

Since  $C(x)$  will pass the fix point, which is “A4” pitch at 440Hz frequency at pitch deviation of 0, thus  $i$  is from 1 and  $x = k - k_{A4}$ , where  $k_{A4}$  is the key number (index) at “A4”.

Thus,  $J(k)$  is the second order polynomial function, which is very easy to minimize by linear regression method to calculate the fitting parameter  $\{c_i\}$ , and rebuild the functions.

Then, we can bring it to the  $J(k)$  function to calculate its deviations.

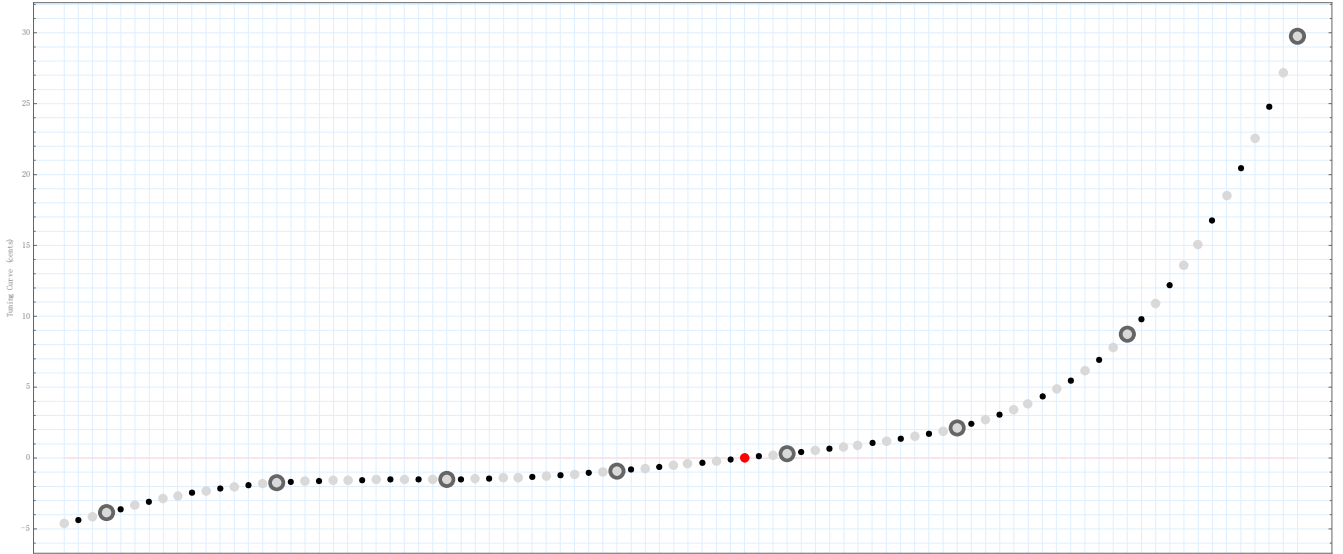


Figure 3-6  $C(x)$  for Grand Piano

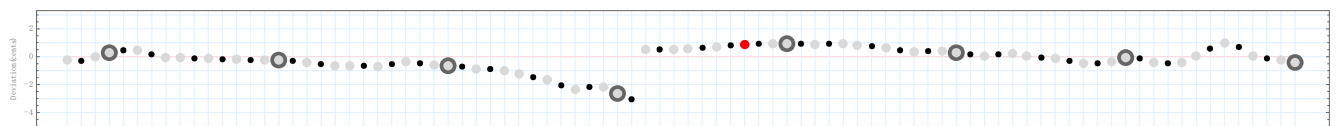


Figure 3-7  $J(x)$  for Grand Piano

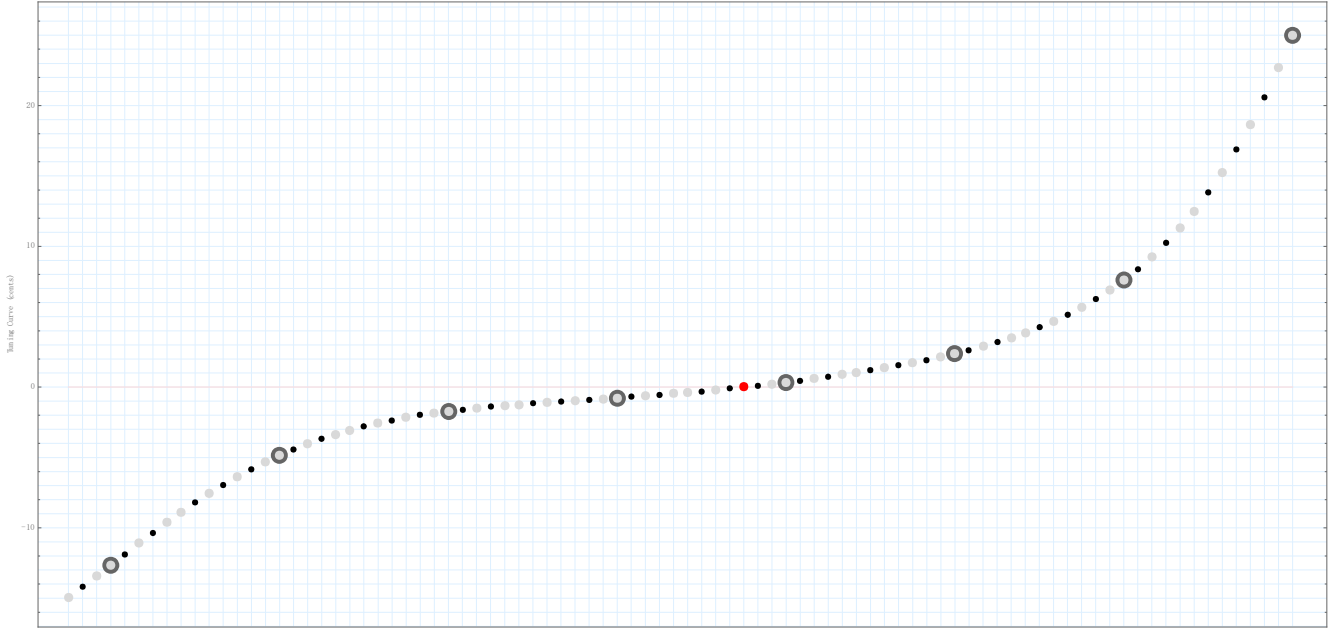


Figure 3-8  $C(x)$  for Upright Piano

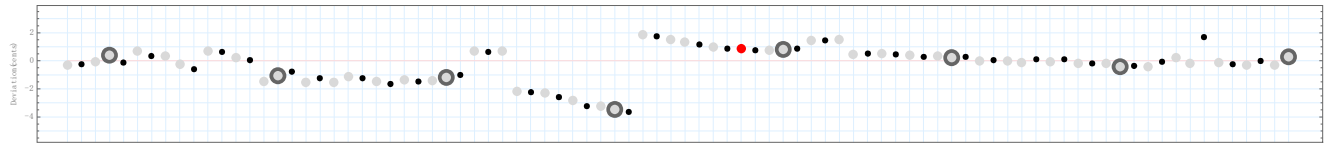


Figure 3-9  $J(x)$  for Upright Piano

The result of two piano is shown above. Horizontal axis is the key number, and the vertical axis the pitch deviation with idea frequencies represented by cents.

From this tuning method, we can see that the bass tuning will consider the deviations from the tenor part, and vice versa, and the effect are inner related. Thus this tuning method is theoretically to optimize almost the whole piano keys tuning.

### 3.7 Temperament Model

With the development of music, various temperament appears and create unique flavor of music. The temperament model is using the pitch deviation tables of different temperament (the unit is cent). We can then create the non 12 equal temperament tuning strategy. The temperament function is defined to be  $T(k)$ .

The tuning table such as “Bach - Bradley Lehman” is:

C	C#	D	D#	E	F	F#	G	G#	A	A#	B
5.87	3.91	1.96	3.91	-1.96	7.82	1.96	3.91	3.81	0	3.91	0

Table 3-1 Table for “Bach - Bradley Lehman” Temperament

Where A note will always be 0 since A is the reference frequency and will always keep to 440 Hz (if is standard situation).

This table shows the situation of “C” major.

The other major tuning will follow the rotation of table. For example: if tuning “D” major, the “D” will rotate to current “D”  $\rightarrow$  “C” place, which is rotating left 2 times. However, we will make sure “A” note will always be 0, then, we can subtract the number at “B”  $\rightarrow$  “A” to make it possible.

Then, add these pitch errors to all the notes of tuning, the modified tuning curve is:

$$C'(k) = C(k) + T(k) \quad (3.14)$$

### 3.8 Creating Tuning Table

The final tuning frequency  $\tau(k, n)$  is:

$$f_{k,1} = F_{+c}(\hat{f}_k, C'(k)) \quad (3.15)$$

$$\begin{aligned} \tau(k, n) &= f_{k,1} \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \\ &= F_{+c}(\hat{f}_k, C'(k)) \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \\ &= F_{+c}(\hat{f}_k, C'(k)) \cdot n \cdot \sqrt{1 + e^{\left(\frac{Ih(k)}{s}\right)}} \cdot n^2 \end{aligned} \quad (3.16)$$

From Eq.(3.16), we can see only  $C$  and  $Ih$  function is modeled function, other function are basic mathematics functions.

From the modeling, we can get a strategy of piano tuning, then we can convert this strategy into a tuning table, which shows all the frequency of fundamental and its harmonics frequencies, and corresponding deviation to ideal frequencies represented by cents.

The grand and upright piano tuning strategy is shown in Figure 7-1 and Figure 7-2.

The red font is the frequencies recommended for the devices to tune.

## 4 FUTURE WORK

Although the Entropy piano tuning method is far more advanced than this tuning method theoretically, however the jumpy tuning curve will make the music scales sound weird. If I have time, I will implement the entropy tuner with much more smooth functions, this construction is easier than original idea since the optimization at his method is only few parameters if using similar polynomial to optimize the curve to achieve more smooth result with entropy function as cost function.

Over-pull tuning is implemented experimentally with their tuning apps, and I do not know its method due to its close source reason. And I am still lack of research on this area, thus I will leave it as future work to think about. I know this effect is caused by the experimental result of the percentage that the string pins will loosen and drop the pitch, the tuner will make up the errors of this effect by over pull and tune higher tones.

## 5 CONCLUSION

This tuning method gives us a solution of piano tuning that works as well as commercial apps Tunelab. The method is presented to optimize the whole piano notes sound. Future work is given to develop maybe in the future.

## 6 REFERENCE

- [1] Hinrichsen, Haye. "Entropy-based tuning of musical instruments." *Revista brasileira de Ensino de Física* 34.2 (2012): 1-8.
- [2] Github for Piano Tuning Project [[https://github.com/RobertBoganKang/piano\\_tuning](https://github.com/RobertBoganKang/piano_tuning)]

# 7 APPENDIX

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
A0	27.4286	54.857	82.3025	109.774	137.284	164.843	192.461	220.152	247.925	275.791	303.762	331.849	360.063	388.414	416.913	445.571
A#0	29.0617	58.1273	87.2084	116.317	145.464	174.661	203.921	233.254	262.672	292.187	321.809	351.55	381.422	411.433	441.601	471.93
B0	30.7944	61.5924	92.4044	123.241	154.113	185.03	216.004	247.044	278.161	309.365	340.667	372.077	403.606	435.262	467.057	499.000
C1	32.6306	65.2641	97.9096	130.576	163.272	196.008	228.791	261.633	294.533	327.515	360.577	393.732	426.988	460.352	493.835	527.445
C#1	34.5761	69.1548	103.744	138.351	172.983	207.649	242.355	277.111	311.922	346.797	381.744	416.769	451.881	487.087	522.394	557.81
D1	36.6375	73.2773	109.926	146.592	183.281	220.01	256.758	293.559	330.412	367.324	404.301	441.35	478.478	515.693	553.001	590.408
D#1	38.8214	77.6456	116.481	155.335	194.216	233.132	272.092	311.103	350.174	389.312	428.526	467.823	507.213	546.701	586.297	626.009
E1	41.1352	82.2735	123.424	164.596	205.798	247.04	288.331	329.68	371.095	412.587	454.164	495.835	537.609	579.494	621.501	663.638
F1	43.5865	87.1758	130.777	174.398	218.047	261.74	305.466	349.253	393.103	437.024	481.025	525.114	569.3	613.592	657.996	702.523
F#1	46.1833	92.3694	138.567	184.783	231.027	277.308	323.632	370.009	416.447	462.954	509.538	556.208	602.972	649.837	696.812	743.905
G1	48.9343	97.8713	146.819	195.786	244.78	293.809	342.882	392.006	441.19	490.441	539.768	589.179	638.681	688.284	737.994	787.82
G#1	51.8485	103.7	155.561	207.441	259.347	311.286	363.267	415.297	467.385	519.537	571.762	624.067	676.46	728.949	781.541	834.243
A1	54.9357	109.874	164.822	219.788	274.779	329.803	384.868	439.98	495.147	550.378	605.678	661.057	716.521	772.078	827.735	883.499
A#1	58.2061	116.415	174.634	232.87	291.133	349.429	407.765	466.151	524.593	583.098	641.676	700.332	759.076	817.914	876.833	935.902
B1	61.6705	123.344	187.027	246.729	308.458	370.221	432.026	492.882	555.795	617.774	679.827	741.962	804.187	866.504	928.935	991.474
C2	65.3494	130.684	196.038	261.411	325.255	392.249	457.725	523.255	588.845	654.503	720.237	786.054	851.963	917.973	984.09	1050.32
C#2	69.2282	138.459	207.703	276.968	346.263	415.598	484.982	554.423	623.932	693.516	763.186	832.949	902.816	972.793	1042.9	1113.13
D2	73.3688	146.697	220.162	293.452	366.879	440.352	513.884	587.484	661.164	734.934	808.806	882.789	956.895	1031.1	1105.52	1180.06
D#2	77.7098	155.424	233.156	310.919	388.727	466.593	544.53	622.551	700.671	778.901	857.256	935.748	1014.39	1093.2	1172.18	1251.35
E2	82.3139	164.669	247.028	329.424	411.874	494.393	576.997	659.704	742.527	825.484	908.59	991.861	1075.31	1158.99	1242.82	1326.91
F2	87.2286	174.463	261.227	343.022	436.382	523.82	611.353	698.999	786.777	874.703	962.797	1051.07	1139.55	1228.25	1317.19	1406.38
F#2	92.4162	184.839	277.29	369.789	462.358	555.016	647.786	740.686	833.739	926.964	1020.38	1114.01	1207.88	1302	1396.39	1491.08
G2	97.912	195.832	293.784	391.792	489.88	588.072	686.392	784.864	883.511	982.358	1081.43	1180.74	1280.33	1380.19	1480.41	1580.94
G#2	103.734	207.477	311.254	415.09	519.01	623.04	727.205	831.531	936.041	1040.76	1145.72	1250.93	1356.43	1462.25	1568.39	1674.89
A2	109.903	219.815	329.763	439.774	549.875	660.092	770.453	880.984	991.712	1102.66	1213.86	1325.34	1437.12	1549.23	1661.7	1774.54
A#2	116.439	232.888	343.38	455.946	568.618	680.428	792.486	904.589	1016.53	1128.65	1240.95	1353.53	1466.39	1579.55	1693.02	1806.79
B2	123.363	246.739	361.186	474.682	587.325	697.135	807.134	917.38	1027.88	1138.63	1249.68	1360.93	1472.37	1583.99	1695.88	1808.05
C3	130.746	261.414	392.362	523.065	634.091	745.308	856.714	968.318	1080.16	1192.16	1304.38	1416.81	1529.45	1642.28	1755.3	1868.53
C#3	138.473	276.963	415.024	554.21	665.036	776.353	887.968	1000.58	1113.35	1226.38	1339.68	1453.25	1567.08	1681.13	1795.45	1910.04
D3	146.708	293.438	442.252	587.215	704.39	821.84	939.61	1057.78	1176.25	1295.02	1414.16	1533.65	1653.36	1773.29	1893.55	2014.36
D#3	155.434	310.892	466.445	622.163	738.17	856.47	975.18	1094.3	1213.83	1333.76	1454.14	1575.02	1696.41	1818.41	1940.99	2064.16
E3	164.68	329.387	494.201	659.294	824.475	990.094	1156.14	1322.7	1489.84	1657.65	1826.2	1995.58	2165.85	2337.1	2509.4	2682.82
F3	174.476	348.985	523.625	698.494	873.69	1049.31	1225.45	1402.21	1579.68	1757.97	1937.16	2117.34	2298.62	2481.05	2664.82	2849.92
F#3	184.856	369.751	554.802	740.123	925.833	1112.05	1298.88	1486.44	1674.85	1864.22	2054.67	2246.29	2439.21	2633.53	2829.36	3026.8
G3	195.854	391.754	587.837	784.239	981.097	1178.55	1376.72	1575.76	1775.8	1976.96	2179.38	2383.19	2588.52	2795.49	3004.23	3214.86
G#3	207.508	415.071	625.855	831.028	1039.75	1249.2	1459.52	1670.89	1883.47	2097.42	2312.88	2530.03	2749.02	2969.99	3193.1	3418.49
A3	219.855	439.774	659.661	880.607	1101.91	1324.07	1547.28	1771.73	2000.67	2225.12	2454.44	2685.76	2919.25	3155.08	3393.47	3634.56
A#3	232.938	465.948	699.244	933.042	1167.55	1402.99	1639.57	1877.5	2116.99	2358.24	2601.45	2846.83	3094.57	3344.87	3597.91	3853.89
B3	246.8	493.68	740.874	988.619	1237.15	1486.7	1737.5	1989.79	2243.79	2499.72	2757.81	3018.28	3281.34	3547.21	3816.1	4088.2
C4	261.89	523.071	785.024	1043.63	1311.16	1575.9	1842.11	2108.108	2380.06	2652.32	2927.13	3204.74	3485.4	3769.36	4056.87	4348.15
C#4	277.052	548.213	831.839	1110.18	1389.63	1670.51	1953.11	2237.78	2524.81	2814.52	3107.22	3403.21	3702.77	4006.19	4313.77	4625.77
D4	293.542	587.211	881.389	1176.79	1472.79	1770.76	2070.75	2372.12	2678.24	2986.46	3298.14	3613.62	3933.24	4257.32	4586.2	4920.18
D#4	311.014	622.169	933.886	1246.58	1560.68	1876.59	2194.73	2515.5	2839.3	3166.53	3497.58	3832.82	4172.62	4517.03	4867.37	5223.01
E4	329.327	659.213	988.532	1320.96	1653.96	1989.01	2326.56	2667.08	3011.02	3358.81	3710.89	4067.7	4429.63	4797.1	5170.51	5550.23
F4	349.143	698.475	1048.57	1399.99	1753.3	2109.07	2467.84	2830.16	3209.57	3597.59	3943.74	4325.53	4713.44	5107.95	5509.32	5918.6
F#4	369.926	740.676	1111.12	1483.73	1858.56	2236.27	2617.52	3002.94	3393.15	3788.78	4190.43	4598.67	5014.07	5437.19	5862.6	6308.67
G4	391.947	784.156	1177.41	1572.5	1970.19	2371.26	2776.45	3186.53	3602.21	4024.21	4453.22	4889.93	5334.97	5788.99	6252.59	6726.36
A4	415.279	830.873	1247.72	1666.77	2088.95	2515.18	2946.36	3383.38	3827.12	4278.41	4738.09	5206.93	5685.72	6175.18	6676.03	7188.93
A#4	440.181	880.377	1322.26	1766.77	2215.07	2668.12	3127.13	3593.11	4067.1	4550.09	5043.04	5546.89	6062.53	6590.82	7132.57	7688.56
B4	466.193	932.825	1401.21	1872.66	2348.47	2829.92	3318.25	3814.69	4320.43	4836.61	5364.35	5904.71	6458.7	7027.31	7611.45	8212.1
C5	493.549	988.395	1484.86	1984.84	2489.81	3001.25	3520.57	4049.18	4588.42	5139.6	5703.97	6282.74	6877.05	7487.99	8116.59	8763.83
C#5	523.35	1047.27	1573.47	2103.65	2639.48	3182.62	3734.68	4297.22	4864.71	5459.78	6062.67	6681.76	7318.34	7973.61	8648.72	9344.72
D5	554.506	1109.69	1657.37	2230.16	2799.45	3360.63	3955.83	4566.67	5181.76	5812.5	6460.81	7128.15	7815.97	8525.65	9258.48	10015.7
D#5	587.517	1175.85	1767.44	2364.71	2970.04	3585.77	4214.16	4857.41	5517.02	6196.79	6896.82	7619.53	8366.58	9139.57	9939.97	10769.1
E5	622.494	1245.95	1873.26	2507.29	3150.84	3806.66	4477.41	5165.65	5873.82	6604.25	7359.12	8140.49	8950.28	9790.28	10662.1	11567.4
F5	659.556	1320.23	1985.4	2658.37	3342.42	4040.72	4756.35	5492.24	6251.21	7035.89	7848.76	8692.16	9568.23	10479.8	11426.2	12411.6
F#5	698.626	1398.93	2124.14	2818.23	3544.91	4287.78	5050.32	5835.84	6647.49	7488.23	8360.61	9267.83	10211.7	11194.5	12218.3	13284.9
G5	740.438	1484.182	2229.99	2987.71	3759.68	4549.97	5362.48	6200.93	7068.83	7969.49	8905.97	9881.1	10897.5	11957.6	13063.6	14217.3
G#5	784.331	1570.17	2363.53	3167.86	3988.49	4830.05	5696.99	6593.51	7523.57	8490.88	9498.86	10550.7	11649.2	12797.7	13966.5	15249.9
A5	831.267	1674.5	2550.67	3360.63	4235.08	5134.52	6064.18	7029.02	8033.64	9124.87	10292.31	11327.2	12530.2	13790.9	15111.9	16548.9
A#5	880.772	1763.94	2656.67	3566.01	4498.8	5461.59</										

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A0	27.2634	-13.522	54.5391	-13.522	81.8635	-13.522	109.272	-13.522	136.805	-13.522	164.403	-13.522	192.376	-13.522	220.487	-13.522	248.861	-13.522	277.533	-13.522	306.537	-13.522	335.905	-13.522	365.67	-13.522	395.657	-13.522	425.957	-13.522	456.514	-13.522	487.337	-13.522	518.427	-13.522	549.782	-13.522	581.403	-13.522	613.291	-13.522	645.446	-13.522	677.869	-13.522	710.561	-13.522	743.531	-13.522	776.779	-13.522	810.306	-13.522	844.113	-13.522	878.201	-13.522	912.571	-13.522	947.224	-13.522	982.161	-13.522	1017.383	-13.522	1052.892	-13.522	1088.689	-13.522	1124.774	-13.522	1161.148	-13.522	1197.811	-13.522	1234.764	-13.522	1272.007	-13.522	1309.541	-13.522	1347.365	-13.522	1385.479	-13.522	1423.884	-13.522	1462.581	-13.522	1501.561	-13.522	1540.825	-13.522	1580.374	-13.522	1620.209	-13.522	1660.331	-13.522	1700.741	-13.522	1741.441	-13.522	1782.431	-13.522	1823.711	-13.522	1865.282	-13.522	1907.145	-13.522	1949.301	-13.522	1991.75	-13.522	2034.496	-13.522	2077.533	-13.522	2120.864	-13.522	2164.491	-13.522	2208.415	-13.522	2252.637	-13.522	2297.158	-13.522	2341.979	-13.522	2387.101	-13.522	2432.524	-13.522	2478.25	-13.522	2524.283	-13.522	2570.617	-13.522	2617.257	-13.522	2664.203	-13.522	2711.456	-13.522	2759.017	-13.522	2806.786	-13.522	2854.864	-13.522	2903.252	-13.522	2951.95	-13.522	3000.969	-13.522	3050.299	-13.522	3099.946	-13.522	3149.901	-13.522	3199.166	-13.522	3248.742	-13.522	3298.629	-13.522	3348.828	-13.522	3399.339	-13.522	3449.163	-13.522	3499.301	-13.522	3549.754	-13.522	3600.523	-13.522	3651.607	-13.522	3702.997	-13.522	3754.694	-13.522	3806.699	-13.522	3859.014	-13.522	3911.639	-13.522	3964.575	-13.522	4017.822	-13.522	4071.381	-13.522	4125.244	-13.522	4179.412	-13.522	4233.885	-13.522	4288.664	-13.522	4343.75	-13.522	4399.151	-13.522	4454.855	-13.522	4510.868	-13.522	4567.191	-13.522	4623.825	-13.522	4680.769	-13.522	4738.024	-13.522	4795.591	-13.522	4853.461	-13.522	4911.635	-13.522	4970.114	-13.522	5028.9	-13.522	5088.0	-13.522	5147.405	-13.522	5207.117	-13.522	5267.137	-13.522	5327.465	-13.522	5388.102	-13.522	5449.049	-13.522	5510.307	-13.522	5571.876	-13.522	5633.757	-13.522	5695.951	-13.522	5758.459	-13.522	5821.282	-13.522	5884.421	-13.522	5947.876	-13.522	6011.648	-13.522	6075.73	-13.522	6140.134	-13.522	6204.855	-13.522	6269.894	-13.522	6335.252	-13.522	6400.929	-13.522	6466.925	-13.522	6533.241	-13.522	6600.0	-13.522	6667.191	-13.522	6734.799	-13.522	6802.825	-13.522	6871.269	-13.522	6940.134	-13.522	7009.419	-13.522	7079.124	-13.522	7149.25	-13.522	7219.799	-13.522	7290.764	-13.522	7362.149	-13.522	7433.954	-13.522	7506.189	-13.522	7578.844	-13.522	7651.919	-13.522	7725.415	-13.522	7799.332	-13.522	7873.67	-13.522	7948.435	-13.522	8023.619	-13.522	8099.229	-13.522	8175.264	-13.522	8251.725	-13.522	8328.612	-13.522	8405.925	-13.522	8483.665	-13.522	8561.834	-13.522	8640.433	-13.522	8719.462	-13.522	8798.921	-13.522	8878.801	-13.522	8959.102	-13.522	9039.825	-13.522	9120.969	-13.522	9202.534	-13.522	9284.529	-13.522	9366.954	-13.522	9449.81	-13.522	9533.097	-13.522	9616.716	-13.522	9699.769	-13.522	9783.256	-13.522	9867.179	-13.522	9951.537	-13.522	10036.33	-13.522	10121.569	-13.522	10207.244	-13.522	10293.359	-13.522	10379.915	-13.522	10466.922	-13.522	10554.38	-13.522	10642.299	-13.522	10730.664	-13.522	10819.479	-13.522	10908.744	-13.522	11000.0	-13.522	11091.215	-13.522	11182.879	-13.522	11274.992	-13.522	11367.555	-13.522	11460.568	-13.522	11554.031	-13.522	11647.944	-13.522	11742.307	-13.522	11837.12	-13.522	11932.385	-13.522	12028.098	-13.522	12124.261	-13.522	12220.874	-13.522	12317.937	-13.522	12415.45	-13.522	12513.419	-13.522	12611.834	-13.522	12710.799	-13.522	12810.214	-13.522	12910.079	-13.522	13010.394	-13.522	13111.159	-13.522	13212.374	-13.522	13314.039	-13.522	13416.154	-13.522	13518.719	-13.522	13621.734	-13.522	13725.2	-13.522	13829.115	-13.522	13933.52	-13.522	14038.459	-13.522	14143.924	-13.522	14249.919	-13.522	14355.444	-13.522	14461.509	-13.522	14568.114	-13.522	14675.259	-13.522	14782.944	-13.522	14890.169	-13.522	14997.934	-13.522	15096.249	-13.522	15195.114	-13.522	15294.529	-13.522	15394.494	-13.522	15494.909	-13.522	15595.874	-13.522	15697.389	-13.522	15799.444	-13.522	15902.049	-13.522	16005.204	-13.522	16108.919	-13.522	16213.184	-13.522	16318.009	-13.522	16423.384	-13.522	16529.319	-13.522	16635.814	-13.522	16742.869	-13.522	16850.484	-13.522	16958.659	-13.522	17067.394	-13.522	17176.689	-13.522	17286.544	-13.522	17396.959	-13.522	17507.934	-13.522	17619.469	-13.522	17731.564	-13.522	17844.219	-13.522	17957.434	-13.522	18071.209	-13.522	18185.544	-13.522	18300.439	-13.522	18415.884	-13.522	18531.889	-13.522	18648.444	-13.522	18765.559	-13.522	18883.234	-13.522	19001.469	-13.522	19120.264	-13.522	19239.619	-13.522	19359.534	-13.522	19479.999	-13.522	19600.024	-13.522	19720.609	-13.522	19841.754	-13.522	19963.459	-13.522	20085.724	-13.522	20208.549	-13.522	20331.924	-13.522	20456.859	-13.522	20582.344	-13.522	20708.379	-13.522	20834.954	-13.522	20962.079	-13.522	21089.754	-13.522	21217.989	-13.522	21346.774	-13.522	21476.219	-13.522	21606.324	-13.522	21737.089	-13.522	21868.514	-13.522	21999.609	-13.522	22131.264	-13.522	22263.579	-13.522	22396.544	-13.522	22530.159	-13.522	22664.424	-13.522	22800.349	-13.522	22936.924	-13.522	23073.159	-13.522	23210.044	-13.522	23347.579	-13.522	23485.764	-13.522	23624.609	-13.522	23764.104	-13.522	23904.259	-13.522	24046.074	-13.522	24188.549	-13.522	24332.674	-13.522	24479.459	-13.522	24627.894	-13.522	24777.989	-13.522	24929.734	-13.522	25083.139	-13.522	25238.194	-13.522	25394.909	-13.522	25552.274	-13.522	25711.309	-13.522	25871.994	-13.522	26034.339	-13.522	26198.334	-13.522	26363.989	-13.522	26531.304	-13.522	26700.279	-13.522	26870.914	-13.522	27043.209	-13.522	27217.154	-13.522	27392.759	-13.522	27569.024	-13.522	27746.949	-13.522	27926.524	-13.522	28107.759	-13.522	28289.644	-13.522	28473.189	-13.522	28658.394	-13.522	28845.259	-13.522	29033.784	-13.522	29223.979	-13.522	29415.834	-13.522	29609.349	-13.522	29804.524	-13.522	29959.359	-13.522	30115.844	-13.522	30273.989	-13.522	30433.794	-13.522	30595.269	-13.522	30758.404	-13.522	30923.199	-13.522	31089.654	-13.522	31257.869	-13.522	31427.744	-13.522	31599.279	-13.522	31772.464	-13.522	31946.309	-13.522	32121.814	-13.522	32297.989	-13.522	32475.834	-13.522	32655.349	-13.522	32836.524	-13.522	33019.359	-13.522	33203.844	-13.522	33389.989	-13.522	33577.794	-13.522	33767.269	-13.522	33958.404	-13.522	34151.209	-13.522	34345.674	-13.522	34541.809	-13.522	34739.604	-13.522	34939.059	-13.522	35140.174	-13.522	35342.959	-13.522	35547.404	-13.522	35753.519	-13.522	35961.294	-13.522	36170.739	-13.522	36381.844	-13.522	36594.609	-13.522	36809.034	-13.522	37025.129	-13.522	37242.884	-13.522	37462.309	-13.522	37683.394	-13.522	37905.149	-13.522	38128.564	-13.522	38353.639	-13.522	38580.374	-13.522	38808.779	-13.522	39038.844	-13.522	39270.569	-13.522	39503.954	-13.522	39739.009	-13.522	39975.724	-13.522	40214.109	-13.522	40455.254	-13.522	40698.069	-13.522	40942.544	-13.522	41188.679	-13.522	41436.474	-13.522	41685.929	-13.522	41937.044	-13.522	42189.819	-13.522	42444.254	-13.522	42690.359	-13.522	42938.124	-13.522	43187.549	-13.522	43438.634	-13.522	43690.379	-13.522	43943.784	-13.522	44198.949	-13.522	44456.774	-13.522	44717.269	-13.522	44979.424	-13.522	45243.249	-13.522	45508.734	-13.522	45775.879	-13.522	46044.684	-13.522	46315.259	-13.522	46588.494	-13.522	46863.399	-13.522	47139.974	-13.522	47418.219	-13.522	47692.134	-13.522	47972.719	-13.522	48254.974	-13.522	48533.909	-13.522	48814.524	-13.522	49096.819	-13.522	49380.804	-13.522	49667.479	-13.522	49955.834	-13.522	50245.879	-13.522	50537.604	-13.522	50831.019	-13.522	51126.114	-13.522	51422.999	-13.522	51721.674	-13.522	52013.149	-13.522	52305.414	-13.522	52609.479	-13.522	52916.344	-13.522	53225.009	-13.522	53535.474	-13.522	53847.739	-13.522	54161.804	-13.522	54477.669	-13.522	54795.334	-13.522	55114.809	-13.522	55436.084	-13.522	55759.159	-13.522	56084.034	-13.522	56410.709	-13.522	56739.174	-13.522	57069.439	-13.522	57401.504	-13.522	57735.369	-13.522	58071.034	-13.522	58408.509	-13.522	58747.784	-13.522	59088.859	-13.522	59431.734	-13.522	59776.409	-13.522	60122.884	-13.522	60481.159	-13.522	60842.234	-13.522	61205.109	-13.522	61569.784	-13.522	61936.259	-13.522	62304.534	-13.522	62674.609	-13.522	63046.484	-13.522	63420.159	-13.522	63795.634	-13.522	64172.909	-13.522	64552.984	-13.522	64935.859	-13.522	65360.534	-13.522	65787.009	-13.522	66215.284	-13.522	66645.359	-13.522	67077.234	-13.522	67510.909	-13.522	67946.384	-13.522	68393.659	-13.522	68842.734	-13.522	69293.609	-13.522	69746.284	-13.522	70200.759	-13.522	70657.034	-13.522	71115.109	-13.522	71575.984	-13.522