

# System Dynamics and Vibrations

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## Chapter 6: Two-degree-of-freedom systems Part 1

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# Contents

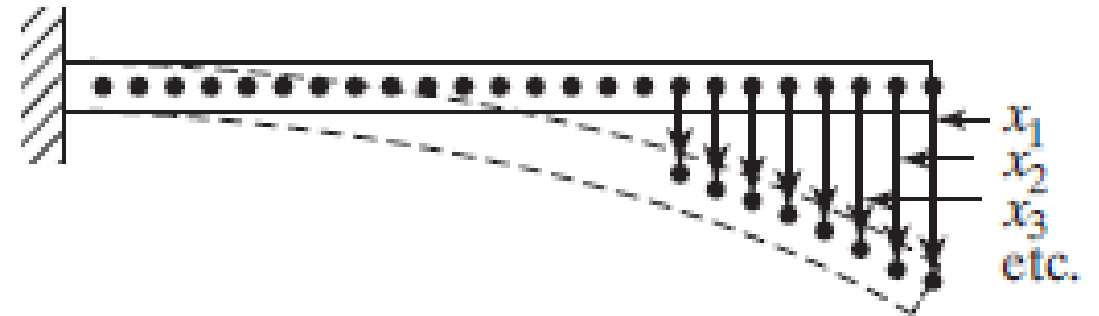
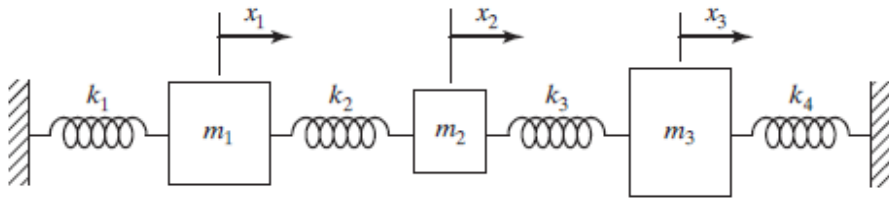
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- The equations of motion of two-degree-of-freedom systems.
- Free vibration of undamped systems. Natural modes.
- Response to initial excitations.
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- Systems admitting rigid-body motions.
- Systems with proportional damping.
- Response to harmonic excitations
- Introduction to multi-degree-of-freedom systems.

# Introduction: Modeling of mechanical systems

- Physical systems are complex → an exact description is not feasible
- In many cases is not even necessary
- Models represent only an approximation of actual physical systems
- Models retain all the essential dynamic characteristics of the system → the behaviour predicted by the model must match the observed behaviour of the actual system

# Introduction: Modeling of mechanical systems

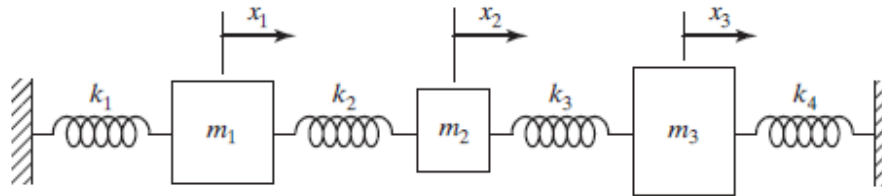
- Models of vibrating mechanical systems
  - Lumped-parameter (discrete)
  - Distributed-parameter
  - Combination of both



# Introduction: Modeling of mechanical systems

- Models of vibrating mechanical systems
  - Lumped-parameter (discrete)

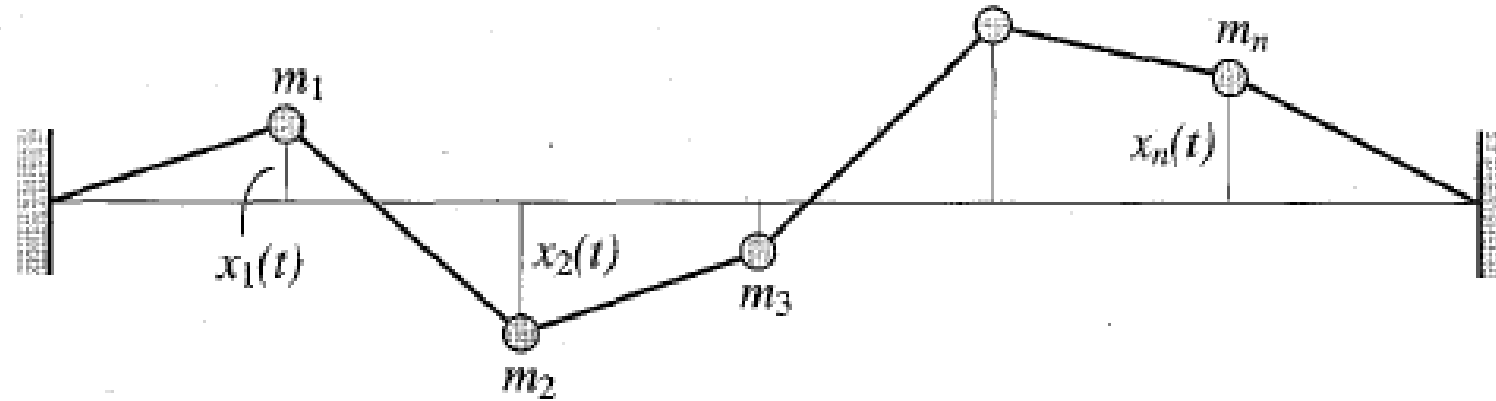
➔ choice in the number of degrees of freedom



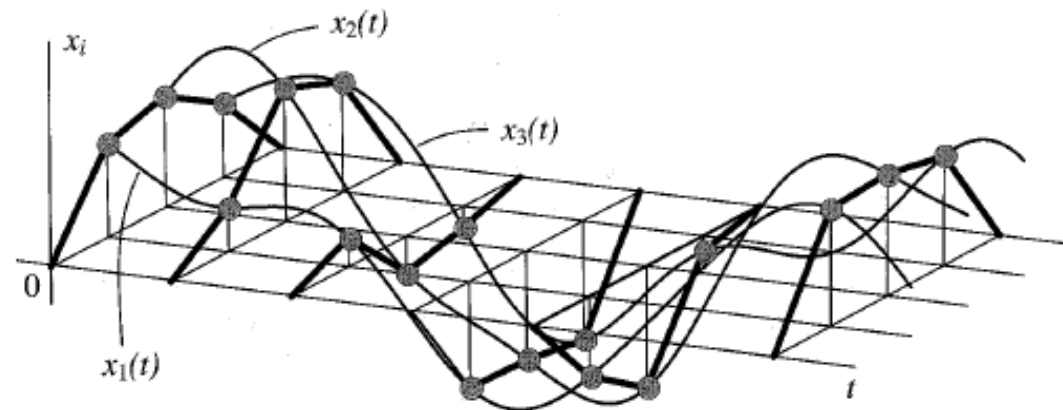
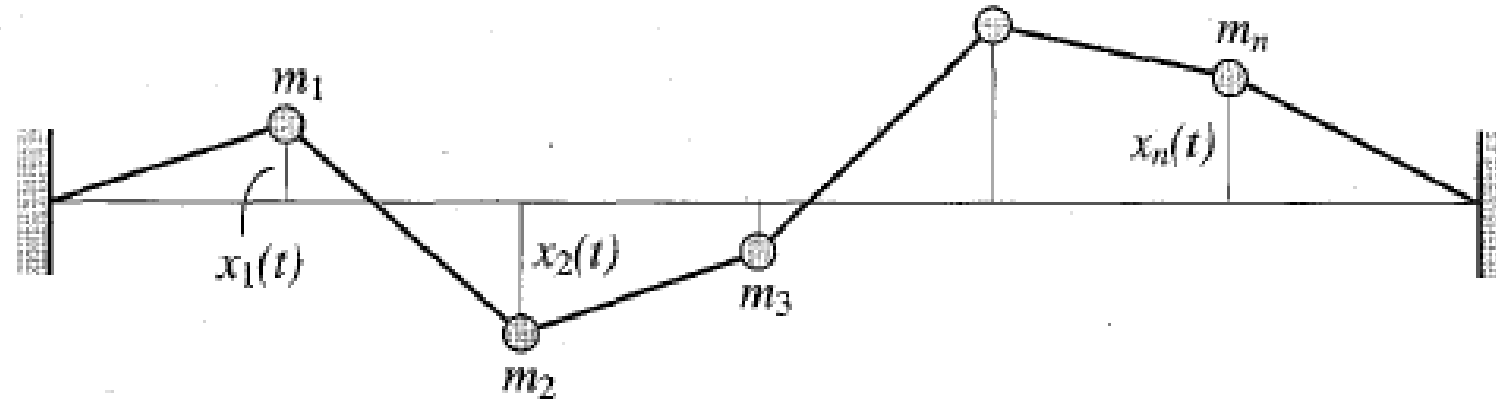
# Introduction: multi-degree-of-freedom systems

- For multi-degree-of-freedom systems natural vibration implies not only a certain natural frequency but also a certain natural displacement configuration assumed by the system masses during motion

# Introduction: system configuration



# Introduction: system configuration





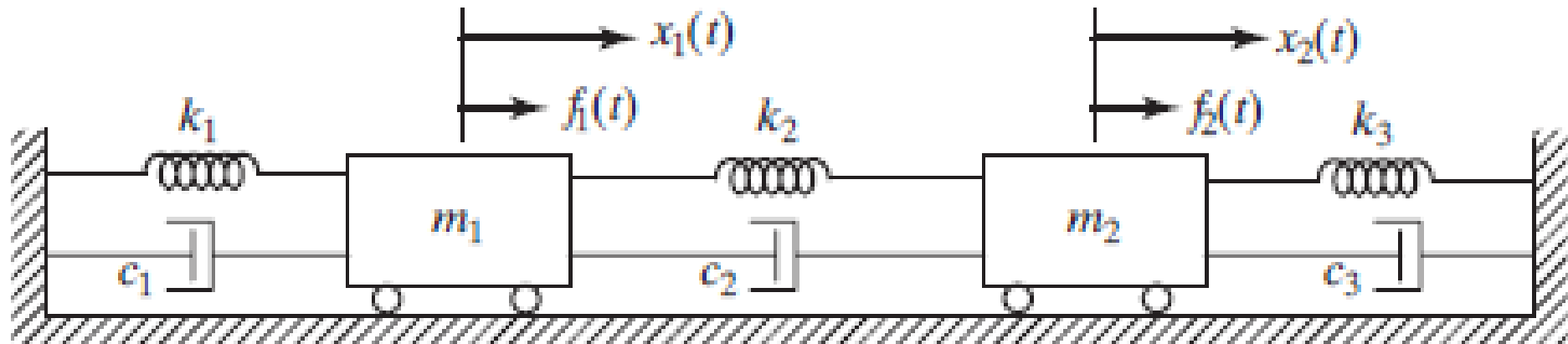
# Introduction: multi-degree-of-freedom systems

- For multi-degree-of-freedom systems natural vibration implies not only a certain natural frequency but also a certain natural displacement configuration assumed by the system masses during motion
- The system possesses as many natural frequencies and natural configurations, known as natural modes of vibrations, as the number of degrees of freedom of the system
- Depending on the initial excitation, the system can be made to vibrate in any of these modes independently
- The mathematical formulation for an  $n$ -degree-of-freedom system consists of  $n$  simultaneous ordinary differential equations of motion. Hence, the motion of one mass depends on the motion of the other  $n - 1$  masses.
- For a proper choice of coordinates, known as principal coordinates, or natural coordinates, the  $n$  differential equations become independent of one another.

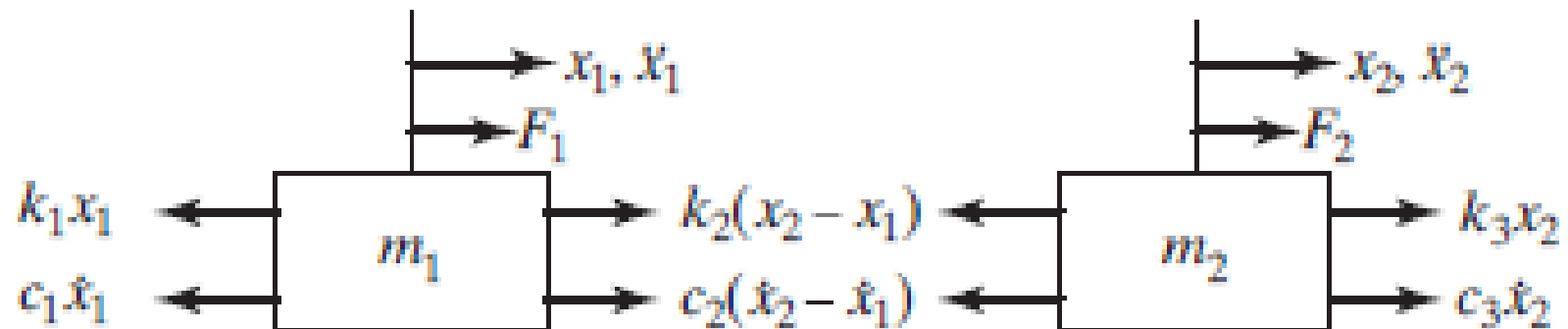
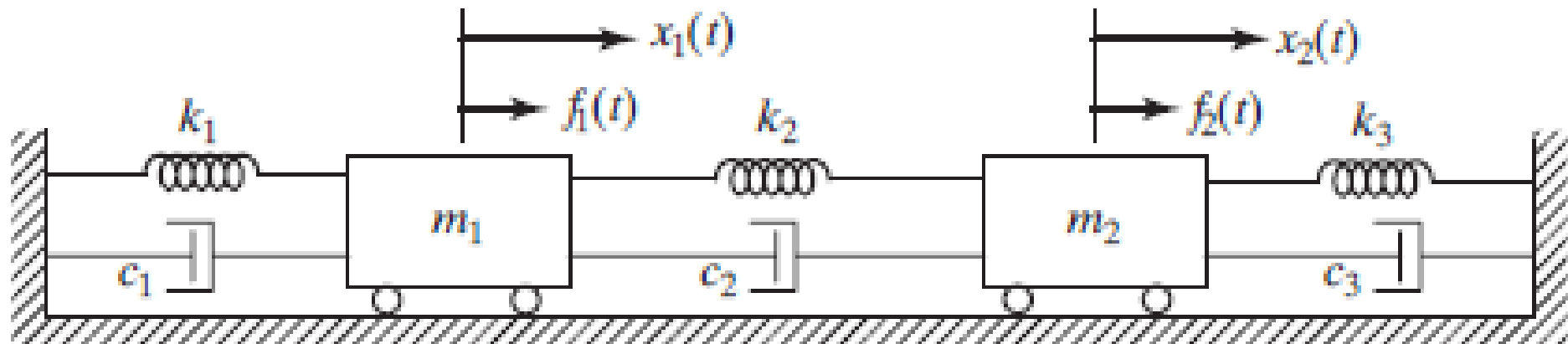
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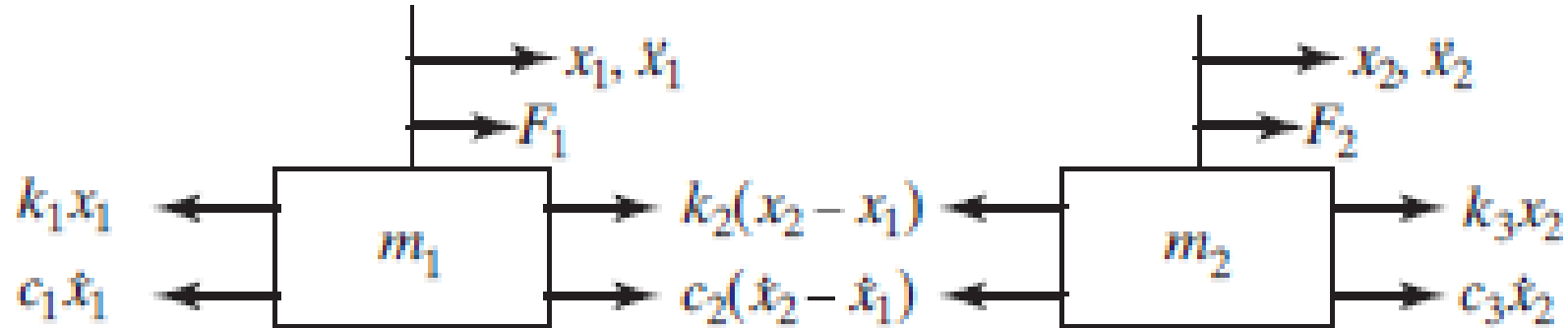
# Equations of motion of 2-DOF systems



# Equations of motion of 2-DOF systems



# Equations of motion of 2-DOF systems



$$m_1 \ddot{x}_1 + (c_1 + c_2) \dot{x}_1 - c_2 \dot{x}_2 + (k_1 + k_2) x_1 - k_2 x_2 = f_1$$

$$m_2 \ddot{x}_2 - c_2 \dot{x}_1 + (c_2 + c_3) \dot{x}_2 - k_2 x_1 + (k_2 + k_3) x_2 = f_2$$

# Equations of motion of 2-DOF systems

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system of two coupled second order differential equations

$$[m] \ddot{\vec{x}}(t) + [c] \dot{\vec{x}}(t) + [k] \vec{x}(t) = \vec{f}(t)$$

# Equations of motion of 2-DOF systems

$$[m]\ddot{\vec{x}}(t) + [c]\dot{\vec{x}}(t) + [k]\vec{x}(t) = \vec{f}(t)$$

mass, damping and stiffness matrices:

$$[m] = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix}$$

$$[c] = \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 + c_3 \end{bmatrix}$$

$$[k] = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 \end{bmatrix}$$

displacement and force vectors:

$$\vec{x}(t) = \begin{Bmatrix} x_1(t) \\ x_2(t) \end{Bmatrix}$$

$$\vec{f}(t) = \begin{Bmatrix} f_1(t) \\ f_2(t) \end{Bmatrix}$$

# Equations of motion of 2-DOF systems

$$[m]\ddot{\vec{x}}(t) + [c]\dot{\vec{x}}(t) + [k]\vec{x}(t) = \vec{f}(t)$$

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$$[k] = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 \end{bmatrix}$$

$$[m]^T = [m]$$

$$[c]^T = [c]$$

$$[k]^T = [k]$$



# Equations of motion of 2-DOF systems

$$m_1 \ddot{x}_1 + (c_1 + c_2) \dot{x}_1 - c_2 \dot{x}_2 + (k_1 + k_2) x_1 - k_2 x_2 = f_1$$

$$m_2 \ddot{x}_2 - c_2 \dot{x}_1 + (c_2 + c_3) \dot{x}_2 - k_2 x_1 + (k_2 + k_3) x_2 = f_2$$

initial conditions:

$$x_1(t = 0) = x_1(0)$$

$$\dot{x}_1(t = 0) = \dot{x}_1(0)$$

$$x_2(t = 0) = x_2(0)$$

$$\dot{x}_2(t = 0) = \dot{x}_2(0)$$

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# Free vibration of undamped systems

$$\begin{aligned} m_1 \ddot{x}_1 + (c_1 + c_2) \dot{x}_1 - c_2 \dot{x}_2 + (k_1 + k_2) x_1 - k_2 x_2 &= f_1 \\ m_2 \ddot{x}_2 - c_2 \dot{x}_1 + (c_2 + c_3) \dot{x}_2 - k_2 x_1 + (k_2 + k_3) x_2 &= f_2 \end{aligned}$$

$$[m] \ddot{\vec{x}}(t) + [c] \dot{\vec{x}}(t) + [k] \vec{x}(t) = \vec{f}(t)$$

# Free vibration of undamped systems

$$m_1 \ddot{x}_1 + (k_1 + k_2) x_1 - k_2 x_2 = 0$$

$$m_2 \ddot{x}_2 - k_2 x_1 + (k_2 + k_3) x_2 = 0$$

$$[m] \ddot{\vec{x}}(t) + [k] \vec{x}(t) = 0$$

# Free vibration of undamped systems

harmonic solutions:

$$\left\{ \begin{array}{l} x_1(t) = X_1 \cos(\omega t + \phi) \\ x_2(t) = X_2 \cos(\omega t + \phi) \end{array} \right.$$

same frequency and phase angle but different amplitudes



$$\left[ \left\{ -m_1 \omega^2 + (k_1 + k_2) \right\} X_1 - k_2 X_2 \right] \cos(\omega t + \phi) = 0$$

$$\left[ -k_2 X_1 + \left\{ -m_2 \omega^2 + (k_2 + k_3) \right\} X_2 \right] \cos(\omega t + \phi) = 0$$

# Free vibration of undamped systems

$$x_1(t) = X_1 \cos(\omega t + \phi)$$

$$x_2(t) = X_2 \cos(\omega t + \phi)$$

$$\left[ \left\{ -m_1 \omega^2 + (k_1 + k_2) \right\} X_1 - k_2 X_2 \right] \cos(\omega t + \phi) = 0$$

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$$\left\{ -m_1 \omega^2 + (k_1 + k_2) \right\} X_1 - k_2 X_2 = 0$$

$$-k_2 X_1 + \left\{ -m_2 \omega^2 + (k_2 + k_3) \right\} X_2 = 0$$

# Free vibration of undamped systems

$$x_1(t) = X_1 \cos(\omega t + \phi)$$

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$$\left\{ -m_1 \omega^2 + (k_1 + k_2) \right\} X_1 - k_2 X_2 = 0$$

$$-k_2 X_1 + \left\{ -m_2 \omega^2 + (k_2 + k_3) \right\} X_2 = 0$$


trivial solution:

$$X_1 = X_2 = 0$$

# Free vibration of undamped systems

non-trivial solution:

$$\det \begin{bmatrix} -m_1\omega^2 + (k_1 + k_2) & -k_2 \\ -k_2 & -m_2\omega^2 + (k_2 + k_3) \end{bmatrix} = 0$$


$$(m_1 m_2) \omega^4 - \{ (k_1 + k_2) m_2 + (k_2 + k_3) m_1 \} \omega^2 + \{ (k_1 + k_2)(k_2 + k_3) - k_2^2 \} = 0$$

characteristic equation



# Free vibration of undamped systems

$$(m_1 m_2) \omega^4 - \{(k_1 + k_2)m_2 + (k_2 + k_3)m_1\} \omega^2 + \{(k_1 + k_2)(k_2 + k_3) - k_2^2\} = 0$$

solutions:

$$\omega_1^2, \omega_2^2 = \frac{1}{2} \left\{ \frac{(k_1 + k_2)m_2 + (k_2 + k_3)m_1}{m_1 m_2} \right\} \mp \frac{1}{2} \left[ \left\{ \frac{(k_1 + k_2)m_2 + (k_2 + k_3)m_1}{m_1 m_2} \right\}^2 - 4 \left\{ \frac{(k_1 + k_2)(k_2 + k_3) - k_2^2}{m_1 m_2} \right\} \right]^{1/2}$$

It is possible for the system to have a non-trivial harmonic solution with two natural frequencies:

$\omega_1$  and  $\omega_2$

# Free vibration of undamped systems. Natural modes

To determine the amplitudes  $X_1$  and  $X_2$  (for each of the two natural frequencies):

$$\left. \begin{aligned} r_1 &= \left\{ X_2^{(1)} / X_1^{(1)} \right\} \\ r_2 &= \left\{ X_2^{(2)} / X_1^{(2)} \right\} \end{aligned} \right\} \text{(because the equation is homogeneous)}$$

$$\begin{aligned} \left\{ -m_1 \omega^2 + (k_1 + k_2) \right\} X_1 - k_2 X_2 &= 0 \\ -k_2 X_1 + \left\{ -m_2 \omega^2 + (k_2 + k_3) \right\} X_2 &= 0 \end{aligned}$$



For  $r_1$ ,  $\omega^2 = \omega_1^2$

For  $r_2$ ,  $\omega^2 = \omega_2^2$

$$\left. \begin{aligned} r_1 &= \frac{X_2^{(1)}}{X_1^{(1)}} = \frac{-m_1 \omega_1^2 + (k_1 + k_2)}{k_2} = \frac{k_2}{-m_2 \omega_1^2 + (k_2 + k_3)} \\ r_2 &= \frac{X_2^{(2)}}{X_1^{(2)}} = \frac{-m_1 \omega_2^2 + (k_1 + k_2)}{k_2} = \frac{k_2}{-m_2 \omega_2^2 + (k_2 + k_3)} \end{aligned} \right\}$$

# Free vibration of undamped systems. Natural modes

$$\vec{X}^{(1)} = \begin{Bmatrix} X_1^{(1)} \\ X_2^{(1)} \end{Bmatrix} = \begin{Bmatrix} X_1^{(1)} \\ r_1 X_1^{(1)} \end{Bmatrix}$$

$$\vec{X}^{(2)} = \begin{Bmatrix} X_1^{(2)} \\ X_2^{(2)} \end{Bmatrix} = \begin{Bmatrix} X_1^{(2)} \\ r_2 X_1^{(2)} \end{Bmatrix}$$

$$\left. \begin{array}{l} \vec{X}^{(1)} \\ \vec{X}^{(2)} \end{array} \right\}$$

modal vectors  $\rightarrow$  normal modes of vibration

# Free vibration of undamped systems. Natural modes

Free vibration solution:

$$\begin{aligned}x_1(t) &= X_1 \cos(\omega t + \phi) \\x_2(t) &= X_2 \cos(\omega t + \phi)\end{aligned}$$

$$\vec{x}^{(1)}(t) = \begin{Bmatrix} x_1^{(1)}(t) \\ x_2^{(1)}(t) \end{Bmatrix} = \begin{Bmatrix} X_1^{(1)} \cos(\omega_1 t + \phi_1) \\ r_1 X_1^{(1)} \cos(\omega_1 t + \phi_1) \end{Bmatrix} = \text{first mode}$$

$$\vec{x}^{(2)}(t) = \begin{Bmatrix} x_1^{(2)}(t) \\ x_2^{(2)}(t) \end{Bmatrix} = \begin{Bmatrix} X_1^{(2)} \cos(\omega_2 t + \phi_2) \\ r_2 X_1^{(2)} \cos(\omega_2 t + \phi_2) \end{Bmatrix} = \text{second mode}$$

Constants  $X_1^{(1)}, X_1^{(2)}, \phi_1, \phi_2$  are determined by the initial conditions

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# Response to initial excitations

The system can be made to vibrate in its  $i_{th}$  normal mode ( $i = 1, 2$ ) by subjecting it to the specific initial conditions:

$$\begin{aligned}x_1(t=0) &= X_1^{(i)} = \text{some constant}, & \dot{x}_1(t=0) &= 0, \\x_2(t=0) &= r_i X_1^{(i)}, & \dot{x}_2(t=0) &= 0\end{aligned}$$

# Response to initial excitations

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For any other general initial conditions, both modes will be excited:


$$\vec{x}(t) = c_1 \vec{x}^{(1)}(t) + c_2 \vec{x}^{(2)}(t)$$

$c_1$  and  $c_2$  are constants

we can choose  $c_1 = c_2 = 1$  since the solution already includes the unknown constants  $X_1^{(1)}$  and  $X_1^{(2)}$

# Response to initial excitations

$$\vec{x}(t) = c_1 \vec{x}^{(1)}(t) + c_2 \vec{x}^{(2)}(t)$$


$$\begin{aligned} x_1(t) &= x_1^{(1)}(t) + x_1^{(2)}(t) = X_1^{(1)} \cos(\omega_1 t + \phi_1) + X_1^{(2)} \cos(\omega_2 t + \phi_2) \\ x_2(t) &= x_2^{(1)}(t) + x_2^{(2)}(t) = r_1 X_1^{(1)} \cos(\omega_1 t + \phi_1) + r_2 X_1^{(2)} \cos(\omega_2 t + \phi_2) \end{aligned}$$

Constants  $X_1^{(1)}, X_1^{(2)}, \phi_1, \phi_2$  are determined by the initial conditions

$$\left\{ \begin{array}{ll} x_1(t=0) = x_1(0), & \dot{x}_1(t=0) = \dot{x}_1(0), \\ x_2(t=0) = x_2(0), & \dot{x}_2(t=0) = \dot{x}_2(0) \end{array} \right.$$



# Response to initial excitations

Introducing the initial conditions in the equations:

$$\left\{ \begin{array}{l} x_1(t) = X_1^{(1)} \cos(\omega_1 t + \phi_1) + X_1^{(2)} \cos(\omega_2 t + \phi_2) \\ x_2(t) = r_1 X_1^{(1)} \cos(\omega_1 t + \phi_1) + r_2 X_1^{(2)} \cos(\omega_2 t + \phi_2) \end{array} \right.$$



$$\left\{ \begin{array}{l} x_1(0) = X_1^{(1)} \cos \phi_1 + X_1^{(2)} \cos \phi_2 \\ \dot{x}_1(0) = -\omega_1 X_1^{(1)} \sin \phi_1 - \omega_2 X_1^{(2)} \sin \phi_2 \\ x_2(0) = r_1 X_1^{(1)} \cos \phi_1 + r_2 X_1^{(2)} \cos \phi_2 \\ \dot{x}_2(0) = -\omega_1 r_1 X_1^{(1)} \sin \phi_1 - \omega_2 r_2 X_1^{(2)} \sin \phi_2 \end{array} \right.$$

four algebraic  
equations with four  
unknowns

# Response to initial excitations

The four unknowns:

$$\left\{ \begin{array}{ll} X_1^{(1)} \cos \phi_1 = \left\{ \frac{r_2 x_1(0) - x_2(0)}{r_2 - r_1} \right\}, & X_1^{(2)} \cos \phi_2 = \left\{ \frac{-r_1 x_1(0) + x_2(0)}{r_2 - r_1} \right\} \\ X_1^{(1)} \sin \phi_1 = \left\{ \frac{-r_2 \dot{x}_1(0) + \dot{x}_2(0)}{\omega_1 (r_2 - r_1)} \right\}, & X_1^{(2)} \sin \phi_2 = \left\{ \frac{r_1 \dot{x}_1(0) - \dot{x}_2(0)}{\omega_2 (r_2 - r_1)} \right\} \end{array} \right.$$

# Response to initial excitations

The four unknowns:

$$\left\{ \begin{array}{ll} X_1^{(1)} \cos \phi_1 = \left\{ \frac{r_2 x_1(0) - x_2(0)}{r_2 - r_1} \right\}, & X_1^{(2)} \cos \phi_2 = \left\{ \frac{-r_1 x_1(0) + x_2(0)}{r_2 - r_1} \right\} \\ X_1^{(1)} \sin \phi_1 = \left\{ \frac{-r_2 \dot{x}_1(0) + \dot{x}_2(0)}{\omega_1 (r_2 - r_1)} \right\}, & X_1^{(2)} \sin \phi_2 = \left\{ \frac{r_1 \dot{x}_1(0) - \dot{x}_2(0)}{\omega_2 (r_2 - r_1)} \right\} \end{array} \right.$$

The desired solution:

$$\left\{ \begin{array}{l} X_1^{(1)} = \left[ \left\{ X_1^{(1)} \cos \phi_1 \right\}^2 + \left\{ X_1^{(1)} \sin \phi_1 \right\}^2 \right]^{1/2} = \frac{1}{(r_2 - r_1)} \left[ \left\{ r_2 x_1(0) - x_2(0) \right\}^2 + \frac{\left\{ -r_2 \dot{x}_1(0) + \dot{x}_2(0) \right\}^2}{\omega_1^2} \right]^{1/2} \\ X_1^{(2)} = \left[ \left\{ X_1^{(2)} \cos \phi_2 \right\}^2 + \left\{ X_1^{(2)} \sin \phi_2 \right\}^2 \right]^{1/2} = \frac{1}{(r_2 - r_1)} \left[ \left\{ +r_1 x_1(0) - x_2(0) \right\}^2 + \frac{\left\{ r_1 \dot{x}_1(0) - \dot{x}_2(0) \right\}^2}{\omega_2^2} \right]^{1/2} \\ \phi_1 = \tan^{-1} \left\{ \frac{X_1^{(1)} \sin \phi_1}{X_1^{(1)} \cos \phi_1} \right\} = \tan^{-1} \left\{ \frac{-r_2 \dot{x}_1(0) + \dot{x}_2(0)}{\omega_1 [r_2 x_1(0) - x_2(0)]} \right\} \\ \phi_2 = \tan^{-1} \left\{ \frac{X_1^{(2)} \sin \phi_2}{X_1^{(2)} \cos \phi_2} \right\} = \tan^{-1} \left\{ \frac{r_1 \dot{x}_1(0) - \dot{x}_2(0)}{\omega_2 [-r_1 x_1(0) + x_2(0)]} \right\} \end{array} \right.$$