

Piano Tuning Method

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ABSTRACT

Since the piano string is consider to be a stick rather than a pure ideal string, it contains stiffness and its harmonics will shift in such way that make piano tuning a difficult work. In this work, the method of the optimization algorithm similar to Tunelab®, however, construct and developed all by the author. The algorithm is divided into several models that using various fitting technique to construct model functions, and finally convert to linear regression problem for optimization. Finally, the piano tuning curve is constructed and final tuning frequencies are calculated. In addition, more functions is introduced, such as the different temperament tuning.

Keyword: piano tuning, Tunelab®, inharmonicity, optimization

Project Location

Reference [2]

1 INTRODUCTION

Piano tuning is a difficult work since the harmonics shift that make the piano hard to tune, and tuning process will be a task to highly reduce the audible cacophonous. There are several factors we need to consider, which the rule of harmony is.

- The cacophonous created by its base frequency and audible harmonics; a good tuning will largely reduce the inharmonic for harmonics (the frequency domain will greatly coincide).
- The inner music scales related pitch; the odd pitch tuning will result in the weird sound when playing music scales.

Other famous related works are:

- Tunelab (closed source; has trial version)
- Rebyburn CyberTuner (closed source; no trial version)
- Entropy Piano Tuner (open source) [1]

The first two are similar, which represent the old tuning techniques, and my work mostly focus on this algorithm. Since it is closed source, I guessed their tuning method and create a similar solution, and will be shown in this article.

As for Entropy Piano Tuner, it represent the new way of piano tuning, however I heard its demo of tuning, I found that it contain two major deficiencies:

- It violate the second rule of harmony – inner scales sound weird.
- It only consider the sound which at the certain striking level of piano keys, which result in the optimization of keys are based only on sampling striking level.

In my work, I will guess the algorithm and model it in the similar way of optimization. Besides, I used more accurate model for inharmonicity coefficients.

In this article, the first part is to introduce the background of knowledge for higher level modeling algorithms. The second part is to introduce my piano modeling and tuning optimization method. Finally, the future work will be introduce and followed a conclusion.

2 BACKGROUND KNOWLEDGE

2.1 Key Names

The left most key name is defined as “A0”, where “A” is the note name, 0 is the scale number. “C” is the starting point of one scale. It only allowed sharp in the note, flat is not allowed in this naming format.

A0, A#0, B0, C1, C#1, ..., B1, C2, ..., B7, C8

There are 88 keys for standard piano.

2.2 Key Numbers

In the real world, the piano key will labeled with numbers when the piano is open and machine part is shown off.

A0 key is labeled to be 1, and C8 is 88.

However, in my program, A0 key is labeled as 0 for easier calculation, which is defined as k .

2.3 Functions

Frequency ratio to cents function:

$$Fr_{\rightarrow c}(\gamma) = 1200 \log_2(\gamma) \quad (2.1)$$

Where cents is from 12 equal temperament, each half note has 100 point, named cents.

Frequency add cents (pitch) function:

$$F_{+c}(f, c) = f \cdot 2^{\left(\frac{c}{1200}\right)} \quad (3.1)$$

This function returns the frequency that added the pitch (cents) c .

The ideal frequency for the key k is:

$$\tilde{f}_k = 440 \cdot 2^{\left(\frac{k-48}{12}\right)} \quad (3.2)$$

Where 440Hz is the international standard pitch for “A4”. Other tuning standard will replace this number, 48 is the key number for “A4”.

3 METHOD

3.1 Sampling Piano

Before tuning a piano, we need to sample a piano by recording the piano keys sound audios. This process will roughly or precisely measure the inharmonicity of piano strings (which will talk about later), such that we could model the inharmonicity for the target piano.

The sampling is suggested to measure keys “C1”, “C2”, “C3”, “C4”, “C5” (and probably “C6”; user could record more piano keys such as “A1” ~ “A6” for better result). The piano key sound should be recorded in a quiet environment, which allows more accuracy for later frequency analysis.

In my program, I use fully or almost fully sampled piano for research purposes.

3.2 Audio Processing

Since the real audio may contains the white space at the start or the end, and the sound length varies. I use this method to process my sampled audio:

- Normalize ($N(x) = x / \max(x)$) the audio file into 1, then, find the peak volume of audio, and start from here.
- Slice these audio pieces into tiny partitions, say 0.1 second is one partition. The maximum number of each partition will be its assumed volume at this time point.
- Select these pieces volume start from some large number to small number – since piano sound is loud from its beginning and decay by the time. Say from 90% to 2% of the sampled sound audio.

3.3 Frequency Analysis

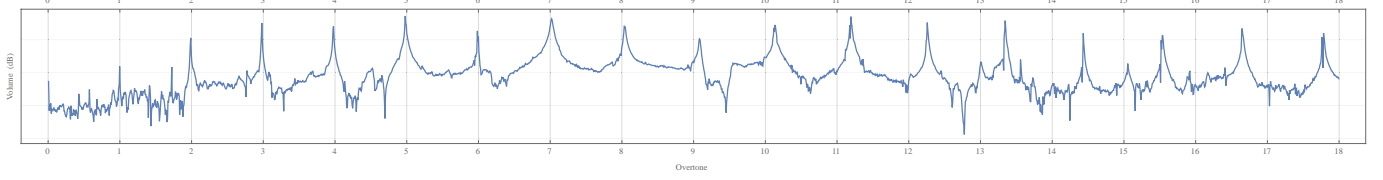


Figure 3-1 “A#0” Key (at Upright Piano Samples) Overtone Plot; Volume at Logarithm Scale

Then, put this audio samples into fourier analysis (FFT algorithm). Then we get the function $G(\omega) = FFT(S(t))$ where $S(t)$ is the audio function, and $G(\omega)$ is the frequency domain function. In our work, the frequency domain is converted to the ratio to its ideal fundamental frequency, thus we can see the Figure 3-1, the peaks will always almost lies in the grid by dividing its ideal frequency.

From Figure 3-1, we can see that the higher overtone (right hand side peaks with larger numbers) shifts higher.

It is a problem to capture all these peaks numbers, since some are not clear: the fundamental frequency (at 1), and some has multiple peaks: at 15 ~ 16.

In my work, I use the frequency *Catchup Method* to get octave values for all these peaks.

3.4 Catchup Overtone

From the charactors of these peaks, there are several charactors will be considered:

- From left to right, the gap between two peaks are increasing gradually.
- The largest value of this plot is probably some peak of overtone
- The valid peak should be nearly larger than fundamental frequency position: at 1.
- The peak may be broken into several peaks, we need centralize the targeted position.

From this characteristics, the *Catchup Method* could be built:

- Analyze the frequency samples which roughly larger than 1 (my program is starting from 0.8), get the peak frequency $f_{k,peak}$ at key number k .
- Comparing with ideal frequency \tilde{f}_k . We can then assume that it is $n = round(f_{k,peak} / \tilde{f}_k)$ harmonics.

Then, we can know its guessed fundamental frequency is $\hat{f}_k = f_{k,peak} / n$. Then, this should be the step size for catchup method.

- The catchup method is forward (goes to the right), and the backward (goes to the left). If we are in the forward operation, the next guessed target frequency is $\hat{f}_{k,peak+1} = f_{k,peak} + f'_k$, where f'_k is the assumed gap between two peak at this position. In the first try, we set this number to $f'_k = \hat{f}_k$, and this number will be increasing for more right harmonics. Then, we get the around data (in a relatively small area) for guessed target frequency $\hat{f}_{k,peak+1} \pm \delta$, we can find its maximum number these data to be the frequency candidate $\hat{f}_{k,peak+1}^{candidate}$, then we get the data of smaller surround area $\hat{f}_{k,peak+1}^{candidate} \pm \delta'$ where $\delta' \ll \delta$. Then, we calculate the weighted average for this smaller area, and the result is the actual frequency of this peak

$f_{k,peak+1} = \int_{-\delta'}^{\delta'} \omega \cdot G(\hat{f}_{k,peak+1}^{candidate}) d\omega$, where ω is proportional to frequency. Then, the assumed gap between two peak at this step is updated to be $f'_k = f_{k,peak+1} - f_{k,peak}$.

- Iterate this method for forward catchup to get all higher frequencies.
- If the highest peak is not fundamental frequency, we will perform the backward catchup. Since there are less peaks and the overtone shift will be far less than the right, the assumed targeted gap between two peaks is set to be the assumed fundamental frequency \hat{f}_k .

From this method, we can get a overtone (frequency) list for the key k . Which is:

$$k \rightarrow \{f_{k,1}, f_{k,2}, \dots\} \quad (3.3)$$

3.5 Inharmonicity Model

From reference [1], we assume that the piano string is a bar, which follows the partial differential equation:

$$\ddot{y} \propto -y'' - \varepsilon y'''' \quad (3.4)$$

Where y is the special position of piano string (bar model). The prime is the derivative to spatial domain, and dots is the derivative to time domain.

Then, use the modal analysis and solved the natural frequencies for this string are:

$$f_{k,n} \propto n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \Rightarrow f_{k,n} = A_k \cdot n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \quad (3.5)$$

Here we have two unknown variables.

Then, we use this function to fit all frequency results at Eq.(3.3). Since A_k value is always almost 1 all the time, we can ignore this number, and focus only on B_k . However in the optimization process, with parameter A_k could achieve much better result, although finally its value is almost 1. We set 0 to be the fundamental frequency is that when $n = 0$ that the equation holds, we will restore this number later.

Then, we can get inharmonicity parameter list $\{\{k, B_k\}\}$.

From my observation, the logarithm of this number has some beautiful properties with the data $\{\{k, \ln(s \cdot B_k)\}\}$, where s is a scaling parameter (I set to 10000).

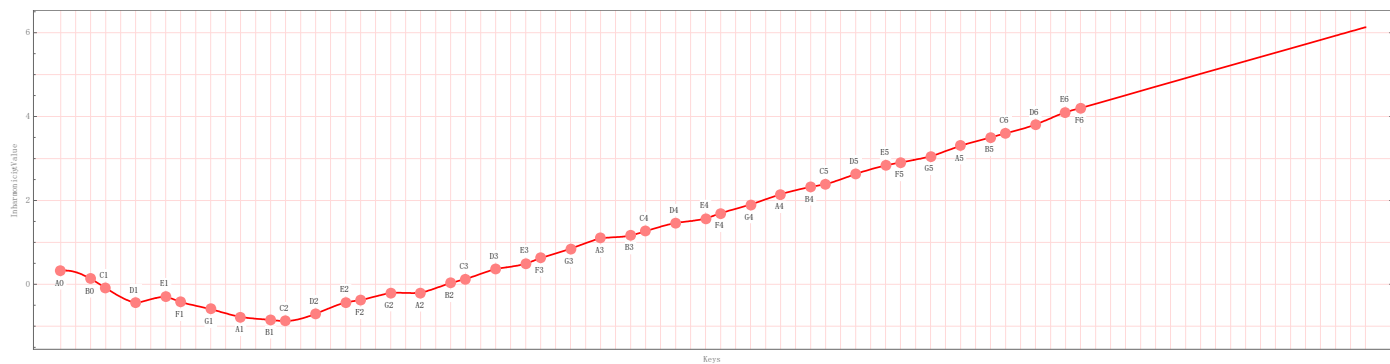


Figure 3-2 Inharmonicity Plot of Grand Piano

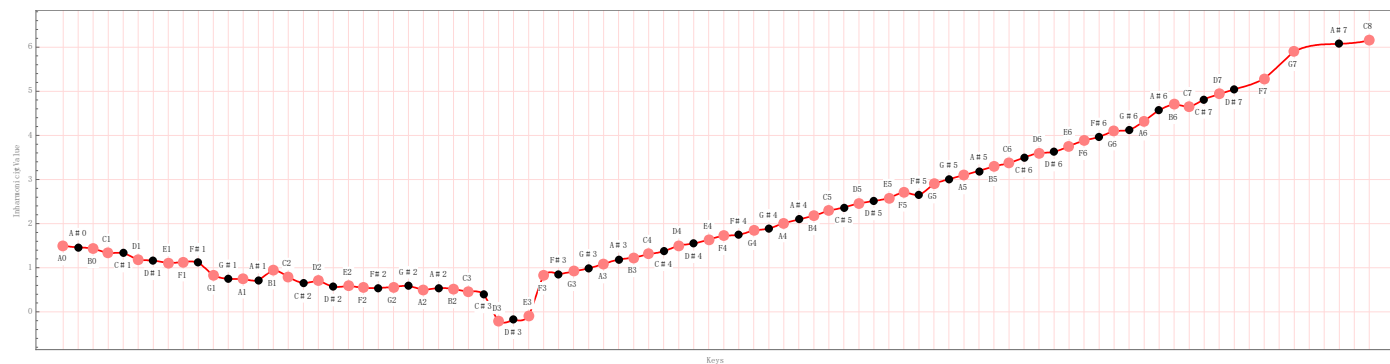


Figure 3-3 Inharmonicity Plot of Upright Piano

From Figure 3-2 and Figure 3-3, we can clearly see the line is divided into 2 parts.



Figure 3-4 Grand Piano String Arrangement



Figure 3-5 Upright Piano String Arrangement

From Figure 3-4 and Figure 3-5, we can clearly see that the string is divided into two parts, the steel string and copper string (may be covered by silver for highly expensive pianos). The upright piano has more copper strings since the steel string cannot go longer, and the string will become thicker to make the string vibrate slower. From spring vibration formula:

$$\omega = \sqrt{\frac{K}{m}} \quad (3.6)$$

Where ω is proportional to frequency, m is the mass of spring, K is the stiffness of spring.

When m increases, K increase a little bit, ω decreases, then frequency decrease.

Since the piano cannot growing longer, it become thick and more like a stick rather than an ideal string. For higher notes strings, it is too short, and the thickness become relatively larger comparing to its length, thus it is more likely to be a bar.

Thus, from the plot, we can see the inharmonicity increases at two ends, and break at the position of separation of two kinds of strings.

Since grand concert piano is longer, and can have more steel strings, less copper strings, thus the break will become more left side.

The figure of inharmonicity plot also tell us that two separate line are almost linear. In my model, I used the valid sampled points are modeled with interpolation function, and two edges are modeled with linear function, and it is method is shown below.

We get several samples from one line, and fit in a linear form.

Get its slope, and build a line which pass the right end point (since I will not wish to have a break for the interpolation function), and add some samples for edges situation to sample pool.

Similar to the left hand side.

We use interpolation for these samples of sample pool – “Left hand side + samples + right hand side”, which is our final model for inharmonicity model function $Ih(k)$.

$$Ih(k) = \ln(s \cdot B_k) \quad (3.7)$$

Thus, we can have the modeled parameter B_k with:

$$B_k = \frac{e^{Ih(k)}}{s} \quad (3.8)$$

Then, the frequencies $\tau(k, n)$ will be:

$$\tau(k, n) = f_{k,1} \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \quad (3.9)$$

Where $f_{k,1}$ is currently unknown but it will be eliminated.

3.6 Tuning Curve Optimization Model

Similar to Tunelab, I set the tuning optimization method to separate the lower tones (bass) and higher tones (tenor) into two tuning target optimization method, the separation point k_0 is “C#4/D4”. And the default tuning method for bass is to set 6:3. Since $6/3=2$ (a/b), this frequency ratio is $\gamma = a/b$, and its corresponding pitch range is $Fr_{\rightarrow c}(\gamma)$ which is 1200, and 1200 is an octave, it means the tone say “A0”’s 6th harmonics will largely match its octave’s “A1”’s 3rd harmonics.

Here pitch is defined by cents.

The error function ε_k is defined as:

$$\begin{aligned} \varepsilon_k &= Fr_{\rightarrow c} \left(\frac{\tau(k, a)}{\tau(k + Fr_{\rightarrow c}(a/b), b)} \right) \\ &= Fr_{\rightarrow c} \left(\sqrt{\frac{1 + B_k \cdot a^2}{1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2}} \cdot \frac{a}{b} \cdot \left(\frac{f_{k,1}}{f_{k+Fr_{\rightarrow c}(a/b),1}} \right) \right) \\ &= Fr_{\rightarrow c} \left(\sqrt{\frac{1 + B_k \cdot a^2}{1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2}} \right) \end{aligned} \quad (3.10)$$

We can do this for all bass strings.

For tenor strings, the default tuning method is set to 4:1 (c/d). But this time we count the higher note as the target to calculate.

$$\varepsilon_k = Fr_{\rightarrow c} \left(\sqrt{\frac{1 + B_{k-Fr_{\rightarrow c}(c/d)} \cdot c^2}{1 + B_k \cdot d^2}} \right) \quad (3.11)$$

The combined expression is:

$$E(k) = \begin{cases} Fr_{\rightarrow c} \left(\sqrt{\frac{1 + B_k \cdot a^2}{1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2}} \right) & k \leq k_0 \\ Fr_{\rightarrow c} \left(\sqrt{\frac{1 + B_{k-Fr_{\rightarrow c}(c/d)} \cdot c^2}{1 + B_k \cdot d^2}} \right) & k > k_0 \end{cases} \quad (3.12)$$

From this equation, we can see $E(k)$ is only a value for calculation.

From this point, we need a function to largely eliminate these errors. The piano tuning curve $C(k)$ is introduced.

The cost function for optimization is:

$$J(k) = \sum_k (C(k) - E(k))^2 \quad (3.13)$$

Which minimize the square error of these functions.

Here I use polynomial for easier calculation:

$$C(x) = \sum_{i=1}^n \chi_i \cdot x^i \quad (3.14)$$

Since $C(x)$ will pass the fix point, which is “A4” pitch at 440Hz frequency at pitch deviation of 0, thus i is from 1 and $x = k - k_{A4}$, where k_{A4} is the key number (index) at “A4”, which is 48.

Thus, $J(k)$ is the second order polynomial function, which is very easy to minimize by linear regression method to calculate the fitting parameter $\{\chi_i\}$, and rebuild the functions.

Then, we can bring it to the $J(k)$ function to calculate its deviations.

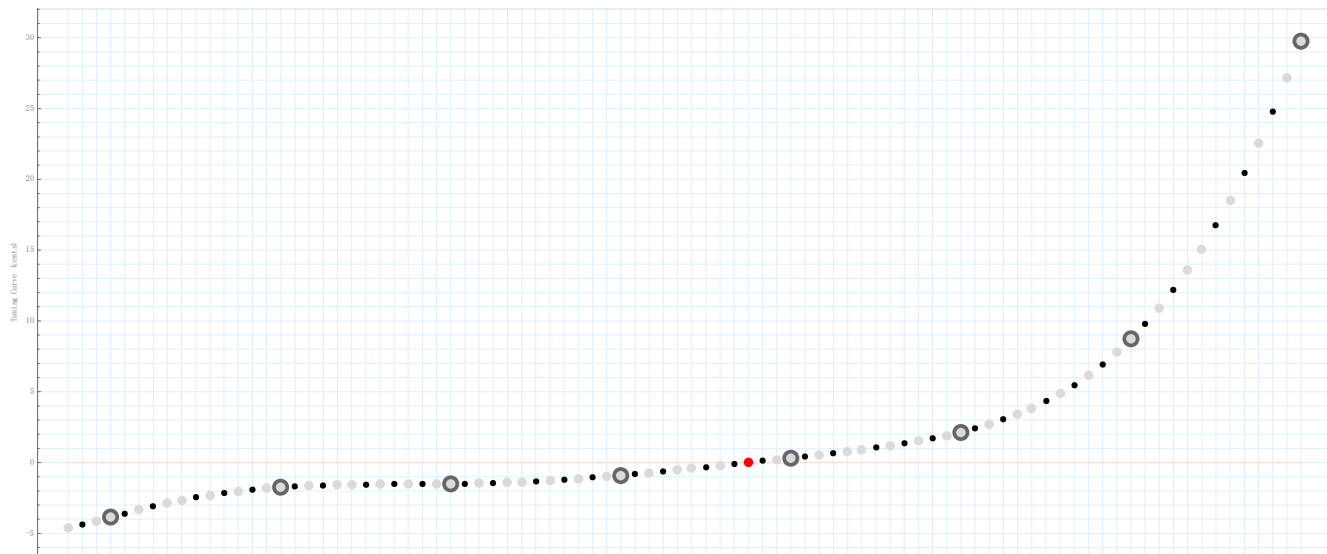


Figure 3-6 $C(x)$ for Grand Piano

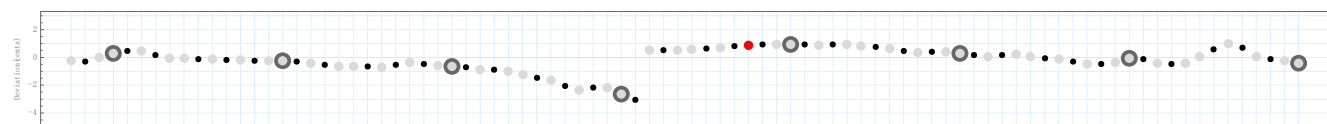


Figure 3-7 $J(x)$ for Grand Piano

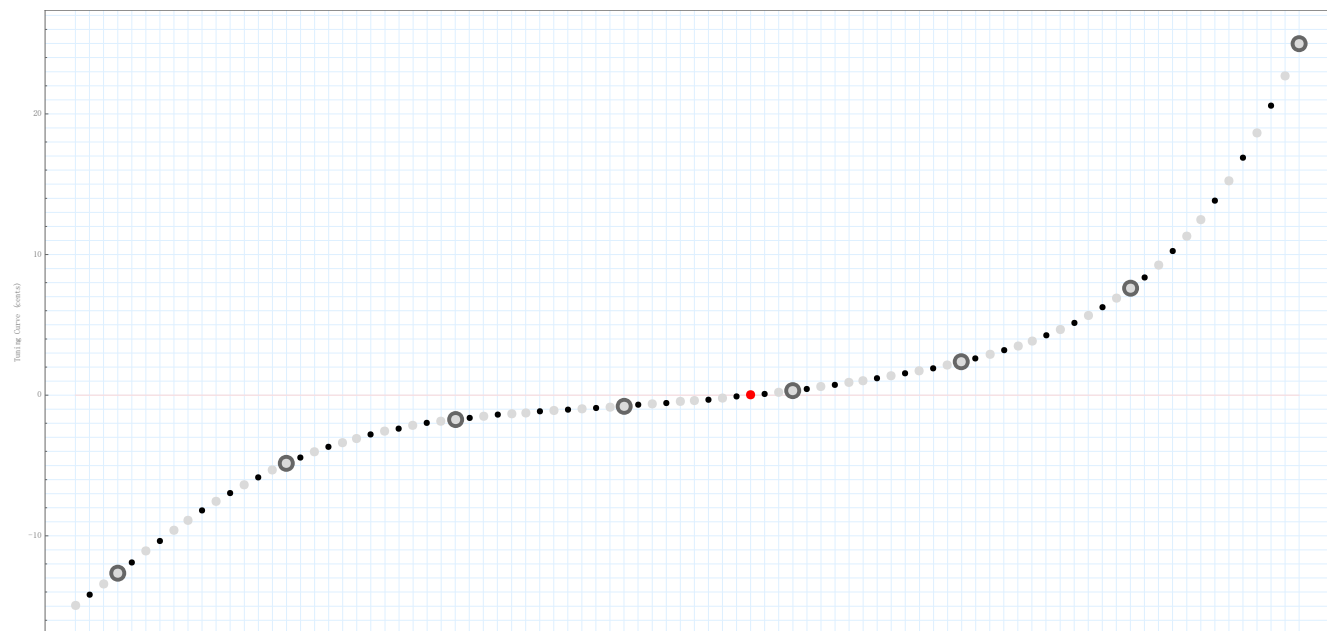


Figure 3-8 $C(x)$ for Upright Piano

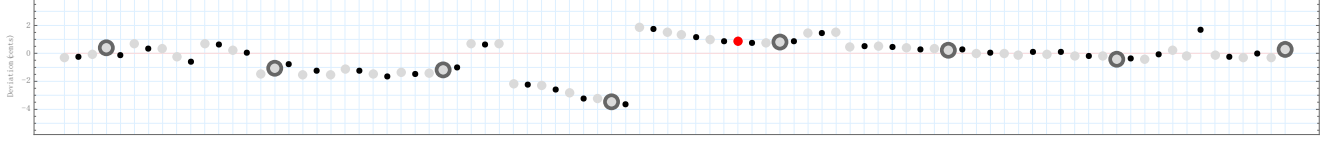


Figure 3-9 $J(x)$ for Upright Piano

The result of two piano is shown above. Horizontal axis is the key number, and the vertical axis the pitch deviation with idea frequencies represented by cents.

From this tuning method, we can see that the bass tuning will consider the deviations from the tenor part, and vice versa, and the effect are inner related. Thus this tuning method is theoretically to optimize almost the whole piano keys tuning.

3.7 Temperament Model

With the development of music, various temperament appears and create unique flavor of music. The temperament model is using the pitch deviation tables of different temperament (the unit is cent). We can then create the non 12 equal temperament tuning strategy. The temperament function is defined to be $T(k)$.

The tuning table such as “Bach - Bradley Lehman” is:

C	C#	D	D#	E	F	F#	G	G#	A	A#	B
5.87	3.91	1.96	3.91	-1.96	7.82	1.96	3.91	3.81	0	3.91	0

Table 3-1 Table for “Bach - Bradley Lehman” Temperament

Where A note will always be 0 since A is the reference frequency and will always keep to 440 Hz (if is standard situation).

This table shows the situation of “C” major.

The other major tuning will follow the rotation of table. For example: if tuning “D” major, the “D” will rotate to current “D” \rightarrow “C” place, which is rotating left 2 times. However, we will make sure “A” note will always be 0, then, we can subtract the number at “B” \rightarrow “A” to make it possible.

Then, add these pitch errors to all the notes of tuning, the modified tuning curve is:

$$C'(k) = C(k) + T(k) \quad (3.15)$$

3.8 Creating Tuning Table

The final tuning frequency $\tau(k, n)$ is:

$$f_{k,1} = F_{+c}(\hat{f}_k, C'(k)) \quad (3.16)$$

$$\begin{aligned}
\tau(k, n) &= f_{k,1} \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \\
&= F_{+c}(\hat{f}_k, C'(k)) \cdot n \cdot \sqrt{1 + B_k \cdot n^2} \\
&= F_{+c}(\hat{f}_k, C'(k)) \cdot n \cdot \sqrt{1 + \frac{e^{Ih(k)}}{s} \cdot n^2}
\end{aligned} \quad (3.17)$$

From Eq.(3.17), we can see only C and Ih function is modeled function, other function are basic mathematics functions.

From the modeling, we can get a strategy of piano tuning, then we can convert this strategy into a tuning table, which shows all the frequency of fundamental and its harmonics frequencies, and corresponding deviation to ideal frequencies represented by cents.

The grand and upright piano tuning strategy is shown in Figure 7-1 and Figure 7-2.

The red font is the frequencies recommended for the devices to tune.

4 FUTURE WORK

Although the Entropy piano tuning method is far more advanced than this tuning method theoretically, however the jumpy tuning curve will make the music scales sound weird. If I have time, I will implement the entropy tuner with much more smooth functions, this construction is easier than original idea since the optimization at his method is only few parameters if using similar polynomial to optimize the curve to achieve more smooth result with entropy function as cost function.

Over-pull tuning is implemented experimentally with their tuning apps, and I do not know its method due to its close source reason. And I am still lack of research on this area, thus I will leave it as future work to think about. I know this effect is caused by the experimental result of the percentage that the string pins will loosen and drop the pitch, the tuner will make up the errors of this effect by over pull and tune higher tones.

5 CONCLUSION

This tuning method gives us a solution of piano tuning that works as well as commercial apps Tunelab. The method is presented to optimize the whole piano notes sound. Future work is given to develop maybe in the future.

6 REFERENCE

- [1] Hinrichsen, Haye. "Entropy-based tuning of musical instruments." *Revista brasileira de Ensino de Física* 34.2 (2012): 1-8.
- [2] Github for Piano Tuning Project [https://github.com/RobertBoganKang/piano_tuning]

7 APPENDIX

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16																
A0	71.4266	-0.009	54.857	-0.009	82.9025	-0.009	109.774	-0.009	137.284	-0.009	164.843	-0.009	192.461	-0.009	220.152	-0.009	247.925	-0.009	275.791	-0.009	303.762	-0.009	331.849	-0.009	360.063	-0.009	388.414	-0.009	416.913	-0.009	445.571	-0.009
A#0	59.0617	-0.009	58.1273	-0.009	87.2084	-0.009	116.317	-0.009	145.464	-0.009	174.661	-0.009	203.921	-0.009	233.254	-0.009	262.672	-0.009	292.187	-0.009	321.800	-0.009	351.55	-0.009	381.422	-0.009	411.435	-0.009	441.601	-0.009	471.93	-0.009
B0	50.7944	-0.010	61.5924	-0.010	92.4044	-0.010	123.241	-0.010	154.113	-0.010	185.03	-0.010	216.004	-0.010	247.044	-0.010	278.161	-0.010	309.365	-0.010	340.667	-0.010	372.077	-0.010	403.606	-0.010	435.262	-0.010	467.057	-0.010	499.0	-0.010
C1	52.6306	-0.009	65.2641	-0.009	97.9096	-0.009	130.576	-0.009	163.272	-0.009	196.008	-0.009	228.791	-0.009	261.63	-0.009	294.535	-0.009	327.515	-0.009	360.577	-0.009	393.732	-0.009	426.988	-0.009	460.352	-0.009	493.835	-0.009	527.445	-0.009
C#1	54.5761	-0.009	69.1548	-0.009	103.744	-0.009	138.351	-0.009	172.983	-0.009	207.649	-0.009	242.355	-0.009	277.111	-0.009	311.922	-0.009	346.797	-0.009	381.744	-0.009	416.769	-0.009	451.881	-0.009	487.087	-0.009	522.394	-0.009	557.81	-0.009
D1	56.6375	-0.009	73.7273	-0.009	109.926	-0.009	146.592	-0.009	183.281	-0.009	220.001	-0.009	256.758	-0.009	293.559	-0.009	330.412	-0.009	367.324	-0.009	404.301	-0.009	441.35	-0.009	478.478	-0.009	515.693	-0.009	553.001	-0.009	590.408	-0.009
D#1	58.8214	-0.009	77.6456	-0.009	116.481	-0.009	155.335	-0.009	194.216	-0.009	233.132	-0.009	272.092	-0.009	311.103	-0.009	350.174	-0.009	389.312	-0.009	428.526	-0.009	467.823	-0.009	507.213	-0.009	546.701	-0.009	586.297	-0.009	626.009	-0.009
E1	61.1352	-0.009	82.2735	-0.009	123.424	-0.009	164.596	-0.009	205.798	-0.009	247.04	-0.009	288.331	-0.009	329.68	-0.009	371.095	-0.009	412.587	-0.009	454.164	-0.009	495.835	-0.009	537.609	-0.009	579.494	-0.009	621.501	-0.009	663.638	-0.009
F1	63.5865	-0.009	87.1758	-0.009	130.777	-0.009	174.398	-0.009	218.047	-0.009	261.734	-0.009	305.466	-0.009	349.253	-0.009	393.103	-0.009	437.024	-0.009	481.025	-0.009	525.114	-0.009	569.3	-0.009	613.592	-0.009	657.996	-0.009	702.323	-0.009
F#1	66.1833	-0.009	92.3694	-0.009	138.567	-0.009	184.783	-0.009	231.027	-0.009	277.308	-0.009	323.632	-0.009	370.009	-0.009	416.447	-0.009	462.964	-0.009	509.538	-0.009	556.208	-0.009	602.972	-0.009	649.837	-0.009	696.812	-0.009	743.905	-0.009
G1	68.9343	-0.009	97.8713	-0.009	146.819	-0.009	195.786	-0.009	244.78	-0.009	293.809	-0.009	342.882	-0.009	392.006	-0.009	441.19	-0.009	490.441	-0.009	539.768	-0.009	589.179	-0.009	638.681	-0.009	688.284	-0.009	737.994	-0.009	787.82	-0.009
G#1	71.8485	-0.009	103.7	-0.009	155.561	-0.009	207.441	-0.009	259.347	-0.009	311.286	-0.009	363.267	-0.009	415.297	-0.009	467.385	-0.009	519.537	-0.009	571.762	-0.009	624.067	-0.009	676.46	-0.009	728.949	-0.009	781.541	-0.009	834.243	-0.009
A1	74.9357	-0.009	109.874	-0.009	164.822	-0.009	219.788	-0.009	274.779	-0.009	329.803	-0.009	384.888	-0.009	439.98	-0.009	495.147	-0.009	550.378	-0.009	605.678	-0.009	661.057	-0.009	716.521	-0.009	772.078	-0.009	827.735	-0.009	883.499	-0.009
A#1	78.2061	-0.009	116.415	-0.009	174.634	-0.009	232.87	-0.009	291.133	-0.009	349.429	-0.009	407.765	-0.009	466.151	-0.009	524.593	-0.009	583.098	-0.009	641.676	-0.009	700.332	-0.009	759.076	-0.009	817.914	-0.009	876.835	-0.009	935.902	-0.009
B1	81.6705	-0.009	123.344	-0.009	185.027	-0.009	246.729	-0.009	308.458	-0.009	370.221	-0.009	432.026	-0.009	493.882	-0.009	555.795	-0.009	617.774	-0.009	679.827	-0.009	741.962	-0.009	804.187	-0.009	866.508	-0.009	928.935	-0.009	991.474	-0.009
C2	85.3404	-0.009	130.684	-0.009	196.038	-0.009	261.411	-0.009	322.245	-0.009	385.475	-0.009	453.255	-0.009	525.585	-0.009	598.845	-0.009	664.503	-0.009	730.237	-0.009	796.054	-0.009	861.963	-0.009	929.973	-0.009	994.025	-0.009	1054.32	-0.009
C#2	89.2282	-0.009	138.459	-0.009	207.703	-0.009	276.988	-0.009	346.263	-0.009	415.598	-0.009	484.982	-0.009	554.423	-0.009	623.932	-0.009	693.516	-0.009	763.186	-0.009	832.949	-0.009	902.816	-0.009	972.795	-0.009	1042.9	-0.009	1113.13	-0.009
D2	93.9688	-0.009	146.697	-0.009	220.062	-0.009	293.453	-0.009	366.879	-0.009	440.352	-0.009	513.884	-0.009	587.484	-0.009	661.164	-0.009	734.934	-0.009	808.806	-0.009	882.789	-0.009	956.895	-0.009	1031.13	-0.009	1105.82	-0.009	1180.06	-0.009
D#2	97.7098	-0.009	155.424	-0.009	233.156	-0.009	310.919	-0.009	388.727	-0.009	466.593	-0.009	544.53	-0.009	622.551	-0.009	700.671	-0.009	778.901	-0.009	857.256	-0.009	935.748	-0.009	1014.39	-0.009	1093.2	-0.009	1172.18	-0.009	1251.35	-0.009
E2	102.3319	-0.009	164.669	-0.009	247.028	-0.009	329.424	-0.009	411.874	-0.009	494.393	-0.009	576.997	-0.009	659.704	-0.009	742.527	-0.009	825.484	-0.009	908.59	-0.009	991.861	-0.009	1075.31	-0.009	1158.96	-0.009	1242.82	-0.009	1326.91	-0.009
F2	107.2286	-0.009	174.463	-0.009	261.722	-0.009	346.022	-0.009	436.382	-0.009	525.82	-0.009	611.353	-0.009	698.999	-0.009	786.777	-0.009	874.703	-0.009	962.79	-0.009	1051.07	-0.009	1139.55	-0.009	1228.25	-0.009	1317.19	-0.009	1406.38	-0.009
F#2	112.4162	-0.009	184.839	-0.009	277.29	-0.009	369.789	-0.009	462.358	-0.009	555.016	-0.009	647.786	-0.009	740.686	-0.009	833.739	-0.009	926.964	-0.009	1020.38	-0.009	1114.01	-0.009	1207.88	-0.009	1302	-0.009	1396.39	-0.009	1491.08	-0.009
G2	117.912	-0.009	195.832	-0.009	293.784	-0.009	391.792	-0.009	489.88	-0.009	588.072	-0.009	686.392	-0.009	784.864	-0.009	883.511	-0.009	982.358	-0.009	1081.43	-0.009	1180.74	-0.009	1280.33	-0.009	1379.25	-0.009	1480.41	-0.009	1580.94	-0.009
G#2	123.734	-0.009	207.477	-0.009	311.254	-0.009	415.09	-0.009	519.01	-0.009	623.04	-0.009	727.205	-0.009	831.531	-0.009	936.041	-0.009	1040.76	-0.009	1145.72	-0.009	1250.93	-0.009	1356.43	-0.009	1462.25	-0.009	1568.39	-0.009	1674.89	-0.009
A2	129.093	-0.009	219.815	-0.009	329.763	-0.009	439.774	-0.009	549.875	-0.009	660.092	-0.009	770.453	-0.009	880.984	-0.009	991.712	-0.009	1102.66	-0.009	1213.86	-0.009	1325.34	-0.009	1437.12	-0.009	1549.23	-0.009	1661.7	-0.009	1774.54	-0.009
A#2	136.439	-0.009	232.888	-0.009	349.38	-0.009	465.946	-0.009	582.618	-0.009	699.428	-0.009	816.408	-0.009	933.589	-0.009	1051.55	-0.009	1168.68	-0.009	1286.65	-0.009	1404.95	-0.009	1523.61	-0.009	1642.65	-0.009	1762.12	-0.009	1882.56	-0.009
B2	143.263	-0.009	246.739	-0.009	370.166	-0.009	493.682	-0.009	617.325	-0.009	741.134	-0.009	865.145	-0.009	989.388	-0.009	1113.93	-0.009	1238.78	-0.009	1363.98	-0.009	1489.58	-0.009	1615.6	-0.009	1742.09	-0.009	1869.08	-0.009	1996.6	-0.009
C3	150.542	-0.009	261.414	-0.009	392.188	-0.009	523.065	-0.009	654.091	-0.009	785.309	-0.009	916.764	-0.009	1048.513	-0.009	1180.56	-0.009	1312.99	-0.009	1445.83	-0.009	1579.13	-0.009	1712.92	-0.009	1847.26	-0.009	1982.18	-0.009	2117.93	-0.009
C#3	157.748	-0.009	276.963	-0.009	415.524	-0.009	554.21	-0.009	693.073	-0.009	832.166	-0.009	971.543	-0.009	1111.263	-0.009	1251.36	-0.009	1391.9	-0.009	1532.93	-0.009	1674.51	-0.009	1816.69	-0.009	1959.51	-0.009	2103.03	-0.009	2247.29	-0.009
D3	163.467	-0.009	293.438	-0.009	452.284	-0.009	597.215	-0.009	734.39	-0.009	881.84	-0.009	1029.63	-0.009	1177.82	-0.009	1326.47	-0.009	1475.65	-0.009	1625.42	-0.009	1775.84	-0.009	1925.96	-0.009	2078.88	-0.009	2231.59	-0.009	2385.22	-0.009
D#3	169.434	-0.009	310.892	-0.009	466.445	-0.009	622.163	-0.009	778.117	-0.009	934.378	-0.009	1091.02	-0.009	1248.1	-0.009	1405.7	-0.009	1563.89	-0.009	1722.74	-0.009	1882.3	-0.009	2042.66	-0.009	2203.88	-0.009	2366.02	-0.009	2529.16	-0.009
E3	174.68	-0.009	329.387	-0.009	494.201	-0.009	659.204	-0.009	824.475	-0.009	990.994	-0.009	1156.14	-0.009	1322.7	-0.009	1489.84	-0.009	1657.65	-0.009	1826.2	-0.009	1995.58	-0.009	2165.85	-0.009	2337.1	-0.009	2509.4	-0.009	2682.82	-0.009
F3	174.476	-0.009	348.985	-0.009	523.625	-0.009	689.494	-0.009	853.69	-0.009	1019.31	-0.009	1185.45	-0.009	1351.68	-0.009	1517.9	-0.009	1684.61	-0.009	1851.67	-0.009	2018.74	-0.009	2186.62	-0.009	2354.81	-0.009	2522.92	-0.009	2692.92	-0.009
F#3	184.856	-0.009	369.751	-0.009	554.802	-0.009	740.123	-0.009	925.833	-0.009	1112.05	-0.009	1298.88	-0.009	1486.44	-0.009	1674.53	-0.009	1864.22	-0.009	2054.67	-0.009	2									

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16																
A0	27.2634	-13.352	54.5391	-11.382	81.8635	-13.352	109.273	-15.374	136.805	-17.397	164.403	-19.420	192.376	-21.443	220.487	-23.461	248.861	-25.484	277.533	-27.503	306.537	-29.526	335.905	-31.551	365.67	-33.576	395.884	-35.601	426.510	-37.626	457.657	-39.651
A#0	28.8972	-14.24	57.8069	-12.502	86.7667	-14.24	115.814	-16.254	144.986	-18.264	174.319	-20.274	203.85	-22.284	233.616	-24.294	263.653	-26.304	293.994	-28.312	324.676	-30.322	355.731	-32.332	387.194	-34.342	418.096	-36.352	451.47	-38.362	484.346	-40.372
B0	30.6292	-15.42	61.2713	-13.69	91.9648	-15.42	122.748	-17.698	153.659	-19.698	184.737	-21.698	216.018	-23.698	247.54	-25.698	279.34	-27.698	311.453	-29.698	343.917	-31.698	376.765	-33.698	410.032	-35.698	443.751	-37.698	477.956	-39.698	512.677	-41.698
C1	32.4652	-16.50	64.9427	-14.77	97.4094	-16.50	130.082	-18.77	162.817	-20.77	195.712	-22.77	228.802	-24.77	262.122	-26.77	295.71	-28.77	329.598	-30.77	363.822	-32.77	398.416	-34.77	433.413	-36.77	468.844	-38.77	504.743	-40.77	541.14	-42.77
C#1	34.4112	-17.58	68.8355	-15.83	103.312	-17.58	137.88	-19.58	172.579	-21.58	207.448	-23.58	242.524	-25.58	277.846	-27.58	313.453	-29.58	349.38	-31.58	385.664	-33.58	422.342	-35.58	459.449	-37.58	497.019	-39.58	535.087	-41.58	573.685	-43.58
D1	36.4736	-18.69	72.9592	-16.93	109.492	-18.69	146.109	-20.69	182.844	-22.69	219.733	-24.69	256.811	-26.69	294.112	-28.69	331.672	-30.69	369.525	-32.69	407.703	-34.69	446.24	-36.69	485.168	-38.69	524.52	-40.69	564.327	-42.69	604.619	-44.69
D#1	38.6593	-19.82	77.3311	-18.09	116.053	-19.82	154.861	-21.89	193.794	-23.89	232.888	-25.89	272.18	-27.89	311.705	-29.89	351.501	-31.89	391.603	-33.89	432.046	-35.89	472.865	-37.89	514.093	-39.89	555.764	-41.89	597.912	-43.89	640.568	-45.89
E1	40.9755	-20.96	81.9635	-19.30	123.001	-20.96	164.126	-22.96	205.374	-24.96	246.783	-26.96	288.39	-28.96	330.231	-30.96	372.341	-32.96	414.757	-34.96	457.514	-36.96	500.647	-38.96	544.189	-40.96	588.174	-42.96	632.636	-44.96	677.607	-46.96
F1	43.4298	-22.09	86.8731	-20.62	130.37	-22.09	173.961	-24.09	217.685	-26.09	261.584	-28.09	305.695	-30.09	350.06	-32.09	394.716	-34.09	430.701	-36.09	485.055	-38.09	530.814	-40.09	577.015	-42.09	623.696	-44.09	670.89	-46.09	718.634	-48.09
F#1	46.0304	-23.21	92.0748	-21.80	138.176	-23.21	184.375	-25.21	230.714	-27.21	277.286	-29.21	323.982	-31.21	370.992	-33.21	418.308	-35.21	465.971	-37.21	514.019	-39.21	562.493	-41.21	611.43	-43.21	660.87	-45.21	710.85	-47.21	761.406	-49.21
G1	48.7857	-24.36	97.5825	-22.97	146.424	-24.36	195.344	-26.36	244.375	-28.36	293.552	-30.36	342.906	-32.36	392.472	-34.36	442.281	-36.36	492.366	-38.36	542.759	-40.36	593.493	-42.36	644.598	-44.36	696.106	-46.36	748.047	-48.36	800.45	-50.36
G#1	51.7049	-25.50	103.421	-24.07	155.181	-25.50	207.017	-27.50	258.963	-29.50	311.051	-31.50	363.314	-33.50	415.783	-35.50	468.492	-37.50	521.472	-39.50	574.754	-41.50	628.371	-43.50	682.352	-45.50	736.729	-47.50	791.532	-49.50	846.79	-51.50
A1	54.7977	-26.69	109.607	-25.16	164.462	-26.69	219.398	-28.69	274.45	-30.69	329.65	-32.69	385.035	-34.69	440.637	-36.69	496.491	-38.69	552.63	-40.69	609.088	-42.69	665.897	-44.69	723.089	-46.69	780.699	-48.69	838.756	-50.69	897.292	-52.69
A#1	58.0742	-27.88	116.16	-26.86	174.294	-27.88	232.51	-29.88	290.845	-31.88	349.333	-33.88	408.011	-35.88	466.912	-37.88	526.071	-39.88	585.524	-41.88	645.304	-43.88	705.446	-45.88	765.982	-47.88	826.944	-49.88	888.371	-51.88	950.289	-53.88
B1	61.5454	-29.03	123.107	-27.97	184.731	-29.03	246.367	-31.93	308.361	-33.93	370.46	-35.93	432.812	-37.93	495.463	-39.93	558.459	-41.93	621.846	-43.93	685.67	-45.93	749.975	-47.93	814.805	-49.93	880.294	-51.93	946.216	-53.93	1012.88	-55.93
C2	65.2226	-30.27	130.459	-29.09	195.754	-30.27	261.149	-32.27	326.687	-34.27	392.411	-36.27	458.365	-38.27	524.589	-40.27	591.127	-42.27	658.019	-44.27	725.307	-46.27	793.033	-48.27	861.237	-50.27	929.958	-52.27	999.236	-54.27	1069.11	-56.27
C#2	69.118	-31.44	138.249	-30.27	207.434	-31.44	276.71	-33.44	346.119	-35.44	415.7	-37.44	485.492	-39.44	555.534	-41.44	625.665	-43.44	696.523	-45.44	767.547	-47.44	838.976	-49.44	910.845	-51.44	983.194	-53.44	1056.06	-55.44	1127.47	-57.44
D2	73.2446	-32.69	150.507	-31.42	219.823	-32.69	293.245	-34.69	366.814	-36.69	440.576	-38.69	514.572	-40.69	588.848	-42.69	663.447	-44.69	738.411	-46.69	813.784	-48.69	889.607	-50.69	965.923	-52.69	1042.77	-54.69	1120.2	-56.69	1198.24	-58.69
D#2	77.6161	-33.99	155.246	-32.92	229.823	-33.99	310.71	-35.99	388.627	-37.99	466.721	-39.99	545.033	-41.99	623.604	-43.99	702.473	-45.99	781.681	-47.99	861.267	-49.99	941.271	-51.99	1021.73	-53.99	1102.69	-55.99	1184.18	-57.99	1266.24	-59.99
E2	82.2469	-35.30	164.509	-34.26	246.829	-35.30	329.787	-37.30	411.825	-39.30	494.588	-41.30	577.587	-43.30	660.865	-45.30	744.465	-47.30	828.431	-49.30	912.806	-51.30	997.632	-53.30	1082.95	-55.30	1168.81	-57.30	1255.24	-59.30	1342.28	-61.30
F2	87.1524	-36.59	174.32	-35.56	267.142	-36.59	348.88	-38.59	436.363	-40.59	524.081	-42.59	611.959	-44.59	700.162	-46.59	788.692	-48.59	877.596	-50.59	966.915	-52.59	1056.69	-54.59	1146.98	-56.59	1237.8	-58.59	1329.22	-60.59	1421.26	-62.59
F#2	92.3489	-37.88	184.714	-36.82	281.577	-37.88	369.682	-39.88	462.38	-41.88	555.284	-43.88	648.442	-45.88	741.9	-47.88	835.705	-49.88	929.904	-51.88	1024.54	-53.88	1119.67	-55.88	1215.32	-57.88	1311.55	-59.88	1408.4	-61.88	1505.92	-63.88
G2	97.8537	-39.27	195.725	-38.02	293.664	-39.27	391.724	-41.27	489.956	-43.27	588.412	-45.27	687.141	-47.27	786.196	-49.27	885.629	-51.27	985.483	-53.27	1085.82	-55.27	1186.67	-57.27	1288.11	-59.27	1390.16	-61.27	1492.89	-63.27	1596.34	-65.27
G#2	103.685	-40.59	207.389	-39.09	311.168	-40.59	415.077	-42.59	519.174	-44.59	623.613	-46.59	728.151	-48.59	833.143	-50.59	938.53	-52.59	1044.41	-54.59	1150.79	-56.59	1257.74	-58.59	1365.32	-60.59	1473.57	-62.59	1582.56	-64.59	1692.37	-66.59
A2	109.863	-41.88	219.743	-40.62	329.697	-41.88	439.777	-43.88	550.038	-45.88	660.535	-47.88	771.321	-49.88	882.45	-51.88	993.976	-53.88	1105.95	-55.88	1218.43	-57.88	1331.46	-59.88	1445.1	-61.88	1559.4	-63.88	1674.4	-65.88	1790.17	-67.88
A#2	115.407	-43.19	232.833	-41.94	349.34	-43.19	465.987	-45.19	582.834	-47.19	699.94	-49.19	817.366	-51.19	935.17	-53.19	1053.41	-55.19	1172.15	-57.19	1291.44	-59.19	1411.34	-61.19	1531.92	-63.19	1653.22	-65.19	1775.33	-67.19	1898.21	-69.19
B2	122.339	-44.50	246.699	-43.30	370.142	-44.50	493.73	-46.50	617.525	-48.50	741.589	-50.50	865.984	-52.50	990.771	-54.50	1116.705	-56.50	1241.76	-58.50	1368.09	-60.50	1495.05	-62.50	1622.71	-64.50	1751.11	-66.50	1880.33	-68.50	2010.92	-70.50
C3	130.683	-45.79	261.387	-44.57	392.173	-45.79	523.103	-47.79	654.238	-49.79	785.64	-51.79	917.369	-53.79	1049.49	-55.79	1182.05	-57.79	1315.13	-59.79	1448.78	-61.79	1583.05	-63.79	1718.01	-65.79	1853.72	-67.79	1990.23	-69.79	2127.6	-71.79
C#3	138.464	-47.09	276.948	-46.04	415.516	-47.09	554.229	-49.09	693.15	-51.09	832.341	-53.09	971.864	-55.09	1111.786	-57.09	1252.15	-59.09	1393.04	-61.09	1534.5	-63.09	1676.6	-65.09	1819.4	-67.09	1962.96	-69.09	2107.32	-71.09	2252.57	-73.09
D3	146.706	-48.39	293.424	-47.44	440.189	-48.39	587.036	-50.39	734.002	-52.39	881.122	-54.39	1028.43	-56.39	1175.96	-58.39	1323.73	-60.39	1471.84	-62.39	1620.25	-64.39	1769.03	-66.39	1918.21	-68.39	2067.82	-70.39	2217.89	-72.39	2368.47	-74.39
D#3	155.458	-49.69	310.889	-48.62	466.392	-49.69	621.987	-51.69	777.712	-53.69	933.607	-55.69	1089.71	-57.69	1246.06	-59.69	1402.7	-61.69	1559.66	-63.69	1716.99	-65.69	1874.72	-67.69	2032.89	-69.69	2191.54	-71.69	2350.92	-73.69	2510.42	-75.69
E3	164.689	-50.99	329.393	-49.86	494.156	-50.99	659.029	-52.99	824.04	-54.99	989.249	-58.99	1154.7	-60.99	1320.43	-62.99	1486.48	-64.99	1652.91	-66.99	1819.75	-68.99	1987.05	-70.99	2154.84	-72.99	2323.19	-74.99	2492.12	-76.99	2661.68	-78.99
F3	174.49	-52.39	349.019	-51.02	523.709	-52.39	698.679	-54.39	874.049	-56.39	1049.94	-58.39	1228.46	-60.39	1403.75	-62.39	1581.9	-64.39	1761.04	-66.39	1941.29	-68.39	2122.75	-70.39	2305.55	-72.39	2489.19	-74.39	2675.57	-76.39	2863.02	-78.39
F#3	184.873	-53.69	369.79	-52.86	554.88	-53.69	740.275	-55.69	926.104	-57.69	1112.5	-59.69	1299.58	-61.69	1487.49	-63.69	1676.34	-65.69	1866.27	-67.69	2057											