

Piano Tuning Method

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ABSTRACT

Since the piano string is consider to be a stick rather than a pure ideal string, it contains stiffness and its harmonics will shift in such way that make piano tuning a difficult work. In this work, the method of the optimization algorithm similar to Tunelab®, however, construct and developed all by the author. The algorithm is divided into several models that using various fitting technique to construct model functions, and finally convert to linear regression problem for optimization. Finally, the piano tuning curve is constructed and final tuning frequencies are calculated. In addition, more functions is introduced, such as the different temperament tuning.

Keyword: piano tuning, Tunelab, inharmonicity, optimization

Project Location

Reference [2]

1 INTRODUCTION

Piano tuning is a difficult work since the harmonics shift that make the piano hard to tune, and tuning process will be a task to highly reduce the audible cacophonous. There are several factors we need to consider, which the rule of harmony is.

- The cacophonous created by its base frequency and audible harmonics; a good tuning will largely reduce the inharmonic for harmonies (the frequency domain will greatly coincide).
- The inner music scales related pitch; the odd pitch tuning will result in the weird sound when playing music scales.

Other famous related works are:

- Tunelab (closed source; has trial version)
- Reyburn CyberTuner (closed source; no trial version)
- Entropy Piano Tuner (open source) [1]

The first two are similar, which represent the old tuning techniques, and my work mostly focus on this algorithm. Since it is closed source, I guessed their tuning method and create a similar solution, and will be shown in this article.

As for Entropy Piano Tuner, it represent the new way of piano tuning, however I heard its demo of tuning, I found that it contain two major deficiencies:

- It violate the second rule of harmony – inner scales sound weird.
- It only consider the sound which at the certain striking level of piano keys, which result in the optimization of keys are based only on sampling striking level.

In my work, I will guess the algorithm and model it in the similar way of optimization. Besides, I used more accurate model for inharmonicity coefficients.

In this article, the first part is to introduce the background of knowledge for higher level modeling algorithms. The second part is to introduce my piano modeling and tuning optimization method. Finally, the future work will be introduce and followed a conclusion.

2 BACKGROUND KNOWLEDGE

2.1 Key Names

The left most key name is defined as “A0”, where “A” is the note name, 0 is the scale number. “C” is the starting point of one scale. It only allowed sharp in the note, flat is not allowed in this naming format.

A0, A#0, B0, C1, C#1, ..., B1, C2, ..., B7, C8

There are 88 keys for standard piano.

2.2 Key Numbers

In the real world, the piano key will labeled with numbers when the piano is open and machine part is shown off.

A0 key is labeled to be 1, and C8 is 88.

However, in my program, A0 key is labeled as 0 for easier calculation.

2.3 Conversion Functions

Frequency ratio to cents function:

$$fr2c(\gamma) = 1200 \log_2(\gamma) \quad (2.1)$$

Where cents is from 12 equal temperament, each half note has 100 point, named cents.

3 METHOD

3.1 Sampling Piano

Before tuning a piano, we need to sample a piano by recording the piano keys sound audios. This process will roughly or precisely measure the inharmonicity of piano strings (which will talk about later), such that we could model the inharmonicity for the target piano.

The sampling is suggested to measure keys “C1”, “C2”, “C3”, “C4”, “C5” (and probably “C6”; user could record more piano keys such as “A1” ~ “A6” for better result). The piano key sound should be recorded in a quiet environment, which allows more accuracy for later frequency analysis.

In my program, I use fully or almost fully sampled piano for research purposes.

3.2 Audio Processing

Since the real audio may contains the white space at the start or the end, and the sound length varies. I use this method to process my sampled audio:

- Normalize ($func(x) = x / \max(x)$) the audio file into 1, then, find the peak volume of audio, and start from here.
- Slice these audio pieces into tiny partitions, say 0.1 second is one partition. The maximum number of each partition will be its assumed volume at this time point.
- Select these pieces volume start from some large number to small number – since piano sound is loud from its beginning and decay by the time. Say from 90% to 2% of the sampled sound audio.

3.3 Frequency Analysis

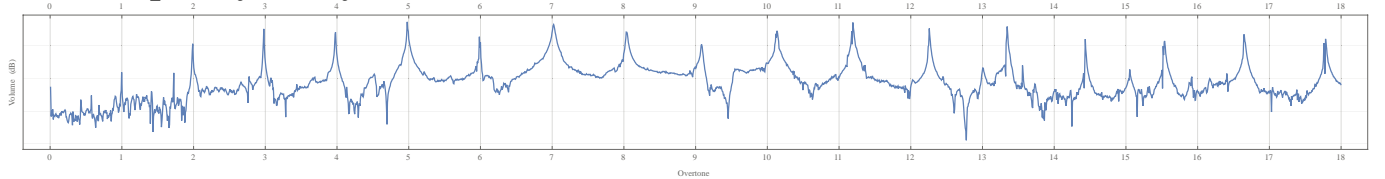


Figure 3-1 “A#0” Key (at Upright Piano Samples) Overtone Plot; Volume at Logarithm Scale

Then, put this audio samples into fourier analysis (FFT algorithm).

From Figure 3-1, we can see that the higher overtone (right hand side peaks with larger numbers) shifts higher.

It is a problem to capture all these peaks numbers, since some are not clear: the fundamental frequency (at 1), and some has multiple peaks: at 15 ~ 16.

In my work, I use the frequency *Catchup Method* to get octave values for all these peaks.

3.4 Catchup Overtone

From the characters of these peaks, there are several characters will be considered:

- From left to right, the gap between two peaks are increasing gradually.
- The largest value of this plot is probably some peak of overtone
- The valid peak should be nearly larger than fundamental frequency position: at 1.
- The peak may be broken into several peaks, we need centralize the targeted position.

From this characteristics, the *Catchup Method* could be built:

- Analyze the frequency samples which roughly larger than 1 (my program is starting from 0.8), get the peak frequency $f_{k,peak}$ at key number k .
- Comparing with ideal frequency \tilde{f}_k . We can then assume that it is $n = \text{round}(f_{k,peak} / \tilde{f}_k)$ harmonics. Then, we can know its guessed fundamental frequency is $\hat{f}_k = f_{k,peak} / n$. Then, this should be the step size for catchup method.
- The catchup method is forward (goes to the right), and the backward (goes to the left). If we are in the forward operation, the next guessed target frequency is $\hat{f}_{k,peak+1} = f_{k,peak} + f'_k$, where f'_k is the assumed gap between two peak at this position. In the first try, we set this number to $f'_k = \hat{f}_k$, and this number will be increasing for more right harmonics. Then, we get the around data (in a relatively small area) for guessed target frequency $\hat{f}_{k,peak+1} \pm \delta$, we can find its maximum number these data to be the frequency candidate $\hat{f}_{k,peak+1}^{candidate}$, then we get the data of smaller surround area $\hat{f}_{k,peak+1}^{candidate} \pm \delta'$ where $\delta' \ll \delta$. Then, we calculate the weighted average for this smaller area, and the result is the actual frequency of this peak $f_{k,peak+1} = \int \phi \cdot (\hat{f}_{k,peak+1}^{candidate} \pm \delta') d\phi$, where ϕ is the frequency. Then, the assumed gap between two peak at this step is updated to be $f'_k = f_{k,peak+1} - f_{k,peak}$.
- Iterate this method for forward catchup to get all higher frequencies.
- If the highest peak is not fundamental frequency, we will perform the backward catchup. Since there are less peaks and the overtone shift will be far less than the right, the assumed targeted gap between two peaks is set to be the assumed fundamental frequency \hat{f}_k .

From this method, we can get a overtone (frequency) list for the key k . Which is:

$$k \rightarrow \{f_{k,1}, f_{k,2}, \dots\} \quad (3.1)$$

3.5 Inharmonicity Model

From reference [1], we assume that the piano string is a bar, which follows the partial differential equation:

$$\ddot{y} \propto -y'' - \varepsilon y'''' \quad (3.2)$$

Where y is the special position of piano string (bar model). The prime is the derivative to spatial domain, and dots is the derivative to time domain.

Then, use the modal analysis and solved the natural frequencies for this string are:

$$f_{k,n} \propto n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \Rightarrow f_{k,n} = A_k \cdot n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \quad (3.3)$$

Here we have two unknown variables.

Then, we use this function to fit all frequency results at Eq.(3.1). Since A_k value is always almost 1 all the time, we can ignore this number, and focus only on B_k . However in the optimization process, with parameter A_k could achieve much better result, although finally its value is almost 1. We set 0 to be the fundamental frequency is that when $n = 0$ that the equation holds, we will restore this number later.

Then, we can get inharmonicity parameter list $\{\{k, B_k\}\}$.

From my observation, the logarithm of this number has some beautiful properties with the data $\{\{k, \ln(s \cdot B_k)\}\}$, where s is a scaling parameter (I set to 10000).

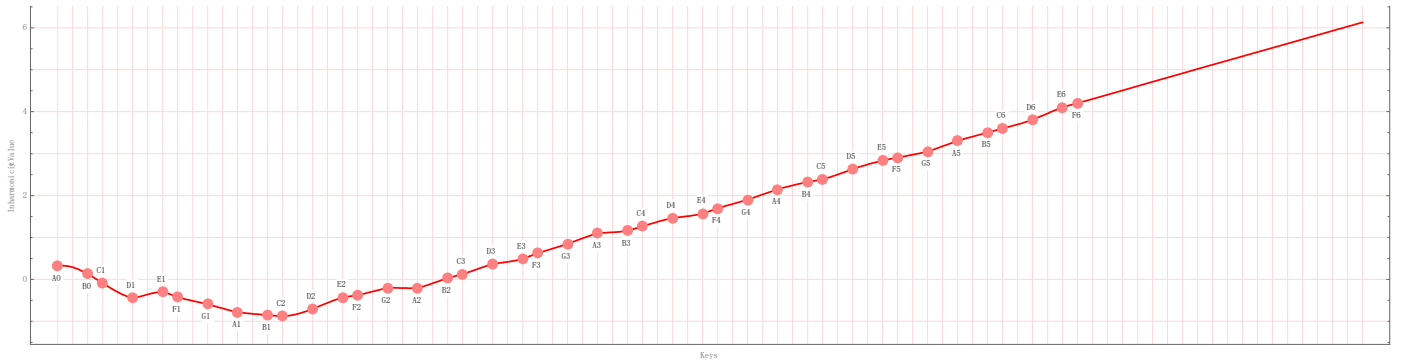


Figure 3-2 Inharmonicity Plot of Grand Piano

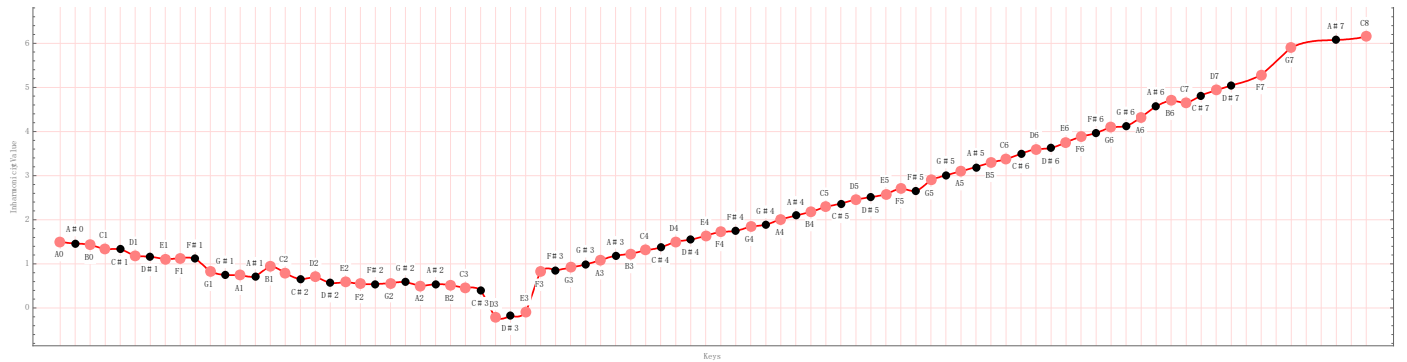


Figure 3-3 Inharmonicity Plot of Upright Piano

From Figure 3-2 and Figure 3-3, we can clearly see the line is divided into 2 parts.



Figure 3-4 Grand Piano String Arrangement



Figure 3-5 Upright Piano String Arrangement

From Figure 3-4 and Figure 3-5, we can clearly see that the string is divided into two parts, the steel string and copper string (may be covered by silver for highly expensive pianos). The upright piano has more copper strings since the steel string cannot go longer, and the string will become thicker to make the string vibrate slower. From spring vibration formula:

$$\omega = \sqrt{\frac{K}{m}} \quad (3.4)$$

Where ω is proportional to frequency, m is the mass of spring, K is the stiffness of spring.

When m increases, K increase a little bit, ω decreases, then frequency decrease.

Since the piano cannot growing longer, it become thick and more like a stick rather than an ideal string. For higher notes strings, it is too short, and the thickness become relatively larger comparing to its length, thus it is more likely to be a bar.

Thus, from the plot, we can see the inharmonicity increases at two ends, and break at the position of separation of two kinds of strings.

Since grand concert piano is longer, and can have more steel strings, less copper strings, thus the break will become more left side.

The figure of inharmonicity plot also tell us that two separate line are almost linear. In my model, I used the valid sampled points are modeled with interpolation function, and two edges are modeled with linear function, and it is method is shown below.

We get several samples from one line, and fit in a linear form.

Get its slope, and build a line which pass the right end point (since I will not wish to have a break for the interpolation function), and add some samples for edges situation to sample pool.

Similar to the left hand side.

We use interpolation for these samples of sample pool – “Left hand side + samples + right hand side”, which is our final model for inharmonicity model function $ih(k)$.

Thus, we can have the modeled parameter B_k with:

$$B(k) = e^{\frac{ih(k)}{s}} \quad (3.5)$$

Then, the modeled frequencies will be:

$$F(k, n) = f_{k,1} \cdot n \cdot \sqrt{1 + B(k) \cdot n^2} \quad (3.6)$$

3.6 Tuning Curve Optimization Model

Similar to Tunelab, I set the tuning optimization method to separate the lower tones (bass) and higher tones (tenor) into tow tuning target optimization method, the separation point k_0 is “C#4/D4”. And the default tuning method for bass is to set 6:3. Since $6/3=2$ (a/b), this frequency ratio is $\gamma = a/b$, and its corresponding pitch range is $fr2c(\gamma)$ which is 1200, and 1200 is an octave, it means the tone say “A0”s 6th harmonics will largely match its octave’s “A1”s 3rd harmonics.

Here pitch is defined by cents.

The error is defined as:

$$\varepsilon_k = F(k, a) - F(k + fr2p(a/b), b) \quad (3.7)$$

We can do this for all low strings.

For tenor, the default tuning method is set to 4:1. But this time we count the higher note as the target to calculate.

$$\varepsilon_k = F(k - fr2p(a/b), a) - F(k, b) \quad (3.8)$$

The combined expression is:

$$E(k) = \begin{cases} F(k, a) - F(k + fr2p(a/b), b) & k \leq k_0 \\ F(k - fr2p(a/b), a) - F(k, b) & k > k_0 \end{cases} \quad (3.9)$$

From this equation, we can see $E(k)$ is only a value for each calculation.

From this point, we need a function to largely eliminate these errors. The piano tuning curve $C(k)$ is introduced.

The cost function for optimization is:

$$J(k) = \sum_k (C(k) - E(x))^2 \quad (3.10)$$

Which minimize the square error of these functions.

Here I use polynomial for easier calculation:

$$C(x) = \sum_{i=1}^n c_i \cdot x^i \quad (3.11)$$

Since $C(x)$ will pass the fix point, which is “A4” pitch at 440Hz frequency at pitch deviation of 0, thus i is from 1 and $x = k - k_{A4}$, where k_{A4} is the key number (index) at “A4”.

Thus, $J(k)$ is the second order polynomial function, which is very easy to minimize by linear regression method to calculate the fitting parameter $\{c_i\}$, and rebuild the functions.

Then, we can bring it to the $J(k)$ function to calculate its deviations.

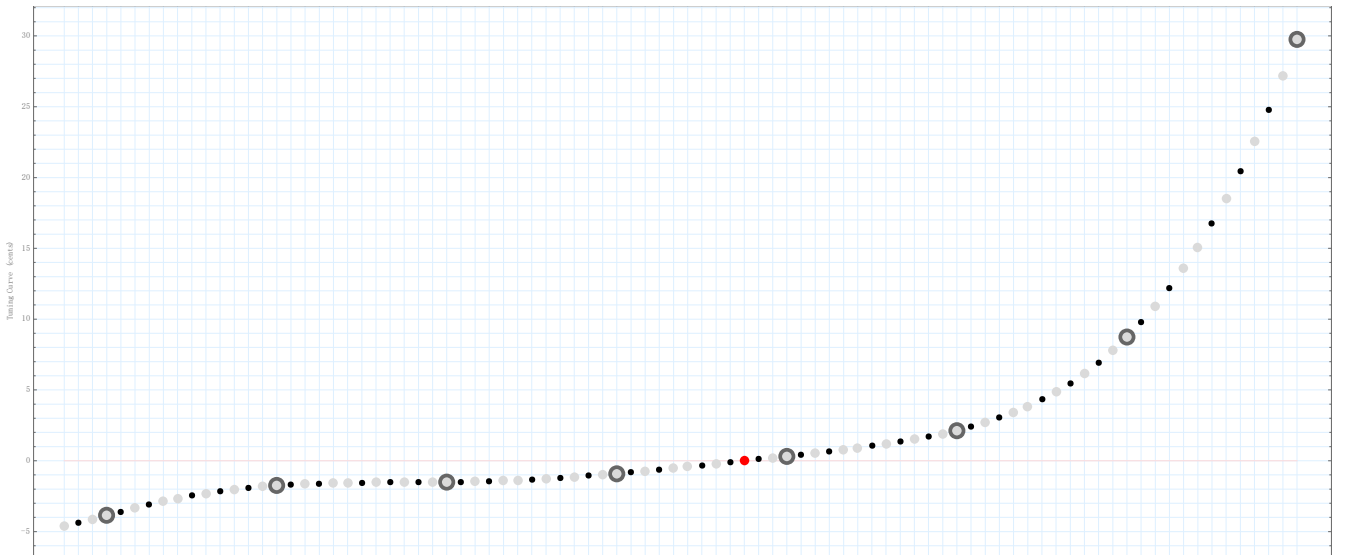


Figure 3-6 $C(x)$ for Grand Piano

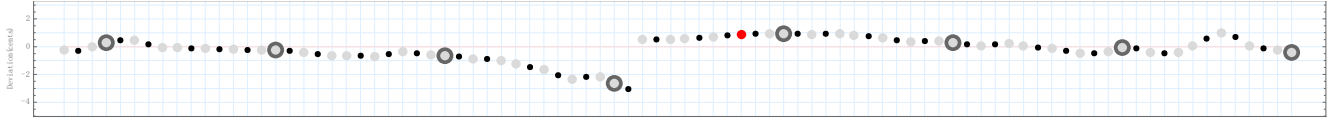


Figure 3-7 $J(x)$ for Grand Piano

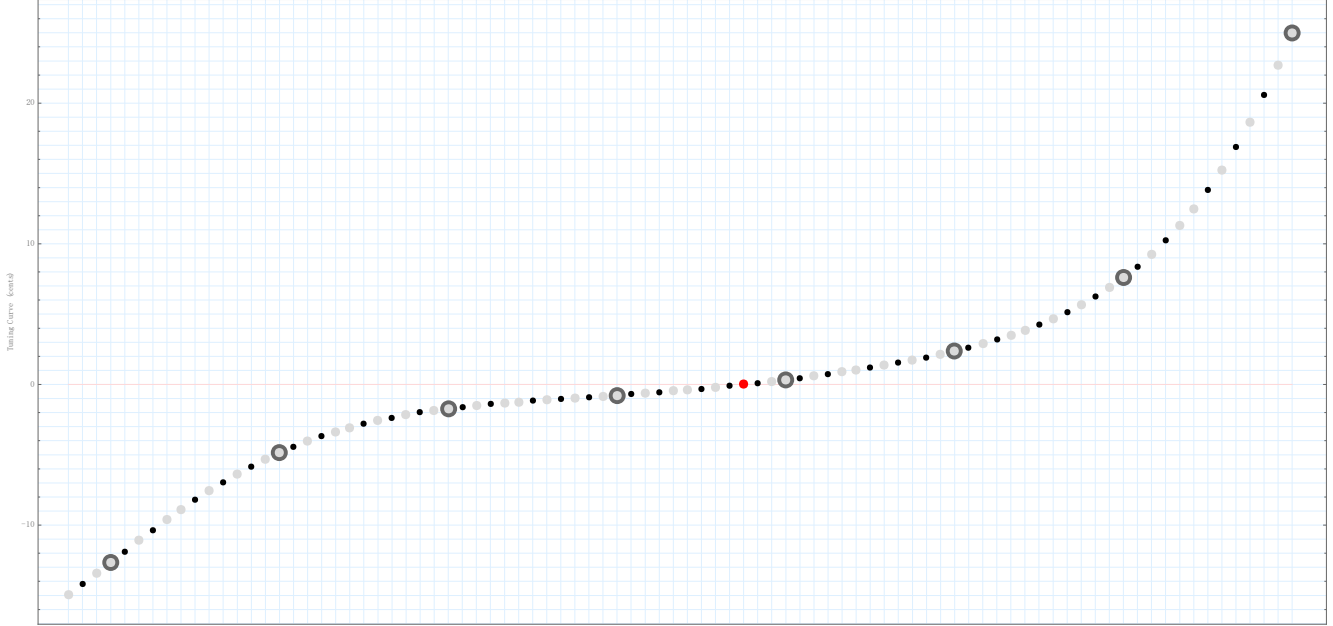


Figure 3-8 $C(x)$ for Upright Piano

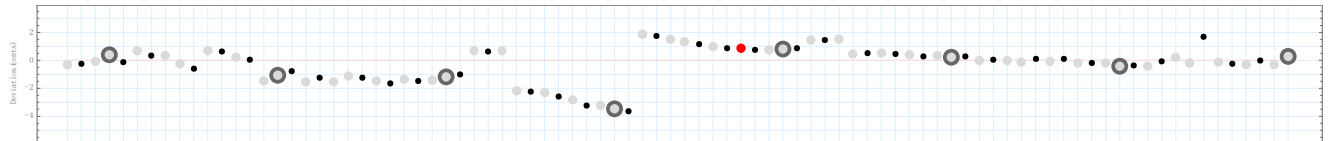


Figure 3-9 $J(x)$ for Upright Piano

The result of two piano is shown above. Horizontal axis is the key number, and the vertical axis the pitch deviation with idea frequencies represented by cents.

From this tuning method, we can see that the bass tuning will consider the deviations from the tenor part, and vice versa, and the effect are inner related. Thus this tuning method is theoretically to optimize almost the whole piano tuning.

3.7 Temperament Model

With the development of music, various temperament appears and create unique flavor of music. The temperament model is using the pitch deviation tables of different temperament (the unit is cent). We can then create the non 12 equal temperament tuning strategy. The temperament function is defined to be $T(k)$.

The tuning table such as “Bach - Bradley Lehman” is:

C	C#	D	D#	E	F	F#	G	G#	A	A#	B
5.87	3.91	1.96	3.91	-1.96	7.82	1.96	3.91	3.81	0	3.91	0

Table 3-1 Table for “Bach - Bradley Lehman” Temperament

Where A note will always be 0 since A is the reference frequency and will always keep to 440 Hz (if is standard situation).

This table shows the situation of “C” major.

The other major tuning will follow the rotation of table. For example: if tuning “D” major, the “D” will rotate to current “D” → “C” place, which is rotating left 2 times. However, we will make sure “A” note will always be 0, then, we can subtract the number at “B” → “A” to make it possible.

Then, add these pitch errors to all the notes of tuning, the modified tuning curve is:

$$C'(k) = C(k) + T(k) \quad (3.12)$$

3.8 Creating Tuning Table

From the modeling, we can get a strategy of piano tuning, then we can convert this strategy into a tuning table, which shows all the frequency of fundamental its harmonics values, and corresponding deviation to ideal frequencies represented by cents.

The grand and upright piano tuning strategy is shown below.

The red font is the frequencies recommended for the devices to tune.

Which shown in Figure 7-1 and Figure 7-2.

4 FUTURE WORK

Although the Entropy piano tuning method is far more advanced than this tuning method theoretically, however the jumpy tuning curve will make the music scales sound weird. If I have time, I will implement the entropy tuner with much more smooth functions, this construction is easier than original idea since the optimization at his method is only few parameters if using similar polynomial to optimize the curve to achieve more smooth result with entropy function as cost function.

Over-pull tuning is implemented experimentally with their tuning apps, and I do not know its method due to its close source reason. And I am still lack of research on this area, thus I will leave it as future work to think about. I know this effect is caused by the experimental result of the percentage that the string pins will loosen and drop the pitch, the tuner will make up the errors of this effect by over pull and tune higher tones.

5 CONCLUSION

This tuning method gives us a solution of piano tuning that works as well as commercial apps Tunelab. The method is presented to optimize the whole piano notes sound. Future work is given to develop maybe in the future.

6 REFERENCE

- [1] Hinrichsen, Haye. "Entropy-based tuning of musical instruments." Revista brasileira de Ensino de Física 34.2 (2012): 1-8.
- [2] Github for Piano Tuning Project [https://github.com/RobertBoganKang/piano_tuning]

7 APPENDIX

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16																
A0	71.4266	-0.009	54.857	-0.009	82.9025	-0.009	109.774	-0.009	137.284	-0.009	164.843	-0.009	192.461	-0.009	220.152	-0.009	247.925	-0.009	275.791	-0.009	303.762	-0.009	331.849	-0.009	360.063	-0.009	388.414	-0.009	416.913	-0.009	445.571	-0.009
A#0	59.0617	-0.009	58.1273	-0.009	87.2084	-0.009	116.317	-0.009	145.464	-0.009	174.661	-0.009	203.921	-0.009	233.254	-0.009	262.672	-0.009	292.187	-0.009	321.800	-0.009	351.55	-0.009	381.422	-0.009	411.435	-0.009	441.601	-0.009	471.93	-0.009
B0	50.7944	-0.010	61.5924	-0.010	92.4044	-0.010	123.241	-0.010	154.113	-0.010	185.03	-0.010	216.004	-0.010	247.044	-0.010	278.161	-0.010	309.365	-0.010	340.667	-0.010	372.077	-0.010	403.606	-0.010	435.262	-0.010	467.057	-0.010	499	-0.010
C1	52.6306	-0.009	65.2641	-0.009	97.9096	-0.009	130.576	-0.009	163.272	-0.009	196.008	-0.009	228.791	-0.009	261.63	-0.009	294.53	-0.009	327.515	-0.009	360.577	-0.009	393.732	-0.009	426.988	-0.009	460.352	-0.009	493.835	-0.009	527.445	-0.009
C#1	54.5761	-0.009	69.1548	-0.009	103.744	-0.009	138.351	-0.009	172.983	-0.009	207.649	-0.009	242.355	-0.009	277.111	-0.009	311.922	-0.009	346.797	-0.009	381.744	-0.009	416.769	-0.009	451.881	-0.009	487.087	-0.009	522.394	-0.009	557.81	-0.009
D1	56.6375	-0.009	73.7273	-0.009	109.926	-0.009	146.592	-0.009	183.281	-0.009	220.001	-0.009	256.758	-0.009	293.559	-0.009	330.412	-0.009	367.324	-0.009	404.301	-0.009	441.35	-0.009	478.478	-0.009	515.693	-0.009	553.001	-0.009	590.408	-0.009
D#1	58.8214	-0.009	77.6456	-0.009	116.481	-0.009	155.335	-0.009	194.216	-0.009	233.132	-0.009	272.092	-0.009	311.103	-0.009	350.174	-0.009	389.312	-0.009	428.526	-0.009	467.823	-0.009	507.213	-0.009	546.701	-0.009	586.297	-0.009	626.009	-0.009
E1	41.1352	-0.009	82.2735	-0.009	123.424	-0.009	164.596	-0.009	205.798	-0.009	247.04	-0.009	288.331	-0.009	329.68	-0.009	371.095	-0.009	412.587	-0.009	454.164	-0.009	495.835	-0.009	537.609	-0.009	579.494	-0.009	621.501	-0.009	663.638	-0.009
F1	43.5865	-0.009	87.1758	-0.009	130.777	-0.009	174.398	-0.009	218.047	-0.009	261.734	-0.009	305.466	-0.009	349.253	-0.009	393.103	-0.009	437.024	-0.009	481.025	-0.009	525.114	-0.009	569.3	-0.009	613.592	-0.009	657.996	-0.009	702.523	-0.009
F#1	46.1833	-0.009	92.3694	-0.009	138.567	-0.009	184.783	-0.009	231.027	-0.009	277.308	-0.009	323.632	-0.009	370.009	-0.009	416.447	-0.009	462.964	-0.009	509.538	-0.009	556.208	-0.009	602.972	-0.009	649.837	-0.009	696.812	-0.009	743.905	-0.009
G1	48.9343	-0.009	97.8713	-0.009	146.819	-0.009	195.786	-0.009	244.78	-0.009	293.809	-0.009	342.882	-0.009	392.006	-0.009	441.19	-0.009	490.441	-0.009	539.768	-0.009	589.179	-0.009	638.681	-0.009	688.284	-0.009	737.994	-0.009	787.82	-0.009
G#1	51.8485	-0.009	103.7	-0.009	155.561	-0.009	207.441	-0.009	259.347	-0.009	311.286	-0.009	363.267	-0.009	415.297	-0.009	467.385	-0.009	519.537	-0.009	571.762	-0.009	624.067	-0.009	676.46	-0.009	728.949	-0.009	781.541	-0.009	834.243	-0.009
A1	54.9357	-0.009	109.874	-0.009	164.822	-0.009	219.788	-0.009	274.779	-0.009	329.803	-0.009	384.888	-0.009	439.98	-0.009	495.147	-0.009	550.378	-0.009	605.678	-0.009	661.057	-0.009	716.521	-0.009	772.078	-0.009	827.735	-0.009	883.499	-0.009
A#1	58.2061	-0.009	116.415	-0.009	174.634	-0.009	232.87	-0.009	291.133	-0.009	349.429	-0.009	407.765	-0.009	466.151	-0.009	524.593	-0.009	583.098	-0.009	641.676	-0.009	700.332	-0.009	759.076	-0.009	817.914	-0.009	876.835	-0.009	935.902	-0.009
B1	61.6705	-0.009	123.344	-0.009	185.027	-0.009	246.729	-0.009	308.458	-0.009	370.221	-0.009	432.026	-0.009	493.882	-0.009	555.795	-0.009	617.774	-0.009	679.827	-0.009	741.962	-0.009	804.187	-0.009	866.508	-0.009	928.935	-0.009	991.474	-0.009
C2	65.3404	-0.009	130.684	-0.009	196.038	-0.009	261.411	-0.009	322.245	-0.009	385.475	-0.009	448.255	-0.009	511.585	-0.009	575.465	-0.009	640.903	-0.009	707.237	-0.009	774.561	-0.009	841.963	-0.009	917.973	-0.009	994.059	-0.009	1070.32	-0.009
C#2	69.2282	-0.009	138.459	-0.009	207.703	-0.009	276.988	-0.009	346.263	-0.009	415.598	-0.009	484.982	-0.009	554.423	-0.009	623.932	-0.009	693.516	-0.009	763.186	-0.009	832.949	-0.009	902.816	-0.009	972.795	-0.009	1042.9	-0.009	1113.13	-0.009
D2	73.3688	-0.009	146.697	-0.009	220.062	-0.009	293.453	-0.009	366.879	-0.009	440.352	-0.009	513.884	-0.009	587.484	-0.009	661.164	-0.009	734.934	-0.009	808.806	-0.009	882.789	-0.009	956.895	-0.009	1031.13	-0.009	1105.82	-0.009	1180.06	-0.009
D#2	77.7098	-0.009	155.424	-0.009	233.156	-0.009	310.919	-0.009	388.727	-0.009	466.593	-0.009	544.53	-0.009	622.551	-0.009	700.671	-0.009	778.901	-0.009	857.256	-0.009	935.748	-0.009	1014.39	-0.009	1093.2	-0.009	1172.18	-0.009	1251.35	-0.009
E2	82.3319	-0.009	164.669	-0.009	247.028	-0.009	329.424	-0.009	411.874	-0.009	494.393	-0.009	576.997	-0.009	659.704	-0.009	742.527	-0.009	825.484	-0.009	908.59	-0.009	991.861	-0.009	1075.31	-0.009	1158.96	-0.009	1242.82	-0.009	1326.91	-0.009
F2	87.2286	-0.009	174.463	-0.009	261.722	-0.009	346.022	-0.009	436.382	-0.009	525.82	-0.009	611.353	-0.009	698.999	-0.009	786.777	-0.009	874.703	-0.009	962.79	-0.009	1051.07	-0.009	1139.55	-0.009	1228.25	-0.009	1317.19	-0.009	1406.38	-0.009
F#2	92.4162	-0.009	184.839	-0.009	277.29	-0.009	369.789	-0.009	462.358	-0.009	555.016	-0.009	647.786	-0.009	740.686	-0.009	833.739	-0.009	926.964	-0.009	1020.38	-0.009	1114.01	-0.009	1207.88	-0.009	1302	-0.009	1396.39	-0.009	1491.08	-0.009
G2	97.912	-0.009	195.832	-0.009	293.784	-0.009	391.792	-0.009	489.88	-0.009	588.072	-0.009	686.392	-0.009	784.864	-0.009	883.511	-0.009	982.358	-0.009	1081.43	-0.009	1180.74	-0.009	1280.33	-0.009	1381.05	-0.009	1480.41	-0.009	1580.94	-0.009
G#2	103.734	-0.009	207.477	-0.009	311.254	-0.009	415.09	-0.009	519.01	-0.009	623.04	-0.009	727.205	-0.009	831.531	-0.009	936.041	-0.009	1040.76	-0.009	1145.72	-0.009	1250.93	-0.009	1356.43	-0.009	1462.25	-0.009	1568.39	-0.009	1674.89	-0.009
A2	109.903	-0.009	219.815	-0.009	329.763	-0.009	439.774	-0.009	549.875	-0.009	660.092	-0.009	770.453	-0.009	880.984	-0.009	991.712	-0.009	1102.66	-0.009	1213.86	-0.009	1325.34	-0.009	1437.12	-0.009	1549.23	-0.009	1661.7	-0.009	1774.54	-0.009
A#2	116.439	-0.009	232.888	-0.009	349.38	-0.009	465.946	-0.009	582.618	-0.009	699.428	-0.009	816.408	-0.009	933.589	-0.009	1051.55	-0.009	1168.68	-0.009	1286.65	-0.009	1404.95	-0.009	1523.61	-0.009	1642.65	-0.009	1762.12	-0.009	1882.56	-0.009
B2	123.263	-0.009	246.739	-0.009	370.166	-0.009	493.682	-0.009	617.325	-0.009	741.134	-0.009	865.145	-0.009	989.388	-0.009	1113.93	-0.009	1238.78	-0.009	1363.98	-0.009	1489.58	-0.009	1615.6	-0.009	1742.09	-0.009	1869.08	-0.009	1996.6	-0.009
C3	130.542	-0.009	261.414	-0.009	392.188	-0.009	523.065	-0.009	654.091	-0.009	785.309	-0.009	916.764	-0.009	1048.51	-0.009	1180.56	-0.009	1312.99	-0.009	1445.83	-0.009	1579.13	-0.009	1712.92	-0.009	1847.26	-0.009	1982.18	-0.009	2117.93	-0.009
C#3	137.478	-0.009	276.963	-0.009	415.524	-0.009	554.21	-0.009	693.073	-0.009	832.166	-0.009	971.543	-0.009	1111.26	-0.009	1251.36	-0.009	1391.9	-0.009	1532.93	-0.009	1674.51	-0.009	1816.69	-0.009	1959.51	-0.009	2103.03	-0.009	2247.29	-0.009
D3	146.703	-0.009	293.438	-0.009	442.284	-0.009	587.215	-0.009	734.39	-0.009	881.84	-0.009	1029.63	-0.009	1177.82	-0.009	1326.47	-0.009	1475.65	-0.009	1625.42	-0.009	1775.84	-0.009	1925.96	-0.009	2078.88	-0.009	2231.59	-0.009	2385.22	-0.009
D#3	155.434	-0.009	310.892	-0.009	466.445	-0.009	622.163	-0.009	778.117	-0.009	934.378	-0.009	1091.02	-0.009	1248.1	-0.009	1405.7	-0.009	1563.89	-0.009	1722.74	-0.009	1882.3	-0.009	2042.66	-0.009	2203.88	-0.009	2366.02	-0.009	2529.16	-0.009
E3	164.68	-0.009	329.387	-0.009	494.201	-0.009	659.204	-0.009	824.475	-0.009	990.994	-0.009	1156.14	-0.009	1322.7	-0.009	1489.84	-0.009	1657.65	-0.009	1826.2	-0.009	1995.58	-0.009	2165.85	-0.009	2337.1	-0.009	2509.4	-0.009	2682.82	-0.009
F3	174.476	-0.009	348.985	-0.009	523.625	-0.009	689.494	-0.009	854.69	-0.009	1020.31	-0.009	1185.93	-0.009	1351.99	-0.009	1519.68	-0.009	1687.97	-0.009	1856.97	-0.009	2026.62	-0.009	2196.93	-0.009	2367.8	-0.009	2539.22	-0.009	2711.93	-0.009
F#3	184.856	-0.009	369.751	-0.009	554.802	-0.009	740.123	-0.009	925.833	-0.009	1112.05	-0.009	1298.88	-0.009	1486.44	-0.009	1674.53	-0.009	1864.22	-0.009	2054.67	-0.009	2246.29									

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
A0	27.2634	-13.532	54.5391	-13.532	81.8635	-13.532	109.273	-13.532	136.805	-13.532	164.403	-13.532	192.376	-13.532	220.487	-13.532
A#0	38.8972	-13.532	57.8069	-13.532	86.7667	-13.532	115.814	-13.532	144.986	-13.532	174.319	-13.532	203.85	-13.532	233.616	-13.532
B0	30.6292	-13.532	61.2713	-13.532	91.9648	-13.532	122.748	-13.532	153.659	-13.532	184.737	-13.532	216.018	-13.532	247.54	-13.532
C1	32.4652	-13.532	64.9427	-13.532	97.4694	-13.532	130.082	-13.532	162.817	-13.532	195.712	-13.532	228.802	-13.532	262.122	-13.532
C#1	34.4112	-13.532	68.8355	-13.532	103.312	-13.532	137.88	-13.532	172.579	-13.532	207.448	-13.532	242.524	-13.532	277.846	-13.532
D1	36.4736	-13.532	72.9592	-13.532	109.492	-13.532	146.109	-13.532	182.844	-13.532	219.733	-13.532	256.811	-13.532	294.112	-13.532
D#1	38.6593	-13.532	77.3311	-13.532	116.053	-13.532	154.861	-13.532	193.794	-13.532	232.888	-13.532	272.18	-13.532	311.705	-13.532
E1	40.9755	-13.532	81.9635	-13.532	123.001	-13.532	164.126	-13.532	205.374	-13.532	246.783	-13.532	288.39	-13.532	330.231	-13.532
F1	43.4298	-13.532	86.8731	-13.532	130.37	-13.532	173.961	-13.532	217.685	-13.532	261.584	-13.532	305.695	-13.532	350.06	-13.532
F#1	46.0304	-13.532	92.0748	-13.532	138.176	-13.532	184.375	-13.532	230.714	-13.532	277.286	-13.532	323.982	-13.532	370.992	-13.532
G1	48.7857	-13.532	97.5825	-13.532	146.424	-13.532	195.344	-13.532	244.375	-13.532	293.552	-13.532	342.906	-13.532	392.472	-13.532
G#1	51.7049	-13.532	103.421	-13.532	155.181	-13.532	207.017	-13.532	258.963	-13.532	311.051	-13.532	363.314	-13.532	415.783	-13.532
A1	54.7977	-13.532	109.607	-13.532	164.462	-13.532	219.398	-13.532	274.45	-13.532	329.65	-13.532	385.035	-13.532	440.637	-13.532
A#1	58.0742	-13.532	116.16	-13.532	174.294	-13.532	232.51	-13.532	290.845	-13.532	349.333	-13.532	408.011	-13.532	466.912	-13.532
B1	61.5454	-13.532	123.107	-13.532	184.731	-13.532	246.467	-13.532	308.361	-13.532	370.46	-13.532	432.812	-13.532	495.463	-13.532
C2	65.2226	-13.532	130.459	-13.532	195.754	-13.532	261.149	-13.532	326.687	-13.532	392.411	-13.532	458.365	-13.532	524.589	-13.532
C#2	69.118	-13.532	138.249	-13.532	207.434	-13.532	276.71	-13.532	346.119	-13.532	415.7	-13.532	485.492	-13.532	555.534	-13.532
D2	73.2446	-13.532	146.504	-13.532	219.823	-13.532	293.245	-13.532	366.814	-13.532	440.576	-13.532	514.572	-13.532	588.848	-13.532
D#2	77.6161	-13.532	155.246	-13.532	232.823	-13.532	310.71	-13.532	388.627	-13.532	466.721	-13.532	545.033	-13.532	623.604	-13.532
E2	82.2469	-13.532	164.509	-13.532	246.829	-13.532	329.753	-13.532	411.825	-13.532	494.588	-13.532	577.587	-13.532	660.865	-13.532
F2	87.1524	-13.532	174.32	-13.532	267.142	-13.532	348.88	-13.532	436.363	-13.532	524.081	-13.532	611.959	-13.532	700.162	-13.532
F#2	92.3489	-13.532	184.714	-13.532	277.142	-13.532	369.682	-13.532	460.584	-13.532	554.284	-13.532	648.442	-13.532	741.9	-13.532
G2	97.8537	-13.532	195.725	-13.532	293.664	-13.532	391.724	-13.532	489.956	-13.532	588.412	-13.532	687.141	-13.532	786.196	-13.532
G#2	103.685	-13.532	207.389	-13.532	311.168	-13.532	415.077	-13.532	519.174	-13.532	623.613	-13.532	728.151	-13.532	833.143	-13.532
A2	109.863	-13.532	219.743	-13.532	329.697	-13.532	439.777	-13.532	550.038	-13.532	660.535	-13.532	771.321	-13.532	882.45	-13.532
A#2	115.407	-13.532	232.833	-13.532	349.34	-13.532	465.987	-13.532	582.834	-13.532	699.94	-13.532	817.366	-13.532	935.17	-13.532
B2	121.239	-13.532	246.699	-13.532	370.142	-13.532	493.73	-13.532	617.525	-13.532	741.589	-13.532	865.984	-13.532	990.771	-13.532
C3	130.683	-13.532	261.387	-13.532	392.173	-13.532	523.103	-13.532	654.238	-13.532	785.64	-13.532	917.369	-13.532	1049.49	-13.532
C#3	138.464	-13.532	278.948	-13.532	415.516	-13.532	554.229	-13.532	693.145	-13.532	832.341	-13.532	971.864	-13.532	1111.78	-13.532
D3	146.706	-13.532	293.424	-13.532	440.189	-13.532	587.036	-13.532	734.002	-13.532	881.122	-13.532	1028.43	-13.532	1175.96	-13.532
D#3	155.458	-13.532	307.389	-13.532	466.392	-13.532	621.987	-13.532	777.712	-13.532	933.607	-13.532	1089.71	-13.532	1246.06	-13.532
E3	164.689	-13.532	329.393	-13.532	494.156	-13.532	659.024	-13.532	824.04	-13.532	989.249	-13.532	1154.7	-13.532	1320.43	-13.532
F3	174.49	-13.532	349.019	-13.532	523.709	-13.532	698.679	-13.532	874.049	-13.532	1049.94	-13.532	1228.46	-13.532	1403.75	-13.532
F#3	184.873	-13.532	369.79	-13.532	554.88	-13.532	740.275	-13.532	926.104	-13.532	1112.5	-13.532	1299.58	-13.532	1487.49	-13.532
G3	195.874	-13.532	391.797	-13.532	587.016	-13.532	784.379	-13.532	981.332	-13.532	1178.92	-13.532	1377.29	-13.532	1576.58	-13.532
G#3	207.529	-13.532	415.114	-13.532	622.921	-13.532	831.118	-13.532	1039.87	-13.532	1249.34	-13.532	1459.7	-13.532	1671.11	-13.532
A3	219.878	-13.532	439.821	-13.532	660.024	-13.532	880.684	-13.532	1101.99	-13.532	1324.15	-13.532	1547.34	-13.532	1771.76	-13.532
A#3	232.961	-13.532	465.98	-13.532	699.341	-13.532	933.218	-13.532	1167.86	-13.532	1404.78	-13.532	1640.32	-13.532	1878.6	-13.532
B3	246.823	-13.532	493.73	-13.532	740.975	-13.532	988.809	-13.532	1237.49	-13.532	1487.25	-13.532	1738.36	-13.532	1991.06	-13.532
C4	261.51	-13.532	523.103	-13.532	785.111	-13.532	1047.78	-13.532	1311.42	-13.532	1576.31	-13.532	1842.74	-13.532	2110.99	-13.532
C#4	277.071	-13.532	554.251	-13.532	831.866	-13.532	1109.24	-13.532	1389.71	-13.532	1670.58	-13.532	1953.17	-13.532	2237.82	-13.532
D4	293.559	-13.532	587.25	-13.532	881.469	-13.532	1176.61	-13.532	1473.07	-13.532	1771.24	-13.532	2071.5	-13.532	2374.23	-13.532
D#4	311.028	-13.532	622.203	-13.532	933.962	-13.532	1248.74	-13.532	1560.98	-13.532	1877.11	-13.532	2195.55	-13.532	2516.74	-13.532
E4	329.538	-13.532	659.246	-13.532	989.631	-13.532	1321.2	-13.532	1654.46	-13.532	1989.91	-13.532	2328.04	-13.532	2699.34	-13.532
F4	349.15	-13.532	698.407	-13.532	1040.13	-13.532	1375.58	-13.532	1753.58	-13.532	2149.66	-13.532	2548.65	-13.532	2931.39	-13.532
F#4	369.931	-13.532	740.074	-13.532	1111.06	-13.532	1483.53	-13.532	1858.1	-13.532	2235.39	-13.532	2616.03	-13.532	3000.62	-13.532
G4	391.95	-13.532	784.148	-13.532	1177.34	-13.532	1572.27	-13.532	1969.67	-13.532	2370.27	-13.532	2774.8	-13.532	3183.96	-13.532
G#4	415.28	-13.532	831.866	-13.532	1247.48	-13.532	1666.03	-13.532	2087.3	-13.532	2512.09	-13.532	2941.18	-13.532	3375.36	-13.532
A4	440.18	-13.532	880.33	-13.532	1321.98	-13.532	1765.93	-13.532	2213.16	-13.532	2664.63	-13.532	3121.29	-13.532	3584.07	-13.532
A#4	466.193	-13.532	932.765	-13.532	1400.85	-13.532	1871.57	-13.532	2346.06	-13.532	2825.4	-13.532	3310.7	-13.532	3803	-13.532
B4	493.947	-13.532	988.331	-13.532	1484.46	-13.532	1983.63	-13.532	2487.14	-13.532	2996.26	-13.532	3512.22	-13.532	4036.26	-13.532
C5	523.555	-13.532	1047.23	-13.532	1574.77	-13.532	2102.73	-13.532	2637.44	-13.532	3178.79	-13.532	3728.25	-13.532	4287.28	-13.532
C#5	554.316	-13.532	1109.62	-13.532	1667.09	-13.532	2228.88	-13.532	2796.13	-13.532	3371.14	-13.532	3955.4	-13.532	4550.53	-13.532
D5	587.533	-13.532	1175.75	-13.532	1766.72	-13.532	2382.46	-13.532	2965.01	-13.532	3576.34	-13.532	4198.37	-13.532	4833	-13.532
D#5	622.52	-13.532	1245.81	-13.532	1842.16	-13.532	2502.87	-13.532	3143.19	-13.532	3792.32	-13.532	4453.43	-13.532	5128.59	-13.532
E5	659.591	-13.532	1320.05	-13.532	1983.98	-13.532	2653.97	-13.532	3332.55	-13.532	4022.23	-13.532	4725.42	-13.532	5444.47	-13.532
F5	698.874	-13.532	1398.8	-13.532	2102.94	-13.532	2814.4	-13.532	3536.28	-13.532	4271.56	-13.532	5023.17	-13.532	5793.9	-13.532
F#5	740.499	-13.532	1482.04	-13.532	2267.35	-13.532	2980.73	-13.532	3744.03	-13.532	4520.63	-13.532	5313.43	-13.532	6125.24	-13.532
G5	784.607	-13.532	1570.64	-13.532	2422.75	-13.532	3163.95	-13.532	3979.57	-13.532	4813.22	-13.532	5668.77	-13.532	6549.91	-13.532
G#5	831.347	-13.532	1664.37	-13.532	2504.08	-13.532	3355.43	-13.532	4223.26	-13.532	5112.27	-13.532	6026.95	-13.532	6971.61	-13.532
A5	880.877	-13.532	1763.72	-13.532	2654.39	-13.532	3558.67	-13.532	4482.23	-13.532	5430.5	-13.532	6408.73	-13.532	7421.83	-13.532
A#5	933.363	-13.532	1868.99	-13.532	2811.6	-13.532	3773.87	-13.532	4756.25	-13.532	5766.99	-13.532	6812.01	-13.532	7896.92	-13.532
B5	988.988	-13.532	1980.65	-13.532	2983.1	-13.532	4003.9	-13.532	5051	-13.532	6131.64					