Piano Tuning Method

Zuheng Kang

CONTENTS

Αŀ	ostract		2
	Project	t Location	2
1	Intro	oduction	2
2	Tecl	hnical Knowledge	3
	2.1	Key Names	3
	2.2	Key Numbers	3
	2.3	Functions	3
	2.4	Tuning Methodology	4
3	Pian	no Tuning Method	4
	3.1	Traditional Method	4
	3.1.	1 Sampling Piano	4
	3.1.2	2 Audio Processing	4
	3.1.3	3 Frequency Analysis	4
	3.1.4	4 Catchup Overtone	5
	3.1.	5 Inharmonicity Model	6
	3.1.6	6 Tuning Curve Optimization Model	8
	3.1.	7 Temperament Model	11
	3.1.8	8 Creating Tuning Strategy Table	12
	3.2	Entropy Tuning Method	12
	3.2.	1 Sampling Piano & Audio Processing	13
	3.2.2	2 Construct Spectrum	13
	3.2.3	3 Tuning with Entropy Optimizer	13
	3.2.4	4 Creating Tuning Strategy Table	15
	3.2.5	5 Tune for Songs	16
4	Aud	lio Processing & Pure Sound Tuner	17
	4.1	Tuning	17
	4.2	Sound Purify	17
5	Futu	ure Work	19
6	Refe	erence	19
7	App	oendix	20

ABSTRACT

Since the piano string is considered to be a stick rather than a pure ideal string, it contains stiffness and its overtone will shift in such way that makes piano tuning a difficult work. In this work, two optimization algorithm for the piano tuning method is presented. The traditional tuning algorithm is divided into several models that using various fitting technique model the target piano, and then convert to linear regression problem for optimization. The entropy tuning method is a trial method to tune the piano to minimize the entropy value when all keys are pressed – to achieve a simpler spectrum in pitch domain. In addition, a pure tuner method is invented to get rid of all inharmonic effect of piano sound.

Keyword: piano tuning, inharmonicity, entropy, audio processing

PROJECT LOCATION

Reference [2]

1 INTRODUCTION

Piano tuning is a difficult work since the frequency peaks shift that makes the piano hard to tune. The tuning process will be a task to highly reduce the audible cacophonous. There are several factors we need to consider, which the rule of harmony is.

- The cacophonous created by its base frequency and audible harmonics; a good tuning will largely reduce the inharmonic effects for harmonies (the frequency domain should be simple, which the frequency peaks should merge or coincide).
- The inner music scales related pitch; the odd pitch tuning will result in the weird effect when playing music scales.

Other famous related works are:

- Tunelab (closed source; has a trial version)
- Reyburn CyberTuner (closed source; no trial version)
- Entropy Piano Tuner (open source) [1]

The first two are similar, which represent the old tuning techniques, and my work mostly focuses on this algorithm.

As for Entropy Piano Tuner, it represents the new way of piano tuning. It can also achieve a very good result for tuning a piano, however, this temperament is not a regular 12-equal temperament, but a piano approximation temperament starting from 12-equal temperament, in order to largely eliminate the non-harmonious effect.

- Since the pitch in the piano does not have relatively same pitch interval, some inner scales sound weird.
- Since the piano optimizes all 88 keys harmony, it values overall harmonious some simpler chord might not sound harmonious.
- It only considers the sound which at the certain striking level of piano keys, which result in the optimization of keys are based only on the given key pressing level. However, it values the average case for piano performance, thus it covers the majority situation of harmony cases.
- The accuracy cannot be too high due to a large amount of calculation, it does not achieve an ideal result.

In my work, I will talk about two piano tuning methods and one audio processing method.

- As for traditional tuning method, since it is closed source, I guessed their tuning method and create a similar solution, and will be shown in this article. Besides, I used more accurate model for inharmonicity coefficients.
- I will reproduce the result for the Entropy Piano Tuning method.

The tuning for audio and a pure sound tuner is introduced.

In this article, the first part is to introduce the technical knowledge of high-level modeling algorithms. The second part is to introduce my piano modeling and tuning optimization method. Then, followed an audio processing technique. Finally, the future work will be introduced.

2 TECHNICAL KNOWLEDGE

2.1 KEY NAMES

The leftmost key name is defined as "A0", where "A" is the note name, 0 is the scale number. "C" is the starting point of one scale. It only allowed sharp in the note, flat is not allowed in this naming format.

There are 88 keys for standard piano.

2.2 KEY NUMBERS

In the real world, the piano key will be labeled with numbers when the piano is open and machine part is shown off.

A0 key is labeled to be 1, and "C8" is 88.

However, in my program, "A0" key is labeled as 0 for easier calculation, which is defined as k.

2.3 Functions

Frequency ratio to cents function:

$$\operatorname{Fr}_{\to c}(\gamma) = 1200 \log_2(\gamma) \tag{2.1}$$

The inverse process is:

$$C_{\rightarrow fr}(c) = 2^{\left(\frac{c}{1200}\right)} \tag{2.2}$$

Where cents is from 12-equal-temperament, each half note has 100 divisions, named cents.

Frequency add cents (pitch) function:

$$F_{+c}(f,c) = f \cdot 2^{\left(\frac{c}{1200}\right)}$$
(2.3)

This function returns the frequency that added the pitch (cents) c.

The ideal frequency for the key k is:

$$\tilde{f}_k = \tilde{f}_{[A4]} \cdot 2^{\left(\frac{k-48}{12}\right)} \tag{2.4}$$

Where $\tilde{f}_{[A4]}$ is the international standard pitch for "A4", usually defined as 440Hz. Another tuning standard will replace this number, 48 is the key number for "A4".

2.4 TUNING METHODOLOGY

Since the minor tuning for each string will rarely affect its stiffness, from Equation (3.3), we assume that the B_k is the constant.

3 PIANO TUNING METHOD

3.1 Traditional Method

The traditional tuning method is to match the specific frequency peaks that aimed at largely eliminating the "beat" (pitch differences from two notes; for example, "A3's" second overtone matches its octave "A4", which is denoted to be 2:1). Then, use a smooth curve to optimize/minimize all the differences to achieve a relatively good result.

Since the piano sound overtone shift (inharmonicity) has a very nice relation, it enables us to just sample very few keys and guess all the properties for all piano; then, get the tuning strategy.

3.1.1 Sampling Piano

Before tuning a piano, we need to sample a piano by recording few piano keys sound audios. This process will roughly or precisely measure the inharmonicity of piano strings (which will talk about later), such that we could model the inharmonicity for the targeted piano.

The sampling is suggested to measure keys "C1", "C2", "C3", "C4", "C5" (and probably "C6"; the user could record more piano keys such as "A1" ~ "A6" for better result). Since the tuning inharmonicity curve is a smooth curve and predictable, thus it is possible to sample fewer notes. The piano key sound should be recorded in a quiet environment, which allows more accuracy for later frequency analysis. In this sampling process, we need to press the key hard in order to get higher harmonic peaks for measurement.

In my program, I use fully or almost fully sampled piano for research purposes.

3.1.2 Audio Processing

Since the real audio may contain the white space at the start or the end, and the sound length varies. I use this method to process my sampled audio:

- Normalize (N(x) = x / max(x)) the audio file into 1, then, find the peak volume of audio, and start from here.
- Slice these audio pieces into tiny partitions, say 0.1 second is one partition. The maximum number of each partition will be its assumed volume at this time point.
- Trim the audio at the volume starting from some large number to a small number since the piano sound is loud from its beginning and decay by the time. Say from 90% to 2% of the sampled sound audio.



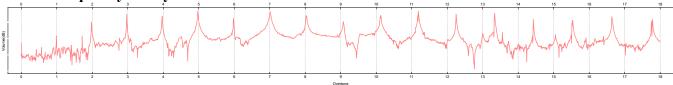


Figure 3-1 "A#0" Key (at Upright Piano Samples) Overtone Plot; Volume at Logarithm Scale

Then, put this audio sample into Fourier analysis (FFT algorithm). Then we get the function $G_k(f) = \|FFT(S_k(t))\|_2$ where $S_k(t)$ is the audio function, and $G_k(f)$ is the frequency domain function, k is

piano key number, f is the frequency variable, $\|\cdot\|_2$ is the 2-norm of complex numbers. In our work, the frequency domain is converted to the ratio to its ideal fundamental frequency, thus we can see the Figure 3-1, the peaks will always almost lies in the grid by dividing its ideal frequency.

From Figure 3-1, we can see that the higher overtone (right-hand side peaks with larger numbers) shifts higher.

It is a problem to capture all these peaks numbers since some are not clear: the fundamental frequency (at 1), and some have multiple peaks: at $15 \sim 16$.

In my work, I use the frequency Catchup Method to get octave values for all these peaks.

3.1.4 Catchup Overtone

From the characters of these peaks, there are several characters will be considered:

- From left to right, the gap between two peaks is increasing gradually.
- The largest value of this plot is probably some peak of overtone
- The valid peak should be nearly larger than fundamental frequency position: at 1.
- The peak may be broken into several peaks, we need to centralize the targeted position.

From this characteristic, the *Catchup Method* could be built:

- Analyze the frequency samples which roughly larger than 1 (my program is starting from 0.8), get the peak frequency $f_{k,peak}$ at the key number k and overtone number peak.
- Comparing with ideal frequency \tilde{f}_k . We can then assume that it is $n = \text{round}\left(f_{k,peak} / \tilde{f}_k\right)$ harmonics. Then, we can know its guessed fundamental frequency is $\hat{f}_k = f_{k,peak} / n$. Then, this should be the step size for catchup method.
- The catchup method is forward (going to the right), and the backward (goes to the left). If we are in the forward operation, the next guessed target frequency is $\hat{f}_{k,peak+1} = f_{k,peak} + f'_k$, where f'_k is the assumed gap between two peaks at this position. On the first try, we set this number to $f'_k = \hat{f}_k$, and this number will be increasing for more right harmonics. Then, we get data around it (in a relatively small area) for guessed target frequency $\hat{f}_{k,peak+1} \pm \delta$. We can find its maximum number these data to be the frequency candidate $\hat{f}_{k,peak+1}^{candidate}$, then we get the data of smaller surrounding area $\hat{f}_{k,peak+1}^{candidate} \pm \delta'$ where $\delta' << \delta$. Then, we calculate the weighted average for this smaller area, and the result is the actual frequency of this peak $f_{k,peak+1} = \int_{\hat{f}-\delta'}^{\hat{f}+\delta'} \omega \cdot G(\omega) d\omega$, where ω is proportional to frequency. Then, the assumed gap between two peaks at this step is updated to be $f'_k = f_{k,peak+1} f_{k,peak}$.
- Iterate this method for "forward catchup" to get all higher frequencies.
- If the highest peak is not fundamental frequency, we will perform the backward catchup. Since there are fewer peaks and the overtone shift will be far less than the right, the assumed targeted gap between two peaks is set to be the assumed fundamental frequency \hat{f}_k .

From this method, we can get an overtone (frequency) list for the key k. Which is:

$$k \to \{f_{k,1}, f_{k,2}, ...\}$$
 (3.1)

3.1.5 Inharmonicity Model

From Figure 3-1, we can see that the overtone will shift higher and higher as the frequency goes higher. This effect is caused by the stiffness of an object, its natural frequency will follow a certain pattern.

From reference [1], we assume that the piano string is a bar with two fixed ends, which approximately follows the partial differential equation:

$$\ddot{y} \propto -y'' - \varepsilon y'''' \tag{3.2}$$

Where y is the special position of piano string (bar model). The prime is the derivative to the spatial domain, and dots are the derivative to the time domain.

Then, use the modal analysis and solved the natural frequencies of this string are:

$$f_{k,n} \propto n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \Rightarrow f_{k,n} = A_k \cdot n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2}$$
(3.3)

Here we have two unknown variables A_k and B_k .

Then, we use this function to fit all frequency results at Equation (3.1). The parameter A_k is set for not all fundamental frequency is guessing perfectly. We can ignore this number by making sure the fundamental frequency always targets at 1, and focus only on B_k .

Then, we can get inharmonicity parameter list $\{\{k, B_k\}\}$.

From my observation, the logarithm of this number has some beautiful properties with the data $\{\{k, \ln(s \cdot B_k)\}\}$, where s is a scaling parameter (I set to 10000).

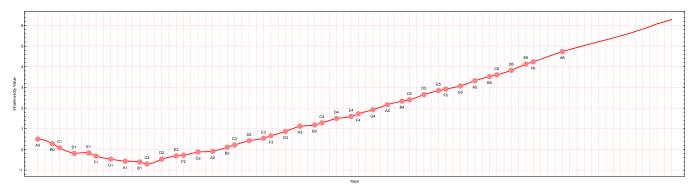


Figure 3-2 Inharmonicity Plot of Grand Piano IH(k)

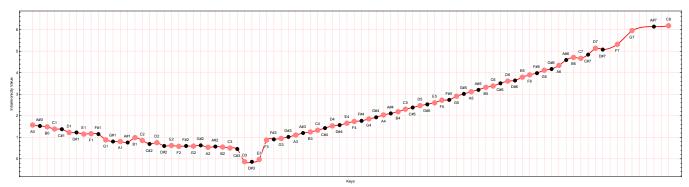


Figure 3-3 Inharmonicity Plot of Upright Piano IH(k)

From Figure 3-2 and Figure 3-3, we can clearly see the line is divided into 2 parts.



Figure 3-4 Grand Piano String Arrangement



Figure 3-5 Upright Piano String Arrangement

From Figure 3-4 and Figure 3-5, we can clearly see that the string is divided into two parts, withhe steel string and copper string (may be covered by silver for highly expensive pianos). The upright piano has more copper strings since the steel string cannot go longer, and the string will become thicker to make the string vibrate slower. From spring vibration formula:

$$\omega = \sqrt{\frac{K}{m}} \tag{3.4}$$

Where ω is proportional to frequency, m is the mass of spring, K is the stiffness of the spring.

When m increases, K increase a little bit, ω decreases, then frequency decrease.

Since the piano cannot grow longer, it becomes thick and more like a stick rather than an ideal string. For higher notes strings, it is too short, and the thickness becomes relatively larger compared to its length, thus it is more likely to be a bar.

Thus, from the plot, we can see the inharmonicity increases at two ends, and break at the position of separation of two kinds of strings.

Since the grand concert piano is longer and can have more steel strings, fewer copper strings, thus the break will become a more left side.

The figure of inharmonicity plot also tells us that two separate lines are almost linear. In my model, I used the valid sampled points are modeled with an interpolation function, and the two edges are modeled with a linear function, and it is method is shown below.

- We get several samples from one line and fit in a linear form.
- Get its slope, and build a line which passes the right-endpoint (since I will not wish to have a break for the interpolation function), and add some samples for edges situation to sample pool.
- Similar to the left-hand side.
- We use interpolation for these samples of sample pool—"left-hand side + samples + right-hand side", which is our final model for inharmonicity model function IH(k).

$$IH(k) = \ln(s \cdot B_k) \tag{3.5}$$

Thus, we can have the modeled parameter B_k with:

$$B_k = \frac{e^{\mathrm{IH}(k)}}{s} \tag{3.6}$$

Then, the frequencies $\tau(k, n)$ will be:

$$\tau(k,n) = f_{k,1} \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}}$$
(3.7)

Where $f_{k,1}$ is currently unknown but it will be eliminated since it is in frequency ratio form. In this equation, we divide a term $\sqrt{1+B_k}$ to make sure the fundamental frequency is $f_{k,1}$.

3.1.6 Tuning Curve Optimization Model

Similar to Tunelab ®, I set the tuning optimization method to separate the lower tones (bass) and higher tones (tenor) into two tuning target optimization method, the separation point k_0 is "C#4/D4". And the default tuning method for bass is to set 6:3. Since 6/3=2 (a/b), this frequency ratio is $\gamma = a/b$, and its corresponding pitch range is $Fr_{\to c}(\gamma)$ which is 1200, and 1200 is an octave, it means the tone say "A0"s 6^{th} harmonics will largely match its octave's "A1"s 3^{rd} harmonics.

Here pitch is defined by cents.

The error function \mathcal{E}_k is defined as:

$$\varepsilon_{k} = \operatorname{Fr}_{\to c} \left(\frac{\tau(k, a)}{\tau(k + Fr_{\to c}(a/b), b)} \right) \\
= \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k} \cdot a^{2}\right) \cdot \left(1 + B_{k + Fr_{\to c}(a/b)}\right)}{\left(1 + B_{k + Fr_{\to c}(a/b)} \cdot b^{2}\right) \cdot \left(1 + B_{k}\right)} \cdot \frac{a}{b} \cdot \left(\frac{f_{k, 1}}{f_{k + Fr_{\to c}(a/b), 1}} \right) \right) \\
= \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k} \cdot a^{2}\right) \cdot \left(1 + B_{k + Fr_{\to c}(a/b)}\right)}{\left(1 + B_{k + Fr_{\to c}(a/b)} \cdot b^{2}\right) \cdot \left(1 + B_{k}\right)}} \right) \tag{3.8}$$

We can do this for all bass strings.

For tenor strings, the default tuning method is set to 4:1 (c/d). But this time we count the higher note as the target to calculate.

$$\varepsilon_{k} = \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k - Fr_{\to c}(c/d)} \cdot c^{2}\right) \cdot \left(1 + B_{k}\right)}{\left(1 + B_{k} \cdot d^{2}\right) \cdot \left(1 + B_{k - Fr_{\to c}(c/d)}\right)}} \right)$$
(3.9)

The combined expression is:

$$E(k) = \begin{cases} Fr_{\to c} \left(\sqrt{\frac{\left(1 + B_k \cdot a^2\right) \cdot \left(1 + B_{k+Fr_{\to c}(a/b)}\right)}{\left(1 + B_{k+Fr_{\to c}(a/b)} \cdot b^2\right) \cdot \left(1 + B_k\right)}} \right) & k \le k_0 \\ Fr_{\to c} \left(\sqrt{\frac{\left(1 + B_{k-Fr_{\to c}(c/d)} \cdot c^2\right) \cdot \left(1 + B_k\right)}{\left(1 + B_k \cdot d^2\right) \cdot \left(1 + B_{k-Fr_{\to c}(c/d)}\right)}} \right) & k > k_0 \end{cases}$$
(3.10)

From this equation, we can see E(k) is only a value for calculation at given k.

From this point, we need a function to largely eliminate these errors. The piano tuning curve C(k) is introduced, it represents the deviation of the actual tuning pitch to the ideal 12-equal temperament pitch.

The optimizer deviation function D(k) is:

$$D(k) = C(k) - E(k)$$
(3.11)

The cost function J(k) for optimization is:

$$J(k) = \sum_{k} (D(k))^{2}$$
(3.12)

Which minimize the square error of these functions.

Here I use polynomial for easier calculation:

$$C(x) = \sum_{i=1}^{n} \chi_i \cdot x^i$$
 (3.13)

Since C(x) will pass the fixed point, which is "A4" pitch at a 440Hz frequency at pitch deviation of 0, thus i is from 1 and $x = k - k_{A4}$, where k_{A4} is the key number (index) at "A4", which is 48.

Thus, J(k) is the second order multi-variable polynomial function, which is very easy to minimize by linear regression method to calculate the fitting parameter $\{\chi_i\}$, and rebuild the functions.

Then, we can bring $\{\chi_i\}$ to the $\mathrm{D}(k)$ function to calculate its deviations.

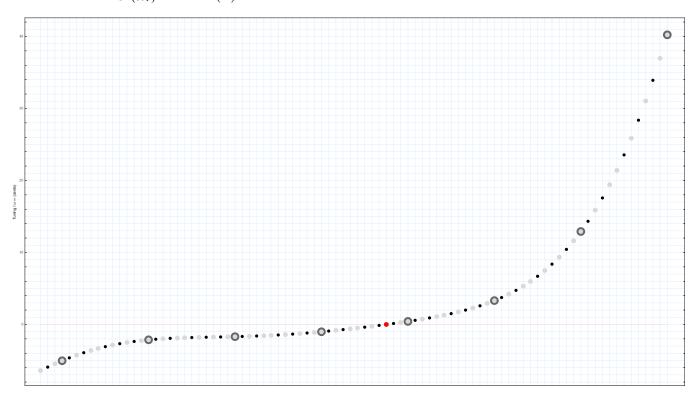


Figure 3-6 C(k) for Grand Piano



Figure 3-7 D(k) for Grand Piano

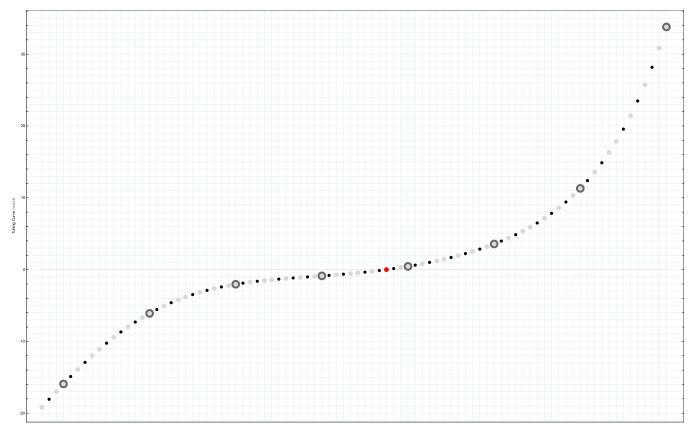


Figure 3-8 C(k) for Upright Piano

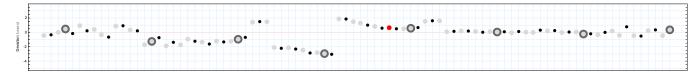


Figure 3-9 D(k) for Upright Piano

The result of two pianos is shown above. The horizontal axis is the key number and the vertical axis of the pitch interval with its ideal frequencies represented by cents.

From this tuning method, we can see that the bass tuning will consider the deviations from the tenor part, and vice versa. The effect is inner related. Thus, this tuning method is theoretically to optimize almost the whole piano keys tuning.

3.1.7 Temperament Model

With the development of music, various temperaments appear and create the unique flavor of music. The temperament model is using the pitch deviation tables of different temperament (the unit is cent). We can then create the non-12 equal temperament tuning strategy. The temperament function is defined to be T(k).

The tuning table such as "Bach - Bradley Lehman" is:

C	C #	D	D#	E	F	F#	G	G#	A	A #	В
5.87	3.91	1.96	3.91	-1.96	7.82	1.96	3.91	3.81	0	3.91	0

Table 3-1 Table for "Bach - Bradley Lehman" Temperament

Where A note will always be 0 since A is the reference frequency and will always keep to 440 Hz (if is standard situation).

This table shows the situation of "C" major.

The other major tuning will follow the rotation of the table. For example: if tuning "D" major, the "D" will rotate to current "D" \rightarrow "C" place, which is rotating left 2 times. However, we will make sure "A" note will always be 0, then, we can subtract the number at "B" \rightarrow "A" to make it possible.

Then, add these pitch errors to all the notes of tuning, the modified tuning curve is:

$$C'(k) = C(k) + T(k)$$
(3.14)

3.1.8 Creating Tuning Strategy Table

The final tuning strategy $\tau(k,n)$ (unit: Hz) is:

$$f_{k,1} = F_{+c}\left(\tilde{f}_k, C'(k)\right)$$

$$\tau(k,n) = f_{k,1} \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}} f$$

$$= F_{+c}\left(\tilde{f}_k, C'(k)\right) \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}}$$

$$= F_{+c}\left(\tilde{f}_k, C'(k)\right) \cdot n \cdot \sqrt{\frac{s + e^{\mathrm{IH}(k)} \cdot n^2}{s + e^{\mathrm{IH}(k)}}}$$

$$(3.16)$$

From Equation (3.16), we can see only $C(\cdot)$ and $IH(\cdot)$ function is modeled function, other functions are basic mathematics functions.

From the modeling, we can get a strategy of piano tuning, then we can convert this strategy into a tuning table, which shows all the frequency of fundamental and its overtone frequencies, and corresponding deviation to ideal frequencies represented by cents.

The grand and upright piano tuning strategy is shown in Figure 7-1 and Figure 7-2.

The red font is the frequencies recommended for the devices to tune.

3.2 Entropy Tuning Method

The entropy tuning method is not to model the exact value of frequencies or pitches, it simulates the condition that simultaneously presses down all piano keys, and uses entropy method as the cost function to largely merge the peaks at pitch domain to create sharper and simpler sound for piano, which optimizes the piano sound. The method is extremely simple, however, it is really computational intensive.

Why simulate pressing all keys? We need to know the philosophy of piano in behind. To deal with all kinds of complicated situations, let us assume several cases. Whether the chord is harmonious is to check the transient pitch domain. In the other word, several notes at certain short time period will contact with each other, and we need to make sure this sound is harmonious. However, the contact cases of notes at all time for all songs are too complicated, and the key pressing level varies all the time. What if assuming that all notes have equal probability to contact, and the key pressing level when playing each small piece of music on average is the same – some pieces are loud, some

are small but they usually approximately on the same level when playing the piano. As for the key pressing level that could change the sound quality, we suggest the sample sound will be played in medium level.

3.2.1 Sampling Piano & Audio Processing

In the entropy piano tuning method, sampling every piano key is necessary. Another requirement is similar to a traditional method. The audio processing is also similar to a traditional method.

3.2.2 Construct Spectrum

Since the human ear is sensitive to the pitch ("pitch" is equivalent to the logarithm of a frequency component for approximation: ignore the nonlinear effect of ear structures) within the hearing range (20Hz ~ 10000 Hz is reasonable for optimizing algorithm). Thus, the model should be built by putting equal significance to the pitch scale. Traditionally, the pitch is represented as music note. If we evaluate the "pitch" content/data by equally sampling from the pitch scale of the spectrum, it puts the equal importance to the pitch scale – the logarithm scale of frequencies. In my experiment, I put 0.1 cents as the precision.

Then, we have the converted the spectrum into pitch domain $I(\kappa)$, to resample the data with the key number:

$$I(\kappa) = \left\| G(f_{\kappa}) \right\|^{\beta} \Big|_{\kappa \to 12 \cdot \log_2\left(\frac{f_{\kappa}}{\hat{f}_{[A0]}}\right), \beta \to 2}$$
(3.17)

Where for each key k we will have 1000 samples in total, each sample's pitch denote as κ . Namely, each sample will represent 0.1 cents. Since the audio is also the limited samples, I use the interpolation function to resample the data.

In this model, I use the square of the spectrum $\beta = 2$. The reason is that: although human ear sensitive to the sound pressure level is based on the logarithm of magnitude of sound, unit could be decibel (dB), however, the human ear also has the auditory mask, which masks small peaks around it, thus we should value more on major peaks, and ignore minor one. From the paper [1], and my trial and error, the power of 2 is actually achieved a very ideal result. I also tried other numbers for β , when $\beta = 1$, the sound is messy at all; $\beta = 2$ is perfect; β is larger, the simpler sound will hear more harmonious, however, the complicated chord may not hear well since the algorithm may value more on merging major peaks of the spectrum and ignore the little ones. If people need to play more simple chord songs, they may try larger numbers of β , if need to play more messy types of songs like Impressionist or Jazz, I suggest they will use smaller β . On average, 2 is a great number for β .

Since for each key sound, the first peak of the spectrum should start from its fundamental frequency, thus, we will set values to 0 for frequencies that lower than fundamental frequency to ignore bass noise.

3.2.3 Tuning with Entropy Optimizer

The tuning process from a programming point of view is to move left or right of the array $I(\cdot)$ as minor tuning process with +c cent shift.

$$I_{k}(\kappa - c) = \left\| G(f_{\kappa - c}) \right\|^{\beta} \tag{3.18}$$

The entropy function is defined as:

$$Entropy(x) = -x \cdot \log(x) \tag{3.19}$$

The entropy for a function is defined as:

Entropy
$$(\phi(x)) = \int_{-\infty}^{+\infty} (-\phi(x) \cdot \log(\phi(x))) dx$$

= $\sum_{x} (-\phi(x) \cdot \log(\phi(x)))$ (3.20)

Where $\phi(\cdot)$ is the density function:

$$1 = \int_{-\infty}^{+\infty} \phi(x) dx$$

$$= \sum_{x} \phi(x)$$
(3.21)

3.2.3.1 How to calculate the entropy value for the optimizer.

Since the algorithm optimize the case that all sound volume is equal, however, the sampling time is different, we will make a standard case to simulate all keys are pressed in an equal key pressing level. In my program, I use density function $\overline{I}_k(\kappa)$ to simulate the equal key pressing level for each piano key sound in pitch domain:

$$\overline{I}_{k}(\kappa) = \frac{I_{k}(\kappa)}{\sum_{\kappa} (I_{k}(\kappa))}$$
(3.22)

When press all piano keys, the total volume $V(\kappa)$ for each key pitch shift $+c_k$ cents for tuning is:

$$V(\kappa) = \sum_{k} (\overline{I}_{k} (\kappa - c_{k}))$$
(3.23)

The density function for this function is:

$$\overline{V}(\kappa) = \frac{V(\kappa)}{\sum_{\kappa} (V(\kappa))}$$
(3.24)

Then, the cost function value J (entropy value for function $\overline{V}(\kappa)$) is:

$$J = \sum_{\kappa} \left(-\overline{V}(\kappa) \cdot \log(\overline{V}(\kappa)) \right)$$
(3.25)

3.2.3.2 Steps to calculate a tuning strategy

In my program, there are several steps to dig out the good strategy for tuning.

- Step 1: Calculate the traditional tuning strategy which is a simpler version of the Traditional Tuning strategy, to be the initial starting point for entropy minimizer to begin. In this algorithm, no inharmonicity model is built, but just uses the captured frequency to optimize.
- Step 2: Randomly change tuning for one key for c_k cents, and check its entropy value. If the entropy value is smaller than last time, we keep this tuning strategy, otherwise, drop. Where the changing pitch is defined as a random number between 0 to some small number p. We will try both sides of tuning by adding and subtracting the pitches. The "A4" key never changes, since it is a standard pitch.
- Step 3: We do "step 2" experiment for all keys and all directions as one round of experiments. Each time we count the times of successfully tuned until we cannot find one round with no improvement.

Step 4: We stop the algorithm with the test for p precision. Then we shrink the p and more accurate spectrum data (more data), and calculate "Step 2" and "Step 3"

Step 5: Calculate tuning strategy and get the report.

In this process, "Step 1" is because the algorithm has many local minimums; although some local minimum can achieve similar simple and sharp harmony, it performs badly in simpler harmonies, such as an octave. A traditional tuning method can roughly optimize major overtones, the best result for entropy minimizer should be around the traditional tuning strategy.

In "Step 2", although there should be more improvement during this step, however from a probability point of view, when it stops, the result is good enough for this precision. It could also use the parallel algorithm. In my program, I modeled several CPUs (not GPU program this time: GPU should calculate array sum much faster) with one shared memory to modify the result altogether. Although all CPUs will affect the overall result, however, if we can understand it will stop at the point that several CPUs could not find improvement, the effect is the same.

In "Step 4", my program uses 3 round with 1, 0.5 and 0.2 cent boundaries as step size for entropy minimizers. Since there are many local minimums, and we need to achieve a smooth tuning strategy for not creating weird music scale sound, we cannot set the step size to be really large. Thus, 1 cent boundary is a good point to start. The next two round are precise tuning, the accuracy will be increased to 0.1 cent, which is desirable.

In "Step 5", the frequency peak frequencies $f_{k,n}$ are also captured by "catchup method", but without weighted average.

3.2.4 Creating Tuning Strategy Table

The method to get the frequency components of each key sound is simple:

$$\tau'(k,n) = f_{k,n} \cdot C_{\to fr}(c_k) \tag{3.26}$$

However, this process is problematic. Since the whole process is based on pitch shift with a certain precision, the "A4" standard frequency will not be the fixed number. Here we need to eliminate this tuning error by introducing a correction factor $\varepsilon_{[A4]}$:

$$\varepsilon_{[A4]} = \frac{\tau'([A4],1)}{\tilde{f}_{[A4]}} \tag{3.27}$$

Thus, the tuning strategy $\tau(k,n)$ is modified to be:

$$\tau(k,n) = f_{k,n} \cdot C_{\to fr}(c_k) \cdot \varepsilon_{[A4]}$$
(3.28)

To build the tuning curve, the pitch deviation to the ideal frequency function C(k) is shown:

$$C(k) = \operatorname{Fr}_{\to c} \left(\frac{\tau(k, n)}{\tilde{f}_k} \right) \tag{3.29}$$

The tuning strategy is shown in Figure 7-3.

The tuning curve is shown in Figure 3-10, the spectrum of the optimized result is shown in Figure 3-11:

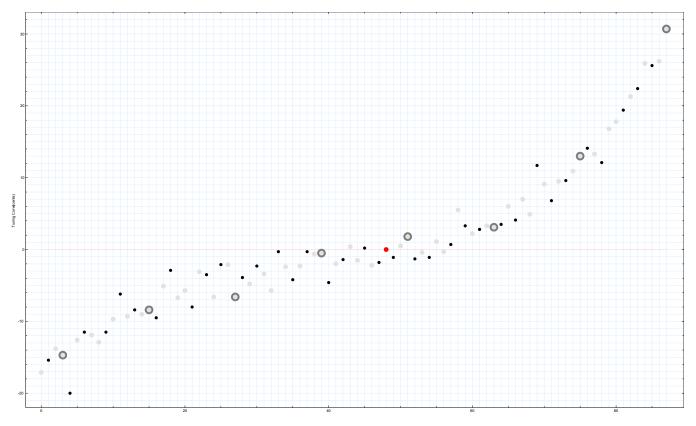


Figure 3-10 Tuning Curve for Upright Piano Optimized by Entropy Minimizer

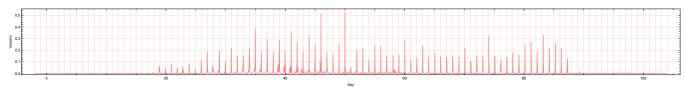


Figure 3-11 Spectrum for Optimized Result

From Figure 3-11, we could see the spectrum are largely merged. From the sound quality point of view, the harmony will sound sharp and clear.

3.2.5 Tune for Songs

In the real world, some of the piano keys have not been used, especially for the simpler tonal music. Since I have mentioned the previous entropy minimizer is not quite suitable for simpler harmony music due to some of the simple harmony like octave sometimes will not sound perfect, we should ignore the keys that have not been used. Thus, I add another coefficient for the entropy minimizer.

We will put the bias $Bias_k$ that will ignore the key k which have not been used.

$$\operatorname{Bias}_{k} = \begin{cases} 1 & k \in used \\ \varepsilon_{\operatorname{Bias}} & k \notin used \end{cases}$$
 (3.30)

Where $\varepsilon_{\text{Bias}}$ is a very small number – to make sure the key which is not used could be tuned by the entropy minimizer. If the bias for one key is 0, there is no spectrum for entropy minimizer for this key, and the algorithm

will stop tuning for this key. However, if we put a very small number as weight on this key, it still can be tuned to a correct place – it just tuned, but does not affect the tuning for other keys.

Then, we will put the bias on the entropy minimizer algorithm and modify the Equation (3.25):

$$J = \sum_{\kappa} \left(-\operatorname{Bias}_{\kappa} \cdot \overline{V}(\kappa) \cdot \log(\overline{V}(\kappa)) \right)$$
(3.31)

Then, we use the method above to minimize this entropy function and get the tuning strategy.

From the example of one tonal music from Mozart Piano Sonata No 11 A major K 331 – Movement 1 (Figure 3-12), we could see only the middle range and several low range keys are used.



Figure 3-12 Song Key Used Cases

The optimized spectrum is shown in Figure 3-13.

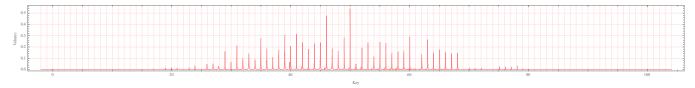


Figure 3-13 Optimized Spectrum

From this example, we can see and hear, the sound will be more optimized whenever in simple and complicated harmonies.

4 AUDIO PROCESSING & PURE SOUND TUNER

4.1 TUNING

Tuning process in an audio is to create samples for the virtual instrument so that we can hear the tuning result before tuning process to make a decision whether to adopt or drop this tuning strategy.

The sound function S(t) tunes in order to add pitch c cents:

$$S_{+c}(t) = S\left(t \cdot 2^{\left(\frac{c}{1200}\right)}\right) \tag{4.1}$$

The S(t) function is modeled as an interpolation function.

4.2 SOUND PURIFY

This audio processing technique is invented by myself. It removes the inharmonic effect of piano sound.

Since the inharmonicity model has been built, it is possible to use the audio processing technique to shrink the harmonics in order to remove the inharmonicity.

If the key k sound with the inharmonicity coefficient $\mathrm{IH}(k)$ and tuned to the fundamental frequency to be the frequency (ideal frequency) \tilde{f}_k ; the f_k is the fundamental frequency.

We firstly get the FFT of the audio sample with $\Gamma_k(f)$ of complex number samples:

$$\Gamma_{k}(f) = FFT(S_{k}(t)) \tag{4.2}$$

Since the FFT is creating an almost symmetry data from the middle, we can extract this data into 4 parts: the real head data $\Gamma_k^{(0)}(f)$, the imaginary head data $\Gamma_k^{(1)}(f)$, the real tail reverse data $\Gamma_k^{(2)}(f)$ and the tail imaginary reverse data $\Gamma_k^{(3)}(f)$. Four of them looks similar, however, it contains all the details of the sound. Since it samples the piano keys, the spectrum is pretty obvious. At its high frequencies, it is almost 0, and it is almost out of hearing range, thus if we need to compress the frequency domain, as for higher frequencies, we could regard it to be 0. For each component we write it as $\Gamma_k^{(m)}(f)$, where m is from 0 to 3 (4 cases), i is the unit imaginary number.

$$\Gamma_{k}(f) = \left\{ \Gamma_{k}^{(0)}(f), \operatorname{rev}\left(\Gamma_{k}^{(2)}(f)\right) \right\} + \left\{ \Gamma_{k}^{(1)}(f), \operatorname{rev}\left(\Gamma_{k}^{(3)}(f)\right) \right\} \cdot i \tag{4.3}$$

From Equation (3.6) and Equation (3.7), we could get the compression functions, which is $\tau(k,n)$. Here the overtone is continuous, which is f/f_k , rather than n. Thus, we have the compressed frequency scaler \ddot{f}_k and its pitch component $\ddot{\Gamma}_k^{(n)}(f)$:

$$\ddot{f}_k = \tilde{f}_k \cdot \tau \left(k, \frac{f}{f_k} \right) \tag{4.4}$$

$$\ddot{\Gamma}_{k}^{(m)}(f) = \begin{cases}
\Gamma_{k}^{(m)}(\ddot{f}_{k}) & \ddot{f}_{k} \in defined \\
0 & \ddot{f}_{k} \notin defined
\end{cases}$$
(4.5)

Where $\Gamma_k^{(m)}(f)$ and $\ddot{\Gamma}_k^{(m)}(f)$ will be the same size as samples.

Use the interpolation function to stretch, and do this for four functions; then, combine them in an original way, and use inverse Fourier function to restore the audio $\ddot{S}_k(t)$.

$$\ddot{\Gamma}_{k}(f) = \left\{ \ddot{\Gamma}_{k}^{(0)}(f), \operatorname{rev}\left(\ddot{\Gamma}_{k}^{(2)}(f)\right) \right\} + \left\{ \ddot{\Gamma}_{k}^{(1)}(f), \operatorname{rev}\left(\ddot{\Gamma}_{k}^{(3)}(f)\right) \right\} \cdot i \tag{4.6}$$

$$\ddot{\mathbf{S}}_{k}(t) = \operatorname{Re}\left(\operatorname{invFFT}\left(\ddot{\Gamma}_{k}(f)\right)\right) \tag{4.7}$$

Where i is an imaginary number, invFFT(\cdot) is the inverse FFT, Re(\cdot) is to get the real part of a number or array, rev(\cdot) is the reverse of an array.

Then, do this for 2 channels and create the audio as Pure Sound Tuner result.

From this function, it needs 3 data: the audio data $S_k(t)$, the inharmonicity coefficient IH(k), and its fundamental frequency f_k (which could be captured by audio data).

5 FUTURE WORK

Over-pull tuning is implemented in some tuning apps, and I do not know its method. Since I am still lacking of research in this area, I will leave it as future work to think about. I know this effect is caused by the experimental result of the percentage that the tuning pins will loosen and drop the pitch, it should have the correction coefficient for the tuner will make up the errors of this effect by over pull to tune the frequency higher than its actual one.

6 REFERENCE

- [1] Hinrichsen, Haye. "Entropy-based tuning of musical instruments." Revista brasileira de Ensino de Física 34.2 (2012): 1-8.
- [2] Github for Piano Tuning Project [https://github.com/RobertBoganKang/piano_tuning]

7 APPENDIX

	1	2			4	5	6		-	9	10		12	13	14	15	16
Α0 Δ#∩	27.3985 -6.36																446.537 -25.547
				87.1556-4.967												442.261+20.617 467.64+17.217	
																494.417-13.617	
			59.1189 -4.427													523.108 -11.267	
																553.821 -10.047	
D#1	38.8028 -3.92	27 7	77.6145-3.727	116.444 -3.397												586.985 -10.727	
E1			32.2444 -3.417													621.949 -10.897	
F1 F#1																658.287 -9.197	
				138.534-2.677 146.789-2.477												697.104 -8.387 738.39 -7.997	
																782.105 -7.577	
																828.478 -7.297	
A#1	58.1912-2.35	57 1	116.391 -2.227	174.609 -2.7	232.853 -1.77	291.133-1.37	349.456-0.827	407.833-0.257	466.271 -0.47	524.78 -1.157	583.368 -1.987	642.044 +2.897	700.817 -3.897	759.695 -4.987	818.688 -6.157	877.803 -7.417	937.049 -8.757
						308.46 -1.217	370.252-0.747	432.099 -0.197	494.009 -0.457	555.991 -1.177	618.055 -1.97?	680.21+2.867	742.464 -3.837	804.827 -4.89?	867.307+6.037	929.913 -7.257	992.654 -8.557
				196.012-1.82?												984.745 -6.437	
C#2																1043.77 +7.217 1106.89 +8.887	
D#2	77 6953 -100	92 1	155.405 - 1701	233 143 -4 52	310 924 - 1 1297	388 763 -0.817	466 672-0002	544.668.0.00	622 764 -1 400	700 973 -2 222	770 311 .0 000	857 792	936 429	1015 24 -0 079	1004 23 .0 000	1173.42 -9.917	1252 82 522
E2				247.017-1.427												1243.78 -10.727	
F2																1318.1 -11.27	
	92.40 10 -1.81															1397.33 -12.26?	
																1481.46 -13.46?	
G#2 A2																1569.7-13.637	
A#2																1663.28 -13.887 1763.73 -15.47	
																1870.79 -17.427	
C3	130.685 -1.85	17 2	261.413-1.47	392.229 -0.927	523.174 -0.257	654.293 -0.617	785.629 -1.66?	917.225-2.917	1049.12 -4.347	1181.37 -5.96?	13147.76?	1447.07 +9.75?	1580.6-11.937	1714.65 -14.297	1849.26 -16.837	1984.47 -19.55?	2120.31 -22.457
	138.458 -1.86	87 2	276.967 -1.347	415.579 -0.817	554.345 -0.087	693.316 -0.97	832.544 -2.087	972.079 - 3.467	1111.97 +5.067	1252.27 -6.887	1393.03 -8.877	1534.3-11.097	1676.13 -13.527	1818.56 -16.147	1961.65 -18.977	2105.45 -22.7	2250.+25.227
																2233.84 -24.487	
E3				466.527 -0.67 494.299 -0.497												2368.58 -25.877	
F3				494.299 -0.497 523.746 -0.317												2512.16 -27.767 2667.14 -31.47	
F#3	184.841-1.46	87 3	369.789 -0.967	554.95 -0.127												2831.82 -35.127	
G3	195.839 -1.47	2 3	391.804 -0.847	588.021 -0.097	784.616 -1.387	981.713 -3.057	1179.44 -5.08?	1377.92 -7.477	1577.27 -10.237	1777.62 -13.347	1979.08+16.87	2181.79 -20.617	2385.85 -24.777	2591.39 -29.267	2798.52 -34.097	3007.36 -39.247	3218.01 -44.727
																3196.98 -45.17	
																3398.16 +50.75?	
																3602.85 -52.017 3821.22 -53.897	
C4	261.472-1.01	17 5	523.2-0.177	785.437 +1.24?	1048.44 +3.27	1312.45 -5.727	1577.74 -8.797	1844.54 -12.47	2113.1 +16.557	2383.67 -21.227	2656.48 +26.427	2931.78 -32.137	3209.8-38.347	3490.76 -45.04?	3774.9-52.227	4062.43 -59.86?	4353.57 +67.957
C#4	277.035 -0.91	17 5	554.368 -0.017	832.294 +1.587	1111.11 +3.717	1391.11 +6.487	1672.58 -9.85?	1955.82 -13.817	2241.1-18.367	2528.72 -23.497	2818.95 -29.197	3112.07 +35.45?	3408.34 -42.247	3708.03 -49.57?	4011.41 +57.427	4318.71 +65.77?	4630.2-74.67
D4	293.526 -0.82	27 5	587.392 -0.197	881.94 - 1.887	1177.51 -4.27	1474.43 -7.197	1773.05 -10.84?	2073.69 - 15.137	2376.67 +20.05?	2682.34 -25.597	2990.99 +31.757	3302.94 +38.57	3618.51 -45.847	3937.99 +53.74?	4261.68 +62.197	4589.86 -71.197	4922.81 -80.897
																4870.31 -73.86?	
				990.223+2357 1049.42+2877												5173.69 -78.487 5514.75 -89.7	
F#4																5873.72 -98.187	
G4																6256.34 -107.437	
G#4																6680.31 -120.947	
A4 A#4	[440.Hz]															7137.1-135.457	
B4	466.2-0.147 493.962.030															7612.45 -147.087 8112.97 -157.327	
C5																8641.77-166.647	
C#5	554.549 -0.58	87 1	1110.87 +3.347	1670.71 -7.91?	2235.81 +14.277	2807.89 -22.39?	3388.63 -32.27	3979.65-43.667	4582.54 -58.89?	5198.84 -71.237	583087.27	6477.44+104.517	7142.5-123.07?	7826.45 -142.827	8530.49 -163.647	9255.77 -185.477	10003.3+208.217
D5																9944.98 -209.817	
D#5 E5																10659.2 -229.897	
F5																11414.9 +248.467 12211.8 +265.287	
F#5																13056.3 -281.067	
G5	784.779 -1.75	57 1	1573.85 -6.477	2371.45+14.287	3181.77 +25.117	4008.85 -38.837	4856.63+55.31?	5728.86 -74.397	6629.1+95.897	7560.72 -119.837	8526.87 +145.42?	9530.49 -173.067	10574.3 -202.347	11660.8 +233.097	12792.2 -265.127	13970.8 -298.257	15198.3 -332.327
G#5																15005.5 -321.957	
A5 A#5													12126.3 -239.457				
B5													7 13019.2 -262.447 13981.7 -285.927				
													14996.7 - 307.257				
C#6	1111.13 +3.74	17 2	2232.9-12.027	3375.81 -25.64?	455044.367	5765.18 -67.84?	7030.46 -95.77	8354.31 -127.517	9744.52 -162.827	11208.1 -201.177	12751.5 -242.127	14380.3 -285.227					
D6	1177.52 -4.22	27 2	2367.45 -13.32?	3581.99 -28.277	4832.92 -48.797	6131.44 -74.47?	7488.02+104.88?	8912.33-139.45?	10413.2 -177.727	11998.5 -219.147	13675.3 -283.27	15449.8 - 309.427					
D#6	1247.92 -4.74	17 2	2510.82 -15.17	3803.39 +32.17	5139.75 -55.35?	6533.24 -84.367	7996.2-118.547	9539.94+157.277	11174.6 -199.97	12909.3 -245.817	14751.8-294.397						
F6				4039.62 -36.427 4290.16 -40.67													
F#6				4290.16 +40.67 4557.47 +45.247													
G6	1574.78 -7.57	2 3	3179.38 -23.817	4842.7-50.337	6591.92 -86.157	8451.89 - 130.137	10444.8 - 181.017	12589.9-237.537									
G#6				5147.04 -55.857													
A6	1769.53 -9.36	37 3	3580.22 -29.37?	5471.67 -61.74?	7480.63 -105.117	9640.07 +157.85?	11978.7 +218.24?	14521284.57?									
				5817.71 -67.97				15603.+309.7									
C7				6187.13 -74.487 6581.8 -81.547													
C#7				7003.8-89.137													
D7	2370.97+15.8	397 4	4828.86 -47.337	7455.52 -97.337	10323.8 -162.87	13495.6 -240.37											
D#7				7939.62+106.247													
E7 F7				8459.22 -115.997		15515.9 -281.817											
F#7				9017.88+126.77 9619.76+138.587													
				9619.76+138.587 10269.8+151.787													
G#7				10209.8 -151./67													
Α7	3583.69 -31.0	167 7	7421.14 -91.287	11738.7 +183.27													
		112 7	7906.05-100.887	12573.1 -202.087													
A#7																	
A#7 B7 C8	4036.34 -38.9	177 8		13459.6 -220.047 14419.6 -239.317													

Figure 7-1 Tuning Table for Grand Piano

```
220.524
                                                                                                                              248.975
                                                                                                                                                                                                                         427.264
A#0
B0
                                                  122 63
                                                                 153.56 -8.757
                                                                                                               247.576 -4.457
                                                                                                                              279 44 -10
                                                                                                                                             311 624
                                                                                                                                                                            377 085
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                                                                                                                                                                                                          444 216
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       30 5664
                    61 1693
                                  91.845
                                                                                184 671
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       2.4038
                   64.8424
                                  97.3508
                                                  129.964
                                                                 162.715 -8.497
                                                                                195.64
                                                                                                228.773
                                                                                                               262.146 -3.447
                                                                                                                              295.793 -8.597
                                                                                                                                             329.746
                                                                                                                                                            364.039
                                                                                                                                                                            398.702
                                                                                                                                                                                           433.768-3
                                                                                                                                                                                                          469.265
                                                                                                                                                                                                                         505.224
                                                                                                                                                                                                                                         541.674 -59.91
C#
       36 4148
                    72 8629
                                   109 378
                                                  145 992
                                                                  182 74 -7 582
                                                                                219 654
                                                                                                256 766
                                                                                                               294 108
                                                                                                                              331 714 -7 022
                                                                                                                                             369 613
                                                                                                                                                             407 839
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                                                  154.761 -8.951
       8.6017
                2.927 77.2388
                                  115.947
                                                                 193.716 -6.587
                                                                                232.847
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F1
       3 3745
                    86 7867
                                   130 274 -9 09
                                                  173 875 -7 343
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                                                                                                305 725 -0.85
                                                                                                               350 147-4 552
                                                                                                                              394 866 -8 737
                                                                                                                                             439 919
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F#
                                                  184.296 -6.571
                                                                 230.663 -4.377 277.225
                                                                                                               371.086 +5.117
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        5.9762
                    91.9917
                                   138.085 -8.287
                                                                                                324.02 -1.487
                                                                                                                                             466.182
                                                                                                                                                            514.286
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G1
        3.7328
                                   146 325
                                                  195 247
                                                                                                342 896
                                                                                                               392 509
                                                                                                                              442.373-5.417
                                                                                                                                                             542.972
                                                                                                                                                                            593 768
                                                                                                                                                                                           644.933
                                                                                                                                                                                                          696 497
       1 6533-8 683
                    103 337 - 8 16
                                   155 084 -7 33
                                                  206 923 -6 003
                                                                 258 885 -4 547
                                                                                311 002
                                                                                                363 304 -0 41
                                                                                                              415 821 -2 162
                                                                                                                              468 583 -5 052
                                                                                                                                             521 62-8 292
                                                                                                                                                             574 963
                                                                                                                                                                            628 639
                                                                                                                                                                                           682 679 - 19 922 737 11 - 24
                                                                                                                                                                                                                         791 962
                                                                                                                                                                                                                                         847 262 -34 3
                                   164.374
                                                  219.319 -5.361
                                                                 274.395 -3.817
                                                                                                385.074
                                                                                                               440.74+2.917
                                                                                                                              496.667 -5.837
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        4.7473
                    109.528
                                                                                329.636
                                                                                                                                             552.888
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                                                                                                                                                                            666.332
Α#
        8 0252
                     116.084
                                   174 209
                                                  232 433
                                                                 290.79-3.347
                                                                                349 313
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                                                                                                                              11740.9 +181.577 13329.1 +218.87 14999.2 +258.18
                    2365.3 -1
                                   3572 83
                    2506.93 -12.427
                                  3787.52 - 24.867 5100.22 - 41.987 6455.07 - 63.527 7861.52 - 88.137
                                                                                               9328.43 -118.457
                                                                                                              10864. -151.097
                                                                                                                              12475.6 -186.667 14170.2 -224.757 15953.8 -264.99
F6
F6
                                  4265.65
                                                  5757 3-51 793
                                                                 7307 22 -78 197
                                                                                8928.19
                                                                                                10632 +144 897
                                                                                                               12429.3 -184.127 14329.7 -226.52
                    2818 59
                    2988.54
                                  4526.12+33.297
                                                 6114.76 -56.073
                                                                 7770.02 -84.57 9506.38 -118.037 11337. -156.067
                                                                                                              13274. +197.957 15327.8 +243.17
G6
G#6
                    3359 66
                                   5094 43
                                                  6893 79-63 6
                                                                 8777 25 -95 522
                                                                                10762 7 -132 931
                                                                                               12866 5 -175 142 15102 9 -221 42
                    3565.3 -22.147
                                  5416.7 -44.28?
                                                  7348.69 -74.37
                                                                 9385.13 -111.457 11547.7 -154.87 13855.7 -203.387
A#6
                                                  7833.16
                                                                 10033.5
                    3783.63
                                  5759.38
В6
                     4015 24
                                  6122 88
                                                  8346.96 -94.83
                                                                 10720 8 - 141 817 13274 - 195 997
                    4255.33 -28.44
                                  6486.34+56.247
                                                  8837.75 -93.737 11344.2 -139.657 14036.3 -192.671
C#7
                                   6905.62
                                                                 12165.3 - 160.647 15115.7 +220.93
D7
                    4798 2
                                   7351.06
                                                  10081 4 - 121 672 13038 - 180 58
D#
                    5083.42
                                  7778.7 -70.79?
                                                  10651.6 -116.927 13751.5 -172.833
E7
                    5735 27
                                   8822 54 -88 797
                                                  12161 6-146 422 15818 9-215 20
F#7
                    6092.43
                                  9395.87 -97.797
                                                  12992.8 - 160.887
G7
G#
                     6874 91
                                   10651 5-114 943
                                                  14811 8 -187 72
                     7302.41 +63.367 11335.3 +122.667 15798.6 +199.397
A#
                     8230.93 -70.587 12799.4 -132.97
                     8741.5 -74
```

Figure 7-2 Tuning Table for Upright Piano

	1	2	3			•						12
	27.4413-3.77		82.0674 -9.17	109.765-3.77	137.463-0.46?	165.417+4377	193.884 +12.417	222.095+16.417	251.075+24.837	280.055 +31.547	309.804 +41.317	339.297 +48
√# U	28.8409-17.577	57.6818-17.577	86.5226-17.577	115.579 -14.35?	144.635 -12.417		204.038 +0.787		264.088+12.317		325.428 +26.497	
	30.6368 -13.7	61.2735 -13.7	91.9103-13.7	122.746-10.197	153.98-4.03?	185.213+0.077	216.845 +6.17?	248.675 +12.117	280.903+19.187	313.33+25.917	345.758 +31.47	378.981 +39.
			97.4898-10.97?			196.454 +2.077	229.626 +5.327	263.72+13.817	297.445+18.247	331.539 +23.77	365.633 +28.167	400.648+35
C#1	34.1767 -23.77	68.502-19.947	102.679 -21.197	137.301 -16.197	171.924 - 13.197	207.14-6.227	242.209 -2.327	277.723+3.387	313.385 +8.627	349.494 +15.01?	385.751 +20.897	422.305+26
			109.748-5.917			220.768+4.087	258.339 +9.37	296.052+14.027	334.189+19.897	372.184 +23.917	410.744 +29.57?	449.304+34
D#1	38.6613 -10.257	77.3226 -10.257	115.984 -10.257	155.044 -5.79?	194.303-1.347	233.761+3.097	273.419 +7.517	313.276+11.927	353.532+17.37	393.787 +21.597	434.441 +26.687	475.295+31
			122 946.0322			247,46+1,687	289 06+3 827	331 371 +9 147	373.826+13.937	416 85+20 122	459.304 +23.027	502 613 -28
1			130.062-11.917			261.867-0.357	306.225 +3.687					
#1												
			138.012-9.27			277.623+0.87	324.516 +4.127					
			146.514-5.717		244.703 -2.077	293.713 -1.677	343.236 +1.227		442.968 +7.737			594.451 +18
J# 1	51.5976 -10.557	103.379-7.477	154.976-8.57	206.941 -5.93?	258.722-5.637	310.687-4.47	363.019 -1.777	415.351+0.27		520.199 +3.567	574.367 +10.057	627.985+13
			164.093-9.547			329.032-5.087	384.435 -2.547	440.049 +0.27	495.874 +3.067	551.7+5.357	608.371 +9.637	665.254 +13
#1	57.9676 -9.027	115.935 -9.027	174.057-7.487	232.487 -4.427	290.609-4.427	349.039-2.897	407.623 -1.147	466.515+1.317	525.562+3.727	585.38+7.937	645.352+11.797	705.632+15
			184.474-8.857		308.41-1.57	370.556+0.687	432.524 +1.517	495.027 +4.017	558.423+8.727	621.641 +11.997	685.573+16.467	749.862 +21
2	65 2473 4 212	130 223 7 822	195.742-4217	261 261 2412	326 78.1332	392.571+0.597	458.906 +4.017	524.969 +5.687	591 576 +8 577	658 454 +11 507	726 148 +16 2	794.386 +20
			207.043-7.037			415.034-3.087	484.785 -1.017	554.693+1.037			766.629+9.927	838.589+14
			220.086-1.287		367.394+1.487	440.829+1317	515.36+4.877	589 453 +6 252	664.641+10.187		815.457 +16.817	
	77.3853 -8.84?		232.523-6.117		387.905-4.477	465.779-3.387	544.876 +1.297	622.995 +2.067			860.407 +9.717	940.482+13
_			246.583-4.477		411.402 -2.667	493.739-2457	576.794 -0.167	660.136+2.327	744.052+5.57?	827.537 +7.287	912.313+11.127	997.09+14.3
			261.544 -2.49?		436.261 -1.087	523.088 -2.497	610.979 -0.487	699.326 +2.167	785.088-1.487	876.78+7.357	966.04+10.187	1056.21 +14
#2	91.9479 -10.337	184.156-7.897	276.623-5.457	368.831 -5.457	461.298-4.477	554.025 -3.017	647.012 -1.277	740.518+1.247	834.284 +3.747	928.57+6.77	1022.86 +9.127	1117.66 +11.
			293.482-3.037		489.227-2.717	587.511 -1.417	686.481 +1.247	785.862+4.137	885.379+6.657	985.171 +9.142	1085.51 +12.057	1186.26 +15
			311.046 -2.47	414.856-1.877	518.283 -2.837	622.86-0.267	727.821 +2.487	832.207 +3.337	938.128+6.837	1043.66 +8.997	1150.16 +12.27	1257.04+15
2			329.643-1877				770 403 +0.912					
110					549.926-0237						1218.18+11.677	
			348.855-3.87		582.478-0.677	698.658-1.457	816.258 +1.017		1051.93+5.067		1289.19+9.757	1409.63+13
	123.074 -5.57?				617.078-0.777	741.007+0.437	865.448 +2.317	989.89+3.727	1115.19 +6.157	1240.99 +8.87	1367.32 +11.617	
:3			392.692+1.127	523.081 -0.56?	654.384 +0.857	785.992+2.467	917.6+3.617	1050.43+6.497	1182.64 +7.827	1316.08 +10.57	1449.82 +13.057	1584.78 +16
#3	137.462 -14.16?	276.483 -4.377	414.88-3.727	553.278-3.397	691.363-3.987	830.072-3.077	969.405 -1.317	1109.67 +1.487	1249.32+2.777	1389.9+4.977	1531.1+7.487	1672.92+10
	146.502 -3.97		440.42-0.37	587.531+0.67	734.642+1.147	881.753+1.497	1029.17 +2.267	1176.28 +2.397	1324.3+3.697	1472.94 +5.447	1621.57 +6.877	1770.51 +8.3
			466.039-2417		777.239-1287	932.908-0.877	1088.85 -0.147	1245.08+0.87	1401 58+1877		1714.99+3.847	1873.02 +5.8
3												
_			493.475-3.387		823.244 -1.737	988.297 -1.027	1153.69 -0.017		1484.47 +1.347			1985.02 +6.3
		348.892-1.667		699.171+1.787		1050.38 +4.457	1227.6+7.57	1404.82 +9.787			1942.5+19.57	2124.35 +23
#3	183.896 -10.337	369.662 -1.55?	554.181 -2.53?	739.323-1.55?	925.713+1.367	1112.1 +3.317	1299.11 +5.527	1486.75 +7.917	1675.63+11.057	1865.76 +14.727	2057.14+18.767	2249.14 +22
3	195.775 -1.97?	391.55-1.97?	587.727-0.787	784.308+0.77	981.694+3.017	1179.48 +5.14?	1378.08 +7.687	1577.48+10.467	1778.09+13.797	1979.9+17.527	2183.33 +21.837	2387.57 +26
#3	206.993 -5.57	413.985-5.57	621.475-4.127	829,463-2397	1038.94+1.147	1247.43+2.11?	1457.9+5.167	1669.38 +8.487	1881.34+11.527	2094.8+15.187	2311.25 +20.417	2527.2+24.4
	219.729-2.137		660 198 522	880.602+1.197	1102 69 242	1325.12+6.717	1548 56 +9 67	1773 35 +12 002	1999.16+16.687	2226 65	2456 17 - 25 002	2687 37
		465.911 -0.937		933.122+1.487		1403.71+6.467						
							1640.57 +9.527					
			740.951+0.37		1237.79+4.327	1487.93+7.337			2246.1+18.317			
			786.111 +2.727		1313.6+7.237	1579.04+10.227	1846.19+13.957	2115.05 +18.157	2386.18+23.057	2660.16 +28.817	2935.84 +34.527	3213.79 +40
#4	276.395 4.927	553.749-1.927	831.104-0.927	1109.42 +1.087	1389.65+4.677	1670.85+8.057	1953.96+12.177	2238.99+16.737	2528.82+23.567	2816.73 +27.837	3110.4 +34.527	3405.99 +41
			881.823+1.637			1773.25+11.047	2073.92+15.327	2376.5+19.927	2683.89+28.67	2992.24 +32.477	3304.92 +39.537	3619.03+46
#4	310 756 2 002	621.512-2.087	933.128-0.467	1245.17+0.937	1559 37-4102	1875.71+8.297	2193 35 252	2515.28+18.177	2841 94	3168 6.21 012	3500.84 +39.247	3834 38
			989.137+0.457									
								2671.13+22.267				
	348.817 -2.04?			1400.52+4.47?				2832.58 +23.857				
#4	369.811 -0.857	739.622-0.857	1110.68 +1.097	1483.61+4.25?	1859.03+8.467	2237.58+13.687	2617.37 +18.237	3002.77 +24.877	3396.28+34.157	3786.67 +40.127	4187.04 +49.117	4590.52 +57
			1178.05 +3.047			2373.64 +15.887	2779.31 +22.167	3187.66 +28.317	3606.71 +38.237	4026.36 +46.37?	4454.64 +56.37?	4885.58 +65
3#4	414.798-2.117	829.597-2.117	1246.18+0.377	1664.53+3.467	2086.45+8.267	2511.93 +13.927	2942.75 +21.097	3371.79 +25.537	3822.2+38.697	4267.26 +46.977	4719.44 +56.347	5178.75 +66
4	[440.Hz]		1324.55+5.967			2671.83+20.767	3131.16 +28.53?	3595.04+36.527	4069.15+47.087	4547.8+57.27	5035.56 +68.587	5525.58 +78
#4	465 705 4 72	932.19-0.257						3803.65+34.177			5340.39+70.337	
4								4039.82 +38.467				
-			1577.04+8.037					4301.47 +47.117				6660.09+10
#5	553.989 -1.177	1110.06 +2.087	1668.2+5.317	2231.55+10.977	2801.13+18.217	3376.94 +26.227	3963.15+38.477	4556.64 +46.887	5169.87 +61.567	5793.5+76.327	6428.56 +91.397	7072.98 +10
		1176.73 +3.067	1769.9+7.767	2367.86+13.627	2973.51+21.67	3588.75+31.547	4212.63 +42.157	4849.95 +54.887	5500.7+68.947	6164.89 +83.897	6844.44 +99.927	7544.15+11
#5	621.43 -2.297	1247.02+3.57	1875.39+7.997	2507.91+13.17	3151.54+22.777	3804.87+32.782	4467.92 +44,017	5142.06+56.137	5838.39+72.002	6543.05 +86.947	7274.06+105 311	7
5			1986.36+7.517					5466.13+61.947				
5	698.14-0.787						5036.58 +51.427			7418.99+104.473		
-	698.14 -0.787 739.78 -0.487											
						4549.84 +42.347		6177.93+73.867				
55			2373.74+15.957				5701.7+66.167	6590.64 +85.827				?
	831.792 +2.477	1666.36+5.357	2510.62+13.027	3367.37 +23.267	4239.37 +35.627	5133.54 +51.37	6049.9+68.787	6996.76 +89.347	7975.5+112.097	8984.74 +135.977		
								7442.7+96.317	8485.33+119.377	9539.33 +139.671		
#5								7920.24+103.977				
5						6165.35 +68.387		8453.62+116.87				
							7761.09+100.7					
++6	1110.51 +2.787							9599.43+136.857				
				4819 83 +44 097	6096.88+64.687	7421.36+89.387	8797.03+116.917					
6	1178.43 +5.557	2368.09+13.797	35/7./3+26.217			704E 12	0040.05					
16 1#6	1178.43 +5.557	2368.09+13.797 2502.88+9.627	3577.73+28.217 3784.44+23.457	5093.+39.537	6451.41+62.54?	7043.13+85.527	9319.85+116.867					
16 1#6 16	1178.43 +5.557 1246.25 +2.427	2502.88+9.627	3784.44 +23.457	5093.+39.537		8382.78+100.277						
6 #6 6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57	2502.88 +9.627 2656.92 +13.027	3784.44 +23.457 4022.84 +29.227	5093.+39.537 5421.22+47.657	6872.03+71.897	8382.78+100.277						
6 #6 6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87	2502.88 +9.627 2656.92 +13.027 2817.04 +14.337	3784.44 +23.457 4022.84 +29.227 4266.11 +30.867	5093.+39.537 5421.22+47.657 5756.75+51.627	6872.03+71.897 7305.6+77.87	8382.78 +100.277 8920.98 +108.7						
6 #6 6 6 #6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387	2502.88 +9.62? 2656.92 +13.02? 2817.04 +14.33? 2994.47 +20.08?	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337	5093.+39.537 5421.22+47.657 5756.75+51.627 6128.92+60.077	6872.03+71.897 7305.6+77.87 7796.12+90.317	8382.78+100.277						
6 #6 6 6 #6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887	2502.88+9.62? 2656.92+13.02? 2817.04+14.33? 2994.47+20.08? 3171.02+19.25?	3784.44 +23.457 4022.84 +29.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57	5093.+39.537 5421.22+47.657 5756.75+51.627 6128.92+60.077 6509.47+64.367	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237	8382.78 +100.277 8920.98 +108.7						
6 #6 6 #6 #6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887 1665.85 +4.837	2502.88 +9.627 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197	5093.+39.537 5421.22+47.657 5756.75+51.827 6128.92+60.077 6509.47+64.367 6892.84+63.437	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 6 #6 6 #6 6 #6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887 1665.85 +4.837 1769.53 +9.357	2502.88 +9.627 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.797	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67	5093.+39.537 5421.22+47.657 5756.75+51.627 6128.92+60.077 6509.47+64.367 6892.84+63.437 7345.16+73.477	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 #6 #6	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887 1665.85 +4.837 1769.53 +9.357	2502.88 +9.627 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.797	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197	5093.+39.537 5421.22+47.657 5756.75+51.627 6128.92+60.077 6509.47+64.367 6892.84+63.437 7345.16+73.477	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 #6 #6 #6 #6	1178.43 +5.557 1246.25 +2.42? 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887 1665.85 +4.837 1769.53 +9.357 1872.73 +7.487	2502.88 +9.527 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.797 3780.37 +23.567	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67	5093. +39.537 5421.22 +47.857 5756.75 +51.827 6128.92 +60.077 6509.47 +64.367 6892.84 +63.437 7345.16 +73.477 7800.13 +77.517	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 # 6 6 # 6 # 6 6 6 6 7	1178.43 +5.557 1246.25 +2.42? 1323.47 +6.57 1399.17 +2.87 1489.74 +11.337 1576.77 +9.887 1665.85 +4.837 1769.53 +9.357 1872.73 +7.487 1986.02 +9.177	2502.88+9.627 2656.92+13.027 2817.04+14.337 2994.47+20.087 3171.02+19.257 3361.63+20.317 3544.05+11.787 3780.37+23.567 3972.05+9.177	3784.44 +23.457 4022.84 +29.227 4266.11 +30.857 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67 5750.35 +47.747 6110.85 +53.017	5093. +39.537 5421.22 +47.657 5756.75 +51.827 6128.92 +60.077 6509.47 +64.367 6892.84 +63.437 7345.16 +73.477 7800.13 +77.517 8310.44 +87.227	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 #6 #7	1178.43 +5.507 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.687 1665.85 +4.837 1769.53 +9.357 1872.73 +7.467 1986.02 +9.177 2108.65 +12.97	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.797 3780.37 +23.557 3972.05 +9.177 4259.78 +30.257	3784.44 +23.457 4022.84 +29.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67 5750.35 +47.747 6110.85 +53.017 6498.35 +59.457	5093. *39.537 5421.22 *47.657 5756.75 *51.627 6128.92 *60.077 6509.47 *64.367 6892.84 *63.437 7345.16 *73.477 7800.13 *77.517 8310.44 *87.227 8834.36 *93.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6#66#6#67#7	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.887 1665.85 +4.837 1769.53 +9.357 1872.73 +7.487 1986.02 +9.177 2108.65 +12.97 2234.48 +13.247	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.797 3780.37 +23.557 3972.05 +9.177 4259.78 +30.257 4461.48 +10.347	3784.44 +22.467 4022.84 +20.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67 5750.35 +47.747 6110.85 +53.017 6498.35 +59.457 6870.33 +55.817	5093. +39.537 5421.22 +47.657 5756.75 +51.627 6128.92 +60.077 6509.47 +64.367 6892.84 +63.437 7345.16 +73.477 7800.13 +77.517 8310.44 +87.227 8834.36 +93.667 9381.31 +97.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 7 #7	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.687 1665.85 +4.837 1769.53 +9.357 1986.02 +9.177 2108.65 +12.97 2234.48 +13.247 2366.71 +12.777	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3780.37 +23.557 3780.37 +23.557 4461.48 +10.347 4798.33 +38.357	3784.44 +23.457 4022.84 +29.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +46.87 5750.35 +47.747 6110.85 +53.017 6498.35 +39.457 6870.33 +58.817 7344.79 +71.427	509399.537 5421.22 -47.657 5756.75 -51.627 6128.92 -60.077 6509.47 -68.367 6892.84 -68.437 7345.16 -78.477 7800.13 -77.517 8310.44 -87.227 8834.36 -93.067 9381.31 -97.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 #6 7 #7 7 #7	1178.43 +5.557 1246.25 +2.427 1323.47 +6.57 1399.17 +2.87 1489.74 +11.387 1576.77 +9.687 1665.85 +4.837 1769.53 +9.357 1986.02 +9.177 2108.65 +12.97 2234.48 +13.247 2366.71 +12.777	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3780.37 +23.557 3780.37 +23.557 4461.48 +10.347 4798.33 +38.357	3784.44 +22.467 4022.84 +20.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +45.67 5750.35 +47.747 6110.85 +53.017 6498.35 +59.457 6870.33 +55.817	509399.537 5421.22 -47.657 5756.75 -51.627 6128.92 -60.077 6509.47 -68.367 6892.84 -68.437 7345.16 -78.477 7800.13 -77.517 8310.44 -87.227 8834.36 -93.067 9381.31 -97.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 7 #7 #7	1178.43 -6567 1246.25 -2.427 1323.47 -657 1399.17 -287 1489.74 -11.387 1576.77 -6887 1665.85 -4837 1769.53 -9357 1872.73 -7.487 1986.02 -6.17 2108.65 -1287 2234.48 -11.247 2366.71 -12.77 2504.12 -10.487	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.707 4259.78 +20.257 4461.48 +10.347 4798.33 +36.357 5072.96 +32.717	3784.44 +23.457 4022.84 +29.227 4266.11 +30.867 4536.7 +37.337 4815.26 +40.57 5094.81 +38.197 5420.89 +46.87 5750.35 +47.747 6110.85 +53.017 6498.35 +39.457 6870.33 +58.817 7344.79 +71.427	509339.537 5421.22 +47.857 5756.75 +51.827 6128.92 +80.077 6509.47 +63.867 6892.84 +63.437 7345.16 +73.477 7800.13 +77.517 8310.44 +87.227 8834.36 +90.067 9381.31 +97.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 #6 7 #7 #7 #7	1178.43 -6557 1246.25 - 247 1323.47 -657 1399.17 -287 1489.74 -11387 1576.77 -687 1665.85 -4837 1769.53 -6357 1872.73 -7487 1986.02 -6177 2108.65 -1297 2234.48 -13287 2669.71 -1277 2504.12 -10487 2669.56 -14787	2502.88 +0.827 2656.92 +13.027 2817.04 +14.337 2994.47 +20.087 3171.02 +19.257 3361.63 +20.317 3544.05 +11.727 3780.37 +23.557 3972.05 +0.177 4259.78 +20.257 4461.48 +10.347 4798.33 +38.357 5072.96 +22.717 5309.16 +11.407	3784.44 - 23.457 4022.84 - 29.227 4266.11 - 20.867 4536.7 - 37.337 4815.26 - 40.57 5094.81 - 28.167 5420.89 - 46.67 5750.35 - 47.747 6110.85 - 53.017 6498.35 - 50.467 6870.33 - 5887 7344.79 - 71.427 7763.77 - 47.477 8130.43 - 47.367	509339.537 5421.22 +47.657 5756.75 +51.627 6128.92 +60.077 6892.84 +63.437 7345.16 +73.477 7800.13 +77.517 8310.44 +87.227 8834.36 +90.067 9381.31 +97.067	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 #6 6 #6 #6 #6 7 #7 #7 #7 #7 #7 #7 #7 #7 #7 #7 #7 #7 #	1178.43 -6.557 1246.25 -2.427 1323.47 -6.57 1329.47 -6.57 1576.77 -6.667 1665.85 -4.637 1769.53 -6.637 1769.53	2502.88 + 9.827 2656.92 - 13.027 2817.04 + 14.33 2994.47 - 20.00 3171.02 - 19.25 3361.63 - 20.31 3544.05 + 117 4259.78 - 30.25 4461.48 + 10.34 4798.33 - 36.35 5072.96 - 32.71 5309.16 + 116.5 5724.95 + 22.03	3784.44 - 22.407 4022.84 - 23.227 4266.11 - 30.607 4536.7 - 97.337 4815.26 - 40.57 5542.089 - 4657 55750.35 - 41.747 6110.85 - 53.607 6498.35 - 59.407 7764.77 8730.43 - 45.747	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 #6 6 #6 #6 #6 7 #7 7 #7 7 7 #7	1178.43 -6.557 1246.25 -2.427 1323.47 -6.57 1323.47 -6.57 1399.17 -6.37 1489.74 -11.327 1476.57 -6.627 1489.74 -11.327 1486.02 -6.17 1486.02 -6.17 1486.02 -6.17 1486.02 -6.17 1486.02 -6.17 1486.03 -6.17 1487 1487 1487 1487 1487 1487 1487 14	2502.88 + 0.827 2656.92 + 10.07 2817.04 + 4.33 317.02 + 20.08 3361.63 + 20.31 3544.05 + 11.70 3780.37 + 23.60 3792.05 + 10.77 4259.78 + 20.77 4259.78 + 20.77	3784.44 - 23.457 4022.84 - 29.227 4266.11 - 20.867 4536.7 - 37.337 4815.26 - 40.57 5094.81 - 28.167 5420.89 - 46.67 5750.35 - 47.747 6110.85 - 53.017 6498.35 - 50.467 6870.33 - 5887 7344.79 - 71.427 7763.77 - 47.477 8130.43 - 47.367	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 0#6 66 66 66 66 66 67 77 77 77 77	1178.43 -6.557 1246.25 - 2.27 1239.17 -227 1489.74 -11.387 1576.77 -0.687 11576.77 -0.687 11576.73 -3.57 1872.73 -7.487 1986.02 -0.177 2108.65 -1207 2234.48 -11.247 2366.71 -1277 2504.12 -10.487 2699.56 -14.747 2816.41 -11.847 2816.41 -11.847	2502.88 + 9.827 2656.92 - 13.027 2817.04 + 14.33 2994.47 - 20.00 3171.02 - 19.25 3361.63 - 20.31 3544.05 + 117 4259.78 - 30.25 4461.48 + 10.34 4798.33 - 36.35 5072.96 - 32.71 5309.16 + 116.5 5724.95 + 22.03	3784.44 - 22.407 4022.84 - 23.227 4266.11 - 30.607 4536.7 - 97.337 4815.26 - 40.57 5542.089 - 4657 55750.35 - 41.747 6110.85 - 53.607 6498.35 - 59.407 7764.77 8730.43 - 45.747	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 #6 6 #6 #6 #6 7 #7 7 #7 7 7 #7	1178.43 -6.557 1246.25 - 2.227 1249.25 - 2.227 1399.17 - 2.227 1489.74 - 11.327 1489.74 - 11.327 1489.74 - 11.327 1489.74 - 11.327 1872.73 - 7.427 1886.02 - 0.177 2108.65 - 12.27 2234.48 - 13.247 2366.71 - 12.27 2504.12 - 10.487 2659.56 - 14.727 2504.12 - 10.487 2659.56 - 14.727 2502.84 - 10.327 2502.84 - 10.327 2502.84 - 10.327 2502.84 - 10.327 2502.84 - 10.327	2502.88 + 0.827 2656.92 + 10.07 2817.04 + 4.33 317.02 + 20.08 3361.63 + 20.31 3544.05 + 11.70 3780.37 + 23.60 3792.05 + 10.77 4259.78 + 20.77 4259.78 + 20.77	3784.44 - 22.457 4022.28 - 4266.11 - 30.807 4266.11 - 30.807 4393.7 - 43.337 4815.26 - 432 55094.81 - 32.197 5420.89 - 45.87 5750.35 - 47.247 6498.35 - 49.457 6498.35 - 49.47 7763.77 - 40.477 7763.77 - 40.477 8130.43 - 47.807 9061.02 - 34.377	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 #6 6 #6 #6 #6 7 #7 7 7 7 7 7 7 7 7 7 7	1178.43 -6.557 1246.25 - 2.27 1399.17 - 2.27 1489.74 - 11.389 1576.77 - 0.687 1665.58 - 4.32 11769.53 - 0.357 1872.73 - 7.488 1986.02 - 0.17 2108.65 - 12.87 2234.48 - 11.327 2504.12 - 10.489 2659.56 - 14.727 2616.41 - 11.327 2616.41 - 11.327 26	2502.88 + 0.827 2656.92 + 10.07 2817.04 + 4.33 3171.02 + 10.087 3361.63 + 20.31 3544.05 + 11.70 3780.37 + 22.67 3792.05 + 11.77 4259.78 + 20.37 4461.48 + 10.34 4798.33 + 20.35 5072.96 + 22.77 5309.16 + 1.69 5509.16 + 1.69 5509.17 + 10.85 5688.17 + 10.86 56471.38 + 54.27	3784.44 - 22.407 4022.84 - 22.27 4266.11 - 20.87 4266.11 - 20.87 4266.11 - 20.87 4815.26 - 40.27 4815.26 - 40.27 5994.81 - 34.107 5420.89 - 46.87 5750.35 - 42.75 6470.33 - 68.47 6470.33 - 68.47 7763.77 - 42.77 8130.43 - 47.267 8806.52 - 46.47 9061.02 - 34.27	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
06 #6 #6 #6 #6 7 #7 7 #7 7 #7 #7 #7 #7 #7 #7 #7 #7 #7	1178.43 -6.587 1246.25 -6.287 1239.17 -6.29 1489.74 -11.387 1576.77 -6.887 1872.73 -7.487 1872.73 -7.487 1208.65 -1.297 12504.12 -1.0487 12504.12 -1.0487 12504.12 -1.0487 12504.13 -1.0487 1375.77 -0.187 1375.77 -0.187 1375.77 -0.187	2502.88 - 0.027 2556.92 - 1.027 2556.92 - 1.027 2594.47 - 2007 3717.10.2 - 10.25 3781.03 - 10.	3784.44 - 22.407 4022.84 1-22.27 4022.84 1-22.27 426.11 - 30.807 4536.7 + 27.27 4815.26 - 40.57 5094.81 1-30.97 5094.81 1-30.97 5750.35 - 47.74 6498.35 - 50.6498	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						
6 #6 6 #6 #6 6 7 #7 #7 7 #7 #7 #7 #7 #7 #7 #7 #7 #7 #7	1178.43 - 6327 1246.25 - 6427 1399.17 - 6327 1489.74 - 11327 1665.85 - 4327 1769.53 - 9327 1769.53 - 9327 1769.55 - 1227 208.65 - 1227 2234.48 - 1327 2254.51 - 1427 250.5	2502.88 - 0.027 2656.92 - 1.027 2657.04 - 1.037 3171.02 - 10.257 3371.02 - 10.257 3371.03 - 10.257 3372.05 - 0.177 4259.78 - 30.257 4461.48 - 10.347 4798.33 - 30.357 5072.96 - 227 5309.16 - 11.407 5724.95 - 4207 5724.95 - 4207 6471.38 - 4207 6471.38 - 4207 6471.38 - 4207 6471.38 - 4207	3784.44 - 22.407 4022.84 - 22.27 4022.84 - 22.27 426.11 - 30.807 4536.7 + 27.27 4815.26 - 40.57 5094.81 - 30.10 5094.81 - 30.10 5094.81 - 30.10 5094.81 - 30.10 5094.81 - 30.10 5094.83 - 5750.35 - 43.57 5095	509398.577 5421.22-47.697 5756.75-48.27 6128.92-40.077 6699.2.84-48.497 7345.16-732.77 800.13-77.517 8310.44-87.227 8834.36-98.087 9381.31-47.697	6872.03+71.897 7305.6+77.87 7796.12+90.317 8273.65+93.237 8788.12+97.677 9376.75+100.917	8382.78 +100.277 8920.98 +108.7 9528.32 +122.037						

Figure 7-3 Entropy Tuning for Upright Piano