



北京航空航天大学  
BEIHANG UNIVERSITY

# Avionics Technology

B31353551

— *Radio Navigation*

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# VI. Radio Navigation



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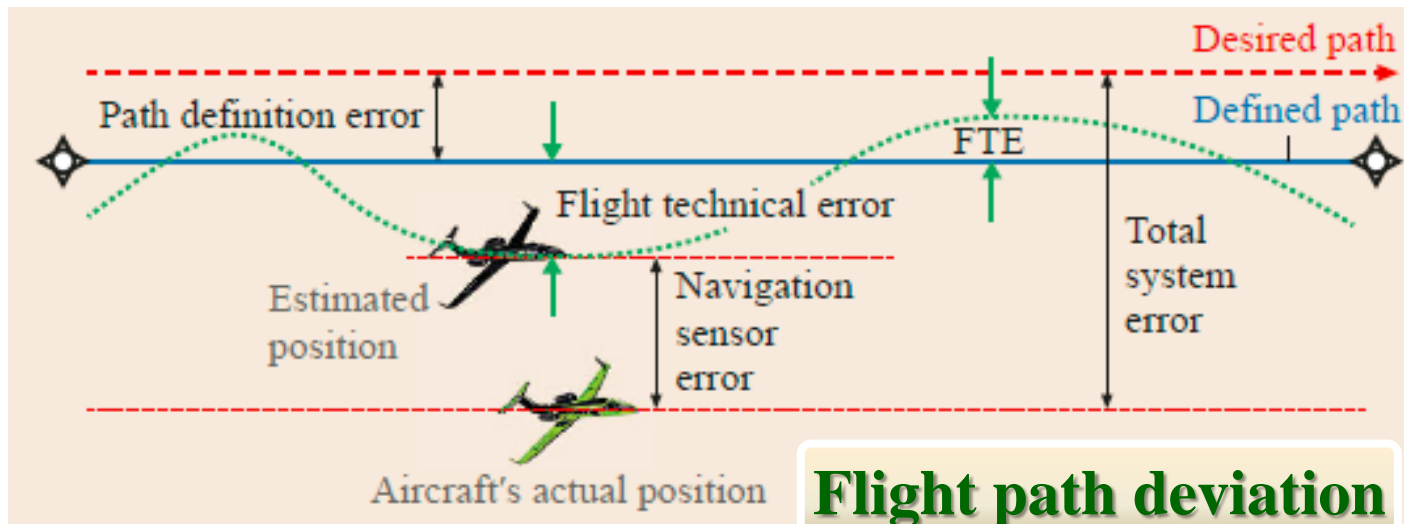
- (1) Some concepts
- (2) Radio landing systems
- (3) Rho-theta navigation systems
- (4) Satellite navigation systems



# (1) Some concepts



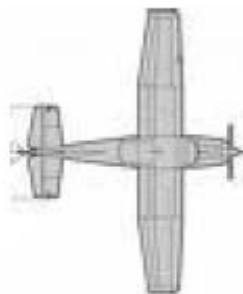
- Radio navigation systems consist of airborne and ground- or satellite-based navigation aids, including range- and direction-measuring radio navigation systems, radio-technical landing systems, short- and long-range systems, and satellite navigation systems.



# (1) Some concepts



- Airborne equipment usually provides the radio navigation signal detection and its processing, and the ground- or satellite-based radio beacons — the forming of the radio signals of required structure and its emission. The systems based on radio waves conditions are exposed to radio interference and are not autonomous in most cases.



**Airborne equipment: radio receiver**



**Radio beacon:  
radio transmitter**

# (1) Some concepts



- **NDB (Non Directional Beacon)** is simply just a ground-based **AM radio transmitter** which radiates radio waves in all directions (**omnidirectional**). In the aircraft, the receiving antenna was **originally manually adjusted** to find the signal **bearing** (azimuth angle), but very quickly became **automated** and is then called **Automatic Direction Finding (ADF)**.

**Station identifier**

**PENZA**  
**591 WH : : : :**

**591kHz**  
**(MF band)**

**NDB station on  
aviation chart**



# (1) Some concepts



- Each NDB is identified by a two- or three-letter Morse code call sign, which is the only (repeated) information modulated on radio signals radiated by the NDB transmitter. Amplitude shift keying (ASK) is used for audible distinction of signals from different NDBs.
- If incoming radio waves hit the ADF antenna loop in any direction other than directly perpendicular, a specific composite voltage  $e$  will be induced over the antenna, and the ADF can deduce down to the relative bearings to the beacon.



# (1) Some concepts



$$e = E \sin(\omega t + \varphi) - E \sin(\omega t - \varphi) \\ = 2E \sin \varphi \cdot \cos \omega t$$

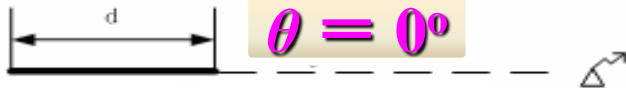
$\sin \varphi \approx \varphi = \omega d / 2c = \pi d / \lambda$  ( $d \ll \lambda$   
due to  $\lambda$  is in the order of km)

$$\text{Hence, } e \approx 2E(\pi d / \lambda) \cdot \cos \omega t$$



If  $\theta = 0^\circ$ , then  $e = e_{\max}$

At other  $\theta$ s,  $e < e_{\max}$

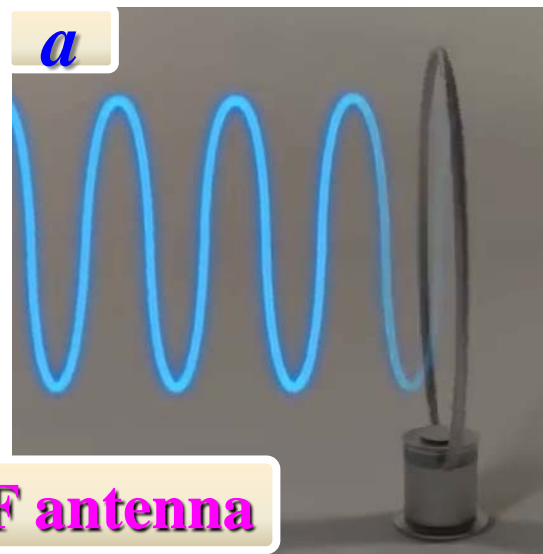
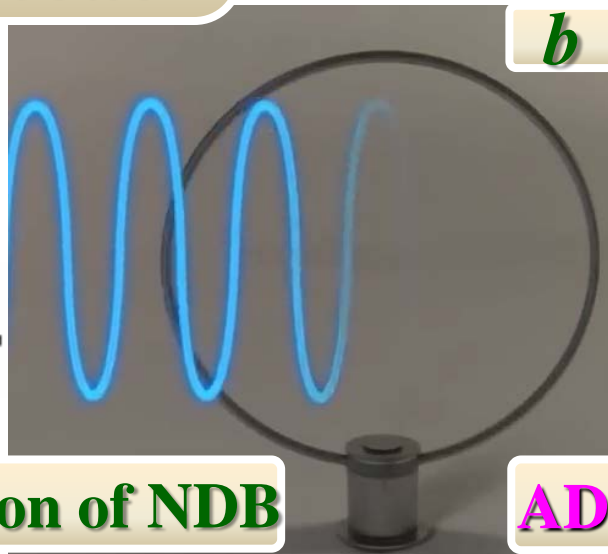
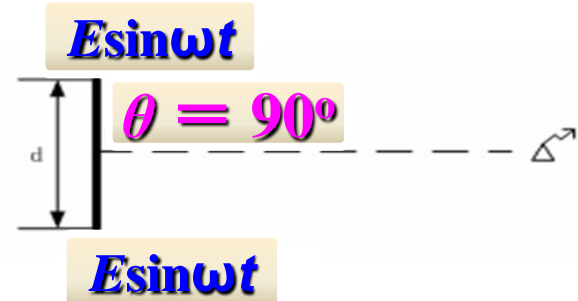


$$E \sin(\omega t - \varphi) \quad E \sin(\omega t + \varphi)$$

Case *b*: point in the direction of NDB

Case *a*: perpendicular direction

$$e = 0$$



ADF antenna



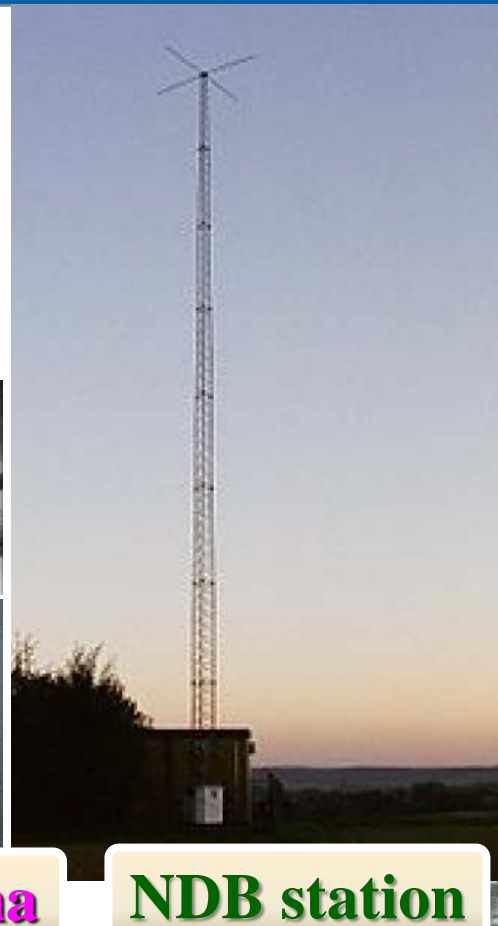
# (1) Some concepts



- Today, **NDB** is considered the most basic navigation aid used in aviation operating on medium frequency (MF) band. Such a system has low accuracy of navigation that worsens with its departure from radio beacon, and serve as a backup for the more accurate systems.



Airborne ADF antenna



NDB station



# (1) Some concepts



- Radio-technical methods of determining **navigation parameters** (distance, direction of signal arrival, etc.) use functional dependence between radio **signals parameters** (amplitude, frequency, phase and time of propagation along the radio path) and navigation parameters.

## Radio navigation signal

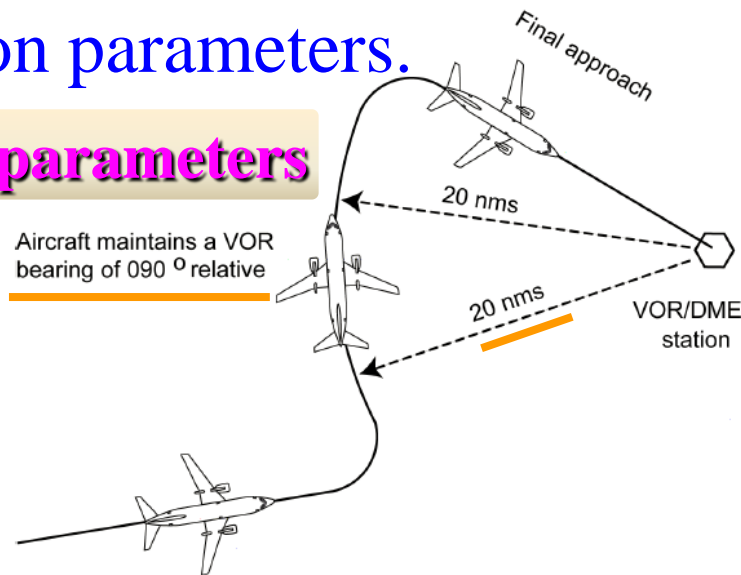
$$e(t) = A \cos(2\pi f_c t + \varphi)$$

Amplitude

Frequency

Phase

## Navigation parameters



# (1) Some concepts



- The aircraft's position determination is based on the *intercept or LOP* (lines of position) *method*. Line of position is the geometric locus on a plane, where each point has the constant navigation parameter value. Two or more lines of position intersection (crossing) is a result of navigation parameter measurement. LOP can be straight lines of specific bearing's values (azimuth), circle lines of equivalent distances, a circle line of equivalent distance and a straight line of specific bearing value (azimuth).



# (1) Some concepts

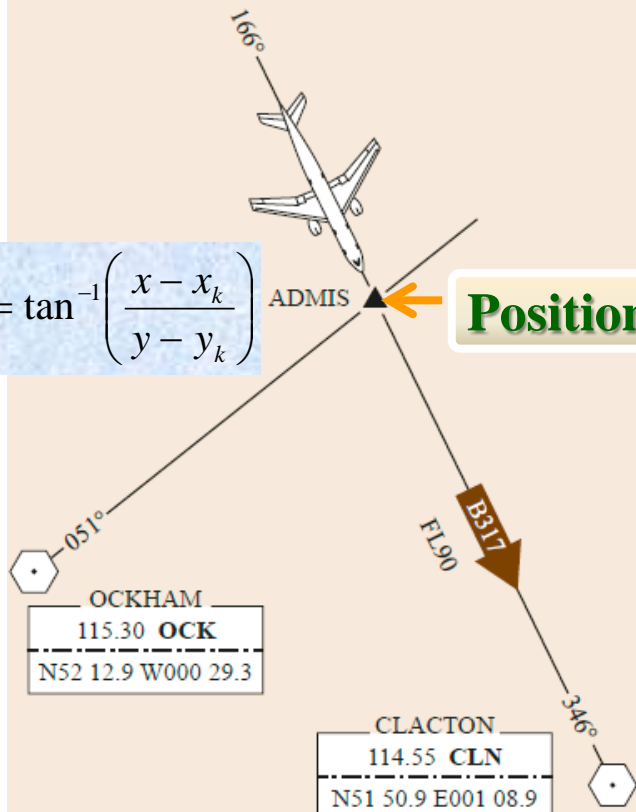


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$$\Theta_k = \tan^{-1} \left( \frac{x - x_k}{y - y_k} \right)$$

ADMIS

**Position fix**



**LOP of specific bearings**

$(x_1, y_1)$

S1

$r_1$

**Position fix**

P

$(x_2, y_2)$

S2

$r_2$

$(x_3, y_3)$

S3

$r_3$

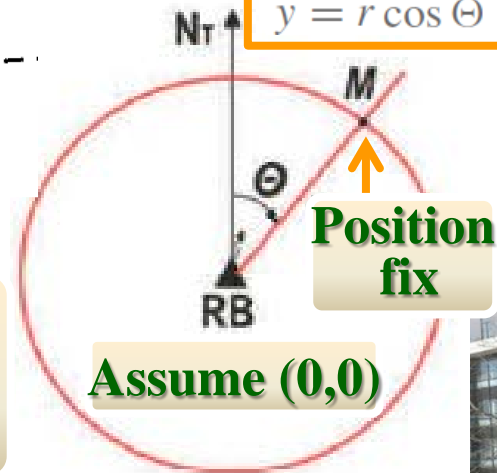
**LOP of equivalent distances**

$$\sqrt{(x_k - x)^2 + (y_k - y)^2} = r_k$$

$$\begin{aligned} x &= r \sin \Theta \\ y &= r \cos \Theta \end{aligned}$$

**Position fix**

**Assume (0,0)**



**LOP of specific bearing and equivalent distance based on single station**

## (2) Radio landing systems



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- Landing is the most complicated stage (phase) of flight at the end of which an aircraft should be taken to the set point on the runway (RW) surface. Radio-technical landing systems are thus able to provide a precise control of the flight path during the final approach of aircraft in all weather conditions.

Poor visibility  
landing condition



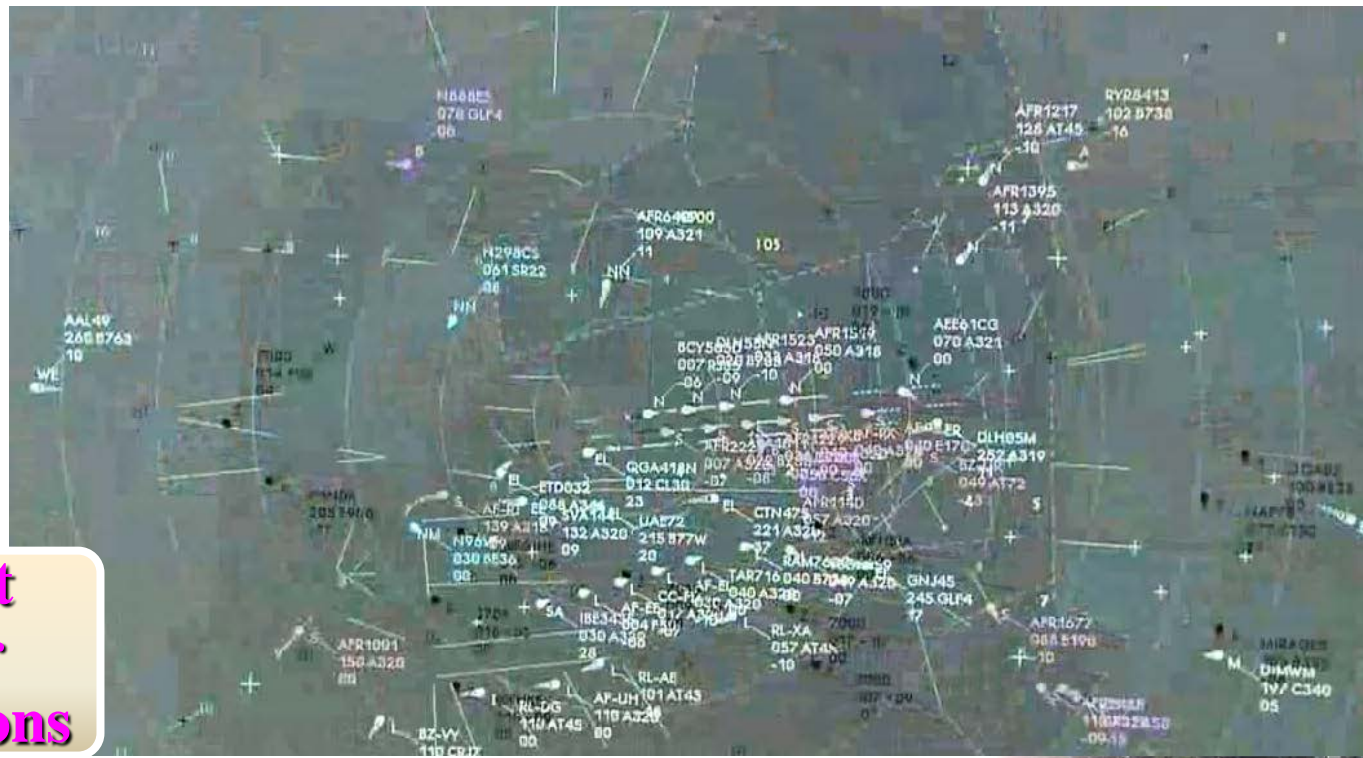
## (2) Radio landing systems



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- Landing is greatly influenced by meteorological factors, density and intensity of air traffic in the vicinity of Airports.

Aircrafts are guided to be lined up for intercepting ILS signal.



Radar screen at  
ATC center for  
landing instructions



## (2) Radio landing systems



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- ILS (*Instrument landing system*) is a approach guidance system installed at major airports and airfields which provides guidance in poor visibility conditions during the approach to the runway. A small number of airports are also equipped with MLS (*Microwave landing system*) which is more accurate.

However, it will still be a long time before ILS is completely replaced by MLS.



Airport equipped with MLS



## (2) Radio landing systems



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- The **ILS** system basically comprises a *localizer* (LOC) transmitter situated at the end of the runway and a *glide slope* (G/S) transmitter situated at the edge of the runway.



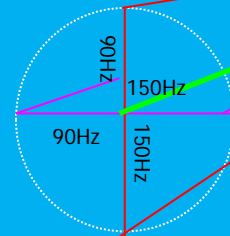
Approximately 25m wide

LOC

Approximately 10m tall

G/S

Runway(RW)



Radio beams indicate RW centerline and glide slope

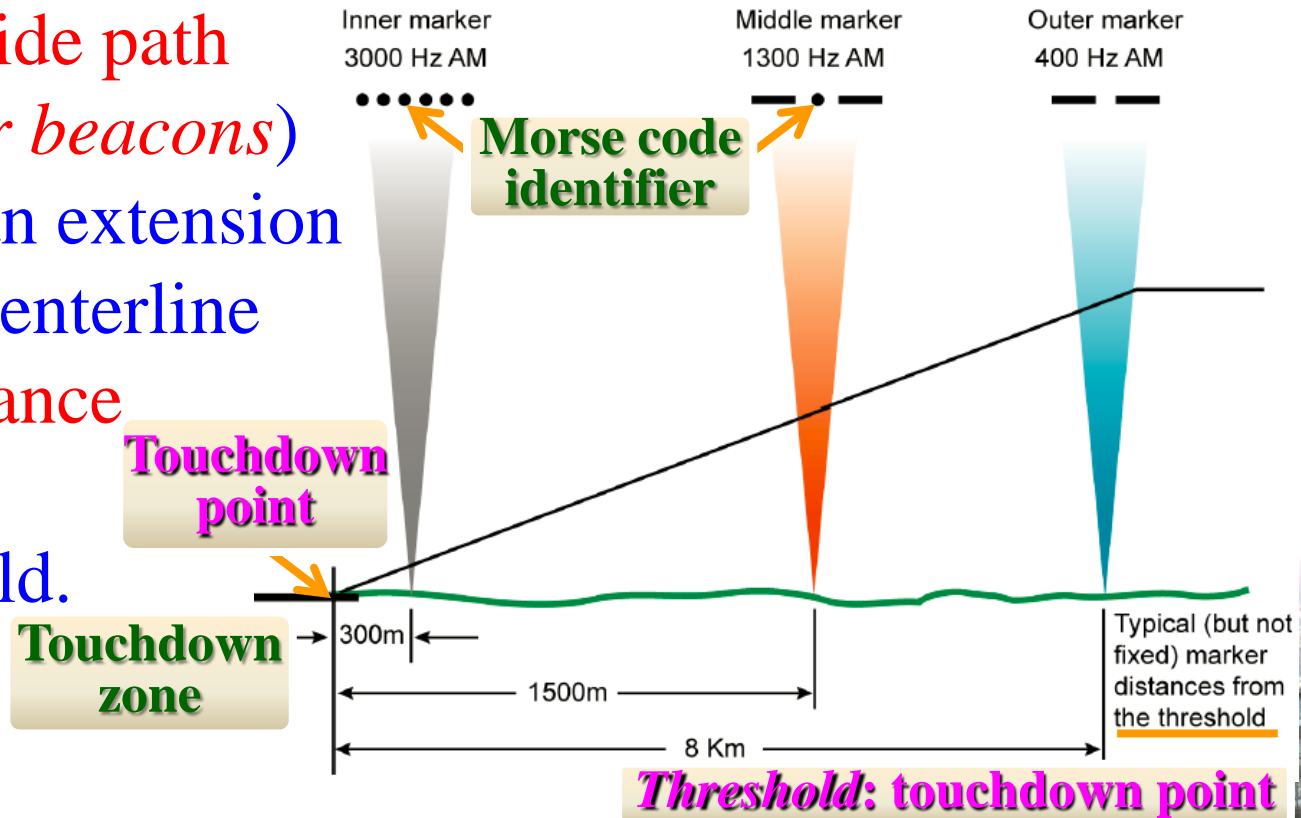


Following the glide path with the aid of ILS

## (2) Radio landing systems



- The ILS also determines the moments of **passing three points on the glide path** (namely *marker beacons*) situated along an extension of the runway centerline at a certain distance relative to the runway threshold.



## (2) Radio landing systems



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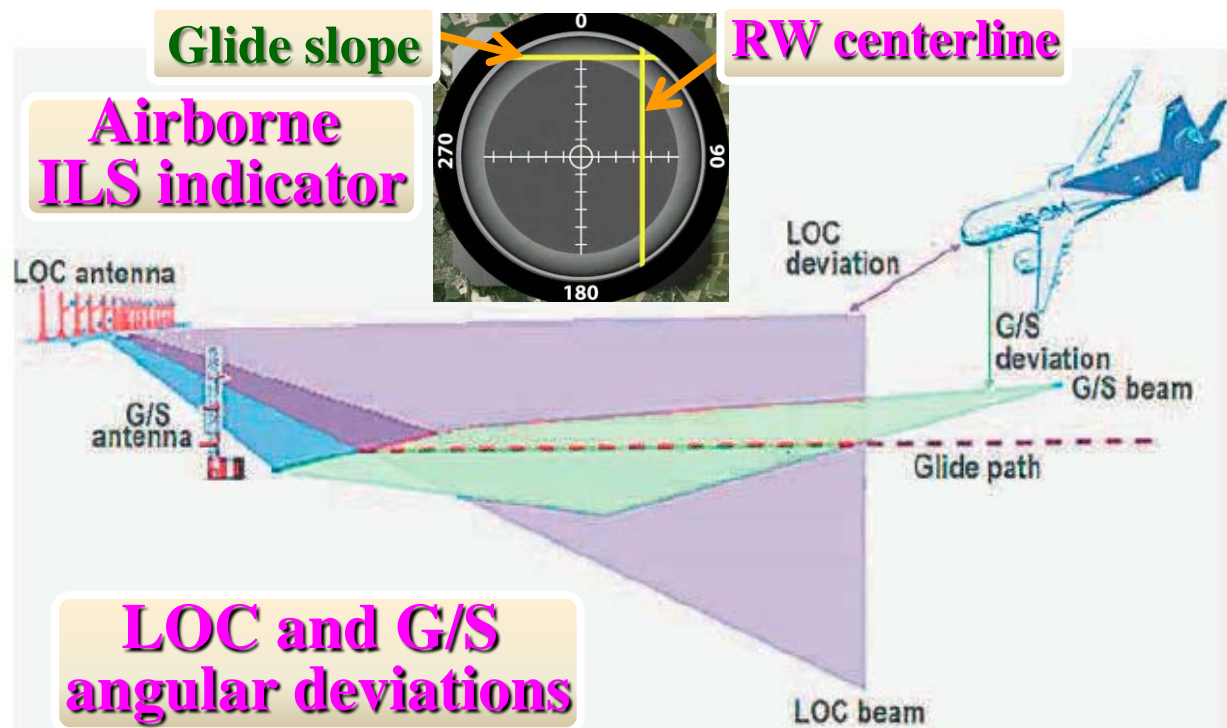
- The landing system aids the aircraft to fly along a specified trajectory, i.e. a glide path, and can be considered as a guidance to a region of admissible lateral and vertical deviations from the ideal descent path.



## (2) Radio landing systems



- LOC and G/S radio beacons form radiation fields defining a **course plane** (a vertical plane passing through the runway centerline) and a **descending/ gliding plane** (a plane sloped to the ground plane at an angle of approximately  $3^\circ$ ).

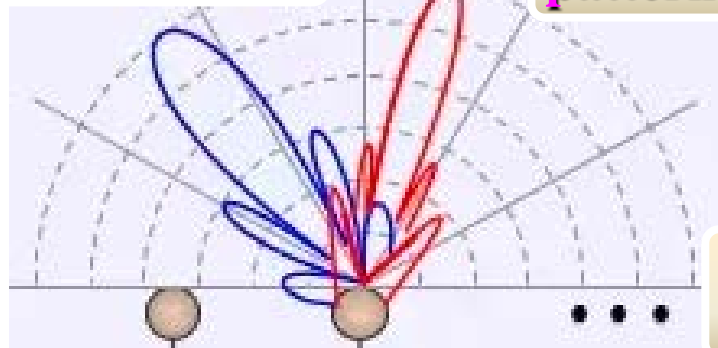


## (2) Radio landing systems

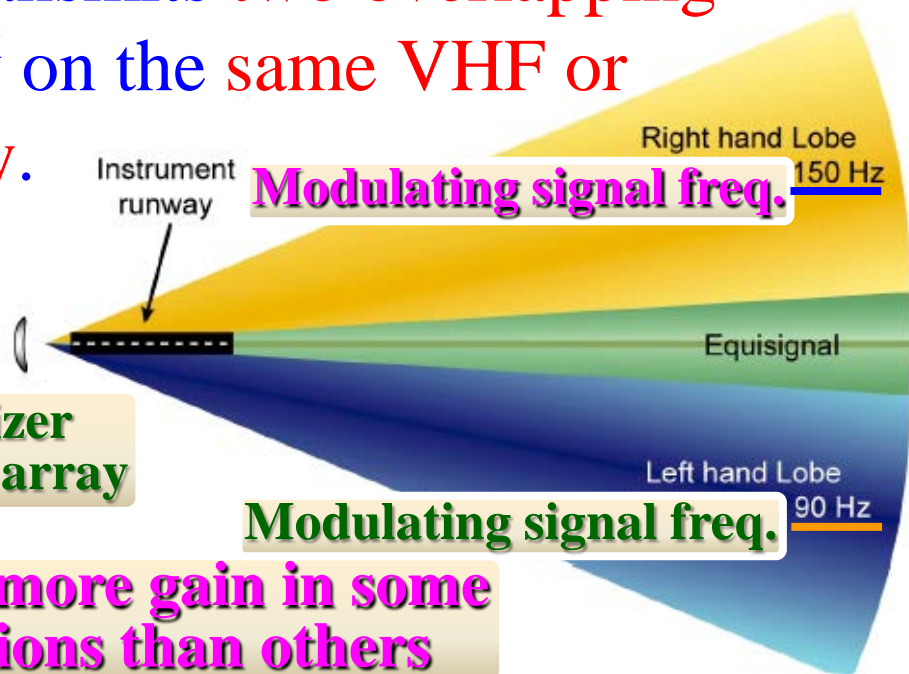


- The main method of **determining the direction** by means of localizers and glide slope beacons is an *equi-signal* method. The LOC or G/S transmits **two overlapping radio beams** of equal energy on the same VHF or UHF carrier wave frequency.

**Radio beam formation**



**Radiation power pattern envelope**



**Localizer antenna array**

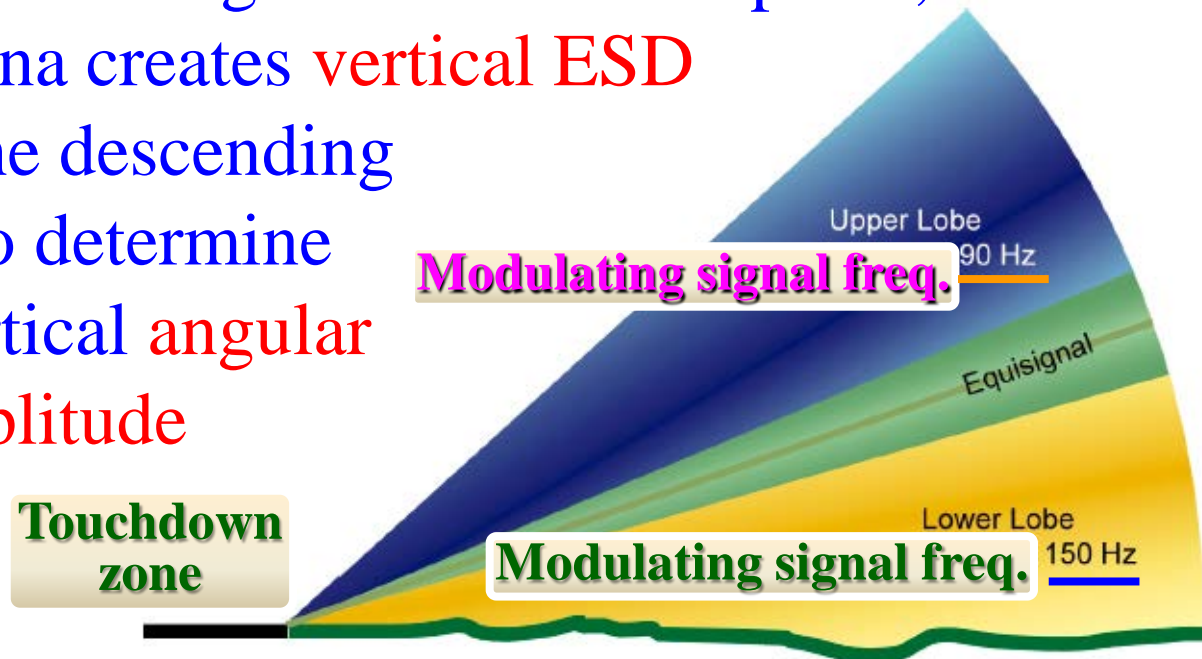
**Having more gain in some directions than others**



## (2) Radio landing systems



- The center of the overlap area defines the ILS equisignal direction (ESD). The LOC antenna creates horizontal ESD coinciding with the course plane, and the G/S antenna creates vertical ESD coinciding with the descending / gliding plane. To determine the lateral and vertical angular deviation, the amplitude modulation (AM) is employed.





## (2) Radio landing systems



- The VHF transmitter at LOC or G/S generates and emits two amplitude-modulated signals:

$$e_1 = E_m F_1(\theta)(1+m\cos \Omega_1 t) \cos \omega t$$

$$e_2 = E_m F_2(\theta)(1+m\cos \Omega_2 t) \cos \omega t$$

**$E_m$  are amplitudes at antenna outputs assumed to be equal**

**$F_1(\theta)$  or  $F_2(\theta)$  is the directivity of antenna, a function of direction (azimuth or elevation angle  $\theta$ ) of the beam pattern**

**$m$  are indexes of amplitude modulation(amplitude sensitivity)**

**$\Omega_1/\Omega_2$  equals to 90Hz or 150Hz;  $\omega$  are frequencies of carriers**

## (2) Radio landing systems



- When combining the radiation fields produced by the transmitting antennas, a resultant amplitude-modulated field  $e$  with modulating frequencies of 90 Hz and 150 Hz is formed in space as:

$$e = e_1 + e_2 =$$

$$E_m[F_1(\theta) + F_2(\theta)][1 + M_1(\theta)\cos \Omega_1 t + M_2(\theta)\cos \Omega_2 t]\cos \omega t$$

$$M_1(\theta) = \frac{mF_1(\theta)}{F_1(\theta) + F_2(\theta)} \quad M_2(\theta) = \frac{mF_2(\theta)}{F_1(\theta) + F_2(\theta)}$$

**$M_1(\theta), M_2(\theta)$  are depths of space modulation (DoSM)**

## (2) Radio landing systems

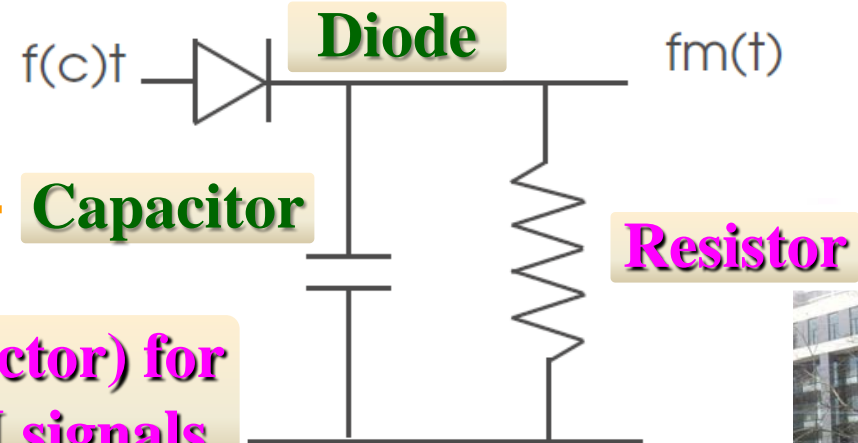


- The airborne ILS equipment extracts the modulation envelopes of 90 Hz and 150 Hz, and determines the difference in modulation envelope amplitudes which is proportional to the difference in depth of modulation (DDM). If the aircraft flies in the ESD, then  $DDM = 0$ .

Modulating (baseband) signal:

$$M_1(\theta)\cos \Omega_1 t + M_2(\theta)\cos \Omega_2 t$$

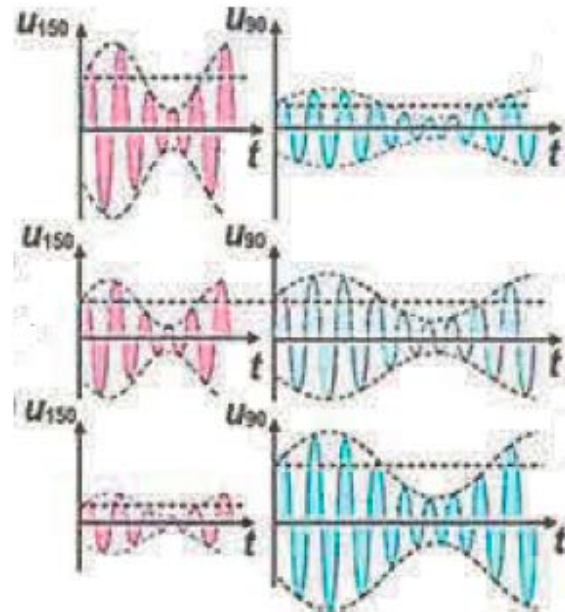
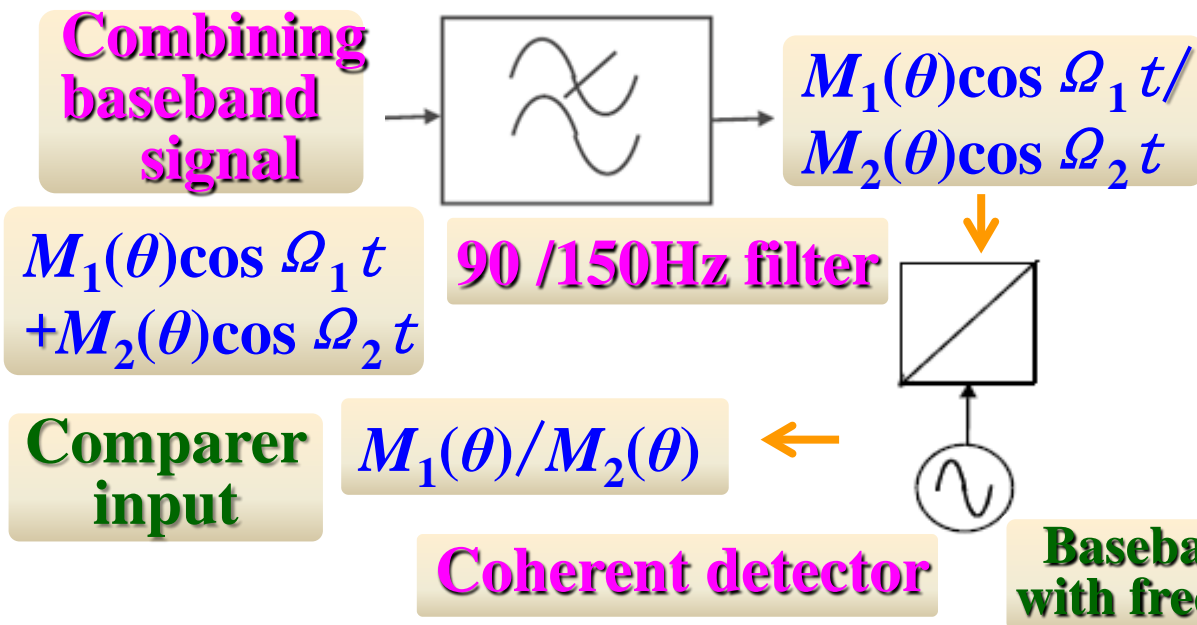
Envelope detector (extractor) for demodulating DSB-AM signals



## (2) Radio landing systems



- The **difference in depth of modulation (DDM)** is finally derived from a comparer:  $DDM = M_1(\theta) - M_2(\theta)$   
 $= m[F_1(\theta) - F_2(\theta)] / [F_1(\theta) + F_2(\theta)]$



Baseband signal  
with freq. of 150Hz

Baseband signal  
with freq. of 90Hz