Piano Tuning Method

Zuheng Kang

CONTENTS

Αł	ostract		2
	Project	t Location	2
1	Intro	oduction	2
2	Tecl	hnical Knowledge	3
	2.1	Key Names	3
	2.2	Key Numbers	3
	2.3	Functions	3
	2.4	Tuning Methodology	4
3	Pian	no Tuning Method	4
	3.1	Traditional Method	4
	3.1.1	1 Sampling Piano	4
	3.1.2	2 Audio Processing	4
	3.1.3	Frequency Analysis	4
	3.1.4	4 Catchup Overtone	5
	3.1.5	5 Inharmonicity Model	6
	3.1.6	6 Tuning Curve Optimization Model	8
	3.1.7	7 Temperament Model	11
	3.1.8	8 Creating Tuning Strategy Table	12
	3.2	Entropy Tuning Method	12
	3.2.1	1 Sampling Piano & Audio Processing	13
	3.2.2	2 Construct Spectrum	13
	3.2.3	3 Tuning with Entropy Optimizer	13
	3.2.4	4 Creating Tuning Strategy Table	15
	3.2.5	5 Tune for Songs	16
4	Aud	lio Processing & Pure Sound Tuner	17
	4.1	Tuning	17
	4.2	Sound Purify	17
5	Futu	ıre Work	19
6	Refe	erence	19
7	App	endix	20

ABSTRACT

Since the piano string is consider to be a stick rather than a pure ideal string, it contains stiffness and its overtone will shift in such way that make piano tuning a difficult work. In this work, two optimization algorithm for piano tuning method is presented. The traditional tuning algorithm is divided into several models that using various fitting technique model the target piano, and then convert to linear regression problem for optimization. The entropy tuning method is a trial method to tune the piano to minimize the entropy value when all key are pressed – to achieve simpler spectrum in pitch domain. In addition, a pure tuner method is invented to get rid of all inharmonic effect of piano sound.

Keyword: piano tuning, inharmonicity, entropy, audio processing

PROJECT LOCATION

Reference [2]

1 INTRODUCTION

Piano tuning is a difficult work since the harmonics shift that make the piano hard to tune. The tuning process will be a task to highly reduce the audible cacophonous. There are several factors we need to consider, which the rule of harmony is.

- The cacophonous created by its base frequency and audible harmonics; a good tuning will largely reduce the inharmonic effects for harmonies (the frequency domain should be simple, which the frequency peaks should merged or coincide).
- The inner music scales related pitch; the odd pitch tuning will result in the weird effect when playing music scales.

Other famous related works are:

- Tunelab (closed source; has trial version)
- Reyburn CyberTuner (closed source; no trial version)
- Entropy Piano Tuner (open source) [1]

The first two is similar, which represent the old tuning techniques, and my work mostly focus on this algorithm.

As for Entropy Piano Tuner, it represents the new way of piano tuning. It can also achieve very good result for tuning a piano, however this temperament is not regular 12-equal temperament, but a piano approximation temperament starting from 12-equal temperament, in order to largely eliminate the non-harmonious effect.

- Since the pitch in the piano does not have relatively same pitch interval, some inner scales sound weird.
- Since the piano optimize all 88 keys harmony, it values overall harmonious some simpler chord might not sound harmonious.
- It only considers the sound which at the certain striking level of piano keys, which result in the optimization of keys are based only on sampling striking level. However, it values the average case for piano performance, thus it covers the majority situation of harmony cases.
- The accuracy cannot be too high due to large amount of calculation, it does not achieve an ideal result.

In my work, I will talk about two piano tuning methods, and one audio processing method.

- As for traditional tuning method, since it is closed source, I guessed their tuning method and create a similar solution, and will be shown in this article. Besides, I used more accurate model for inharmonicity coefficients.
- I will reproduce the result for Entropy Piano Tuning method.

• The tuning for audio and a pure sound tuner is introduced.

In this article, the first part is to introduce the technical knowledge for high level modeling algorithms. The second part is to introduce my piano modeling and tuning optimization method. Then, followed an audio processing technique. Finally, the future work will be introduced.

2 TECHNICAL KNOWLEDGE

2.1 KEY NAMES

The left most key name is defined as "A0", where "A" is the note name, 0 is the scale number. "C" is the starting point of one scale. It only allowed sharp in the note, flat is not allowed in this naming format.

There are 88 keys for standard piano.

2.2 KEY NUMBERS

In the real world, the piano key will be labeled with numbers when the piano is open and machine part is shown off.

A0 key is labeled to be 1, and "C8" is 88.

However, in my program, "A0" key is labeled as 0 for easier calculation, which is defined as k.

2.3 Functions

Frequency ratio to cents function:

$$\operatorname{Fr}_{\to c}(\gamma) = 1200 \log_2(\gamma) \tag{2.1}$$

The inverse process is:

$$C_{\rightarrow fr}\left(c\right) = 2^{\left(\frac{c}{1200}\right)} \tag{2.2}$$

Where cents is from 12 equal temperament, each half note has 100 divisions, named cents.

Frequency add cents (pitch) function:

$$F_{+c}(f,c) = f \cdot 2^{\left(\frac{c}{1200}\right)} \tag{2.3}$$

This function returns the frequency that added the pitch (cents) c.

The ideal frequency for the key k is:

$$\tilde{f}_k = \tilde{f}_{[A4]} \cdot 2^{\left(\frac{k-48}{12}\right)}$$
 (2.4)

Where $\tilde{f}_{[A4]}$ is the international standard pitch for "A4", usually defined as 440Hz. Other tuning standard will replace this number, 48 is the key number for "A4".

2.4 TUNING METHODOLOGY

Since the minor tuning for each string will rarely affect its stiffness, from Equation (3.3), we assume that the B_k is the constant.

3 PIANO TUNING METHOD

3.1 TRADITIONAL METHOD

The traditional tuning method is to match the specific frequency peaks that aimed at largely eliminating the "beat" (pitch differences from two notes; for example, "A3's" second overtone matches its octave "A4", which is denoted to be 2:1). Then, use a smooth curve to optimize/minimize all the differences to achieve relatively good result.

Since the piano overtone shift (inharmonicity) has a very nice relation, it enables us to just sample very few keys and guess all the properties for all piano; then, get the tuning strategy.

3.1.1 Sampling Piano

Before tuning a piano, we need to sample a piano by recording few piano keys sound audios. This process will roughly or precisely measure the inharmonicity of piano strings (which will talk about later), such that we could model the inharmonicity for the targeted piano.

The sampling is suggested to measure keys "C1", "C2", "C3", "C4", "C5" (and probably "C6"; user could record more piano keys such as "A1" ~ "A6" for better result). Since the tuning inharmonicity curve is a smooth curve and predictable, thus it is possible to sample fewer notes. The piano key sound should be recorded in a quiet environment, which allows more accuracy for later frequency analysis. In this sampling process, we need to press the key hard in order to get higher harmonic peaks for measurement.

In my program, I use fully or almost fully sampled piano for research purposes.

3.1.2 Audio Processing

Since the real audio may contain the white space at the start or the end, and the sound length varies. I use this method to process my sampled audio:

- Normalize (N(x) = x / max(x)) the audio file into 1, then, find the peak volume of audio, and start from here.
- Slice these audio pieces into tiny partitions, say 0.1 second is one partition. The maximum number of each partition will be its assumed volume at this time point.
- Trim the audio at the volume start from some large number to small number since piano sound is loud from its beginning and decay by the time. Say from 90% to 2% of the sampled sound audio.



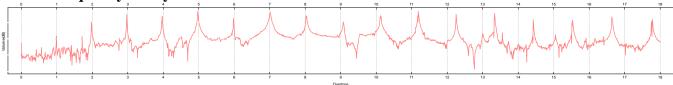


Figure 3-1 "A#0" Key (at Upright Piano Samples) Overtone Plot; Volume at Logarithm Scale

Then, put this audio samples into fourier analysis (FFT algorithm). Then we get the function $G_k(f) = \|FFT(S_k(t))\|_2$ where $S_k(t)$ is the audio function, and $G_k(f)$ is the frequency domain function, k is

piano key number, f is the frequency variable, $\|\cdot\|_2$ is the 2-norm of complex numbers. In our work, the frequency domain is converted to the ratio to its ideal fundamental frequency, thus we can see the Figure 3-1, the peaks will always almost lies in the grid by dividing its ideal frequency.

From Figure 3-1, we can see that the higher overtone (right hand side peaks with larger numbers) shifts higher.

It is a problem to capture all these peaks numbers, since some are not clear: the fundamental frequency (at 1), and some has multiple peaks: at $15 \sim 16$.

In my work, I use the frequency Catchup Method to get octave values for all these peaks.

3.1.4 Catchup Overtone

From the charactors of these peaks, there are several charactors will be considered:

- From left to right, the gap between two peaks are increasing gradually.
- The largest value of this plot is probably some peak of overtone
- The valid peak should be nearly larger than fundamental frequency position: at 1.
- The peak may be broken into several peaks, we need centralize the targeted position.

From this charactoristics, the Catchup Method could be built:

- Analyze the frequency samples which roughly larger than 1 (my program is starting from 0.8), get the peak frequency $f_{k,peak}$ at key number k, and overtone number peak.
- Comparing with ideal frequency \tilde{f}_k . We can then assume that it is $n = \text{round}\left(f_{k,peak} / \tilde{f}_k\right)$ harmonics. Then, we can know its guessed fundamental frequency is $\hat{f}_k = f_{k,peak} / n$. Then, this should be the step size for catchup method.
- The catchup method is forward (goes to the right), and the backward (goes to the left). If we are in the forward operation, the next guessed target frequency is $\hat{f}_{k,peak+1} = f_{k,peak} + f'_k$, where f'_k is the assumed gap between two peak at this position. In the first try, we set this number to $f'_k = \hat{f}_k$, and this number will be increasing for more right harmonics. Then, we get the around data (in a relatively small area) for guessed target frequency $\hat{f}_{k,peak+1} \pm \delta$. We can find its maximum number these data to be the frequency candidate $\hat{f}_{k,peak+1}^{candidate}$, then we get the data of smaller surround area $\hat{f}_{k,peak+1}^{candidate} \pm \delta'$ where $\delta' << \delta$. Then, we calculate the weighted average for this smaller area, and the result is the actual frequency of this peak $f_{k,peak+1} = \int_{\hat{f}-\delta'}^{\hat{f}+\delta'} \omega \cdot G(\omega) d\omega$, where ω is proportional to frequency. Then, the assumed gap between two peak at this step is updated to be $f'_k = f_{k,peak+1} f_{k,peak}$.
- Iterate this method for forward catchup to get all higher frequencies.
- If the highest peak is not fundamental frequency, we will perform the backward catchup. Since there are less peaks and the overtone shift will be far less than the right, the assumed targeted gap between two peaks is set to be the assumed fundamental frequency \hat{f}_k .

From this method, we can get a overtone (frequency) list for the key k. Which is:

$$k \to \left\{ f_{k,1}, f_{k,2}, \dots \right\} \tag{3.1}$$

3.1.5 Inharmonicity Model

From Figure 3-1, we can see that the overtone will shift higher and higher as the frequency goes higher. This effect is caused by the stiffness of an object, its natural frequency will follow a certain pattern.

From reference [1], we assume that the piano string is a bar with two fixed ends, which approximately follows the partial differential eqution:

$$\ddot{y} \propto -y'' - \varepsilon y'''' \tag{3.2}$$

Where y is the special position of piano string (bar model). The prime is the derivative to spatial domain, and dots is the derivative to time domain.

Then, use the modal analysis and solved the natural frequencies for this string are:

$$f_{k,n} \propto n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2} \Rightarrow f_{k,n} = A_k \cdot n \cdot f_{k,1} \sqrt{1 + B_k \cdot n^2}$$
(3.3)

Here we have two unknown variables A_k and B_k .

Then, we use this function to fit all frequency results at Equation (3.1). The parameter A_k is set since not all fundamental frequency is guessing perfectly. We can ignore this number by making sure the fundamental frequency always target on 1, and focus only on B_k .

Then, we can get inharmonicity parameter list $\{\{k, B_k\}\}$.

From my observation, the logarithm of this number has some beautiful properties with the data $\{\{k, \ln(s \cdot B_k)\}\}$, where s is a scaling parameter (I set to 10000).

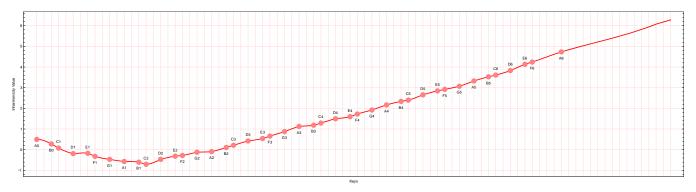


Figure 3-2 Inharmonicity Plot of Grand Piano IH(k)

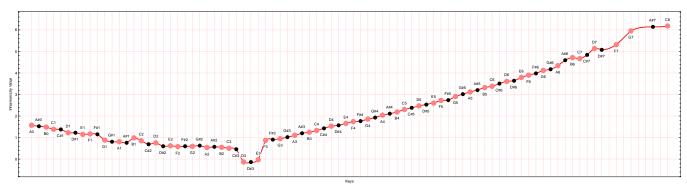


Figure 3-3 Inharmonicity Plot of Upright Piano IH(k)

From Figure 3-2 and Figure 3-3, we can clearly see the line is divided into 2 parts.

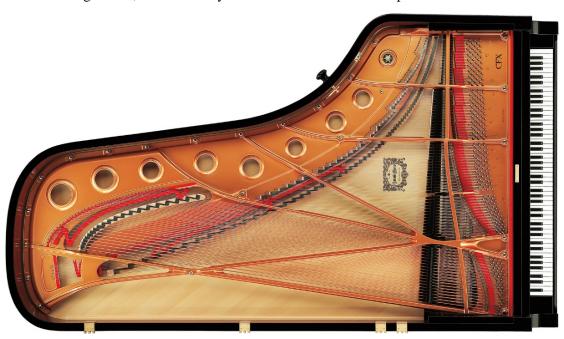


Figure 3-4 Grand Piano String Arrangement



Figure 3-5 Upright Piano String Arrangement

From Figure 3-4 and Figure 3-5, we can clearly see that the string is divided into two parts, the steel string and copper string (may be covered by silver for highly expensive pianos). The upright piano has more copper strings since the steel string cannot goes longer, and the string will become thicker to make the string vibrate slower. From spring vibration formula:

$$\omega = \sqrt{\frac{K}{m}} \tag{3.4}$$

Where ω is proportional to frequency, m is the mass of spring, K is the stiffness of spring.

When m increases, K increase a little bit, ω decreases, then frequency decrease.

Since the piano cannot growing longer, it become thick and more like a stick rather than an ideal string. For higher notes strings, it is too short, and the thickness become relatively larger comparing to its length, thus it is more likely to be a bar.

Thus, from the plot, we can see the inharmonicity increases at two ends, and break at the position of separation of two kinds of strings.

Since grand concert piano is longer, and can have more steel strings, less copper strings, thus the break will become more left side.

The figure of inharmonicity plot also tell us that two separate line are almost linear. In my model, I used the valid sampled points are modeled with interpolation function, and two edges are modeled with linear function, and it is method is shown below.

- We get several samples from one line, and fit in a linear form.
- Get its slope, and build a line which pass the right end point (since I will not wish to have a break for the interpolation function), and add some samples for edges situation to sample pool.
- Similar to the left hand side.
- We use interpolation for these samples of sample pool "left hand side + samples + right hand side", which is our final model for inharmonicity model function H(k).

$$IH(k) = \ln(s \cdot B_k) \tag{3.5}$$

Thus, we can have the modeled parameter B_k with:

$$B_k = \frac{\mathrm{e}^{\mathrm{IH}(k)}}{s} \tag{3.6}$$

Then, the frequencies $\tau(k,n)$ will be:

$$\tau(k,n) = f_{k,1} \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}}$$
(3.7)

Where $f_{k,1}$ is currently unknown but it will be eliminated, since it is in frequency ratio form. In this equation, we divide a term $\sqrt{1+B_k}$ to make sure the fundamental frequency is $f_{k,1}$.

3.1.6 Tuning Curve Optimization Model

Similar to Tunelab ®, I set the tuning optimization method to separate the lower tones (bass) and higher tones (tenor) into two tuning target optimization method, the separation point k_0 is "C#4/D4". And the default tuning method for bass is to set 6:3. Since 6/3=2 (a/b), this frequency ratio is $\gamma=a/b$, and its corresponding pitch range is $Fr_{\to c}(\gamma)$ which is 1200, and 1200 is an octave, it means the tone say "A0"s 6^{th} harmonics will largely match its octave's "A1"s 3^{rd} harmonics.

Here pitch is defined by cents.

The error function \mathcal{E}_k is defined as:

$$\varepsilon_{k} = \operatorname{Fr}_{\to c} \left(\frac{\tau(k, a)}{\tau(k + Fr_{\to c}(a/b), b)} \right) \\
= \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k} \cdot a^{2}\right) \cdot \left(1 + B_{k + Fr_{\to c}(a/b)}\right)}{\left(1 + B_{k + Fr_{\to c}(a/b)} \cdot b^{2}\right) \cdot \left(1 + B_{k}\right)} \cdot \frac{a}{b} \cdot \left(\frac{f_{k, 1}}{f_{k + Fr_{\to c}(a/b), 1}} \right) \right) \\
= \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k} \cdot a^{2}\right) \cdot \left(1 + B_{k + Fr_{\to c}(a/b)}\right)}{\left(1 + B_{k + Fr_{\to c}(a/b)} \cdot b^{2}\right) \cdot \left(1 + B_{k}\right)}} \right) \tag{3.8}$$

We can do this for all bass strings.

For tenor strings, the default tuning method is set to 4:1 (c/d). But this time we count the higher note as the target to calculate.

$$\varepsilon_{k} = \operatorname{Fr}_{\to c} \left(\sqrt{\frac{\left(1 + B_{k - Fr_{\to c}(c/d)} \cdot c^{2}\right) \cdot \left(1 + B_{k}\right)}{\left(1 + B_{k} \cdot d^{2}\right) \cdot \left(1 + B_{k - Fr_{\to c}(c/d)}\right)}} \right)$$
(3.9)

The combined expression is:

$$E(k) = \begin{cases} Fr_{\rightarrow c} \left(\sqrt{\frac{(1 + B_k \cdot a^2) \cdot (1 + B_{k+Fr_{\rightarrow c}(a/b)})}{(1 + B_{k+Fr_{\rightarrow c}(a/b)} \cdot b^2) \cdot (1 + B_k)}} \right) & k \le k_0 \\ Fr_{\rightarrow c} \left(\sqrt{\frac{(1 + B_{k-Fr_{\rightarrow c}(c/d)} \cdot c^2) \cdot (1 + B_k)}{(1 + B_k \cdot d^2) \cdot (1 + B_{k-Fr_{\rightarrow c}(c/d)})}} \right) & k > k_0 \end{cases}$$
(3.10)

From this equation, we can see E(k) is only a value for calculation at given k.

From this point, we need a function to largely eliminate these errors. The piano tuning curve C(k) is introduced, it represent the deviation of the actual tuning pitch to the ideal 12-equal temperament pitch.

The optimizer deviation function D(k) is:

$$D(k) = C(k) - E(k)$$
(3.11)

The cost function J(k) for optimization is:

$$J(k) = \sum_{k} (D(k))^{2}$$
(3.12)

Which minimize the square error of these functions.

Here I use polynomial for easier calculation:

$$C(x) = \sum_{i=1}^{n} \chi_i \cdot x^i$$
 (3.13)

Since C(x) will pass the fix point, which is "A4" pitch at 440Hz frequency at pitch deviation of 0, thus i is from 1 and $x = k - k_{A4}$, where k_{A4} is the key number (index) at "A4", which is 48.

Thus, J(k) is the second order multi-variable polynomial function, which is very easy to minimize by linear regression method to calculate the fitting parameter $\{\chi_i\}$, and rebuild the functions.

Then, we can bring $\{\chi_i\}$ to the $\mathrm{D}(k)$ function to calculate its deviations.

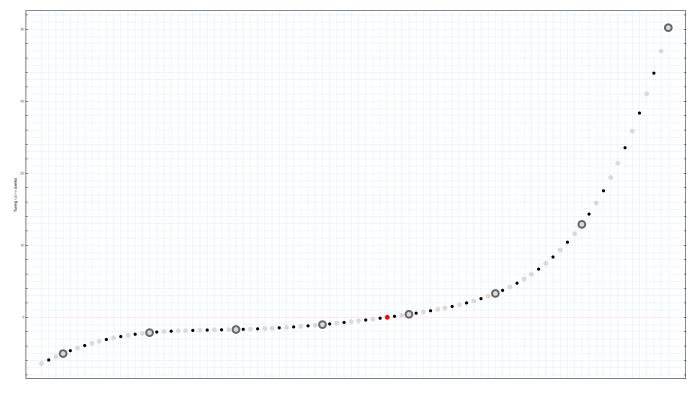


Figure 3-6 C(k) for Grand Piano



Figure 3-7 D(k) for Grand Piano

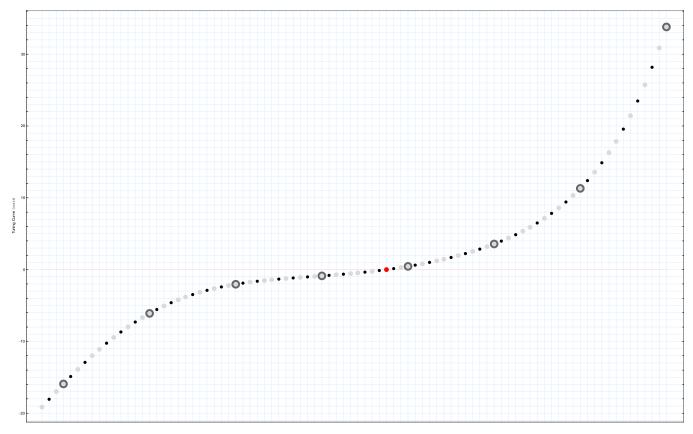


Figure 3-8 C(k) for Upright Piano

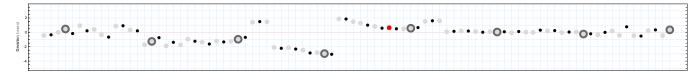


Figure 3-9 D(k) for Upright Piano

The result of two piano is shown above. Horizontal axis is the key number, and the vertical axis the pitch interval with its ideal frequencies represented by cents.

From this tuning method, we can see that the bass tuning will consider the deviations from the tenor part, and vice versa. The effect is inner related. Thus this tuning method is theoretically to optimize almost the whole piano keys tuning.

3.1.7 Temperament Model

With the development of music, various temperament appears and create unique flavor of music. The temperament model is using the pitch deviation tables of different temperament (the unit is cent). We can then create the non-12 equal temperament tuning strategy. The temperament function is defined to be T(k).

The tuning table such as "Bach - Bradley Lehman" is:

C	C #	D	D #	E	F	F#	G	G#	A	A#	В
5.87	3.91	1.96	3.91	-1.96	7.82	1.96	3.91	3.81	0	3.91	0

Table 3-1 Table for "Bach - Bradley Lehman" Temperament

Where A note will always be 0 since A is the reference frequency and will always keep to 440 Hz (if is standard situation).

This table shows the situation of "C" major.

The other major tuning will follow the rotation of table. For example: if tuning "D" major, the "D" will rotate to current "D" \rightarrow "C" place, which is rotating left 2 times. However, we will make sure "A" note will always be 0, then, we can subtract the number at "B" \rightarrow "A" to make it possible.

Then, add these pitch errors to all the notes of tuning, the modified tuning curve is:

$$C'(k) = C(k) + T(k)$$
(3.14)

3.1.8 Creating Tuning Strategy Table

The final tuning strategy $\tau(k,n)$ (unit: Hz) is:

$$f_{k,1} = F_{+c} \left(\tilde{f}_k, C'(k) \right)$$

$$\tau(k,n) = f_{k,1} \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}} f$$

$$= F_{+c} \left(\tilde{f}_k, C'(k) \right) \cdot n \cdot \sqrt{\frac{1 + B_k \cdot n^2}{1 + B_k}}$$

$$= F_{+c} \left(\tilde{f}_k, C'(k) \right) \cdot n \cdot \sqrt{\frac{s + e^{\mathrm{IH}(k)} \cdot n^2}{s + e^{\mathrm{IH}(k)}}}$$

$$(3.16)$$

From Equation (3.16), we can see only $C(\cdot)$ and $IH(\cdot)$ function is modeled function, other function are basic mathematics functions.

From the modeling, we can get a strategy of piano tuning, then we can convert this strategy into a tuning table, which shows all the frequency of fundamental and its harmonics frequencies, and corresponding deviation to ideal frequencies represented by cents.

The grand and upright piano tuning strategy is shown in Figure 7-1 and Figure 7-2.

The red font is the frequencies recommended for the devices to tune.

3.2 Entropy Tuning Method

Entropy tuning method is not to model the exact value of frequencies or pitches, it simulates the condition that simultaneously press down all piano keys, and uses entropy method as cost function to largely merge the peaks at pitch domain to create more sharp and simple sound for piano, which optimize the piano sound. The method is extremely simple, however, it is really computational intensive.

Why simulate pressing all keys? We need to know the philosophy of piano in behind. To deal with all kinds of complicated situations, let us assume several cases. Whether the chord is harmonious is to check the transient pitch domain. In other word, several notes at certain short time period will contact with each other, and we need to make sure this sound is harmonious. However, the contact cases of notes at all time for all songs are too complicated, and the key pressing level varies all the time. What if assuming that all notes has equal probability to contact, and the key pressing level when playing each small pieces of music in average is the same – some pieces are loud, some

are small but they usually approximately on the same level when playing the piano. As for the key pressing level which change the sound quality, we suggest the sample sound will be played in medium level.

3.2.1 Sampling Piano & Audio Processing

In entropy piano tuning method, sampling every piano key is necessary. Other requirement is similar to traditional method. The audio processing is also similar to traditional method.

3.2.2 Construct Spectrum

Since human ear is sensitive to the pitch ("pitch" is equivalent to the logarithm of frequency component for approximation: ignore non-linear effect of ear structures) within the hearing range (20Hz ~ 10000Hz is reasonable for optimizing algorithm). Thus, the model should be built by putting equal significance to the pitch scale. Traditionally, the pitch is represented as music note. If we evaluate the "pitch" content/data by equally sampling from the pitch scale of spectrum, it put the equal importance to the pitch scale – logarithm scale of frequencies. In my experiment, I put 0.1 cent as the precision.

Then, we have the converted the spectrum into pitch domain $I(\kappa)$, to resample the data with the key number:

$$I(\kappa) = \left\| G(f_{\kappa}) \right\|^{\beta} \Big|_{\kappa \to 12 \cdot \log_2 \left(\frac{f_{\kappa}}{\hat{f}_{[A0]}}\right), \beta \to 2}$$
(3.17)

Where for each key k we will have 1000 samples in total, each sample pitch denote as κ . Namely, each sample will represent 0.1 cent. Since the audio is also the limited samples, I use the interpolation function to resample the data.

In this model, I use the square of spectrum $\beta=2$. The reason is that: although human ear sensitive to the sound pressure level is based on logarithm of magnitude of sound, unit could be decibel (dB), however human ear also has the auditory mask, which mask small peaks around it, thus we should value more on major peaks, and ignore minor one. From the paper [1], and my trial and error, the square is actually achieve very ideal result. I also tried other numbers for β , when $\beta=1$, the sound is messy at all; $\beta=2$ is perfect; β is larger, the simpler sound will hear more harmonious, however the complicated chord may not hear well since the algorithm may value more on merging major peaks of spectrum and ignore the little ones. If people need to play more simple chord songs, they may try larger numbers of β , if need to play more messy types songs like Impressionist or Jazz, I suggest they will use smaller β . On average, 2 is great number for β .

Since for each key sound, the first peak of spectrum should start from its fundamental frequency, thus, we will set it 0 to ignore these noise.

3.2.3 Tuning with Entropy Optimizer

The tuning process from programming point of view is to move left or right of array $I(\cdot)$ as minor tuning process with +c cent shift.

$$I_{k}(\kappa - c) = \left\| G(f_{\kappa - c}) \right\|^{\beta} \tag{3.18}$$

The entropy function is defined as:

Entropy
$$(x) = -x \cdot \log(x)$$
 (3.19)

Entropy for a function is defined as:

Entropy
$$(\phi(x)) = \int_{-\infty}^{+\infty} (-\phi(x) \cdot \log(\phi(x))) dx$$

$$= \sum_{x} (-\phi(x) \cdot \log(\phi(x)))$$
(3.20)

Where $\phi(\cdot)$ is the density function:

$$1 = \int_{-\infty}^{+\infty} \phi(x) dx$$

$$= \sum_{x} \phi(x)$$
(3.21)

3.2.3.1 How to calculate entropy value for optimizer.

Since the algorithm optimize the case that all sound volume is equal, however the sampling time are different, we will make a standard case to simulate all keys are pressed in an equal key pressing level. In my program, I use density function $\overline{I}_{k}(\kappa)$ to simulate the equal key pressing level for each piano key sound in pitch domain:

$$\overline{I}_{k}(\kappa) = \frac{I_{k}(\kappa)}{\sum_{\kappa} (I_{k}(\kappa))}$$
(3.22)

When press all piano keys, the total volume $V(\kappa)$ for each key pitch shift $+c_k$ cents for tuning is:

$$V(\kappa) = \sum_{k} (\overline{I}_{k} (\kappa - c_{k}))$$
(3.23)

The density function for this function is:

$$\overline{V}(\kappa) = \frac{V(\kappa)}{\sum_{\kappa} (V(\kappa))}$$
(3.24)

Then, the cost function value J (entropy value for function $\overline{V}(\kappa)$) is:

$$J = \sum_{\kappa} \left(-\overline{V}(\kappa) \cdot \log(\overline{V}(\kappa)) \right)$$
(3.25)

3.2.3.2 Steps to calculate tuning strategy

In my program, there are several steps to dig out the good strategy for tuning.

- Step 1: Calculate the traditional tuning strategy which is simpler version of Traditional Tuning strategy, to be the initial starting point for entropy minimizer to begin. In this algorithm, no inharmonicity model is built, but just use the captured frequency to optimize.
- Step 2: Randomly change tuning for one key for c_k cents, and check its entropy value. If entropy value is smaller than last time, we keep this tuning strategy, otherwise, drop. Where the changing pitch is defined as a random number between 0 to some small number p. We will try both side of tuning by adding and subtracting the pitches. The "A4" key never change since it is standard pitch.
- Step 3: We do "step 2" experiment for all keys and all directions as one round of experiment. Each time we count the times of successfully tuning, until we cannot find a round with no improvement.

Step 4: We stop the algorithm with the test for p precision. Then we shrink the p and more accurate spectrum data (more data), and calculate "Step 2" and "Step 3"

Step 5: Calculate tuning strategy and get report.

In this process, "Step 1" is because the algorithm has many local minimums; although some local minimum can achieve similar simple and sharp harmony, it perform badly in simpler harmonies, such as an octave. A traditional tuning method can roughly optimize major overtones, the best result for entropy minimizer should be around the traditional tuning strategy.

In "Step 2", although there should be more improvement during this step, however from probability point of view, when it stops, the result is good enough for this precision. It could also use the parallel algorithm. In my program, I modeled several CPUs (not GPU program this time: GPU should calculate array sum much faster) with one shared memory to modify the result altogether. Although all CPUs will affect the overall result, however, if we can understand it will stop at the point that several CPUs could not find improvement, the effect are the same.

In "Step 4", my program uses 3 round with 1, 0.5 and 0.2 cent boundaries as step size for entropy minimizers. Since there are many local minimums, and we need to achieve a smooth tuning strategy for not creating weird music scale sound, we cannot set the step size to be really large. Thus, 1 cent boundary is a good point to start. The, next two round is accurate tuning, the accuracy will be increased to 0.1 cent, which is desirable.

In "Step 5", the frequency peaks frequencies $f_{k,n}$ are captured also by "catchup method", but without weighted average.

3.2.4 Creating Tuning Strategy Table

The method to get the frequencies components for each key sound is simple:

$$\tau'(k,n) = f_{k,n} \cdot C_{\to fr}(c_k)$$
(3.26)

However, this process is problematic. Since the whole process is based on pitch shift with certain precision, the "A4" standard frequency will not be the fix number. Here we need to eliminate this tuning error by introducing a correction factor $\varepsilon_{[A4]}$:

$$\varepsilon_{[A4]} = \frac{\tau'([A4],1)}{\tilde{f}_{[A4]}} \tag{3.27}$$

Thus, the tuning strategy $\tau(k,n)$ is modified to be:

$$\tau(k,n) = f_{k,n} \cdot C_{\rightarrow fr}(c_k) \cdot \varepsilon_{[A4]}$$
(3.28)

To build the tuning curve, the pitch deviation to the ideal frequency function C(k) is shown:

$$C(k) = \operatorname{Fr}_{\to c} \left(\frac{\tau(k, n)}{\tilde{f}_k} \right) \tag{3.29}$$

The tuning strategy is shown in Figure 7-3.

The tuning curve is shown in Figure 3-10, the spectrum of optimized result is shown in Figure 3-11:

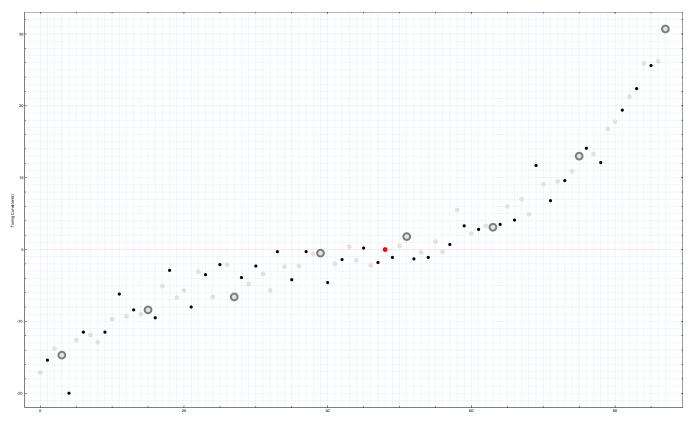


Figure 3-10 Tuning Curve for Upright Piano Optimized by Entropy Minimizer

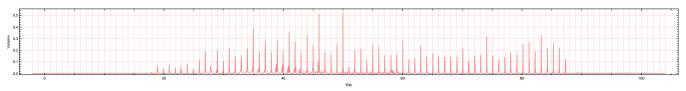


Figure 3-11 Spectrum for Optimized Result

From Figure 3-11, we could see the spectrum are largely merged. From sound quality point of view, the harmony will sound sharp and clear.

3.2.5 Tune for Songs

In the real world, some of the piano keys are not been used, especially for the simpler tonal music. Since I have mentioned the previous entropy minimizer is not quite suitable for simpler harmony music due to some of the simple harmony like octave sometimes will not sound perfect, we should ignore the keys that have not been used. Thus, I add another coefficient for the entropy minimizer.

We will put the bias $Bias_k$ that will ignore the key k which is not been used.

$$\operatorname{Bias}_{k} = \begin{cases} 1 & k \in used \\ \varepsilon_{\operatorname{Bias}} & k \notin used \end{cases}$$
 (3.30)

Where $\varepsilon_{\text{Bias}}$ is a very small number – to make sure the key which is not used could be tuned by the entropy minimizer. If the bias for one key is 0, there are no spectrum for entropy minimizer for this key, and algorithm will

stop tuning for this key. However, if we put a very small number as weight on this key, it still can tuned to a correct place – it just tuned, but does not affect the tuning for other keys.

Then, we will put the bias on the entropy minimizer algorithm and modify the Equation (3.25):

$$J = \sum_{\kappa} \left(-\operatorname{Bias}_{\kappa} \cdot \overline{V}(\kappa) \cdot \log(\overline{V}(\kappa)) \right)$$
(3.31)

Then, we use the method above to minimize this entropy function, and get the tuning strategy.

From the example of a tonal music from Mozart (Figure 3-12), we could see only the middle range and several low range keys are used.



Figure 3-12 Song Key Used Cases

The optimized spectrum is shown in Figure 3-13.

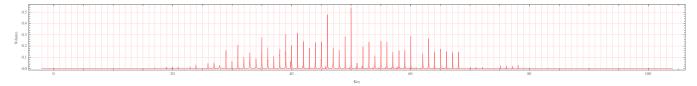


Figure 3-13 Optimized Spectrum

From this example, we can see and hear, the sound will be more optimized whenever in simple and the complicated harmonious.

4 AUDIO PROCESSING & PURE SOUND TUNER

4.1 TUNING

Tuning process for an audio is to create samples for virtual instrument so that we can hear the tuning result before tuning process to make a decision whether to adopt or drop this tuning strategy.

The sound function S(t) tunes in order to add pitch c cents:

$$S_{+c}(t) = S\left(t \cdot 2^{\left(\frac{c}{1200}\right)}\right) \tag{4.1}$$

The S(t) function is modeled as interpolation function.

4.2 SOUND PURIFY

This audio processing technique is invented by myself. It removes the inharmonic effect of piano sound.

Since the inharmonicity model has been built, it is possible to use audio processing technique to shrink the harmonics in order to remove the inharmonicity.

If the key k sound with the inharmonicity coefficient $\mathrm{IH}(k)$ and tuned to the fundamental frequency to be the frequency (ideal frequency) \tilde{f}_k ; the f_k is the fundamental frequency.

We firstly get the FFT of the audio sample with $\Gamma_k(f)$ of complex number samples:

$$\Gamma_{k}(f) = \text{FFT}(S_{k}(t)) \tag{4.2}$$

Since the FFT is creating an almost symmetry data from the middle, we can extract this data into 4 parts: the real head data $\Gamma_k^{(0)}(f)$, the imaginary head data $\Gamma_k^{(1)}(f)$, the real tail reverse data $\Gamma_k^{(2)}(f)$ and the tail imaginary reverse data $\Gamma_k^{(3)}(f)$. Four of them looks similar, however it contains all the details of the sound. Since it samples the piano keys, the spectrum is pretty obvious. At its high frequencies, it is almost 0, and it is almost out of hearing range, thus if we need to compress the frequency domain, as for higher frequencies, we could regard it to be 0. For each component we write it as $\Gamma_k^{(m)}(f)$, where m is from 0 to 3 (4 cases), i is the unit imaginary number.

$$\Gamma_{k}(f) = \left\{ \Gamma_{k}^{(0)}(f), \operatorname{rev}\left(\Gamma_{k}^{(2)}(f)\right) \right\} + \left\{ \Gamma_{k}^{(1)}(f), \operatorname{rev}\left(\Gamma_{k}^{(3)}(f)\right) \right\} \cdot i \tag{4.3}$$

From Equation (3.6) and Equation (3.7), we could get the compression functions, which is $\tau(k,n)$. Here the overtone is continuous, which is f/f_k , rather than n. Thus, we have the compressed frequency scaler \ddot{f}_k and its pitch component $\ddot{\Gamma}_k^{(m)}(f)$:

$$\ddot{f}_k = \tilde{f}_k \cdot \tau \left(k, \frac{f}{f_k} \right) \tag{4.4}$$

$$\ddot{\Gamma}_{k}^{(m)}(f) = \begin{cases}
\Gamma_{k}^{(m)}(\ddot{f}_{k}) & \ddot{f}_{k} \in defined \\
0 & \ddot{f}_{k} \notin defined
\end{cases}$$
(4.5)

Where $\Gamma_k^{(m)}(f)$ and $\ddot{\Gamma}_k^{(m)}(f)$ will be same size of samples.

Use the interpolation function to stretch, and do this for four functions; then, combine them in original way, and use inverse Fourier function to restore the audio $\ddot{S}_k(t)$.

$$\ddot{\Gamma}_{k}(f) = \left\{ \ddot{\Gamma}_{k}^{(0)}(f), \operatorname{rev}\left(\ddot{\Gamma}_{k}^{(2)}(f)\right) \right\} + \left\{ \ddot{\Gamma}_{k}^{(1)}(f), \operatorname{rev}\left(\ddot{\Gamma}_{k}^{(3)}(f)\right) \right\} \cdot i \tag{4.6}$$

$$\ddot{\mathbf{S}}_{k}(t) = \operatorname{Re}\left(\operatorname{invFFT}\left(\ddot{\Gamma}_{k}(f)\right)\right) \tag{4.7}$$

Where i is imaginary number, $invFFT(\cdot)$ is the inverse FFT, $Re(\cdot)$ is to get the real part of a number or array, $rev(\cdot)$ is the reverse of an array.

Then, do this for 2 channels and create the audio as Pure Sound Tuner result.

From this function, it needs 3 data: the audio data $S_k(t)$, the inharmonicity coefficient IH(k), and its fundamental frequency f_k (which could be captured by audio data).

5 FUTURE WORK

Over-pull tuning is implemented in some tuning apps, and I do not know its method. Since I am still lack of research on this area, I will leave it as future work to think about. I know this effect is caused by the experimental result of the percentage that the tuning pins will loosen and drop the pitch, it should have the correction coefficient for the tuner will make up the errors of this effect by over pull to tune the frequency higher than its actual one.

6 REFERENCE

- [1] Hinrichsen, Haye. "Entropy-based tuning of musical instruments." Revista brasileira de Ensino de Física 34.2 (2012): 1-8.
- [2] Github for Piano Tuning Project [https://github.com/RobertBoganKang/piano_tuning]

7 APPENDIX

March Marc	1722 442.261.0049 472.729.014 14433 467.64.1221 499.708.02 14421 252.108.1129 558.684.114 1422 553.108.1129 558.684.114 1422 553.108.1129 558.684.114 1422 553.108.1129 558.684.114 1423 568.587.100 591.412.12 1434 568.587.100 591.412.12 1434 568.587.100 591.412.12 1434 568.587.100 592.594.12 1435 662.27 197 702.871 102.871 1436 787.803.271 788.295.04 1436 787.803.271 788.295.04 1436 787.803.271 788.295.04 1437 1437.100.899.04 1438 117.100.899.04 1439 117.100.899.04 1430 117.100.899.
Dec	484.0 467.64-1/21 499.708 au 499.708 au 499.708 au 494.417-au 499.708 au
CF 10.0000 1	1420 494.417 1321 528.155 134.155
Column	1922 523.108 139 558.684 134 132 1
Description	
Def 1.11 1.15 1	4.40 586.985 + 6.77 626.843 121 4.40 521.949 - 6.80 64.175 121 4.40 621.949 - 6.80 64.175 121 4.40 621.949 - 6.80 64.175 121 4.40 627.104 - 6.80 74.254 6.80 4.40 78.339 - 7.80 74.254 6.80 4.40 78.339 - 7.80 74.254 6.80 4.40 78.339 - 7.80 74.254 6.80 4.40 78.339 - 7.80 74.254 6.80 4.40 78.339 - 7.80 74.254 6.80 4.40 92.913 - 7.20 92.654 6.80 4.40 92.913 - 7.20 92.654 6.80 4.40 1043.77 - 7.20 1114.17 - 6.40 4.40 1043.77 - 7.20 1114.17 - 6.40 4.40 1043.77 - 7.20 1114.17 - 6.40 4.40 1043.77 - 7.20 1114.17 - 6.40 4.40 1043.78 - 7.20 1114.17 - 6.40 4.40 1043.79 - 7.20 1114.17 - 6.40 4.40
Fig.	782 658.287 419 702.871 102 4-017 697.104 425 428 4-027 783.397 425 425 428 4-027 783.397 425 4-027 78
FFF 16.78 19.2 23.413 19.0 19.57 19.2 19.57 19.2 19.57 19.2 19.57 19.2 19.57 19.2 19.57 19.2 19.57 19.2	4.00 697.104 ass 744.254 ass 4.00 697.104 ass 744.254 ass 4.00 788.397 ass 744.254 ass 4.00 788.397 ass 749.254 as
German State 1	4.60 738.39 r/m 788.295 a/4 4.60 732.105 r/m 788.295 a/4 4.60 782.105 r/m 788.294 a/9 4.60 828.473 r/m 788.294 a/9 4.60 829.913 r/m 937.049 a/7 4.60 929.913 r/m 937.049 a/7 4.60 929.913 r/m 937.049 a/7 4.60 1043.77 r/m 1114.17 a/4 4.60 1043.77 r/m 1114.17 a/4 4.60 1043.78 r/m 122 1114.17 a/4 4.60 1124.378 a/7 4.60 11
GFF Section 100.87 m 100.87 m 100.87 m 100.87 m 100.88	4.20 782.105 -37 834.924 asin 4.20 824.78 -220 884.397 asin 4.20 929.913 -220 992.654 asin 4.20 929.913 -220 992.654 asin 4.20 929.913 -220 992.654 asin 4.20 1043.77 -220 1114.17 asin 4.20 1043.77 -220 1114.17 asin 4.20 1043.77 -220 1114.17 asin 4.20 1043.77 -220 1124.77 asin 4.
Aff	14-020 828.478 - 200 883.397 - 684.585 - 200 843.397 - 684.585 - 200 843.397 - 684.585 - 200 847.895 - 200 847.8
April 1.0192 11.0197	4.619 877.803 -441 937.049 674 4.629 929.913 -229 925.654 685 39.847.64 1051.11 7-324 4.629 1043.77 -221 1114.17 -444 4.620 1043.77 -221 1114.17 -444 4.620 1043.77 -221 1114.17 -444 4.620 1174.24 1252.82 1112.62 1252.82 4.620 1318.1 -162 1252.82 11252.82 11252.82 4.620 1318.1 -162 1462.65 1544 4.620 1369.7 -1629 1650.38 451 4.620 1569.7 -1
BT	4809 929.913 -229 992.654 ass 994.745 -439 1051.11 787 104.727 104.71 114.17 -434 104.81 104.89 -489 1181.7 -434 104.81 124.81 124 1407.43 124 104.81 124.81 124 1407.43 124 104.81 124.81 138.81 1422 154 104.81 168.81 168.81 1582.13 148 104.81 168.81 168.81 1582.13 148 104.81 168.81 168.81 1582.13 148 104.81 168.81 168.81 1687.38 158 104.81 168.81 1687.38 158 104.81 168.81 1687.38 158 104.81 1688.38 1687.38 1688.38 1688.38 1687.38 1688.38 1688.
C2	\$\ \text{44.77} \ \text{45.77} \ \te
DZ 13.022 Las 14.667 Las 20.046 Las 20.445 Las 36.908 Las 46.925 Las 54.018 Las 56.07 Las 56.07 Las 54.018 Las 56.07 Las	174.0 100.89 ass 1181.7 ass 1181.
DRZ	143.00 1773.42 4371 1252.82 1154 1417 1244.78 4372 1328.02 124 1418 1244.78 4372 1407.43 124 1418 1418.46 434 1582.13 151 1418 1652.86 438 1582.13 151 1418 1652.86 438 1763.36 431 1418 1763.73 444 1833.86 177 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 1833.86 173 1418 1763.73 444 183 1418 1763.73
E2 2 37474 at	441 244.78 -
Fig. 17-14 is 174.46 is 174.46 is 261.713 is 36.033 is 48.033 is 48.034 is 523.904 is 611.69 is 69.21 is 767.05 is 69.00 is 69.246 ir 1051.83 is 114.02 is 122.71 is 1051.83 is 114.02 is 127.74 is 1361.75 is 1051.83 is 114.02 is 127.74 is 1361.75 is 1051.83 is 114.02 is 127.74 is 1361.75 is 1361.74 is 1361.75 is 1361.74 is 1361.	1318.1 - 1127 1407.43 121 1407.43 121 1407.43 121 1407.43 121 1408.15 141 1407.43 121 1408.15 141 1408
F#2 \$2,4016 at 194,823 at 27,7286 at 391,823 at 58,1008 at 462,413 at 58,1008 at 194,241 at 195,814 at 27,7286 at 195,814 at 27,7286 at 195,814 at 28,114 at 195,814 at 195,814 at 27,7486 at 195,814 at 28,114 at 195,814	1987.33 - 1289 1492.15 141 1481.46 - 1481.46 - 1482.13 1452.13
CF CF CF CF CF CF CF CF	1481.46 - 1487 1582.13 - 1481.46 - 1487 1582.13 - 1481 1680.7 - 1487 1676.38 - 1576.38
G#2 (0.372) 27.7 27.745 291.865 201.259	1676.38 st.3 st.3 st.3 st.3 st.3 st.3 st.3 st.3
A2 16.24 17.2 23.2873 1.00 2.00	11.887 1663.28 13.887 1776.36 18.6 1763.73 16.47 1883.86 13.7 14.97 1870.79 17.427 1998.53 20.6 11.887 2105.45 22 2250.45.22 21.14 2233.84 24.89 237.66 237.2 2233.84 24.89 237.66 237.2 22372 2365.8 5.87 2531.94 20.6
B2 123.44 177 246.734 187 390.232 231.74 187 664.233 187.48 18	1870.79+17.42 1998.53-30 1984.47+19.55 2120.31-32 1984.47+19.55 2120.31-32 1984.77+19.57 2250.85.22 21.14 2233.84-34.48 2387.66-38 22.337 2368.58-35.87 2531.94-324 24.02 2512.16-37.89 2685.8-31.74
C3 130.865 132.2667 134.2667 134.2667 134.2667 134.267	1984.47 19557 2120.31 222 1105.45 22.7 2250.2522? 221.34 2233.84 28487 2387.66 283 22.377 2368.58 2587 2531.94 236 24.020 2512.16 27.787 2685.8 31.74
C#3 38.458 18.276.967 11.2 415.579 11.2 557.376 11.2 12.2 12.2 11.2 12.	1-18.977 2105.45-22.7 225025.227 -21.147 2233.84-24.487 2387.66-28.0 22.377 2368.58-25.877 2531.94-22.6 -24.027 2512.16-27.767 2685.8-31.74
D3 146.694 as 293.477 as 440.221 as 567.376 as 734.677 as 882.265 as 1091.69 as 1091.69 as 1274.477 as 1276.89 as 1276.84 as	-21.147 2233.84-24.487 2387.66-28.0 22.377 2368.58-25.877 2531.94-29.6 24.027 2512.16-27.767 2685.8-31.74
DH3 55.42 183 310.906 127 466.527 481 52.246 137 778.439 137 136.64 137 136.64 137 136.64 137 136.64 137 137.64 137 137.64	22.377 2368.58 -25.877 2531.94 -29.6 -24.027 2512.16 -27.787 2685.8 -31.74
E3 164.865 tas 220.466 tas 240.466 tas 240.466 tas 260.875 tas 252.476 tas 260.866 tas 240.466 tas 360.769 tas 360.769 tas 360.769 tas 360.769 tas 360.769 tas 360.875 tas	-24.027 2512.16 -27.767 2685.8 -31.74
F3 174.461 141 396.799 141 141 396.799 141 1	
Fig. 3 84.841 141 360.769 360 554.95 207 740.432 340 526.54 201 740.432 340 526.54 341.73	
GS 195.839 tax 391.861 as 580.24 as 784.616 as	
AB3 228.92 129 600.25 27 721 72 68.01 600.25 72 72 72 72 72 72 72 72 72 72 72 72 72	
AB3 228.92 129 600.25 27 721 72 68.01 600.25 72 72 72 72 72 72 72 72 72 72 72 72 72	-39.237 3196.98 -45.17 3422.41 -51.5
B3 266.784 to 407.785 say 785.437 and 988.302 and 128.254 say 1911.11 arm 1981.11 say 198.302 and 1991.24 say 1991	-44.197 3398.16 -50.757 3639.3 -57.71
Cft de 277.035 on	
C#4 277.035 car	
D4 203.526 au 687.392 au 881.94 au 177.75 au 773.05 au 80.73 au 177.75 au 773.05 au 77	
DHS 310.988 277 62.231 420 934.483 427 124 124 124 125 62.47 428 125 124 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 124 125 125 124 125 125 124 125 125 125 125 125 125 125 125 125 125	
E4 29.512 or 659.446 str 990.223 str 1322.26 str 152.26 str 1991.79 str 1991.7	
F#4 89.914 arm 740.425 arm 1198.7 arm 145.6 ar	
G44 391.988 297 784.57 297 1178.59 288 1574.69 298 1574.69 298 1573.55 297 2575.64 298 2575.40 2782.23 288 3159.37 148 3609.91 207 245.65 208 2575.40 288 258 24 249.15 249.24 249.25 258.64 298 258.34 298 258 258 258 258 258 258 258 258 258 25	
G#4 415 274 ctr 831 382 -str 1249.16 -str 1669.42 -str 269.53 -str 2749.15 -str 274	-88.037 5873.72 -98.187 6311.78 -110
A#4 440.1½ 880.988.377 1323.99.327 1769.95.377 2219.877.657 2219.877.6	+94.227 6256.34 -107.437 6727.22 -121
A## 462 4 str 933.555 2 str 1401.29 4 str 1576.32 4 str 15	
B4 4 439 962 239 989 239 989 1487.14 447 1988.96 1379 2495.99 4487 3009.48 237 350.66 244 4000.73 424 4000.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6883.87 4380.74 4000.73 424 4000.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6883.87 4380.74 4000.73 424 4000.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6883.87 4380.74 4300.73 424 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.74 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.74 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.74 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.87 4300.74 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.87 4300.74 4300.86 2487 5152.18 1322 5715.76 428 6292.66 1310 6892.77 4300.87 4300.74 4300.86 2400.87 4400.86 2400.87 4400.86 2400.87 4400.87 4400.86 2400.87 4400.86 2400.87 4	
C5 523.379 641 1048.24 2281 1576.06 6391 2108.3 1261 2 2646.4 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1981 3191.78 1982 3745.62 1982 374	
C45 564.549 cast 1110.87 cast 167.71 cast 223.681 cast 220.89 cast 388.63 cast 387.85 cast 4582.54 cast 5198.84 cast 5198.84 cast 5198.84 cast 589.0.0 cast 587.64 cast 587.65 cast 687.64 cast 5198.84 cast 5198.84 cast 549.0.0 cast 5198.84 cast 589.0.0 cast 5198.84 cast 589.0.0 cast 5198.84 cast 589.0.0 cast 5198.84 cast 5198.84 cast 589.0.0 cast 5198.84 cast 589.0.0 cast 5198.84 cast 589.0.0 cast 5198.84 cast 5198.84 cast 589.0.0 cast 5198.84 cast 5188.84 cast 589.0.0 cast 5198.84 cast 5188.84	
DF5 687.58 ±10 177.31 ±10 177.32 ±10 277.172 ±10 278.02 ±10 177.32 ±10 278.02 ±10 177.32 ±10 278.02 ±10 177.32 ±10 278.02 ±10 178.02	
55 55.07.2 1322.26 -23 190.02 1.0 1322.6 -23 190.02 1.0 132.2 1.0	
F5 099.978 137 1401:29 4.27 2110.24 4.232 2823.1 0.727 3561.03 370 4309.12 4.237 5076.34 4.607 5865.53 4.607 5865.	-203.447 10659.2 -229.897 11551.3 -257
F#5 740.633 150 1485.04 4320 2236.97 1320 3000.11 2330 3778.03 36.10 4574.22 1530 5392.02 46.00 6234.6 46.07 7104.96 112 8005.95 1820 8940.2 102.00 9910.17 100.00 10918.2 1130 1130 1130 1130 1130 1130 1130 113	+220.157 11414.9 +248.467 12383.5 +277
G5 784.779 1391 1573.85 4.87 2371.45 4.329 3181.77 43.11 4008.85 4827 4856.65 4331 5728.86 4.339 6623.1-6287 7505.72 14627 8526.87 46.22 9530.49 172.02 10574.3 1053.01 11650.8 10509 12792 6623.1-6287 1650.8 10574.3 1053.01 11650.8 10509 12792 12792 1668.11 41877 12514.55 4329 10574.3 1053.01 11650.8 10509 12792 12792 1668.11 41877 12514.55 4329 10574.3 1053.01 11650.8 10509 12792 12792 1668.11 41877 12514.55 4329 10574.3 1053.01 11650.8 10509 12792 127	
G#5 831.568 27 1668.11 17.17 2514.55 15.72 3375.71 17.54 4256.28 42.517 5160.78 40.47 6093.5 41.27 7058.51 104.55 8059.63 100.28 190.041 118.12 10184.2 192.9 11313.9 193.91 12492.4 193.91 13722	
A#5 833.723 2597 1874.29 8397 2828.47 18397 3802.85 3381 4803.82 5220 5837.44 13397 6909.45 1874.27 8025.22 128.787 9188.71 157.437 10407.5 105.447 11682.7 128.567 13019.2 128.447 14420.3 100382 15889	
B5 989.441 2347 1986.89 0327 3000.26 21.467 4037.23 07.267 5105.21 07.277 6211.23 061.217 7361.86 108.577 8563.26 130.117 9821.03 172.467 11140.3 028.277 12525.8 248.27 13981.7 026.207 15511.6 027.127	
C6 1048.51 1.327 2106.25 10.327 3182.32 23.62 4285.56 40.627 5424.44 42.337 6606.96 48.147 7840.6-117.627 9132.28 1054.87 10488.3 108.237 11914.4 224.681 13415.6 206.017 14996.7 207.237	
C#6 1111.13 -320 2232.9 -12207 3375.81 -02407 455044.30 5765.18 -02407 7030.46 -6277 8354.31 -127317 9744.52 -102207 11208.1 -001.177 12751.5 -002.177 14380.3 -08.227	
DG 1177.52 4292 2367.45 13.27 3581.99 3827 4832.92 4839 6131.44 74.47 7488.02 104.89 8912.33 138.40 10413.2 10732 11998.5 293.41 13675.3 2832 15449.8 293.427 DFG	
D#6 1247.92 4341 2510.82 1517 3803.39 12:17 5139.75 15	
F6 1401.74 - 587 2824.85 19.27 4203.62 - 9.87 5468.69 - 9.78 6966.24 - 9.88 5546.82 193.80 10223.6 197.80 12008.2 204.40 13910.8 195.17 15940.5 198.50 1401.74 - 587 2824.85 19.27 4290.16 - 9.87 5817.51 - 9.87 7425.33 195.80 19130.41 - 148.17 10947.7 195.50 12890.5 197.00 14970.1 1922.22	
F#6 1485714 2996.69 457547 4290 16 1913 27420 179196 17934 17944 17948 12905 26 1913 17949	
G6 157.78 7.79 3179.39-341 4842 7-9337 6591.92 4451.89 1451.89 1452 110589.9 2023 11059.9 2023 11050.9 20449	
G#6 1669.27 4339 3373.65 38-49 5147.04-65.89 7021.12 95.89 9024.59 148.89 1182.8 199.29 13517.4 200.69	
A6 1769.53 9387 3580.22 92.577 5471.67 61.747 7480.63 105.117 9640.07 157.857 11978.7 14521. 1284.577	
A#6 1875.92 19487 3799.82 19487 5817.71 19787 7971.96 115247 10300.2 175287 12834.8 1927.79 15603.1982.7	
B6 1988.83	
C7 2108.67 (231) 4282.08 (3) 29 6581.8 (4) 59 9063.63 (3) 20 20 11776.1 (204.35) 14759.9 (7) 2017	
- 1000 0 100 100 0	
D#7 2570.97sam 4828.86-47 337 7455.52 -97 337 10323.8-18287 13495.6 -38.37 D#7 2514.417280 5129.51 -5137 7939.62 -98.847 11027.9 -177.07 14463.8 -88.257	
271 (4.4 - 1728 - 1512.5) - 4328 / 1939.62 - 10328 - 11022 - 1728 - 14463.8 - 20328 / 1728 -	
F7 2225.57 3-10. 5792.73 20.41 9017.88 1-10.04 1	
F#7 3000.49 -2257 6158.79 -8.407 9619.76 -128.59 13506.5 -222.07	
G7 3183.18-3889 6550.54-75.29 10269.8 151.79 14481.2-34869	
G#7 3377.32 48.377 6970.39 42.27 10973.8 1482.547 15547.5 2271.647	
A7 3583.69 -1105* 7421.14-91.207 11738.7-18327	
A#7 3803.07 - 33517 7906.05 - 100 887 12573.1 - 000 887	
87 4036.34 xssr 8421.62 nszsr 13459.6 zszsr 1	
C8 4284.41 -40.227 8974.67 -120.267 14419.6 -220.517	

Figure 7-1 Tuning Table for Grand Piano

	1	2 3		4	5	6	7	8	9	10	11	12	13	14	15	16
		54.4302 -18.027 81								277.736 -17.14?			366.185 -41.58?			458.525 -71.4?
		57.7015 -16.987 86														
\sim		61.1693 -15.947 91														
0 4		64.8424 - 14.997 97 68.7389 - 13.967 10										398.702 -27.427				
- I		72.8629 -13.997 10														
		77.2388 -12.127 11														
		81.8729 -11.257 12														
	3.3745-11.17	86.7867-10.347 13	0.274 -9.097	173.875 -7.347	217.625 -5.17	261.563-2.37?	305.725 -0.857	350.147 -4.55?	394.866 -8.737	439.919-13.377	485.339 -18.477	531.162-24.037	577.422 -30.027	624.152+36.45?	671.387 -43.31?	719.159 -50.577
	15.9762 -10.257	91.9917-9.517 13	8.085 -8.287	184.296 -6.577	230.663 -4.37?	277.225 -1.687	324.02 -1.487	371.086 -5.117	418.461 -9.27	466.182 -13.76?	514.286 -18.777	562.809 -24.227	611.787 +30.117	661.254 - 36.42?	711.246 -43.15?	761.797 +50.297
		97.4972 -8.887 14														
		103.337 -8.167 15														
		109.528 -7.45? 16 116.084 -6.8? 17														
- I		123.04-6.057 18														
		130.394-5.557 19										793.782 -19.547				
		138.184-5.097 20														
		146.445 -4.577 21														
		155.188 -4.187 23														
		164.456 -3.767 24														
r		174.271 -3.47 26 184.671 -3.057 27				524.149 -1.027 555.454 -1.457										
		195.687 -2.747 29														
G#2	03.653-2882	207.358 -2.457 31	1.168-1727	415.133-0717	519 307 -0 592	623 741 -2 182	728.486 -4.067	833 593-6212	939 114 -8 852	1045 1-11 377	1151.6 -14.382	1258.66-17.632	1366.34+21.162	1474 68 -24 977	1583 73 -29 632	1693.53 -33.367
		219.716 -2.247 32										1332.38 -16.177				
A#2		232.812-2.7 34														
~~		246.683 -1.817 37				741.88 -2.477										
0 "0		261.375 -1.657 39				785.979 -2.447						1584.41 -16.097				
		276.94-1.517 41			693.378 +1.087							1678.03-15.487				
Duo		293.403 -1.547 44 310.872 -1.427 46				933.778 -0.747										
		310.872-1.427 46 329.383-1.287 49														2511.29 -15.437
		349.055-0.857 52														
F#3		369.834 -0.747 55				1113.42 +5.367										
		391.85 -0.647 58														
		415.18-0.517 62														
A // C		439.902 -0.387 66				1325.4 -7.087										
- I		466.098 -0.247 69 493.845 -0.137 74														
_ · [523.253 -0.017 78														
		554.41 -0.147 83														
D4		587.437 -0.327 88														
- 4		622.412 -0.447 93														
		659.494+0.637 99														
		698.788 +0.837 10 740.398 +0.987 11				2112.81 -14.357 2239.08 -14.847										
[784.531 +1.27 11														
044		831.291+1.427 12				2517.52 -17.777										
A4	440.Hz]	880.879 +1.737 13	23.51 -4.617	1768.77 -8.61?	2217.51 -13.737	2670.6 -19.957	3128.85 -27.257	3593.1+35.597	4064.14 -44.947	4542.76 -55.287	5029.71 -66.577	5525.74 -78.767	6031.55+91.827	6547.83 -105.71?	7075.25 -120.387	7614.43 -135.87
D 4		933.401 +2.7 14														
B4 C5		989.077 +2.37 14 1048.12 +2.687 15														
C#5		1110.67 +3.037 16														
D5		1177. +3.447 17														
D#5	22.615 -1.017	1247.24 -3.87 18	75.87 -8.447	2510.5 -14.887	3153.05 -23.17	3805.45 -33.047	4469.54 -44.64?	5147.12 -57.837	5839.94 -72.557	6549.66 -88.77	7277.87 +106.227	8026.1 -125.7	8795.78 - 144.96?	9588.29 -166.027	10404.9 -188.087	11246.8 +211.057
	559.719 -1.227	1321.72 -4.227 19	88.29 - 9.197	2661.67+16.117	3344.06 -24.927	4037.63 -35.577	4744.47 -47.997	5466.63 -62.17	6206.05 -77.817	6964.6 -95.05?	7744.08 -113.717	8546.18 -133.77	9372.5-154.917	10224.6 -177.257	11103.8 +200.627	12011.4 -224.927
F5 F#5		1400.82 -4.847 21														
~ - I		1484.38 -5.147 22														
- ·		1573.4 - 5.987 23 1667.59 - 6.637 25														
		1767.31 -7.187 26														
A		1873.19 -7.917 28														
		1985.71 -8.97 29											15057.1 -275.847			
		2104.68 -9.637 31														
		2231.37+10.837 33										15661.2 -282.31?				
D#6		2365.3 +11.747 35 2506.93 +12.427 37														
		2658.08 -13.777 40									.0000.0 *284.997					
F6		2818.59 +15.287 42														
F#6		2988.54 -16.647 45														
		3168.81 +18.047 48														
		3359.66 +19.37 50						15102.9 -221.427								
A6 A#6		3565.3 -22.147 54														
		3783.63 -25.047 57 4015.24 -27.97 61					14913.+230.697									
~-		4255.33 -28.447 64														
~		4518.63 -32.387 69														
D7	2 367.82 +13.58?	4798.2+38.317 73	51.06+72.97	10081.4-121.677	13038.+180.587											
		5083.42 -36.277 77														
_ / '		5396.27 -39.677 82														
		5735.27 +45.157 88			15818.9 -215.297											
F7		6092.43 -49.747 93														
F7 F#7		0474.00														
F7 F#7 G7	3175.03-21.447	6471.88 -54.347 10														
F7 F#7 G7 G#7	8175.03+21.44? 8367.81+23.49?	6471.88 +54.347 10 6874.91 +58.927 10 7302.41 +63.367 11	651.5+114.947	14811.8 -187.727												
F7 F#7 G7 G#7 A7	8175.03 -21.447 8367.81 -23.497 8572.7 -25.737	6874.91 +58.927 10	651.5+114.947 335.3+122.667	14811.8 -187.727												
F7 F#7 G7 G#7 A7 A#7 B7	8175.03 -21.447 8367.81 -23.497 8572.7 -25.737 8790.51 -28.187 8022.13 -90.877	6874.91 +58.927 10 7302.41 +63.367 11	651.5-114.947 335.3-122.667 056.3-129.417 799.4-132.977	14811.8 -187.727												

Figure 7-2 Tuning Table for Upright Piano

۸۸	1	2	•						•		•	12
A0	27.4413 3.77	54.6261 -11.817		109.765-3.77	137.463 -0.467	165.417+4.377		222.095 +16.417		280.055 +31.547	309.804 +41.317	339.297 +48.1
A#0	28.8409 47.577	57.6818 -17.577	86.5226-17.577	115.579 -14.357	144.635 -12.417	173.906 -8.987	204.038 +0.787	233.525 +3.297	264.088 +12.317	294.65+19.497	325.428 +28.497	356.422 +33.3
В0	30.6368 -13.7	61.2735 -13.7	91.9103-13.7	122.746 -10.197	153.98 4.037	185.213+0.077	216.845 +6.177	248.675 +12.117	280.903+19.187	313.33 +25.917	345.758 +31.47	378.981 +39.5
C1	32.4352 -14.247	64.8703 -14.247	97.4898-10.977	130.109-9.337	163.097-4.437	196.454 +2.077	229.626 +5.327	263.72+13.817	297.445+18.247	331.539 +23.77	365.633 +28.167	400.648+35.8
C#1	34,1767 -23.77	68.502-19.947	102,679-21.197	137.301-16.197	171.924-13.197	207.14-6.227	242.209 -2.327	277.723+3.387	313.385+8.827	349,494 +15.017	385,751 +20,897	422.305 +28.9
D1	36 5828 - 012	73 0243 0 000	109.748-5917	146 614 2 502	183 338 + 012	220,768+4,087	258.339 +9.37	296.052	334 189	372.184 +23.917	410 744 ===	449 304
D#1			115.984 -10.257			233.761+3.097		313.276+11.927				
E1												
F1			122.946-9.327			247.46+1.687	289.06 +3.827		373.826 +13.937		459.304 +23.027	
			130.062 -11.917			261.867 -0.357	306.225 +3.687	350.899 +8.277		440.723 +16.537		
F#1	45.9597 -10.877	91.9195-10.877	138.012-9.27	184.372 -5.867	230.731 -3.867	277.623+0.87	324.516 +4.127	371.808 +8.477	419.366+12.947	467.191 +17.57	515.282 +22.127	564.039 +28.7
G1		97.5044 -8.757	146.514-5.717	195.694 -2.687	244.703 -2.077	293.713-1.677	343.236 +1.227	392.931 +4.137	442.968 +7.737	493.005 +10.617	543.557 +14.6?	594.451 +18.9
G#1	51.5976 -10.557	103.379-7.477	154.976-8.57	206.941 -5.937	258.722 -5.637	310.687 -4.47	363.019 -1.777	415.351 +0.27	465.664 -5.767	520.199 +3.567	574.367 +10.05?	627.985+13.9
41	54.5567 -14.7	109.325 -10.657	164.093-9.547	218.861 -8.987	273.841-7.317	329.032 -5.087	384.435 -2.547	440.049 +0.27	495.874 +3.067	551.7+5.357	608.371 +9.637	665.254+13.7
۹#1	57.9676 -9.027	115.935 -9.027	174.057-7.48?	232.487 -4.427	290.609 4.427	349.039 2.897	407.623 -1.147	466.515+1.317	525.562 +3.727	585.38 +7.937	645.352+11.797	705.632+15.7
B1	61 2533 49 579	122 864	184,474-6.857	246 442 0 00	308.41-1.57	370 556 40 687	432,524 +1.517	495.027+4.017	558.423+8.727	621 641 411 997	685.573+16.46?	749.862.010
22			195.742-4.217			392.571+0.597	458.906 +4.017			658.454 +11.597		794.386 +20.8
C#2			207.043-7.037			415.034 -3.087	484.785 -1.017	554.693+1.037			766.629 49 927	838.589 +14.6
0					367.394 +1 482	440.829 41.312			664.641 410.187		815.457 a16.812	
		146.432 4.737					515.36 +4.877	589.453 +6.257				
D#2	77.3853 -8.847		232.523-6.117		387.905 -4.477	465.779-3.387	544.876 +1.297		702.336 +5.687		860.407 +9.71?	940.482+13.1
=2	82.0508-7.497	164.102 -7.497	246.583-4.47?	328.921 -3.717	411.402 -2.667	493.739 -2.457	576.794 -0.16?	660.136 +2.32?	744.052 +5.57?	827.537 +7.287	912.313+11.127	997.09+14.31
-2	86.8265 -9.557	173.957 -6.527	261.544-2.497	348.827 -1.997	436.261 -1.087	523.088 -2.497	610.979 -0.487	699.326 +2.167	785.088 -1.487	876.78 +7.357	966.04+10.187	1056.21 +14.0
-#2	91.9479 -10.337	184.156 -7.897	276.623-5.457	368.831 -5.457	461.298 4.477	554.025 3.017	647.012 -1.277	740.518+1.247	834.284 +3.747	928.57+6.77	1022.86 +9.127	1117.66 +11.9
32	97.5987.7082	195.746 -2 222	293,482-3.037	391 629 4 622	489.227-2717	587.511 -1.417	686,481 +1.247	785.862 +4.137	885.379+6.657	985,171 +9.147	1085.51 +12.05?	1186 26 415
G#2					518.283 -2.837	622.86-0.267	727.821 +2.487	832.207 +3.337	938.128 +6.837	1043.66 +8.997	1150.16 +12.27	1257.04 +15.4
42			329.643-1877		549.926.0237	659 677 0842	770.403 40.912	882 298 44 522	993.024+5297		1218.18+11.877	
ـــ 4#2		232.675 3.027			582.478 -0.877	698.658 -1.457	816.258 +1.01?	933.859 +2.857	1051.93 +5.087		1289.19+9.757	
32												
23	123.074 -5.57?				617.078-0.777	741.007+0.437	865.448 +2.317	989.89+3.727		1240.99 +8.87	1367.32+11.617	
			392.692+1.127		654.384+0.857	785.992 +2.467	917.6+3.617			1316.08 +10.57	1449.82 +13.057	
C#3		276.483 4.37?		553.278-3.397	691.363-3.987	830.072 -3.077	969.405 -1.317	1109.67 +1.48?	1249.32 +2.777		1531.1+7.487	1672.92 +10.3
23		293.308 -2.17	440.42 -0.37	587.531 +0.67	734.642+1.14?	881.753+1.497	1029.17 +2.267	1176.28 +2.397	1324.3+3.697	1472.94 +5.44?	1621.57 +6.87?	1770.51 +8.36
D#3	155.115 4.997	310.646 -2.67?	466.039-2.41?	621.57 -1.97	777.239-1.287	932.908 -0.877	1088.85 -0.14?	1245.08+0.87	1401.58 +1.877	1558.49 +3.187	1714.99 +3.847	1873.02 +5.83
≣3	164.043 8.127	328.759 4.587	493.475-3.387	658.528-1.917	823.244-1.737	988.297 -1.027	1153.69 -0.017	1319.08+0.757	1484.47+1.347	1650.53 +2.527	1811.54 -1.347	1985.02 +6.34
-3	173.983 6.287	348.892-1.667	523.8 0.137	699.171 +1.787		1050.38+4.457	1227.6+7.57	1404.82 +9.787	1583.43+13.077		1942.5+19.57	2124.35 +23.7
=#3	183 896 40 222	369 662 4 552	554 181 2592	739 323 - 552	925.713+1.367	1112.1 +3.317	1299.11 +5.527	1486.75+7.917	1675 63 052	1865.76 +14.727	2057 14 707	2249 14
33	195.775 -1.977		587.727-0.787		981.694+3.017	1179.48 +5.147	1378.08 +7.687		1778.09+13.797		2183.33 +21.837	
3#3 43	206.993 -5.57		621.475 -4.127		1038.94+1.147	1247.43 +2.11?	1457.9+5.16?		1881.34+11.527		2311.25 +20.41?	
	219.729 -2.13?		660.198+0.527			1325.12+6.717	1548.56 +9.67			2226.65 +20.857		
۱#3	232.696 -2.877	465.911 -0.937	699.127-0.297	933.122+1.487	1167.38 +2.93?	1403.71 +6.46?	1640.57 +9.527	1878.72 +13.027	2119.48 +17.88?	2360.75 +22.17	2604.63 +27.297	2850.59 +32.8
33	246.266 4.74?	493.394 -1.717	740.951 +0.37	988.94 +2.06?	1237.79+4.327	1487.93+7.337	1738.5+9.97	1992.52 +14.837	2246.1+18.317	2503.13 +23.487	2761.88 +28.787	3023.22 +34.6
24	261.469 -1.037	523.505 +0.857	786.111 +2.727	1049.28 +4.67	1313.6+7.237	1579.04+10.227	1846.19 +13.957	2115.05 +18.157	2386.18+23.057	2660.16 +28.817	2935.84 +34.527	3213.79 +40.4
C#4	276.395 4.927	553,749-1.927	831.104-0.927	1109.42 +1.08?	1389.65+4.677	1670.85 +8.057	1953.96 +12.177	2238.99 +16.737	2528.82+23.587	2816.73 +27.837	3110.4 +34.527	3405.99 +41.
04			881.823+1.837					2376.5+19.927				
)#4				1245.17+0.937		1875.71+8.297		2515.28+18.177			3500.84 +39.247	
Ξ4	310.730 -2.007		989.137+0.457					2671.13+22.287				
 -4												
-4 -#4	348.817 -2.04?		1048.42+1.227					2832.58 +23.857				
			1110.68 +1.097		1859.03+8.467	2237.58+13.687	2617.37 +18.237	3002.77 +24.87?	3396.28+34.15?	3786.67 +40.127	4187.04 +49.117	4590.52 +57.7
34 		784.275 +0.637	1178.05 +3.047	1574.2 +6.86?	1972.14+10.717	2373.64+15.887	2779.31 +22.167	3187.66 +28.317	3606.71 +38.237	4026.36 +46.377	4454.64+56.377	4885.58 +65.6
G#4	414.798 -2.11?	829.597-2.117	1246.18+0.37?	1664.53 +3.48?	2086.45 +8.267	2511.93 +13.927	2942.75 +21.097	3371.79 +25.537	3822.2+38.697	4267.26 +46.977	4719.44 +56.34?	5178.75 +66.4
44	[440.Hz]	881.137 +2.247	1324.55 +5.967	1769.1 +8.937	2219.33+15.157	2671.83 +20.78?	3131.16 +28.537	3595.04 +36.527	4069.15+47.08?	4547.8 +57.27	5035.56 +68.587	5525.58 +78.7
4#4	465.705 4.77	932.19-0.257	1401.01 +3.137	1872.18+6.987	2348.03+12.747	2828.55+19.447	3316.88 +28.287	3803.65 +34.177	4312.26+47.547	4819.3+57.597	5340.39 +70.337	5863.04 +81.3
34	493.727 -0.54?	987.974+0.377	1484.82 +3.717	1985.31 +8.557	2490.49+14.717	3000.86 +21.817	3518.52 +30.457	4039.82 +38.467	4578.81 +51.377	5122.48 +63.217	5678.64 +76.657	6244.69 +90.5
25	524 062	1048 12	1577.04+8.037	2108 74	2645 3	3189 49	3739.93 +38.17	4301 47	4872 73	5456.49 +72.577	6045 1 . 0 . 0 22	6660.09 +102
C#5		1110.06 +2.087						4556.64 +46.887			6428.56 +91.397	
))5		1176.73 +3.067						4849.95 454.887				
										6164.89 +83.897		/544.15 +117
D#5	621.43 -2.297							5142.06+56.137				
≣5	659.347 +0.257	1318.69+0.257	1986.36 +7.51?	2660.27 +15.27	3342.5+24.117	4035.12+34.497	4738.15 +45.687	5466.13+61.947	6200.36 +78.237	6963.71 +94.837	7735.37 +111.767	
-5	698.14-0.787	1400.02+3.857	2104.39 +7.45?	2821.23+16.917	3545.56 +26.217	4282.34 +37.44?	5036.58 +51.427	5817.+69.65?	6607.4+88.37	7418.99 +104.473	8262.99+125.997	
- #5	739.78 -0.48?	1481.48+1.767	2230.84 +8.467	2990.74+17.927	3762.14+28.877	4549.84 +42.34?	5351.9+58.557	6177.93 +73.867	7025.03+92.417	7900.89 +113.427	8755.66 +126.263	
35	786.154 +4.787	1576.47 +9.367	2373.74+15.957	3179.34+23.797	4003.+38.37	4840.54 +49.58?	5701.7+66.167	6590.64 +85.827	7505.97 +107.057	8437.96 +127.273	9419.96+152.881	
3#5						5133.54 +51.37			7975.5+112.097			
45								7442.7+98.317				
٠. ۱#5								7920.24+103.977		=		
35												
26						6165.35 +68.387		8453.62 +116.87	9002.12+142.537			
	1048.61 +3.487	2108.33 +12.637	3180.55 +22.497	4272.21 +35.297	5391.65 +51.877	6559.7+75.727	/761.09 +100.7	8983.3+122.017				
ン#り この								9599.43+138.857				
26						7421.36 +89.38?						
	1246.25 +2.427	2502.88 +9.627	3784.44 +23.457	5093.+39.537	6451.41+62.547	7845.13+85.527	9319.85 +116.867					
=6						8382.78+100.277						
-6					7305.6+77.87							
#6						9528.32+122.037						
36					8273.65+93.237	+122.US						
3#6												
۶#۵ ۱6					8788.12+97.677							
					9376.75+109.917							
			5750.35 +47.74?									
36	1986.02 +9.177	3972.05 +9.177	6110.85 +53.017	8310.44+87.227								
27	2108.65 +12.97	4259.78+30.25?	6498.35+59.457	8834.36 +93.067								
C#7			6870.33+55.817									
07	2204.40413.241		7344.79+71.427									
)#7												
5#1 ≣7	2004.12 +10.401		7763.77 +67.477									
			8130.43 +47.367									
-7 			8805.32 +85.417									
			9061.02+34.977									
	3175.77 +21.847											
		6726.09+21.047										
3#7												
3#7 \7	2571 F											
۱7	3571.5 +25.157											
\7 \#7	3782.77 +24.65?	7735.22+63.047										
7	3782.77 +24.657 4010.53 +25.877											

Figure 7-3 Entropy Tuning for Upright Piano