

Power Circuit Theory - 2018 – 48572 Group Assignment

Investigation on Electrical System

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Acknowledge of contribution

For the following report, the initial plan was each member to do the following sections:

Georgios Statiris 12403616	Phi Dinh 12026530		
Report	making contribution		
Wind energy research	Introduction		
Wind farm design	Energy Demand analysis		
Wind turbines design	Location analysis of substation and power		
_	stations		
Energy output	Cost analysis		
Part2	Transmission network		

There has been a bad communication established between the students. It appears that some of the members did not manage to do their part of the assignment as initially had been discussed. As a result, the contribution of the 2 students, has clearly not been equal. Below is a detailed summary of how the workload ended up being.

Section	Completion	Georgios Statiris	Phi Dinh	
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	Pages done	All pages but 5-8	Pages 5,6,7,8	
Report making	Done	100%	No contribution	
Introduction	Done	100%	No contribution	
"Wind energy"	Done	100%	Not responsible	
"The structure"	Done	100%	No contribution	
"Energy Output"	Done	100%	No contribution	
"Transmission Network"	Done	100%	No contribution	
Part2	Done	100%	Not responsible	
Cost	-	Not responsible	-	
Location analysis	-	Not responsible	-	
Demand Analysis	-	Not responsible	-	



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Subject Coordinator: Ha Pham N.

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Assignment Title:

Investigation on Electrical System

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Declaration of Originality:

Declaration of Originality:

The work contained in this assignment, other than that specifically attributed to another source, is that of the author. It is recognised that, should this declaration be found to be false, disciplinary action could be taken and the assignments of all students involved will be given zero marks. In the statement below, I have indicated the extent to which I have collaborated with other students, whom I have named.

Statement of Collaboration:

Marks

Question 1	/10
Question 2	/5
Tatal	71.5
Total	/15

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Introduction

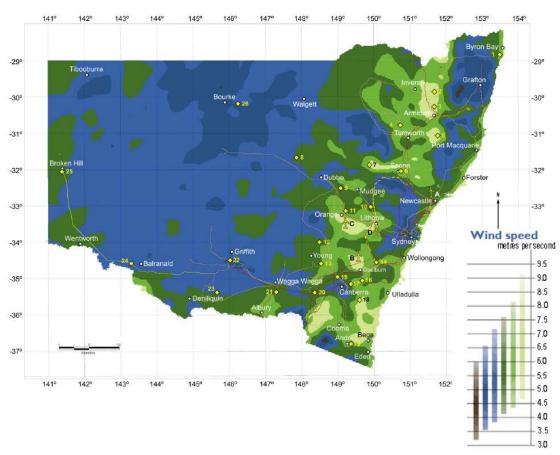


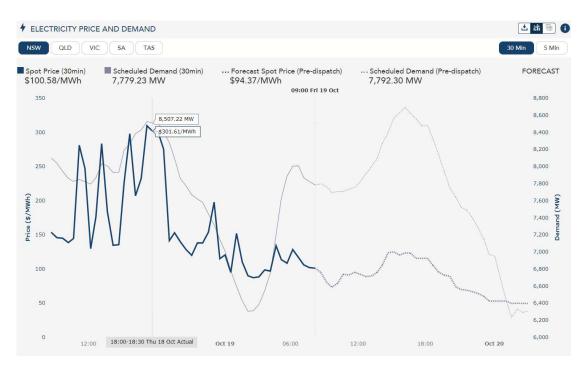
Figure 1 Wind speed intensity NSW

One of the largest generators in NSW is the Eraring Generator. Eraring produces a maximum capacity of 2,880 MW of power. With this power it supplies a quarter of NSW total power. However it generates its power by using burning coal. As a consequence it produces a biproduct of 0.92 tonnes of CO2 per KWH. Seeing as how its estimated closure is around 2032, we propose to 2 wind farm generators to replace the coal-fired generator and use that generator as a target for output generation. With the replacement with a renewable energy generator it will bring Australia one step closer to eradicating Green House gas emissions.

The proposed wind farms will be placed in 2 different locations; the first to the west of Sydney, 30Km towards the west, the other is offshore 20Km east of Sydney.

Estimated Population of Cities in	n New South Wales by June 2018		
Cities: Population (people):			
Sydney	5,640,000		
Newcastle	446,227		
Canberra	406,057		
Wollongong	215,079		
Orange	38,029		
New South Wales	7,880,000		

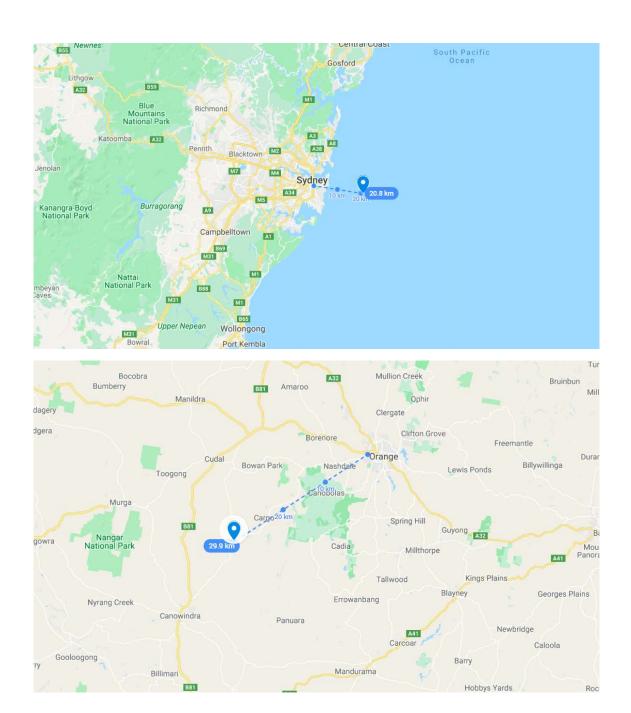
The current demand of NSW is 8500MW as the peak across the span of a day which is roughly 354MWh. Knowing Sydney takes up 70% of the population, the ratio is shown similar for energy demand and consumption.

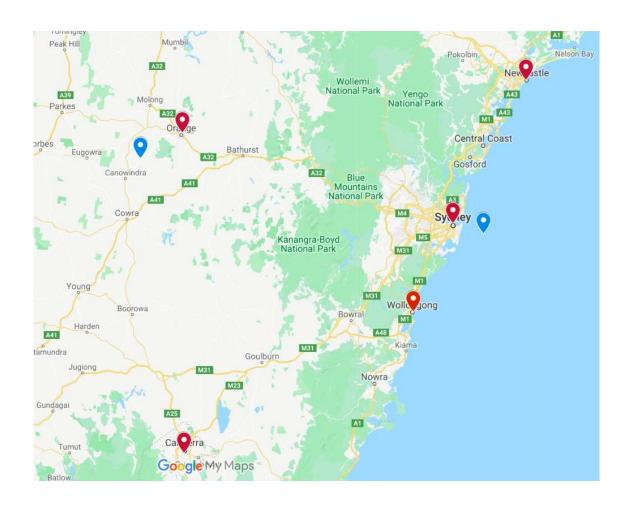


The Inland Generator will power Orange, Canberra, New Castle and Wollongong, while the offshore wind farm will solely power the Sydney bus.

Offshore Cable:

The type of cable proposed will be the submarine cables running underwater from the offshore wind farm 20Km into shore to a substation to step down the voltage. The cable has a cross sectional area of a circle. The cable itself is different to a typical overhead transmission line as the cable has all three phase lines within one cable. Furthermore, the cables are below water and does not use air to regulate the temperature within it. Therefore, it must include an optic cable to measure the temperature. To regulate the temperature, oil is used for its high boiling point. The cable also has a strong insulation to prevent magnetic and electrical leakage as well as the oil leakage. The material of the insulation is cross-linked polyethylene which allows conduction of up to 420 kV to pass through.





Wind energy is one of the most promising source of renewable energy in the world. As it will be discussed, it might be more expensive to establish the windfarm but once it is established, it is very cheap to run and produce energy.

Australia is one of the most promising countries in the world for this source, because the amount of wind is enormous in many areas.

There have already been established 29 wind farms all over Australia with the biggest capacity ones being:

•	Macarthur Wind farm	Victoria,	Capacity: 420MW
•	Snowtown Group	South Australia	Capacity: 369MW
•	Hallett Group	South Australia	Capacity: 351MW
•	Hornsdale Wind Farm	South Australia	Capacity: 316MW

^{*}It is worth mentioning that the Macarthur Wind farm is the largest wind farm in the southern hemisphere.

And 7 more being under construction, including:

•	Coopers Gap	Queensland	Capacity: 453MW
•	Sapphire Wind Farm	New South Wales	Capacity: 270MW

While many more projects have already been planned and approved, with the biggest one being the Liverpool Range windfarm project, which will consist of 267 wind turbines with a combined output of more than 1000MW.

Wind Energy

How wind turbines work

Wind flows through a turbine which then forces the rotor blades of the tower to rotate. This translates to the transformation of the kinetic energy of the wind into mechanical energy of the rotating turbine.

While the turbine rotates, it drives a shaft which drives a power generator. Through the principal of electromagnetic induction, current is generated at a lower voltage and then transformed to a higher voltage via a step-up transformer usually located on the bottom of the turbine, in order to deliver the electricity through long transmission lines to a stepdown substation and then be distributed to the consumers.

The typical modern wind turbine has an electric power output between 600 and 3000 kW (while new models are already being built that can reach even up to 9000kW)

How offshore wind turbines work

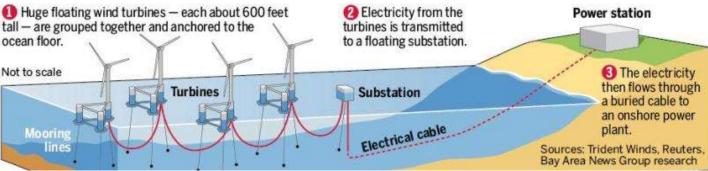


Figure 2 Offshore wind farm diagram

How onshore wind turbines work

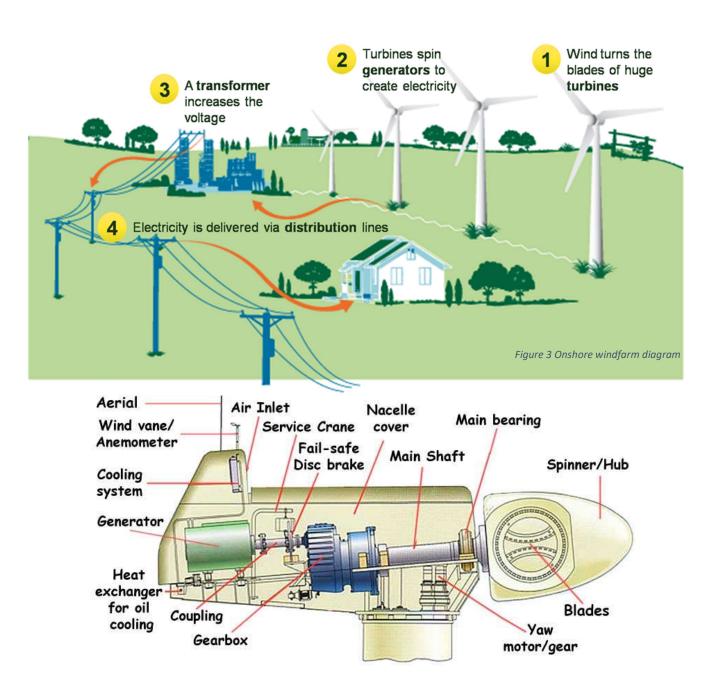


Figure 4 Main components of a wind turbine

Main components of wind turbine:

- Tower and blades
- Main shaft with mechanical gearbox
- Electrical Generator
- Cooling unit
- Sensors, control, anemometer and wind vane
- Yaw mechanism

Wind turbines usually they consist of 2 or 3 blades. They can be upwind (facing into the wind) or downwind (facing away from wind).

They can be of different type or shape, tall or short. In our wind farms we have chosen to use the typical 3 blade Horizontal Axis Wind turbines.

In terms of shape, they are mainly divided into two categories (Dylan LU 2018):

- HAWT (Horizontal-Axis Wind Turbines): they are used in both small or large systems or wind farms
 - Advantages: can be very tall, and reach high heights were the wind speed is much higher; they are very efficient
 - O Disadvantages: Complex system with high installation cost because the generator and the gearbox need to be placed on top of the tower
- VAWT (Vertical-Axis Wind Turbines): They are usually used in small system (for example on top of medium size building, like UTS Building 11 has)
 - Advantages: they are much cheaper to be built because the generator and the gearbox can be installed on the ground of the tower; they are easier to transport; they do not need yaw mechanism
 - O Disadvantages: less efficient/less energy generation because wind speed is much slower on the ground level; require more maintenance

In our design we are going to use only HAWT wind turbines with a 3-blade configuration, for both the onshore and offshore wind farm. That is because we need them to be tall and strong because both of our wind farms will be in open space with strong wind currents and space restriction will not be an issue.

Wind Turbines

Most of the wind turbines types are shown below in the diagram:

Horizontal axis turbines Horizontal axis turbines Primarily drag-type Savonius Multi-bladed Savonius Multi-bladed Savonius Multi-bladed Flates Source Primarily lift-type Double bladed Double bladed Double bladed Savonius Multi-bladed Savonius Multi-bladed Savonius Multi-bladed Savonius Multi-bladed Savonius Magnus Airfoil Combinations Combinations Combinations Others

Figure 5 Different types of wind turbines

paddles

Cross-wind Savonius Diffuser

Various concepts for horizontal axis turbines (Eldridge, 1980)

Sunlight

Various concepts for vertical axis turbines (Eldridge, 1980)

Confined Vortex

Wind Speed and Energy:

Table 1 Wind characteristics

Symbol	Symbol Discerption	
m	Mass of wind	Kg
v	Speed of wind	m/s
P	P Mechanical power of air	
ρ	ρ Air density	
A	A Area covered by the rotation of	
	the blades	
V	V Upstream wind velocity	
Vo Downstream wind velocity		m/s

Wind blade diameter: $A = \pi * r^2 = \frac{\pi}{4} * D^2$

$$\rho = \frac{P}{RT} = 1.225 \, K_T K_A$$

Where K_T and K_A are correction factors for ρ for referencing to $15^{\circ}C$ and sea level respectively

Kinetic Energy: $K.E = \frac{1}{2}m * v^2$

$$Power = \frac{1}{2}(mass\ flow\ per\ second) * v^2$$

Mass flow rate of the air = $\rho * A * \frac{V + V_o}{2}$

The mechanical power in the turbine:

$$\begin{split} P &= \frac{1}{2} \left[\rho A \, \frac{V + V_o}{2} \right] (V^2 - V_o^2) \\ \Rightarrow P &= \frac{1}{2} \rho A V^3 \left(\frac{\left(1 + \frac{V_o}{V}\right) \left(1 + \frac{V_o^2}{V^2}\right)}{2} \right) \\ \Rightarrow P &= \frac{1}{2} \rho A V^3 C_p, where \, C_p = \frac{\left(1 + \frac{V_o}{V}\right) \left(1 + \frac{V_o^2}{V^2}\right)}{2} \\ \left(\frac{P}{P_o}\right) &= \left(\frac{U}{U_o}\right)^3 = \left(\frac{H}{H_o}\right)^{3\alpha} \end{split}$$

Power, Wind speed and tower height

How height affects the wind speed and the power output

Everywhere on earth, the higher you go from the surface to the atmosphere/sky, the stronger the wind will be.

The scientific reason behind this is because the higher you are in the atmosphere the thinner the air becomes (less dense). That means that wind will need less force to be pushed on the air when it is in higher altitudes.

On the other hand, the closer you get to the ground level (earth) wind is slowed down due to the friction on the wind created by obstacles such as buildings, mountains, trees etc.

Of course, offshore wind turbines hold a strong advantages over onshore, because out in the ocean there are no obstacles and the tower can be built very high, drawing very high wind speeds.

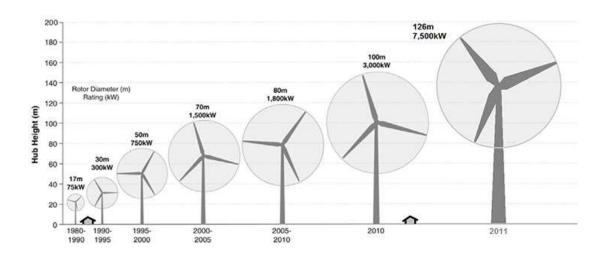


Figure 6 Wind turbines height evolution

A historical fact: The first wind turbines back in 1980s where around 17m and since then, due to news machinery and ways of construction, it has been made easier for engineers to keep increasing the height of the towers. Back in 2000 an average wind turbine was 60m tall while today, an average wind tower is around 120m tall.

It is also worth mentioning that offshore wind turbines are easier to be built higher because there are no restrictions in the logistics side of it. For example, for an onshore wind farm to be built, if the parts of the wind turbine need to go through a tunnel to reach a destination, the cannot be more than 5-6 meters wide. And that puts some restrictions on the width of the onshore wind turbines, which also restricts its height, because in order to build a very height tower, its diameter needs to be re-enforced and be wider, to withstand the weight.

To calculate the wind speed in different heights the following formula is being used:

$$V_2 = V_1 \left(\frac{h_2}{h_1}\right)^{\alpha}$$

We are then going to use this formula to calculate how much the speed of the wind will be at specific heights, to help us choose which model of wind turbine to use for our project. Results are attached below.

Where:

 V_1 is the windspeed measured at reference height 10 meters (h_1) V_2 is the windspeed at h_2

a is the ground surface friction coefficient.

Table 2 Friction Coefficient table

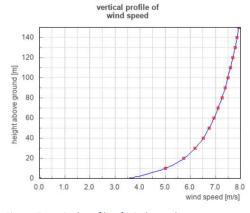


Figure 7 Vertical profile of wind speed

Terrain Characteristics	Friction Coefficient α (approx.)
Smooth hard ground, calm water	0-0.10
Tall grass on ground earth level	0.15
High crops, hedges and shrubs	0.2
Wooded countryside, many trees	0.25
Small town with trees and shrubs	0.30
Large city with tall buildings	0.40

So, for both wind farms (onshore and offshore our coefficient will be around 0) Below are attached the results we got for different values of surface friction coefficient:

Table 3 Wind speed vs height vs Friction Coefficient

roughness							
- class	0.0	0.5	1.0	1.5	2.0	3.0	4.0
- length m	0.0002	0.0024	0.03	0.055	0.1	0.4	1.6
150 m	10.52	9.89	9.03	8.78	8.5	7.75	6.78
140 m	10.46	9.83	8.96	8.70	8.42	7.66	6.67
130 m	10.4	9.77	8.88	8.62	8.33	7.56	6.56
120 m	10.34	9.69	8.8	8.53	8.24	7.45	6.44
110 m	10.27	9.62	8.70	8.43	8.14	7.34	6.31
100 m	10.20	9.53	8.6	8.33	8.03	7.22	6.17
90 m	10.12	9.44	8.49	8.21	7.91	7.08	6.01
80 m	10.03	9.33	8.37	8.08	7.77	6.92	5.84
70 m	9.92	9.21	8.23	7.93	7.62	6.75	5.64
60 m	9.8	9.07	8.06	7.76	7.44	6.55	5.41
50 m	9.66	8.91	7.87	7.56	7.22	6.31	5.14
40 m	9.49	8.71	7.63	7.31	6.96	6.02	4.8
30 m	9.26	8.45	7.33	6.99	6.63	5.64	4.37
20 m	8.95	8.09	6.9	6.54	6.16	5.11	3.77
10 m	8.41	7.47	6.16	5.77	5.35	4.21	2.73

For the windfarm to be placed into the sea(offshore: α almost 0) then it is seen that the average wind speed will increase up to 10.52 m/s (for a chosen tower of 150m high), while if the windfarm is built at an area of ground surface friction of 0.2 it will drop down to 9.89m/s (for a chosen tower of 150m high).

The structure

As already mentioned, we are going to propose the design of two wind farms, one to be onshore and the other one offshore.

We cannot use the same wind towers for both wind farms. That is because in the offshore windfarm because the maintenance is more difficult and expensive to do at the sea, the towers need to have much higher reliability and be resistant to corrosion and the more severe weather conditions that occur in the sea.

They also need to be stronger (thicker and wider) to make the most of the strong wind current in the sea.

This also is done by increasing the cut-out, which is the wind speed at which the wind turbine will shut down automatically to avoid any damage.

For our design on the land, the process of installing the towers on the ground is quite simple, quick and not as expensive as the offshore wind farm.

Type of offshore towers: Monopile

For the offshore wind farm we are going to use monopile which is the most common type of offshore wind farm foundations, for water up to 30m deep, because it is simple, cost efficient and has the least environmental impact compared to other support structures.

The tower is made up of steel pipe and will have a very large diameter (6m) and a thick wall of 150mm. (see "b" in the figure below)

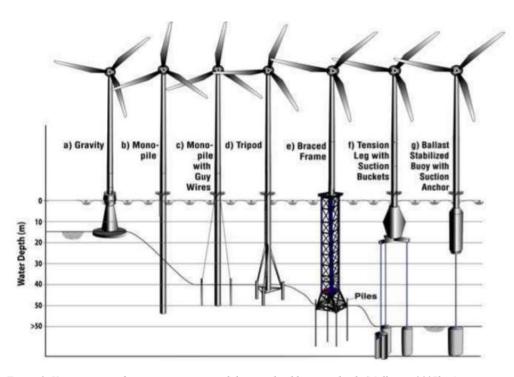


Figure 8 Various types of support structures and their applicable water depth (Malhotra, 2007b, c)

Type of onshore type: Octagonal gravity base foundation

For the installation of the onshore wind tower we are going to implement octagonal gravity base method which is one of the most common methods used for onshore wind farms. The diameter of the foundation will be 15m and the thickness 70cm on the edge and 3.0m at the center, with a total of 300 cubic meters of concrete and it will be buried to 2.5 meters beneath the ground.



Figure 9 Octagonal Base Foundation

Driven Pipe Pile

The driven pipe pile option is a very commonly used way to install the tower in either deep waters or near shore wind farms, due to its efficiency.

It basically floats the structure (i our case monopile) into the desired location and position, and then by using hydraulic hammers, the piles are driven inside the bottom of ocean. To do so, a floating crane vessel needs to be used.

The only disadvantage of using driven pipe pile would be the noise pollution in the sea waters generated by the hammers, which might disturb and impact the aquatic life for a short-time period, but it will definitely not create any long-term issues in the area. The strongest advantage though is the very short time needed to install a tower. It usually takes even less

than 24 hours to install one unit.

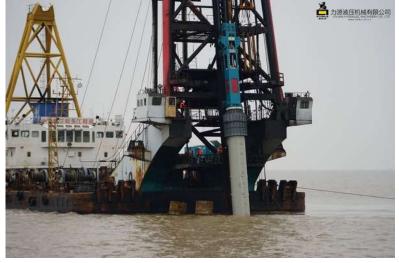


Figure 10 HHP30 hydraulic hammer hammering φ 1700mm, 82 meters long steel pipe pile

Wind turbines model selection

After doing all the research and analysis, we came to the conclusion to use these two different models. Our supplier was chosen to be Siemens, one of the leading manufacturers of wind farms in the world.

Table 4 Off Shore Wind Turbine Selection

On Shore wind tower Model Number SG 3.4-132 Nominal Power 3.465MW Hub Height 101.5 Rotor Diameter 132m Blades 64.5m fiberglass Swept Area $13,685m^2$ Power Density 253.2 W/m² Generator Type **Doubly-fed induction** machine Voltage 690 V AC Frequency 50 Hz/60Hz Protection class IP 54 0.925 CAP - 0.925 INDPower factor Yaw System Type Active Yaw bearing Externally geared Yaw drive Electric gear motors Yaw brake Passive friction brake

Table 5 On Shore wind turbine model

Off Shore wind tower				
Model Number	SWT-7.0-154			
Туре	3-bladed, horizontal axis			
Nominal Power	7.0MW			
Blades	75m fiberglass			
Rotor Diameter	154m			
Rotor tilt	6 degrees			
Swept Area	18,600m ²			
Position	upwind			
Power Density	253.2 W/m ²			
Generator				
Туре	Synchronous, PMG, direct			
	drive			
Voltage	690 V AC			
Frequency	50 Hz/60Hz			
Protection class	IP 54			
Power factor	0.925 CAP – 0.925 IND			
Y	Yaw System			
Туре	Active			
Yaw bearing	Externally geared			
Yaw drive	Electric gear motors			
Yaw brake Passive friction brake				
Operational data				
Cut-in wind speed	3 - 5 m/s			
Nominal power at	13 - 15 m/s			
Cut-out wind speed	25 m/s			
Maximum 3 s gust 70 m/s (IEC version)				

Energy Output

Wind turbines are designed to generate enormous amount of energy. Sometimes they can blow constantly at high speeds for hours generating energy. Other times they might get stuck on low speeds for hours or days. Wind turbines unfortunately only operate at a fraction of their capacity throughout the year. That is what has been named as the **Capacity factor** of a power plant and below is some information gathered for the year 2015-2016 for each state and their main source of energy (Electricity Gas Australia, 2017)

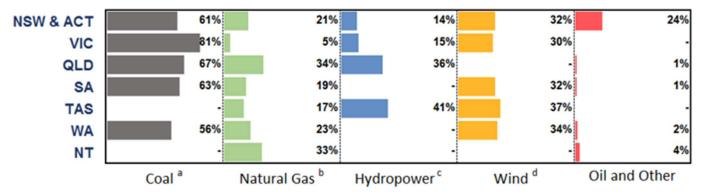
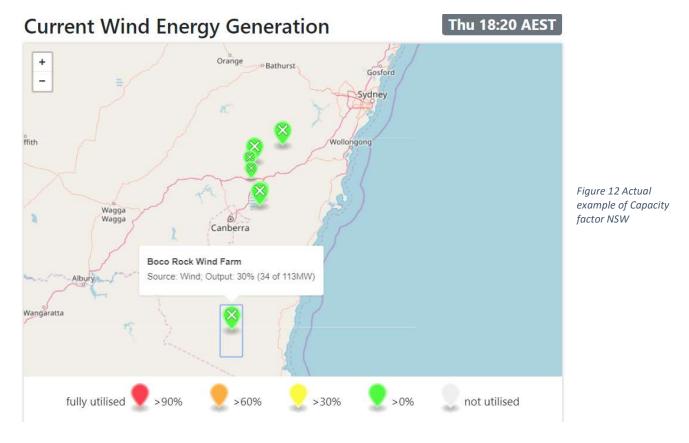


Figure 11 Capacity factor of power plants Australia

We can see that in NSW the capacity factor sits around 32%.

Below I am also attaching a live example taken on Thursday 11 October 2018 @18:20 AEST(19:20 in NSW, AEDT), and the stats are here verified, where we can see that the current wind generation at that time was at 30% of the maximum possible. (meaning that the capacity factor is 30%)



The above average of 32 capacity factor is expected to be slightly higher (near 39%) at an offshore wind farm.

We are going to design our windfarms to have a total of 35 wind turbines.

15 turbines for the Onshore windfarm and 20 Turbines for the Offshore windfarms.

Calculations for the estimated annual energy output, considering the capacity factors for each wind farm, are presented below:

Table 6 Energy Output calculation

OnShore	Offshore			
Number of wind turbines: 15	Number of wind turbines: 20			
Capacity each: 3.465MWh	Capacity each: 7.0MWh			
Total capacity Onshore: 52MWh	Total Capacity Offshore: 140MWh			
Total Capacity combined: 192MWh				
Estimated Energy generated / per year				
OnShore Expected = OffSShore Expected =				
Capacity*CapacityFactor*24(hours)*365(days)	Capacity*CapacityFactor*24(hours)*365(days)			
=52MWh*0.32*24*365=145,766MWh	=140MWh*0.39*24*365=478,296MWh			
=145.8GWh/year	=478.3GWh/year			
Combined Energy Generated per year = 145.8 + 478.3 = 624.1GWh/year				

Energy translated in household usage:

After doing some research, we found out that the average home in NSW consumes 15.7kWh per day(Ausgrid,2017).

That translates to 5,730kWh/year for an average household in NSW.

$$\frac{\textit{energy produced/year}}{\textit{average house use/year}} = \frac{624.1 * 10^9}{5.730 * 10^6} = 108.918 \, \textit{homes}$$

So, if our design successfully produces around 624.1GWh/year, that will be enough to provide electricity to 108,917 households in NSW.

Table 7 Average home energy consumption NSW (Ausgrid, 2017)

	Residential						
	Daily average (kWh		MWh	Customer Numbers			
Local Government Area	per customer per day)	General Supply	Off Peak Hot Water	Total	Off Peak	Total	
BAYSIDE*	12.9	269.303	31,193	300,496	15,897	63,900	
BURWOOD	13.2	63,531	4,236	67,766	2.342	14,058	
CANADA BAY	13.8	180.327	9.447	189,773	5.537	37,636	
CANTERBURY-BANKSTOWN*	15.6	630,841	86.489	717,330	38,166	126,201	
CENTRAL COAST*	17.1	750.526	175.870	926,396	81,922	148,370	
CESSNOCK	19.5	142,360	23,377	165,737	10,907	23,228	
CUMBERLAND**	13.6	102,561	9,804	112,365	4,208	22,634	
GEORGES RIVER*	15.2	271.564	43.852	315,416	19,890	56,750	
HORNSBY*	19.3	310,228 42,095 348,985	53,082 3,233 14,563	363,310 45,328 363,549	21,443 1,458 9,515	51,511 5,506 83,393	
HUNTERS HILL	22.6						
INNER WEST*	11.9						
KU-RING-GAI	23.3	333,938	36.749	370,687	15,723	43.562	
LAKE MACQUARIE	17.9	435.783	107,728	543,511	54,139	83,415	
LANE COVE	16.6	87,738	4,848	92,587	2.531	15,268	
MAITLAND	18.7	185,285	28,097	213,382	13,311	31,215	
MOSMAN	18.4	89,569	4,443	94,012	2,032	14,030	
MUSWELLBROOK	21.9	47,720	10.333	58,052	4,492	7,252	
NEWCASTLE	14.3	313,018	55,725	368,743	30,805	70,509	
NORTH SYDNEY	11.9	163,674	5,743	169,417	2,970	38,914	
NORTHERN BEACHES*	16.4	562,962	67,712	630,674	33,251	105,181	
PARRAMATTA**	12.7	72,016	6.022	78,038	2,627	16,818	
PORT STEPHENS	17.8	169,421	46,757	216,178	23,729	33,346	
RANDWICK	13.1	271,944	21,584	293,527	10,775	61,518	
RYDE	14.7	231,969	23,250	255,220	10,891	47,713	
SINGLETON	23.9	70,209	14,410	84,620	6,166	9,687	
STRATHFIELD	14.8	77,597	4,777	82,373	2,395	15,208	
SUTHERLAND	19.8	516,586	112,234	628,820	43,591	86,846	
SYDNEY	10.4	405,503	9,774	415,278	5,102	109,526	
UPPER HUNTER	21.9	37,246	8,141	45,386	3,551	5,673	
WAVERLEY	13.3	159,598	5,826	165,425	3,520	34,204	
WILLOUGHBY	15.5	164,958	9,290	174,248	5,092	30,747	
WOOLLAHRA	19.4	187,078	9,150	196,228	4,241	27,774	
Not assigned High voltage customer	2.	847	113	960	47	104	
Total	15.7	7.696.982	1.047.851	8.744.833	492.265	1,521,699	

Transmission Network

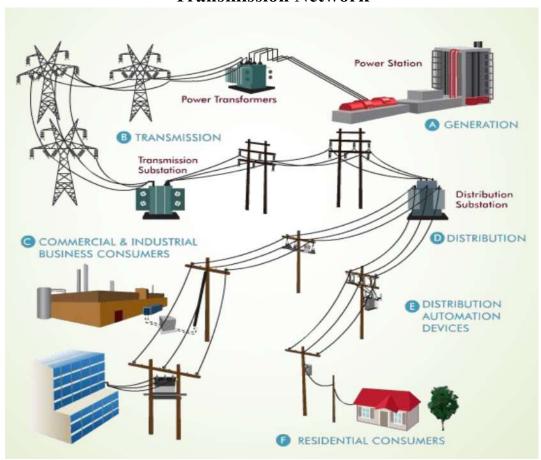


Figure 13 Transmission Network (Ha Pham 2018)

Once we have designed the power plants and the power is generated, we need to design an efficient network to distribute the electricity to the consumers, with the lowest energy loss possible.

For this to be done there are some steps:

- 1. Step up power transformers: These transformers will step up the generated voltage from 25kV to 500kV to be suitable for long distance transmission lines.
- 2. Overhead transmission lines from the power station to the substation (including towers, conductors, insulators and quad bundle conductors).
- 3. Step down transformers (transmission substation): These transformers will step down the voltage from 500kV to 330kV to be suitable for the existing distribution substation and transmission lines in the areas of Wollongong, Newcastle, Sydney, Orange and Canberra.

Substations

Substations are used to increase or decrease the voltage, for it to be transmitted. Common voltages are usually 11kV, 22kV, 33kV, 66kV, depending on the purpose of use. For example, if it is to be transmitted to a residential area it will be usually 11kV.

There are mainly 4 different types of substations:

- Step-up transmission substation
- Step-down transmission substation
- Distribution substation
- Underground distribution substation (not used in our design)

Step-up transmission substation:

Power is delivered here from the power plant and large power transformers are used to increase the voltage, for it to be delivered to long distances.

Step-down transmission substation:

They change transmission voltage to sub transmission voltage, which are then appropriate to be delivered to distribution substations. In some cases, between the process of transmission from the step-down substation to the distribution substation, power can be tapped to be used for an industrial facility or something similar.

Distribution Substation:

They are located near the end-users. Voltage is changed from transmission or sub transmission level to lower level, for them to be used by the end-users. Here in Australia, it is usually 11k/415V. It is translated as a 3-phase circuit with grounded neutral source.

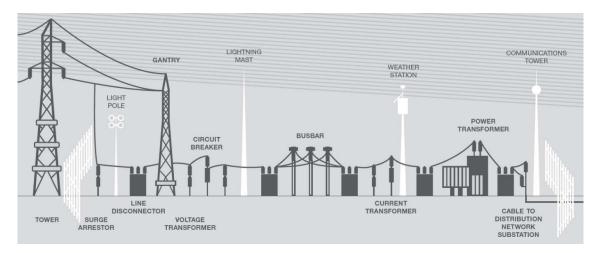


Figure 14 Distribution Substation diagram

Main components of a substation

Table 8 Main components of a Substation

Air circuit breakers

Used to interrupt the circuit when there is current flowing through them (when there is short circuit or overload)

Bus support insulators

Made from porcelain or fiberglass to prevent current leakage on the structure or the ground



Capacitor bank

Control the level of voltage by reducing or eliminating the voltage drop in the system caused by inductive reactive loads

Circuit switcher

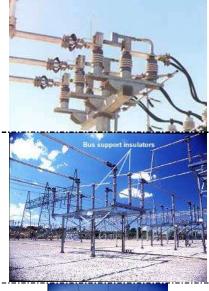
Equipment protection for transformers, lines, cables and capacitor banks. Used to energize and deenergize capacitor banks

Control house

Where the switchboard panels, the meters, relays, supervisory control etc. are.

Potential Transformers

They provide accurate voltages for reading, for the customers to by billed









Transformers	Raising or lowering the voltage	
Rectifiers	Connecting alternating current to direct	
Distribution Bus	It routes power out of the station	
Grounding Resistors	Limiting ground fault current	1000000 00000 000000 000000 0000000 00000
Lightning Arresters	Preventing damage by limiting the surge voltage due to lighting strikes or faults.	Lightning Arresters Bushings
Relays	Used to trigger the circuit breakers and other switches	

Suspension insulators Separating the line conductors



Transmission bus Leading power in the substation



^{*} All pictures were taken from OSHA(OSHA, 2002)

Transformers

Each wind turbine will have a step-up transformer to boost the generated power of the generator. These are small transformers, located either on the basement(onshore) or on the hub of the wind turbine(offshore) and they are already included with the purchase of the wind turbine.

Then, all the wind turbines are interconnected to a collector step-up transformer at the substation (Transporco, 2016). We are not going to build a new substation, but we will investigate the most appropriate use of a transformer for the distribution system.

For the transformer on the distribution end of the system, we propose to be used a Delta to Wye transformer (Δ -Y).

It can also be seen in the diagram attached below, that by using a Delta-Wye transformer, the 3-wire system is transformed to a 4-wire system. That is desirable because the end user of this distribution line will mostly be unbalanced single phase residential houses.

Having the 4th line on the receiving end, prevents overload in the phases, thus making the circuit balanced, by providing a path for the unbalanced line current to flow through (ground fault protection).

Delta-Wye transformers are capable of handling unbalanced.

In a Y-Y circuit, where there are 4 wires in each side, when there is unbalanced current in one side it can affect the other side, causing eventually damages in the circuit.

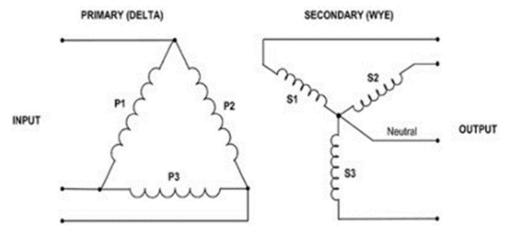


Figure 15 Delta-Wye circuit diagram

Transmission lines

Transmission lines are used to transmit the electricity that has been generated from the power plant to the substations and then to the consumers. In the process of designing them, the following considerations must be made:

- Distances between towers
- Configuration of towers
- Conductors arrangements
- Materials used
- Capacitance and inductance of the transmission lines
- What bundle type will be used

Conductor arrangement on the tower

Power lines and tower can have many different type of structures or material. They are usually made of steel or aluminum (lattice or tubular poles), concrete and sometimes from wood.



Figure 17 Double circuit Conductor arrangement

The material and the structure of the tower depends on the voltage level, the weather conditions of the area (if its extreme conditions then stronger materials need to be used), the space availability, carrying weights and more. We are going to use Double Circuit overhead powerlines with each side supporting and insulating 6 conductors.

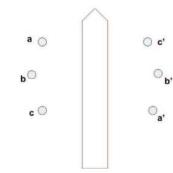


Figure 16 Double circuit arrangement (PCT Spring 2018 Lecture slides)

Conductors

Due to its attractive cost/efficiency ratio, we are using Aluminium Conductor Steel Reinforced(ACSR) conductors for our design, which are commonly used in high voltage transmission lines due to their durability and efficiency.

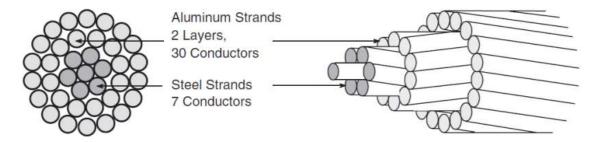


Figure 18 PCT Spring 2018 Lecture 3 slides

ACSR are cheaper and the weight less than copper conductors. "Aluminum possesses a conductivity-to-weight ratio twice that of copper and its strength-to-weight ratio is 30% greater than copper." (F. Ridley Thrash, 2017). They also have a bigger diameter, which helps reduce corona effect, minimizing the power loss.

For our design of the transmission lines we are choosing to use the following conductor supplied from Prysmian with:

- cross sectional area of 2000mm or 2500mm
- Maximum DC-resistance at 20°C 0.0149 Ω /km and 0.0127 Ω /km respectively

Sample constructions		550kV cables 290/500kV					
Rated voltage U _V /U = 290/3 U _m = 550 k U _p = 1550	00 kV V			Single o	ore, XL oltage p		
Nominal cross	-sectional area of conduct	or		mm ³	1600	2000	2500
Construct	ional data						
Outer diamete		duminium conductor		mm	131	142 142	147 147
Net weight with Pb sheat	ht With aluminium conductor			kg/m kg/m	32.1 40.5	34.1 45.2	36.2 51.2
	ding radius during cable lay			m	1.4	3.6	3.7
Electrical	properties at 66kV	and 50 Hz					
Aluminium	Max. DC-resistance	at 20°C		Ω/km	0.0186	0.0149	0.0127
conductor	AC resistance	at 90°C, ag	oprox.	Ω/km	0.0242	0.0195	0.0168
Copper	Max. DC-resistance	at 20°C		Ω/km	0.0113	0.0090	0.0072
conductor	AC resistance	at 90°C, ag	oprax.	Ω/km	0.0158	0.0132	0.0113
DC-resistance	of metallic sheath at 2010			Ω/km	0.184	0.185	0.187
Reactance	Metallic sheath closed	Trefoil	touching	Ω/km	0.119	0.115	0.111
(approx.)		Flat	0.15m	Ω/km	0.136	0.130	0.124
	770000000000000000000000000000000000000	Flat	0.30m	Ω/km	0.162	0.157	0,151
	Metallic sheath open	Flat	0.15m	Ω/km	0.143	0.136	0.130
		Flat	0.30m	Ω/km	0.187	0.179	0,173
	- Albanda -	Flat	0.45m	Ω/km	0.212	0.205	0.199
Operating cag				μF/km	0.18	0.19	0.21
Charging curre	ent.			A/km	16.5	17.7	18.9

Figure 19 Conductor Specifications

In our design we are also including spacers, which are used to establish the distance between the conductors, to prevent any damage from potential high movement.



Figure 20 Transmission lines Spacers

Capacitance and Inductance

When handling power and transmitting it in large distances, there is always power lose. All transmission lines exhibit the electrical properties of conductance, resistance, inductance and capacitance. The last two are an effect of Electromagnetic fields around the conductor. Inductance is based on the induced voltage in the circuit due to the of flux, a result of change in current, while conductance appears due to the potential difference between the transmission line conductors (Saadat, 1999).

To design a transmission line model, these parameters are essential, and even though values are small, they add up in long distances.

To calculate the inductance and capacitance, we first have to calculate the Geometrical Mean Distance (GMD) and Radius (GMR) where by definition and from Lecture 3,4 notes, for a Quad bundle conductor double circuit, we have:

$$GMR = \sqrt[n^2]{(D_{11}D_{12}D_{13} \dots D_{1n}) \dots (D_{n1'}D_{n2'} \dots D_{nm})}$$

$$D_{s-bundle} = 1.09\sqrt[4]{D_s d^3}$$

$$D_s = r' = re^{-\frac{1}{4}}$$

$$r = 0.028, d = 0.3$$

$$D_{s-bundle} = 1.09\sqrt[4]{0.028 * 0.3^3} = 0.181m$$

$$GMD = \sqrt[mn]{(D_{11'}, D_{12'} \dots D_{1m}) \dots (D_{n1'}D_{n2'} \dots D_{nm})}$$

 $\Rightarrow GMD = \sqrt[3]{D_{AB}D_{BC}D_{AC}}$
Where:

$$D_{AB} = \sqrt[4]{D_{ab}D_{ab}, D_{a'b}D_{a'b'}}$$

$$D_{BC} = \sqrt[4]{D_{bc}D_{bc'}D_{b'c}D_{b'c'}}$$

$$D_{AC} = \sqrt[4]{D_{ac}D_{ac'}D_{a'c}D_{a'c'}}$$

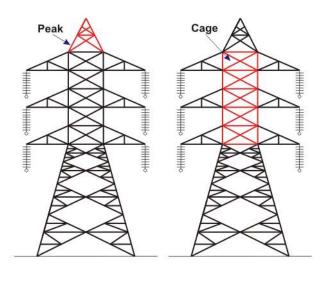
$$L_p = 2 \times 10^{-7} \ln \left(\frac{GMD}{GMR} \right)$$
$$C_n = \frac{2\pi\epsilon_0}{\ln \left(\frac{GMD}{r} \right)}$$

For a quad bundle conductor, the resistance is simple calculated by adding each resistance in parallel (PCT spring 2018 lecture 3 slides):

$$R_{eq} = \frac{1}{\frac{1}{R} + \frac{1}{R} + \frac{1}{R} + \frac{1}{R}} \xrightarrow{R = 0.0149} R_{eq} = 3.725 * 10^{-3} \Omega/km$$

Transmission towers

Transmission tower are large steel structures used to carry high voltage powerlines. They required to be strong and high when in long distances (>250km) but also for medium



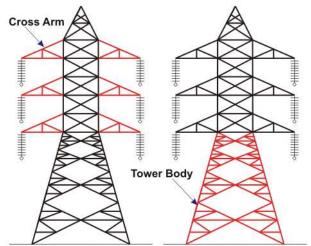


Figure 21 Main components of transmission towers

transmission lines 80-250 km, because they need to withstand the heavy weight, the conductors and the insulators high above the ground (30-60m). The also serve the purpose of keeping the lines as far away as possible from contact with surrounding, to eliminate any risks or incidents. The higher you go above ground level, the stronger the wind speed is and that is why

The higher you go above ground level, the stronger the wind speed is and that is why towers need to be carefully engineered to sustain any severe weather conditions.

Lighting strike protection:

We are including in our design a protection against lightings striking direct to the phase conductors. That is done by adding an earth wire (shield wire) on top of the structure (on the peak of the tower as seen in the figure). The conductors are kept within 30° angle below earth wire. In case of a lightning strike, the lighting is more likely to hit the earth and discharge there without causing any damages.

We are using the same transmission tower as the existing ones on the current grid of NSW provided by Transgrid, with a separation distance of 450m between the peak each tower.

Distribution towers

In our design we are using the existing distribution system. The distribution system in NSW is mainly divided into 3 categories:

- The primary consumers, that need the electricity for commercial use and the voltage varies from 4-35 kV
- The secondary consumers that is a typical Australian home with 415V supply
- And as already mentioned in the section of substations, the sub transmission system, that is used to supply sub-stations, usually of 33kV, 66kV or 132kV

All these distribution lines are usually made of wood or concrete.

Most commonly used distribution lines are found below (SA GOV, 2017):

415V distribution lines

Number of conductors: 4

Type and number of insulators: small pin

insulators

Height: usually 6-7m



Figure 23 415V power line with 4 conductors



Figure 22 415V insulator

11kV lines

They are usually mounted above 415V lines (as seen in the picture)

Number of conductors: 3 bare

Type and number of insulators: single disc insulator or pin insulator made of 3 discs

Height: usually 8-9m



Figure 25 11kV power like mouned on top of 415V



Figure 24 11kV insulator

33kV lines

Number of conductors: 3 bare wires Type and number of insulators: 3-disc insulators or pin insulators made of 3 discs Height: 10-20m



Figure 27 33kV powerline with



Figure 26 Glass disc insulator on 33kV powerline

66kV lines

Number of conductors: 3 bare active wires Type and number of insulators: 5or 6 discs insulators or a post insulator made of 12 small discs

Height: 10-20m



Figure 28

stack of discs



Figure 29 Disc insulators

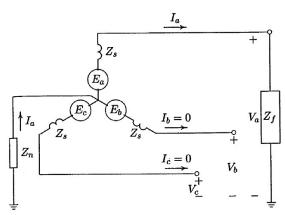
PART 2

Analyse all types of possible bolted faults (symmetrical and unsymmetrical) which may occur at Sydney bus. Discuss how to protect against those faults.

Unsymmetrical faults are the ones that lead to unequal currents and phase shifts in a 3-phase circuit and they occur when there is an open or short circuit of a line in the system. Some unsymmetrical faults that can possibly occur at the Sydney bus are listed below. When $Z_f=0$ then we have a direct short circuit, which is called bolted fault (Grainger, 1994).

Types of possible bolted faults

Single line-to-ground fault:



This is the most common type of fault. It usually happens due to a lighting or when conductor drops or makes conduct with grounded structures (Grainger, 1994).

The fault current can be found as:

$$I_f = I_a = 3I_a^0 = \frac{3E_a}{Z^0 + Z^1 + Z^2 + 3Z_f}$$

*methodogy and calculations can be found in Grainger textbook

Figure 31 Single line-to-ground fault (Saadat 1999)

Below is the connection of the Thevenin equivalents of the sequence networks to simulate a single line-to-ground fault on phase α at bus k of the system. Once the currents are known, the components of voltages at all other buses of the system can be determined from the bus impedance matrices of the sequence networks.

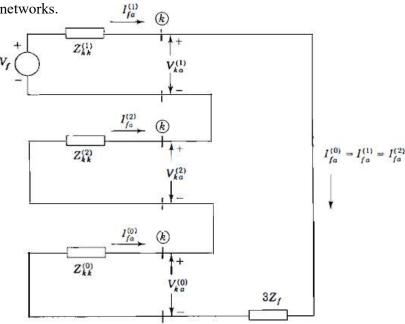


Figure 32 Sequence network for Single line-to-ground fault (Grainger, 1994)

Line-to-Line faults:

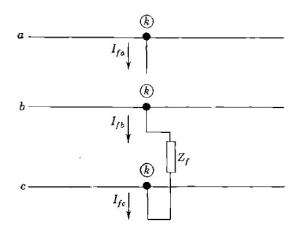


Figure 33 Line-to-Line fault (Grainger, 1994)

Double Line-to-Line fault is when two lines are short circuited. This type of fault happens 5-15% of the time.

In this example, bus k is the fault point and the line-to-line fault is on phased b and c. Assuming that the generator is initially at no load:

$$I_{fb} = -I_{fc}$$

$$V_{kb} - V_{kc} = I_{fb}Z_{f}$$

$$Z_{f} = 0$$

$$Z_{g}$$

$$I_{a} = 0$$

$$Z_{g}$$

$$Z_{g}$$

$$I_{b}$$

$$Z_{g}$$

$$I_{c}$$

$$I$$

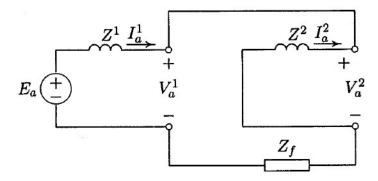


Figure 35 Sequence network connection for line-to-line (Saadat, 1999)

The fault current is found to be

(Saadat, 1999)

$$I_b = (a^2 - a)I_a^1$$

$$\Rightarrow I_b = -j\sqrt{3}I_a^1$$

*methodogy and calculations can be found in Grainger textbook

Substituting for symmetrical components of currents, the symmetrical components of voltages and phase voltages at the fault point are obtained.

Double Line-to-Ground faults:

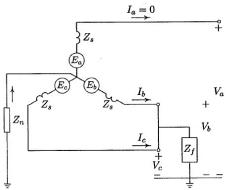
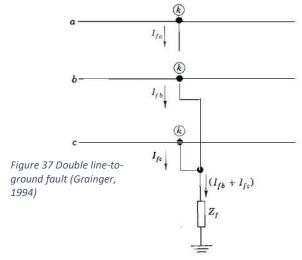


Figure 36 Double Line-to-Ground fault (Saadat, 1999)

This fault occurs when two lines are short circuited, and they come in contact with the ground.

This type of fault occurs around 20-25% of the time.



The characterizing equations of the double line-toground fault are satisfied when all three of the sequence networks are connected in parallel: *methodology and calculations can be found in Grainger textbook

$$I_{fa}^{(2)} = -I_{fa}^{(1)} \left[\frac{Z_{kk}^{(0)} + 3Z_{f}}{Z_{kk}^{(2)} + Z_{kk}^{(0)} + 3Z_{f}} \right] \Rightarrow I_{f} = 3I_{a}^{0}$$

$$I_{fa}^{(0)} = -I_{fa}^{(1)} \left[\frac{Z_{kk}^{(2)}}{Z_{kk}^{(2)} + Z_{kk}^{(0)} + 3Z_{f}} \right] \underbrace{I_{fa}^{(1)}}_{V_{f}} \underbrace{I_{fa}^{(2)}}_{V_{ka}^{(1)}} \underbrace{I_{fa}^{(2)}}_{V_{ka}^{(2)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(2)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0)}}_{V_{ka}^{(0)}} \underbrace{I_{fa}^{(0$$

$$I_{fa}^{(1)} = \frac{V_f}{Z_{kk}^{(1)} + \left[\frac{Z_{kk}^{(2)} \left(Z_{kk}^{(0)} + 3Z_f \right)}{Z_{kk}^{(2)} + Z_{kk}^{(0)} + 3Z_f \right]} \right]}$$

Figure 38 Sequence network for Double line-to-ground fault

Protection Suggestion

Switch to underground distribution system

A lot of faults often happen on buses, due to severe weather conditions, such as strong winds, fires, storms but also vegetation and debris falling or blowing into lines etc.

Furthermore, medium and short transmission and distribution lines are in areas where there is high traffic activity. Many times, we have seen car accidents or trucks to come in contact or hit transmission towers or lines and cause different types of faults.

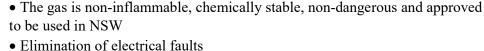
All of these faults can easily be eliminated by switching to underground transmission and distribution line system (just like it has already been done in Sydney CBD, same can also be done for other areas nears Sydney Bus)

Use SF6(Sulfur Hexafluoride) switchgear circuit breaker

Another way to avoid such fault is to use SF6 circuit breakers, which are of live tank design. Thanks to auto puffer breaking technique, they do not generate operating voltages. SF6 is an electronegative gas which has a strong tendency of absorbing the free electrons(current). The contacts of the breaker remain open in a high-pressure flow SF6 gas and an arc is struck between them. The gas captures the conducting free electrons in the arc and forms relatively immobile negative ions. This loss of conducting electrons in the arc quickly builds up enough insulation strength to extinguish the arc (StudyElectrical, 2014).

These circuit breakers are available for all voltages ranging from 144kV to 765kV and currents up to 8kA.

This type of circuit breaker can be supplied by ABB, a global leader in power. Some of the advantages of SF6 are listed below:



- Excellent insulating properties
- It is not affected by weather conditions
- It produced no noise pollution
- Easy maintenance (once in 4-10 years)
- Same gas is re-circulated in the circuit, minimizing the need of SF6

IEC outdoor gas insulated (SF6) circuit breaker OHB

Medium Voltage circuit breaker with mechanical operating mechanism designed for distribution systems up to 40.5 kV, 2500 A, 31.5 kA.

These circuit breakers are of live tank design. They are used in power distribution for control and protection of lines and for control and protection of transformers, rectifier units, capacitor banks, etc. Thanks to the autopuffer breaking technique, they do not generate operating overvoltages. This means they are also highly suitable for retrofitting, where the plant insulating materials may be sensitive to dielectric stresses.



Figure 39 SF6 circuit breaker

Why ABB?

- Maintenance-free poles
- Upper and lower terminals with NEMA4 drilling
- Gas pressure control device for each pole
- Poles made with porcelain insulators, assembled by means of flanges with terminals
- Inspection window in the pole supporting casing near the operating mechanism signals.

In the figure in the below is an illustration of how the breaker will work:

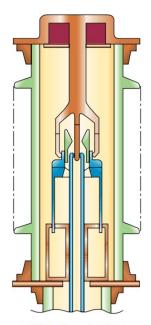


FIG. 1: Closed position

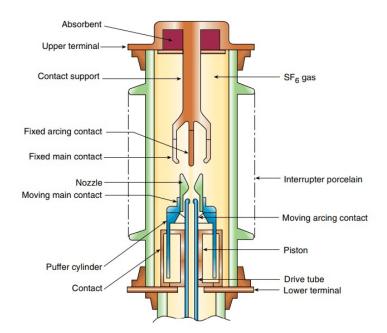
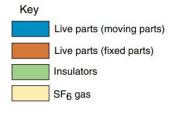


FIG. 2: Open position



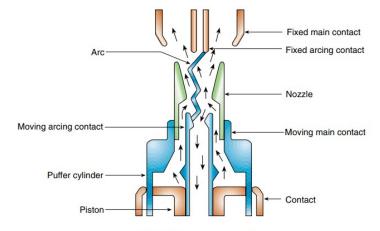


FIG. 3: Interrupting principle

Figure 40 Breaking procedure

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