

# **MASTER THESIS**

Thesis submitted in fulfillment of the requirements for the degree of  
Master of Science in Engineering at the University of Applied Sci-  
ences Technikum Wien - Degree Program Robotics Engineering

## **Alogrithmic Payload Estimation**

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Vienna, November 27, 2025

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# Kurzfassung

Im Kontext der digitalen Fabrik an der UAS Technikum Wien, wo Menschen und Roboter sich die Aufgaben und den Arbeitsbereich teilen, ist die sichere und effiziente Handhabung von Nutzlasten von entscheidender Bedeutung. In der digitalen Fabrik der UAS werden Nutzlasten derzeit noch ohne Kenntnis ihrer internen Parameter gehandhabt, was zu potenziellen Manipulationsfehlern führen kann, die Menschen Schaden zufügen. Diese Studie beschreibt die Entwicklung einer fortschrittlichen Methode zur Kraft-/Drehmomentabschätzung, um die Fähigkeit eines UR5-Roboters zu verbessern, verschiedene Nutzlastbedingungen zu erkennen und zu handhaben. Diese Fähigkeit gewährleistet die Wahrnehmung des auf einer mobilen Industrieroboterplattform montierten UR5-Roboters, um den sicheren und effizienten Transfer von Nutzlasten zwischen verschiedenen Arbeitsbereichen innerhalb der Fabrik zu erleichtern. Die modernsten Methoden zur Kraft-/Drehmomentabschätzung für Industrieroboter nutzen neuronale Netze und Gauß-Prozesse als führende Methoden für genaue Nutzlastabschätzungen. Es wurde ein Gauß-Prozess-Modell entwickelt, um die Kräfte und Drehmomente abzuschätzen, die vom Roboter bei der Ausführung von Trajektorien erzeugt werden. In einem zukünftigen Projekt kann das Bewusstsein für Nutzlasten auf dem UR5-Roboter hinzugefügt werden. Auf diese Weise zielt die Studie darauf ab, die Intelligenz von Robotersystemen in industriellen Umgebungen zu verbessern und den Weg für eine höhere Produktivität und Sicherheit in digitalen Fertigungsumgebungen zu ebnen. Dieses Projekt führte auch zu einer Simulation, die eine Grundlage für die Aufzeichnung der Sensordaten aus dem UR5-Interieur.

**Schlagworte:** Gaussian Process, Force Estimation, Newton/Euler, UR5 Robot, Rigid Body

# Abstract

In the context of the digital factory, at UAS Technikum Vienna, where humans and robots share the tasks and the workspace, the safe and efficient handling of payloads is essential. At the UAS digital factory payload is still handled without recognising anything about the payloads internal parameters, leading to potential manipulation failures causing human harm. This study describes the development of an advanced force/torque estimation method to improve a UR5 robots ability to recognize and handle different payload conditions. This capability ensures the perception of the UR5 robot mounted on a mobile industrial robot platform to facilitate the safe and efficient transfer of payloads between different workspaces within the factory. The state of the art methods of force/torque estimation for industrial robots serve neuronal networks and gaussian processes as the leading methods for accurate payload estimations. A gaussian process model has been developed to estimate the forces and torques generated by the robot when executing trajectories. In a future project face, an awareness of payloads can be added on the UR5 robot. In this way, the study aims to improve the intelligence of robotic systems in industrial environments and pave the way for higher productivity and safety in digital manufacturing environments. This project face also yeelted in a simulation that provides a basis to record the sensor data from the UR5's internal sensors and a force/torque sensor and a pipeline to train and evaluate gaussian process models.

**Keywords:** Gaussian Process, Force Estimation, Newton/Euler, UR5 Robot, Rigid Body

# Acknowledgements

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# 1 Introduction

This chapter provides the common thread of the work and positions it within the broader field of robotic manipulation and human-robot collaboration. We first develop the motivation for the study, followed by a precise problem description, a formal problem statement, and the resulting aim of the work. Subsequent chapters present the State of the Art, the proposed methods, the experimental evaluation, a discussion of the results and their implications, and an outlook on future research directions.

## 1.1 Motivation

The motivation for this work is given in two subsections, where the Context subsection outlines the growing role of industrial and collaborative manipulators, while the Use Case subsection specifies a concrete manipulation scenario that requires accurate online identification of robot and payload parameters.

### 1.1.1 Context

As the robotics industry grows year over year, so does the number of robots operating around the world. It is estimated that there were approximately 3.4 million industrial robots in use worldwide in 2023 [1]. At the same time, the number of newly installed industrial robots has been increasing steadily since 2014; between 2021 and 2024, around 541 000 new industrial robots were installed per year [2]. Within this landscape, collaborative robots (cobots) represent about 10.5% of the industrial robot market, with 57 040 new units deployed in 2023, and annual cobot installations since 2020, 2022, and 2023 reaching roughly 50 000 units per year; importantly, these cobots are expected to complement rather than replace traditional industrial robots [3].

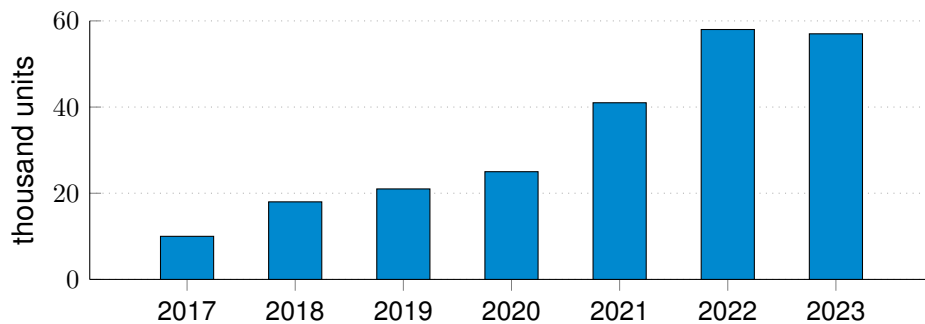


Figure 1: Global annual installations of collaborative robots from 2017 to 2023 (in thousand units). Data from [3].

The growing deployment of, and increasing collaboration with, robots imposes stringent requirements on safety and performance. As tasks become more complex and humans and robots share workspaces more closely, two closely related problems become central: safe manipulation of payloads and safe physical human-robot interaction. Addressing both problems requires accurate knowledge of the inertial parameters of the manipulated object together with consistent estimation of the robot's dynamic state and interaction forces. A collaborative robot must therefore maintain an internal representation of the mass-inertia properties of the payload or tool it manipulates and of the forces exchanged with its environment. This dynamic awareness is a prerequisite for compliant, contact-rich behaviour and for precise, high-performance manipulation in close proximity to humans. [4–15].

### 1.1.2 Use Case

The considerations above motivate a concrete use case in which a collaborative robotic arm must manipulate previously unseen objects in a shared workspace. A vision system can provide geometric information such as shape and dimensions of the payload, but it does not directly reveal its mass, center of mass (CoM), or inertia tensor. For safe and precise execution of contact-rich tasks, however, these inertial properties are indispensable.

In practice, the only viable way to obtain this information during operation is to exploit the robot's own sensor data, such as joint positions, velocities and accelerations, motor currents/torques, and optionally wrist force/torque measurements. From these signals, one can estimate both the robot's rigid-body parameters and the inertial properties of the attached payload. This leads to the dual identification problem of robot dynamic parameter identification (RDPI) and payload dynamic parameter identification (PDPI).

The targeted application scenario comprises typical industrial and collaborative tasks such as pick-and-place, human-assisted manipulation, and precise tool use. In all these cases, RDPI and PDPI must be performed online so that the controller maintains an up-to-date model of the combined robot-payload dynamics and the resulting contact forces. Robust online identification methods are therefore a key enabling technology for safe human-robot collaboration and high-performance manipulation with arbitrary payloads and tools.

Next is: use case, problem description (mathematical background), problem statement, contribution. Then state of the art.

## 1.2 Problem Statement

The subsection Kinematic and Dynamic Background of Robot Manipulation and Environment Interaction analyses why endowing a robotic manipulator with awareness of its own dynamics, payload, and tools is mathematically demanding and cannot be achieved by simple calculation or direct measurement alone. The subsection Limitations of the Current State of the Art then identifies the main shortcomings of existing identification and estimation methods in the literature, thereby motivating the contribution of this work.



### 1.2.1 Kinematic and Dynamic Background of Robot Manipulation and Environment Interaction

The inertial properties of a rigid body are collected in the standard 10-dimensional parameter vector

$$\phi^T = \begin{bmatrix} m & mc_x & mc_y & mc_z & J_{xx} & J_{xy} & J_{xz} & J_{yy} & J_{yz} & J_{zz} \end{bmatrix} \in \mathbb{R}^{10}, \quad (1)$$

which enters the Newton-Euler equations

$$\begin{bmatrix} \mathbf{f} \\ \boldsymbol{\tau} \end{bmatrix} = m \begin{bmatrix} \mathbf{I}_{3 \times 3} & -[\mathbf{c}]^\times \\ [\mathbf{c}]^\times & \mathbf{J}_s \end{bmatrix} \begin{bmatrix} \mathbf{a} \\ \boldsymbol{\alpha} \end{bmatrix} + \begin{bmatrix} m[\boldsymbol{\omega}]^\times [\boldsymbol{\omega}]^\times \mathbf{c} \\ [\boldsymbol{\omega}]^\times \mathbf{J}_s \boldsymbol{\omega} \end{bmatrix}, \quad (2)$$

so that the wrench  $(\mathbf{f}, \boldsymbol{\tau})$  depends nonlinearly on the motion  $(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega})$  but linearly on  $\phi$ .

For the equipment rigidly attached to the tool flange (gripper/tool, with or without payload/load) we define an effective rigid-body parameter vector

$$\phi_{\text{eff}} = \begin{cases} \phi_{\text{tool}}, & \text{no load,} \\ \phi_{\text{tool}} + \phi_{\text{load}}, & \text{with load,} \end{cases} \quad (3)$$

which acts on top of the nominal robot dynamics. In contrast, with a clean flange (no tool/no load) only the robot parameters  $\phi_{\text{robot}}$  contribute to the system dynamics.

The robot structure itself is described by its own parameter vector  $\phi_{\text{robot}}$ , which enters the standard joint-space rigid-body dynamics. We denote this contribution by  $\boldsymbol{\tau}_{\text{robot}}$  (clean flange),

$$\boldsymbol{\tau}_{\text{robot}} = \mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) + \boldsymbol{\tau}_f(\dot{\mathbf{q}}), \quad (4)$$

where  $\boldsymbol{\tau}_f(\dot{\mathbf{q}})$  models joint-level non-idealities such as Coulomb and viscous friction, possible Stribeck effects, and drive-train phenomena like backlash.

The wrench generated by the effective rigid body at the flange induces an additional joint-space torque

$$\boldsymbol{\tau}_{\text{ext}} = \mathbf{J}^T(\mathbf{q}) \vec{F}_{\text{ext}}(\phi_{\text{eff}}), \quad (5)$$

where  $\mathbf{J}(\mathbf{q})$  is the end-effector Jacobian. In the clean-flange case (no tool/no load),  $\vec{F}_{\text{ext}}$  reduces to purely external interaction forces with the environment (e.g. contacts or collisions).

The motor torques are therefore

$$\boldsymbol{\tau}_{\text{motor}} = \boldsymbol{\tau}_{\text{robot}} + \boldsymbol{\tau}_{\text{ext}}(\phi_{\text{eff}}), \quad (6)$$

and for brushless DC actuators with torque constant  $k_t$  one obtains the current–torque relation

$$\boldsymbol{\tau}_{\text{motor}} = k_t \mathbf{I} \quad \Rightarrow \quad \mathbf{I} = \frac{\boldsymbol{\tau}_{\text{robot}} + \boldsymbol{\tau}_{\text{ext}}(\phi_{\text{eff}})}{k_t}. \quad (7)$$

If a force/torque sensor is mounted at the flange, the measured wrench can be written, using the relations derived in the Appendix, as

$$\vec{F}_{\text{measured}} = Y(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega}) \phi_{\text{eff}} + \vec{F}_{\text{bias}} + \vec{n}, \quad (8)$$

where  $Y(\cdot)$  is the  $6 \times 10$  Newton-Euler regressor matrix defined in the Appendix. It is linear in the inertial parameter vector  $\phi_{\text{eff}}$ , but depends nonlinearly on the motion variables  $(\mathbf{a}, \alpha, \omega)$ . The terms  $\vec{F}_{\text{bias}}$  and  $\vec{n}$  denote sensor bias and noise, respectively.<sup>1</sup> The motion variables  $(\mathbf{a}, \alpha, \omega)$  are in turn determined by the joint state and motor torques through the nonlinear dynamics (4)–(7).

From an identification viewpoint, this creates two tightly coupled challenges. First, all available measurements (joint currents, positions, velocities and flange wrench) depend on the combined dynamics of robot, tool and load via the nonlinear relationships (4)–(8), so the contribution of the load parameters  $\phi_{\text{load}}$  cannot be isolated by simple computation or direct measurement. Second, accurate payload or load dynamic parameter identification (PDPI) presupposes an equally accurate compensation of the underlying robot–tool dynamics, including unmodelled effects such as friction and joint transmission nonlinearities. Together, these aspects make dynamic awareness of payload, tool and robot a mathematically demanding inverse problem rather than a straightforward calculation from geometric or sensor data.

## 1.2.2 Limitations of the Current State of the Art

From the Q1 literature review in Section 2.2, several limitations are particularly relevant for this work:

- **Separate treatment of robot, tool and payload.** Most approaches either perform robot dynamic parameter identification (RDPI) in joint or motor space [13, 16, 17], payload dynamic parameter identification (PDPI) in the FT frame [4, 7, 8, 11], or sensorless interaction-force estimation via observers [6, 14, 18–20], but they rarely provide a unified view of robot, tool and payload dynamics.
- **Payload inertia is hard to identify robustly.** While payload mass (and often CoM) can be estimated accurately, inertia tensors are frequently weakly excited, poorly conditioned or only partially validated, in particular under cobot-safe excitation [4, 7, 8, 11, 21].
- **Heavy reliance on dedicated excitation and offline calibration.** Strong RDPI/PDPI results typically require carefully designed, long trajectories executed with and without payload and substantial offline processing [4, 7–10, 13, 16, 17, 21], which is at odds with continuous online awareness during everyday collaborative tasks.
- **Sensitivity to friction and transmission nonlinearities.** Observer-based force estimators and classical LS/NE pipelines depend on reasonably accurate friction and transmission models; residual errors increase around velocity reversals and at higher speeds, even when advanced observers or learned friction models are used [6, 16–20].

These limitations show that, within Q1, there is still no compact, online representation of robot, tool and payload dynamics that is robust to friction and transmission effects and applicable under normal cobot operating conditions.

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<sup>1</sup>All experiments in this work are simulation-based; in the subsequent method formulation, sensor bias and noise are therefore neglected and (8) is used without  $\vec{F}_{\text{bias}}$  and  $\vec{n}$ .

## 2 State of the Art

### 2.1 Research Strategy

The literature search was organised around five content clusters  $C_1, \dots, C_5$  and the goal/context term sets  $C_{mt}$  and  $C_{ct}$ . The clusters capture the main methodological families, while  $C_{mt}$  and  $C_{ct}$  constrain the queries to estimation-related objectives in robotic manipulation:

- $C_1$  = Classical / Observers
- $C_2$  = Gaussian Process (GP)
- $C_3$  = Deep Sequence Models (MLP / GRU / TCN / Transformer / LSTM)
- $C_4$  = Physics-Informed / Differentiable
- $C_5$  = Surveys
- $C_T$  = Goal & Domain Terms
  - $C_{mt}$  = Estimation & Modeling Terms
  - $C_{ct}$  = Robotics Context Terms

The detailed index terms associated with each set are listed in Appendix B. For each content cluster  $C_i$ , a family of queries  $Q_i$  was constructed by combining (disjunctions of) its index terms with estimation & modelling terms from  $C_{mt}$  and robotics context terms from  $C_{ct}$ . Figure 2 illustrates this logic schematically as a generalised set intersection over the three term groups.

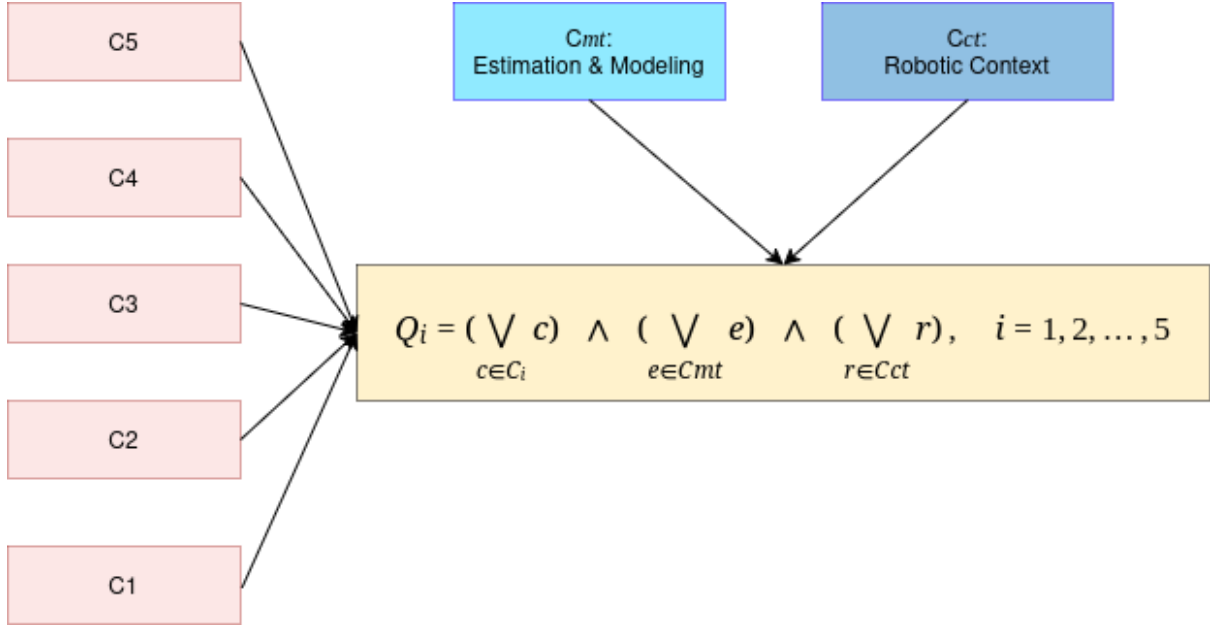


Figure 2: Query logic used to categorise the SoA papers. Each category  $Q_i$  is formed by combining content clusters  $C_i$  with estimation & modelling terms  $C_{mt}$  and robotics context terms  $C_{ct}$ . The combined representation  $C$  and query set  $Q$  are formed by the union of their respective subsets.

This process yielded 36 papers that are directly relevant to robot and payload dynamics, interaction force estimation and related identification problems. Table 1 summarises how these works are distributed across the five query categories and distinguishes whether each paper focuses on robot rigid-body dynamics, payload dynamics, or both.

Table 1: Overview of query results by category.

Query	Relev. SoA	Rigid-body	Payload	Both
$Q_1$ = Classical / Observers	17	7	7	3
$Q_2$ = Gaussian Process (GP)	4	4	0	0
$Q_3$ = Deep Sequence Models	8	4	4	0
$Q_4$ = Physics-Informed / Diff.	5	5	0	0
$Q_5$ = Surveys	2	—	—	—
<b>Total</b>	<b>36</b>	<b>20</b>	<b>11</b>	<b>3</b>

## 2.2 SoA for Q1

Category Q1 groups classical model-based methods for robot and payload dynamics and interaction force estimation, mostly based on linearly parameterised rigid-body dynamics (RBD) and LS/WLS-type Newton-Euler regressors, sometimes combined with observers and Kalman filters [4–11, 13, 14, 16–21]. Across these works, three main lines of research can

be distinguished: (i) payload dynamic parameter identification (PDPI) using force/torque (FT) sensing [4, 7, 8, 11], (ii) robot and payload dynamic parameter identification in joint or motor-current space without FT sensors [9, 10, 13, 16, 17, 21], and (iii) observer-based sensorless force/torque estimation and online payload identification using proprioceptive data [5, 6, 14, 18–20]. Across Q1, mass is usually identified accurately, CoM moderately well, and inertia emerges as the hardest quantity to estimate robustly [4, 7, 8, 11, 21].

A first group of methods performs PDPI directly in the FT frame [4, 7, 8, 11]. They typically exploit static poses to identify the payload mass and centre of mass, and then use dedicated dynamic excitation trajectories together with LS or TLS-type Newton-Euler regressors to estimate the inertia tensor. Representative works demonstrate that, given a sufficiently informative excitation and an FT sensor rigidly mounted at the flange, payload mass can be recovered very accurately and CoM can be estimated with reasonable precision, even for heavy payloads [4, 8]. However, inertia estimates are systematically more fragile—especially under cobot-typical safety constraints with short trajectories and low accelerations—and in several cases quantitative ground truth for CoM and inertia is missing or only partially available (validation is often given in terms of residual gravitational/inertial wrench after compensation rather than direct parameter error) [4, 7, 8, 11]. Moreover, these approaches require additional FT hardware and considerable experimental effort in the form of carefully designed calibration motions.

A second group tackles robot dynamic parameter identification (RDPI) and PDPI in joint space or motor-current space without FT sensors [9, 10, 13, 16, 17, 21]. Here, fully or partially decoupled identification schemes are designed to separate gravitational, frictional and inertial effects, often using families of S-curve or Fourier trajectories executed both with and without payload [9, 10, 13, 16]. Double-weighted WLS and optimisation-enhanced LS methods achieve very accurate joint-torque prediction and good agreement with CAD-based payload models, confirming that classical LS/NE pipelines—as systematised, for example, by Swevers et al. [13]—remain a strong baseline for RDPI and PDPI [9, 10, 13, 16, 17, 21]. At the same time, most of these methods are offline, rely on repeated execution of long, highly exciting trajectories, and assume that payloads are rigidly mounted and change only between identification runs; even in works that introduce an online payload-identification stage [21], the base robot model is still obtained by an offline procedure. They therefore provide an excellent commissioning tool, but do not by themselves endow the robot with continuous online awareness of changing tools and payloads during normal task execution.

A third line of work focuses on sensorless estimation of external joint torques and end-effector wrenches using observers and filters [6, 14, 18–20]. Momentum observers, higher-order sliding-mode observers, adaptive Kalman filters and high-order finite-time observers use a nominal RBD model together with controller torques and joint measurements to reconstruct external forces, sometimes with probabilistic covariance information. These methods achieve good performance in collision detection, binary contact decisions and execution monitoring, and some approaches augment classical friction models with learned nonlinear terms such as neural-network Stribeck approximations [6, 14, 20]. Nevertheless, their accuracy depends critically on the quality of the underlying RBD and friction models, and residual force errors remain significant in highly dynamic phases or around velocity reversals [6, 19, 20]. Importantly, most

observer-based schemes treat payloads and tools as fixed parts of the nominal model or as lumped disturbances, and do not explicitly estimate payload parameters.

More recent contributions bridge RDPI/PDPI and observer-based estimation by using proprioceptive data to identify payload parameters online [5, 21]. Momentum-observer-based schemes and parameter-difference methods compute external joint torques as residuals between measured and model-based torques and apply LS/RLS Newton-Euler regressors to recover payload mass, CoM and, in some cases, inertia during regular robot operation. These works demonstrate that accurate online PDPI is possible without FT sensors, provided that a reasonably accurate base robot model, friction compensation and sufficiently exciting motions are available [5, 21]. At the same time, they underline several structural limitations: inertia remains the hardest quantity to identify robustly; nonlinear friction, backlash and transmission effects must be modelled or learned carefully (with several authors explicitly noting residual error peaks near motion reversal due to unmodelled friction [13, 17]); and the resulting estimators still rely on a clear separation between “robot model” and “payload” rather than providing a unified, continuously updated representation of robot, tool and load.

Taken together, the Q1 literature shows that classical model-based techniques can deliver high-quality RDPI and PDPI, as well as useful sensorless interaction-force estimates, but typically only under carefully controlled excitation and with significant offline calibration [4, 7–10, 13, 16, 17, 19–21]. From the perspective of this work, the main gaps are the lack of a unified, online notion of dynamic awareness that jointly covers robot, tool and payload; the persistent difficulty of reliably identifying and exploiting payload inertia in cobot-safe regimes; and the sensitivity of existing approaches to friction and transmission nonlinearities. These limitations directly motivate the methodological choices and objectives formulated in the problem statement and aim of work.

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# A Appendix Kinematic and Dynamic Background of Robot Manipulation and Environment Interaction

The external wrench  $\vec{F}_{\text{ext}}$  in (5) is a 6-dimensional vector expressed in the sensor/tool frame  $S$ ,

$$\vec{F}_{\text{ext}} = \begin{bmatrix} \mathbf{f} \\ \boldsymbol{\tau} \end{bmatrix} \in \mathbb{R}^6, \quad (9)$$

with  $\mathbf{f} \in \mathbb{R}^3$  the linear force and  $\boldsymbol{\tau} \in \mathbb{R}^3$  the moment about the frame origin. For a rigid body with parameters  $\phi_{\text{eff}}$  (mass, CoM and inertia) moving with linear and angular motion  $(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega})$ , the Newton–Euler equations (cf. (2)) give

$$\begin{bmatrix} \mathbf{f} \\ \boldsymbol{\tau} \end{bmatrix} = m \begin{bmatrix} \mathbf{I} & -[\mathbf{c}]^\times \\ [\mathbf{c}]^\times & \mathbf{J}_s \end{bmatrix} \begin{bmatrix} \mathbf{a} \\ \boldsymbol{\alpha} \end{bmatrix} + \begin{bmatrix} m[\boldsymbol{\omega}]^\times [\boldsymbol{\omega}]^\times \mathbf{c} \\ [\boldsymbol{\omega}]^\times \mathbf{J}_s \boldsymbol{\omega} \end{bmatrix}. \quad (10)$$

The translational part  $\mathbf{f}$  can be written as

$$\mathbf{f} = m\mathbf{a} - m[\mathbf{c}]^\times \boldsymbol{\alpha} + m[\boldsymbol{\omega}]^\times [\boldsymbol{\omega}]^\times \mathbf{c}, \quad (11)$$

where the first term  $m\mathbf{a}$  is the familiar inertial force, while  $-m[\mathbf{c}]^\times \boldsymbol{\alpha}$  and  $m[\boldsymbol{\omega}]^\times [\boldsymbol{\omega}]^\times \mathbf{c}$  collect the additional centripetal and Coriolis contributions induced by the angular motion  $\boldsymbol{\omega}$  and the CoM offset  $\mathbf{c}$ . Similarly, the rotational part  $\boldsymbol{\tau}$  can be written as

$$\boldsymbol{\tau} = m[\mathbf{c}]^\times \mathbf{a} + \mathbf{J}_s \boldsymbol{\alpha} + [\boldsymbol{\omega}]^\times \mathbf{J}_s \boldsymbol{\omega}, \quad (12)$$

where  $\mathbf{J}_s \boldsymbol{\alpha}$  is the inertial moment due to angular acceleration,  $m[\mathbf{c}]^\times \mathbf{a}$  is the torque induced by the translational acceleration of the offset CoM, and  $[\boldsymbol{\omega}]^\times \mathbf{J}_s \boldsymbol{\omega}$  represents gyroscopic effects associated with the angular velocity  $\boldsymbol{\omega}$ .

In compact form, for a given motion  $(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega})$  this can be written as

$$\vec{F}_{\text{ext}} = \vec{F}_{\text{dyn}}(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega}; \phi_{\text{eff}}) = Y(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega}) \phi_{\text{eff}}, \quad (13)$$

where  $Y(\cdot)$  is a  $6 \times 10$  regressor matrix that is linear in  $\phi_{\text{eff}}$  but nonlinear in the motion variables. Hence,  $\vec{F}_{\text{ext}}$  is not simply  $m\mathbf{a}$ , nor can it be written as  $\phi_{\text{eff}} \ddot{\mathbf{q}}$ ; the mapping from joint accelerations  $\ddot{\mathbf{q}}$  to  $\vec{F}_{\text{ext}}$  passes through the robot kinematics and the Newton–Euler relations.

Once the wrench at the flange is known, the corresponding joint torques are obtained via

$$\boldsymbol{\tau}_{\text{ext}} = {}^S J(\mathbf{q})^\top \vec{F}_{\text{ext}}, \quad (14)$$

where  ${}^S J(\mathbf{q})$  is the Jacobian of the sensor/tool frame  $S$ . Combining the relations above yields the identification-friendly form

$$\boldsymbol{\tau}_{\text{ext}} = \mathbf{J}^T(\mathbf{q}) Y(\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega}) \boldsymbol{\phi}_{\text{eff}}, \quad (15)$$

which makes explicit that  $\boldsymbol{\tau}_{\text{ext}}$  is linear in  $\boldsymbol{\phi}_{\text{eff}}$ , but nonlinear in  $\mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}$  through the dependence on  $\mathbf{a}, \boldsymbol{\alpha}, \boldsymbol{\omega}$ .

## B Query Categories - Index Terms

This appendix lists the index terms used to construct the query categories illustrated in Fig. 2. The original nine term groups were consolidated into five content clusters  $C_1, \dots, C_5$  and the goal/context term sets  $C_{mt}$  and  $C_{ct}$ .

### Content Clusters $C_i$

#### $C_1$ : **Classical / Observers**

- momentum observer (MO)
- generalized momentum observer (GMO)
- disturbance observer (DOB)
- reaction force observer (RFOB)
- Kalman filter (KF)
- extended Kalman filter (EKF)
- unscented Kalman filter (UKF)
- state observer
- least squares (LS)
- weighted least squares (WLS)
- iterative reweighted least squares (IRLS)
- recursive least squares (RLS)
- momentum-based observer
- dynamic state observer
- observer
- force observer
- torque observer

## **$C_2$ : Gaussian Process (GP)**

- gaussian process regression (GPR)
- sparse gaussian process (SGP, SGPR)
- multi-output gaussian process (MOGP)
- multi-task gaussian process (MTGP)
- gaussian process state space model (GPSSM)
- hybrid gaussian process
- GP residual
- gaussian process dynamics
- GP inverse dynamics
- bayesian nonparametric regression (BNPR)

## **$C_3$ : Deep Sequence Models (MLP / GRU / TCN / Transformer / LSTM)**

- neural network inverse dynamics (NN-ID)
- deep learning
- multi layer perceptron (MLP)
- residual network (ResNet)
- long short-term memory (LSTM)
- gated recurrent unit (GRU)
- temporal convolutional network (TCN)
- causal convolution
- dilated convolution
- transformer model
- attention model
- sequence-to-sequence (seq2seq, S2S)
- sequence GAN (SeqGAN, TimeGAN)
- GAN
- Generative Adversarial Networks
- residual neural network (ResNN)

- residual GAN
- domain adaptation (DA)
- transfer learning (TL)
- meta learning (ML)
- context variable dynamics
- latent variable model (LVM)
- amortized inference (AI)
- test time adaptation (TTA)
- online adaptation (OA)
- feature invariance
- domain invariant features (DIF)
- few shot learning (FSL)
- zero shot transfer (ZSL)
- reinforcement
- reinforcement learning
- Isaac Gym differentiable
- Isaac Lab differentiable
- Isaac Gym
- Isaac Lab

#### **$C_4$ : Physics-Informed / Differentiable**

- residual learning dynamics
- hybrid model dynamics
- analytical dynamics neural network (ADNN)
- physics residual
- rigid body dynamics residual (RBD residual)
- Newton Euler residual (NE residual)
- nominal dynamics model (NDM)
- neural correction



- learning inverse dynamics residual (ID residual)
- physics-informed neural network (PINN)
- differentiable physics
- differentiable simulation (DiffSim)
- differentiable robot model
- differentiable dynamics
- neural ODE (NODE)
- torchdiffeq
- ODE-net
- physics-guided machine learning robotics (PGML)

#### $C_5$ : **Surveys**

- survey
- benchmarking
- review
- overview
- systematic comparison

## Goal & Domain Terms $C_T$

#### $C_{mt}$ : **Estimation & Modeling Terms**

- external force
- force measurement
- force estimation
- force/torque estimation
- wrench estimation
- joint torque estimation
- end-effector force
- end-effector torque
- inertial parameters

- inertial parameter identification (IPI)
- online payload identification
- payload identification
- payload estimation
- object parameter estimation
- parameter identification
- inertia tensor
- inertia tensor estimation
- center of mass (CoM)
- rigid body dynamics
- friction approximation
- nonlinear friction model
- external perturbations
- force torque sensor (F/T sensor)
- external force estimation (EFE)
- external torque estimation (ETE)
- torque estimation
- parameter identification differentiable simulation
- payload identification (PI)
- payload estimation (PE)
- contact force
- nonlinear systems
- noise
- signal noise
- noise estimation

Note that the last four entries (nonlinear systems, noise, signal noise, noise estimation) are generic terms that occur across many physical systems beyond robotic manipulators. Including them in the queries significantly increased the number of retrieved results.

$C_{ct}$ : **Robotics Context Terms**

- robotic manipulator
- robotic arm
- robotic manipulation
- robot payload