

$$1a) \quad S_l = 0,005 \text{ m}^3$$

$$2\% : 0,005 \cdot 0,02 = 0,0001 \text{ m}^3$$

$$\text{Zylinder Volume: } V = \pi r^2 L = \frac{\pi d^2 L}{4}$$

$$\Rightarrow L = \frac{4V}{\pi d^2} \approx \underline{\underline{2,598 \cdot 10^6 \text{ m}}}$$

b)

$$N = \frac{L}{l} = \frac{2,598 \cdot 10^6}{1,2 \cdot 10^{-3}} = \underline{\underline{2,165 \cdot 10^9 \text{ capillaries}}}$$

c)

$$Q = \frac{\pi R^4}{8\mu_{\text{eff}}} \frac{\Delta p}{L}$$

$$\Delta p = \frac{8\mu_{\text{eff}} L Q}{\pi R^4} \approx \underline{\underline{26\,72,69 \text{ Pa}}}$$

$$\approx \underline{\underline{20,047 \text{ mmHg}}}$$

$$Q = \frac{4,5 \text{ l/min}}{2 \cdot 10^9} = \frac{0,0045/60 \text{ m}^3/\text{s}}{2 \cdot 10^9} = 3,75 \cdot 10^{-14} \text{ m}^3/\text{s}$$

$$L = 1,2 \cdot 10^{-3} \text{ m}$$

$$R = 3,5 \cdot 10^{-6} \text{ m}$$

$$\mu_{\text{eff}} = 0,0035 \text{ Pa}\cdot\text{s}$$

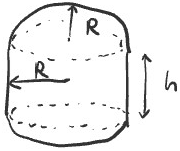
$$\Delta p_{\text{tot}} = 85 \text{ mmHg}$$

$$\frac{\Delta p}{\Delta p_{\text{tot}}} \approx \underline{\underline{23,59 \%}}$$

2 a)

$$V_{\text{sphere}} = \frac{4\pi R^3}{3} \Rightarrow R = \sqrt[3]{\frac{3V}{4\pi}} \approx \underline{\underline{2,86 \mu\text{m}}}$$

b)



min, mum pore radius is there for R

$$V_{\text{tot}} = \frac{4\pi R^3}{3} + \pi R^2 h$$

$$A_{\text{tot}} = 4\pi R^2 + 2\pi R h$$

$$h = \frac{A_{\text{tot}} - 4\pi R^2}{2\pi R}$$

$$V_{\text{tot}} = \frac{4\pi R^3}{3} + \pi R^2 \left( \frac{A_{\text{tot}} - 4\pi R^2}{2\pi R} \right)$$

$$V_{\text{tot}} = \frac{4\pi}{3} R^3 + \frac{A_{\text{tot}}}{2} R - 2\pi R^3$$

$$-\frac{2\pi}{3} R^3 + \frac{A_{\text{tot}}}{2} R - V_{\text{tot}} = 0$$

$$\Leftrightarrow \boxed{R^3 - \frac{3A_{\text{tot}}}{4\pi} R + \frac{3V_{\text{tot}}}{2\pi} = 0}$$

$$R \approx \begin{cases} -6,21 \mu\text{m} \\ \underline{\underline{1,65 \mu\text{m}}} \\ 4,55 \mu\text{m} \end{cases}$$

c) As shown in a) and b) non-spherical red blood cells can pass through smaller pores even if the volume of the blood cells are the same. This ensures better blood flow and therefore oxygen transport.

3a)

$$\tau = \tau_y + \mu \dot{\gamma} \quad | \quad \dot{\gamma} = \frac{dv}{dr}$$

$$\tau(r) = \frac{r}{2} \frac{dp}{dx} \quad \dots \text{steady flow}$$

$$\Rightarrow \frac{r}{2} \frac{dp}{dx} = \tau_y + \mu \frac{dv}{dr}$$

$$\mu dv = \left( \frac{r}{2} \frac{dp}{dx} - \tau_y \right) dr$$

$$v = \frac{1}{\mu} \int \left( \frac{r}{2} \frac{dp}{dx} - \tau_y \right) dr$$

$$v = \frac{1}{\mu} \left( \frac{r^2}{4} \frac{dp}{dx} - \tau_y r + c \right)$$

$$v(R) = 0 = \frac{1}{\mu} \left( \frac{R^2}{4} \frac{dp}{dx} - \tau_y R + c \right)$$

$$\Rightarrow c = \tau_y R - \frac{R^2}{4} \frac{dp}{dx}$$

$$\Rightarrow v(r) = \frac{1}{\mu} \left( \frac{1}{4} \frac{dp}{dx} (r^2 - R^2) - \tau_y (r - R) \right)$$

b)

$$\tau_y = \frac{R_c}{2} \frac{dp}{dx} \quad \left| \quad \hat{r} = \frac{r}{R} \quad ; \quad \hat{R}_c = \frac{R_c}{R} \right.$$

$$\frac{dp}{dx} = \frac{2\tau_y}{R_c}$$

$$v(\hat{r}) = \frac{R\tau_y}{\mu} \left( \frac{1}{2\hat{R}_c} (\hat{r}^2 - 1) - \hat{r} + 1 \right)$$

$$v(\hat{R}_c) = \frac{R\tau_y}{\mu} \left( \frac{1}{2\hat{R}_c} (\hat{R}_c^2 - 1) - \hat{R}_c + 1 \right) = \frac{R\tau_y}{\mu} \left( 1 - \frac{\hat{R}_c}{2} - \frac{1}{2\hat{R}_c} \right)$$

$$Q = \int_0^{\hat{R}_c} v(\hat{R}_c) 2\pi r dr + \int_{\hat{R}_c}^1 v(\hat{r}) 2\pi r dr = \left| dr = R d\hat{r} \right.$$

$$= 2\pi R^2 \left( \int_0^{\hat{R}_c} v(\hat{R}_c) \hat{r} d\hat{r} + \int_{\hat{R}_c}^1 v(\hat{r}) \hat{r} d\hat{r} \right) =$$

$$= \frac{2\pi R^3 \tau_y}{\mu} \left( \int_0^{\hat{R}_c} \left( 1 - \frac{\hat{R}_c}{2} - \frac{1}{2\hat{R}_c} \right) \hat{r} d\hat{r} + \int_{\hat{R}_c}^1 \left( \frac{1}{2\hat{R}_c} (\hat{r}^2 - 1) - \hat{r} + 1 \right) \hat{r} d\hat{r} \right) =$$

$$= \frac{2\pi R^3 \tau_y}{\mu} \left( \frac{\hat{R}_c^2}{2} \left( 1 - \frac{\hat{R}_c}{2} - \frac{1}{2\hat{R}_c} \right) + \frac{1}{2\hat{R}_c} \left( \frac{\hat{r}^4}{4} - \frac{\hat{r}^3}{3} \right) - \frac{\hat{r}^3}{3} + \frac{\hat{r}^2}{2} \right) \Bigg|_{\hat{R}_c}^1 =$$

$$= \frac{2\pi R^3 \tau_y}{\mu} \left( \frac{\hat{R}_c^2}{2} - \frac{\hat{R}_c^3}{4} - \frac{\hat{R}_c}{4} + \left( -\frac{1}{8\hat{R}_c} + \frac{1}{6} - \left( \frac{\hat{R}_c}{8} - \frac{\hat{R}_c^2}{4} - \frac{\hat{R}_c^3}{3} + \frac{\hat{R}_c^2}{2} \right) \right) \right)$$

$$= \frac{2\pi R^3 \tau_y}{\mu} \left( -\frac{1}{8\hat{R}_c} + \frac{1}{6} - \frac{\hat{R}_c^3}{24} \right)$$

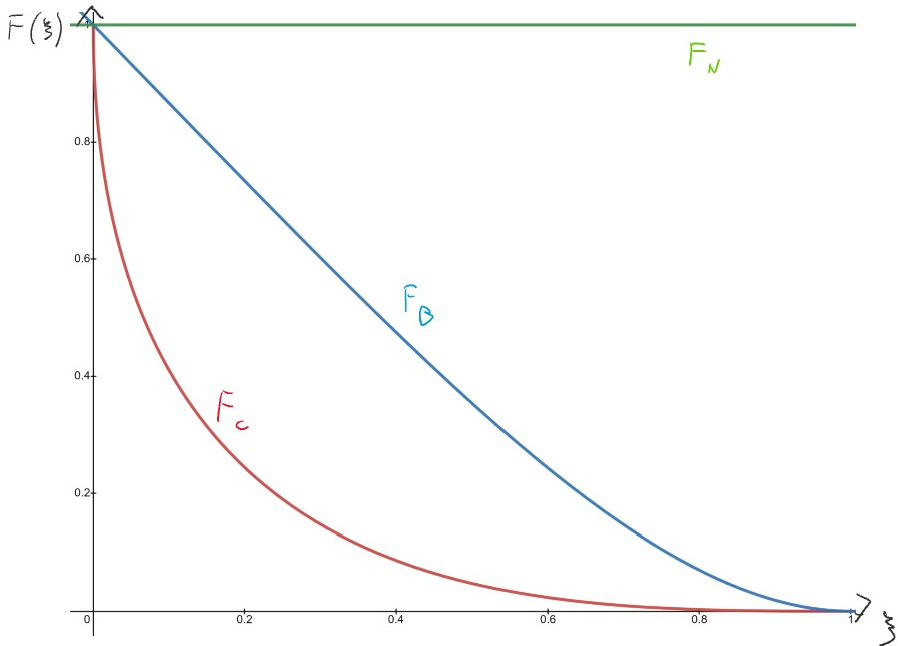
$$= -\frac{2\pi R^3 \tau_y}{8\mu \hat{R}_c} \left( \frac{1}{3} \hat{R}_c^3 - \frac{4}{3} \hat{R}_c + 1 \right) \quad \left| \quad \tau_y = \frac{R\hat{R}_c}{2} \frac{dp}{dx} \right.$$

$$Q = -\frac{\pi R^4}{8\mu} \frac{dp}{dx} F(\hat{R}_c), \quad F(\hat{R}_c) = \frac{1}{3} \hat{R}_c^3 - \frac{4}{3} \hat{R}_c + 1$$

c)  $F_B(\xi) = \frac{1}{3} \xi^3 - \frac{4}{3} \xi + 1 \dots$  Bingham

$F_C(\xi) = 1 - \frac{16}{7} \sqrt{\xi} + \frac{4}{3} \xi - \frac{1}{27} \xi^3 \dots$  Casson

$F_N(\xi) = 1 \dots$  Newtonian



It can be seen from the plot, that the flow rate of a Bingham-Fluid lies between the flowrate of a Newtonian-Fluid and a Casson-Fluid.

(assuming all other variables to be equal) For small  $\xi$  ( $\xi \rightarrow 0$ ) they all tend towards 1 ( $F(\xi) \rightarrow 1$ ) and for  $\xi \rightarrow 1$  the Bingham and Casson flow rate both approach zero ( $F(\xi) \rightarrow 0$ ).

This difference is due to the difference in the shear stress