1 PROVENENCE 1

Boardwalk and Trail Bridge Span Calculations

January 21, 2025 walton@acm.org

1 Provenence

This document contains a copy of the equations in

ASD/LRFD Structural Wood Design Solved Example Problems, 2005 Edition, Problem 6, Span of a Floor Joist

This is because this document is a bit expensive and not available on the web.

Southern Pine Reference Design Values are obtained from the Southern Forest Products Association:

www.southernpine.com/wp-content/uploads/2023/09/TABLE01_L1.pdf

Acton snow load is obtained from the MA government:

https://www.mass.gov/doc/16table1604pdf/download

Reference Design Values 2

For #1 Standard Southern Pine 2"-4" dimensional width.

 F_b = (bending, C_D and $C_M[F_b]$ apply)

stringer

dimensional height F_b 2"-4" 1,500 psi 5"-6" 1,350 psi

> 1,250 psi 10" 1,050 psi 1.0

 $C_M[F_b]$

0.85

0.85

0.85

12" 1,000 psi 1.0

 $F_v = 175$ psi (shear parallel to grain, C_D and $C_M[F_v]$ apply)

 $E = 1,600,000 \text{ psi (modulus of elasticity, } C_M[E] \text{ applies)}$

 $F_{c\perp}$ = 565 psi (compression perpendicular to grain, $C_M[F_{c\perp}]$ applies)

 $C_M[F_b]$ (wet service factor) = 0.85 when $F_b > 1,150$ psi, = 1.0 when $F_b \le 1,150$ psi

 $C_M[F_v]$ (wet service factor) = 0.97

 $C_M[E]$ (wet service factor) = 0.9

 $C_M[F_{c\perp}]$ (wet service factor) = 0.67

 C_D (duration factor) = 1.6 (ten minutes); = 1.25 (seven days); = 0.9 (permanent - dead load)

 $C_t, C_L, C_F, C_{fu}, C_i, C_r, C_b = 1.0$

deflection limit = span/240 (from MA construction code)

design bearing length = 1.5 in (from boardwalk construction)

Acton snow load = 55 psf (from MA government table)

3 EQUATIONS 3

3 Equations

In the following:

w =stringer actual width in inches h =stringer actual height in inches span =stringer span in feet W =weight on stringer in pounds force per linear foot (lbf/ft)

When necessary span in inches is computed using

$$span$$
 in inches = $span$ in feet $\times \frac{12 \text{ inches}}{1 \text{ foot}}$

3.1 Momentum Capacity (Bending)

$$\begin{split} F_b' &= C_D \cdot C_M[F_b] \cdot F_b \\ S_x &= \frac{w \cdot h^2}{6} \\ M' &= S_x \cdot F_b' \text{ (allowable moment)} \\ M_{load} &= W \cdot \frac{span^2}{8} \\ M_{load} &\leq M' \end{split}$$

3.2 Shear

$$V_{load} = W \cdot \frac{span}{2}$$

$$F'_v = C_D \cdot C_M[F_v] \cdot F_v$$

$$f_v = 3 \cdot \frac{V_{load}}{2 \cdot w \cdot h}$$

$$f_v \le F'_v$$

3 EQUATIONS 4

Deflection

$$\begin{split} E' &= C_M[E] \cdot E \\ W_{defl} &= 1.5 \cdot W_{\text{dead load}} + W_{\text{live load}} \\ \Delta &= \frac{5 \cdot W_{defl} \cdot span^4}{384 \cdot E' \cdot \frac{w \cdot h^3}{12}} \quad \text{(deflection)} \\ Delta &\leq \text{deflection limit} = \frac{span}{240} \end{split}$$

Bearing Length

$$\begin{split} P_{load} &= W \cdot \frac{span}{2} \\ F'_{c\perp} &= C_M [F_{c\perp}] \cdot F_{c\perp} \\ Area_{bearing} &= \frac{P_{load}}{F'_{c\perp}} \\ Length_{bearing} &= \frac{Area_{bearing}}{w} \\ \text{design bearing length} &\geq Length_{bearing} \end{split}$$