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# Motion Planning for Reconfigurable Magnetic Modular Cubes in the 2-Dimensional Special Euclidean Group

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### **Statement of Originality**

This thesis has been performed independently with the support of my supervisor/s. To the best of the author's knowledge, this thesis contains no material previously published or written by another person except where due reference is made in the text.

Braunschweig, April 21, 2023

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# Aufgabenstellung / Task Description

**Deutsch:** Um spezifische Aufgaben besser zu bewältigen, lassen sich modulare, rekonfigurierbare Roboter zu größeren Strukturen zusammensetzen und wieder auseinandernehmen. Magnetic-modular-cubes sind skalierbare Einheiten, bei welchen Permanentmagneten in einen würfelförmigen Körper eingebettet sind. Diese Einheiten zählen als rekonfigurierbare Roboter, obwohl sie selber keine Logik oder Stromversorgung beinhalten. Stattdessen lassen sich diese durch ein externes, gleichmäßiges und sich zeitlich änderndes Magnetfeld steuern. Durch diese Steuerung können die magnetic-cubes auf der Stelle gedreht oder durch pivot-walking nach rechts und links bewegt werden. Obwohl sich das Magnetfeld auf alle Einheiten gleichermaßen auswirkt, kann durch Kollision mit der Arbeitsflächenbegrenzung eine Änderung der Anordnung bewirkt werden. Befinden sich zwei magnetic-cubes nah genug beieinander können sich diese durch die Permanentmagneten miteinander verbinden und so Polyominos als größere Strukturen aufbauen, welche auf die gleiche Weise wie einzelne cubes gesteuert werden können. Frühere Arbeiten betrachteten das "tilt-model", bei welchem sich Strukturen jeder Größe mit gleicher Geschwindigkeit in ganzzahligen Schritten und mit ausschließen 90° Drehungen bewegen lassen.

Herr Keunes Aufgabe in dieser Bachelorarbeit ist es, einen motion-planner für die beschriebenen magnetic-cubes zu entwerfen, welcher mit beliebigen Positionen und Rotationen umgehen kann. Dabei ist es erforderlich, eine Simulationsumgebung zu schaffen, welche das Verhalten der magnetic-cubes repliziert. Es soll ein lokaler motion-planner entwickelt werden, um zwei Polyominos an gewünschten Kanten zu verbinden. Dieser local-planner soll Heuristiken und optimale Bewegungsabläufe mit möglichst wenig Schritten realisieren. Ebenfalls soll dieser global eingesetzt werden, um Bewegungsabläufe zu finden, die gewünschte Polyominos aus einer zufällig gegebenen Startkonfiguration erzeugen. Ein interessantes Ergebnis wird es sein, zu sehen, wie gut Problem instanzen dieser Art in der Realität gelöst werden können und welche Parameter die gravierendsten Auswirkungen auf die Schwierigkeit von motion-planning Problemen haben.

**English:** Reconfigurable modular robots can dynamically assemble/disassemble to better accomplish a desired task. Magnetic modular cubes are scalable modular subunits with embedded permanent magnets in a 3D-printed cubic body. These cubes can act as reconfigurable modular robots, even though they contain no power, actuation or computing. Instead, these cubes can be wirelessly controlled by an external, uniform, time-varying magnetic field. This control allows the cubes to spin in place or pivot walk to the left or right direction. Although the applied magnetic field is the same for each magnetic modular cube, collisions with workspace boundaries can be used to rearrange the cubes. Moreover, the cubes magnetically self-assemble when brought in close proximity of another cube, and form polyominoes, which can be controlled the same way as single cubes. Related work has considered the “tilt model,” where similar cubes and polyominoes move between integer positions, all move at the same speed, and only rotate by 90 degree steps.

In his thesis, Mr. Keune’s task is to design a motion planner for magnetic cubes that can assume arbitrary positions and orientations in the workspace. This requires designing a simulation environment that replicates the behavior of magnetic cubes. He will design local planners for moving two polyominoes to assemble at desired faces. Designing the local planner includes heuristics and computing optimal motion plans that minimize the number of steps. The local planner will be used to search for global planning sequences to generate desired polyominoes from a given starting configuration. One exciting outcome will be studying how well instances can be solved in practice and analyzing which parameters have the most significant effect on the difficulty of the motion planning problem.

# Abstract

Abstract





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# 1 Introduction

Self-assembling modular parts forming bigger structures is a well-known concept in nature and most functionalities of living organisms follow this principle [6]. DNA for example has the ability to self-replicate by using differently shaped proteins, that combine themselves in various ways. At larger sizes, these cells can be combined to assemble things like tissue, organs and even whole organisms. Complex structures can be assembled and disassembled depending on the task they should accomplish at a given point in time. Using self-reconfiguring robot swarms in such a way has promising applications in the future. Biomedical applications could be targeted drug delivery or drug screening [18], or a robot swarm could be used for milliscale and microscale manufacturing [14].

Designing robots at these small sizes faces challenging problems. Equipping each robot with its own sensors, actuation-system, connection-system and power supply seem infeasible, in terms of the miniaturization required and power-limitations [19]. Therefore, the use of external global control, effecting every robot in the workspace with the same torque and force, is a promising solution [19]. Using robots with embedded permanent magnets, has all the desired effects. Robots can be controlled by an external magnetic field and also connect to each other without any internal power supply and for sensing an external camera can be used [15].

One example for magnetically controlled robots are the magnetic modular cubes by Bhattacharjee et al. [5], which are the subjects of this thesis. We will develop a simulation that simulates the behavior of magnetic modular cubes, without assuming discrete movement or limiting rotations to a certain amount. The simulation will be used for developing closed-loop planning algorithms, which provide a control sequence to assemble desired target shapes. For that it is necessary to develop a local planner that is able to connect structures at desired faces. We will look at the difficulties and problems that occur, when working with magnetic modular cubes in the 2-dimensional special Euclidean group  $SE(2)$ , the space of rigid movements in a 2-dimensional plane.

## 1.1 Related Work

Continues motion planning is a crucial subject in the field of robotics. The goal is to find a path from the initial state of a robot to a desired goal state, by performing actions which the robot is capable of. The movement may result in collision with static obstacles and with other robots. The state of the system is also called a configuration. All possible configurations one or multiple robots can be in is defined as the configuration-space. Increasing the dimension of the configuration-space gains rapidly in complexity by increasing the number of robots and possible actions. It is difficult to engineer algorithms

## 1 Introduction

that explore these huge configuration-spaces and provide continuous path from the initial to the goal configuration, or report failure, if the goal is not reachable. A lot of research was done on motion planning and the textbooks [8] and [12] offer a great overview and also explain a lot of important concepts in detail.

When working with configuration-spaces that are uncountable infinite, like the special Euclidean group, one concept that has been successful for many robotics problem is sample-based motion planning. By taking samples, you can reduce the planning problem from navigating a configuration space to planning on a graph, but you might lose possible solutions. Algorithms like that are not complete anymore, but by using a good sampling technique you can get arbitrarily close to any point, and therefore these algorithms can be called resolution complete. Ways of sampling include random sampling or using a grid with a resolution that is dynamically adjustable. After sampling, conventional discrete planning algorithms can be applied [8].

One state-of-the-art sampling-based approach are algorithms that use rapidly-exploring random trees (RRT). This method tries to grow a tree-shaped graph in the configuration space by moving into the direction of randomly chosen samples from already explored configuration. That way the space gets explored uniformly without being too fixated on the goal configuration [9, 10].

When working with multiple robots, the interaction of robots with each other becomes important. One interesting idea is that single robots can connect to form bigger structures. This is referred to as self-assembly and E. Winfree [20] proposed the abstract Tile Assembly Model (aTAM) in the context of assembling DNA. In this model, particles can have different sets of glues and connect according to certain rules regarding the glue type. However, he considers this process as nondeterministic, so there is no exact instruction on how to assemble a desired structure.

One model more related to the magnetic modular cubes used in this thesis is the Tilt model from Becker et al. [2]. In the Tilt model, all tiles move into one of the cardinal directions until hitting an obstacle. Different variations of the model include moving everything only one step, or the maximally possible amount. It offers a solution when robots are controlled uniformly by external global control inputs.

In [2] it is shown that transforming one configuration into another, known as the reconfiguration-problem, is NP-hard. Caballero et al. [7] also researched complexity of problems regarding the Tilt model. Following work [3] also proves that finding an optimal control sequence, minimizing the number of actions, for the configuration-problem is PSPACE-complete. Furthermore, research is done on designing environments in which the Tilt model can be used to accomplish certain tasks. In particular, Becker et al. [3] create connected logic gates that can evaluate logical expressions.

More on the side of self-assembly, in [4] the construction of desired shapes using the tilt model is researched. It presents a method that can determine a building sequence for a polyomino by adding one tile at a time, considering the rules of Tilt. Also examined are ways of modifying the environment to create factories that construct shapes in a pipeline by repeating the same global control inputs. Shapes can be constructed more efficiently by combining multi-tiled shapes to an even bigger structure. One article considering the

construction with so-called sub-assemblies is proposed by A. Schmidt [17].

Most recently, Bhattacharjee et al. [5] developed the magnetic modular cubes. These robots contain embedded permanent magnets and have no computation or power supply. Instead, they are controlled by an external time-varying magnetic field and are able to perform various actions. Most importantly, they can rotate in place or use a technique called pivot walking to move either left or right. The magnets also act as glues and allow the cubes to perform self-assembly. Although it is theoretically possible to assemble 3-dimensional structures, most research was done by only connecting cubes in two dimensions. Since all cubes are the same size, the assembled 2-dimensional shapes can be represented as polyominoes. An enumeration was done on the amount of possible polyominoes that can be created by cubes with different magnet configurations [11].

By limiting the controls to only 90 degree turns and assuming a uniform pivot walking distance for all structures per step, magnetic modular cubes follow rules similar to the Tilt model. Following these limitations, a simple discrete motion planner was developed, that explores a finite configuration-space and lists all the possible polyominoes that can be created from an initial configuration [5]. One interesting paper from Blumenberg et al. [13] explores the assembly of polyominoes in arbitrary environments, when cubes obey the tilt model. He provides different algorithmic approaches using various distance heuristics and even a solution making use of RRTs. For that he follows the rules of Tilt in a discrete setting.

## 1.2 Contribution





## 2 Preliminaries

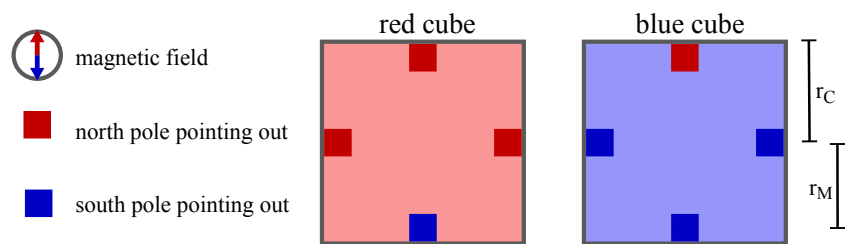


Figure 2.1: Simplified top-down view of the two magnetic modular cube types with their outward pointing magnet poles, illustrated as red and blue squares. Also visualizes the lengths  $r_C$  and  $r_M$

## 2.1 Magnetic Modular Cubes

The magnetic modular cubes are cube-shaped bodies embedded with permanent magnets on the four side faces. The magnets have different orientations of their north and south pole. One pole is always pointing outside and the other straight to the center of the cube. The magnet at the front face has its north pole pointing outwards and the magnet at the back its south pole. These two magnets ensure that the cube is always aligned with the global magnetic field and this orientation holds true for both cube types. The two other side faces must have the same outwards pointing pole, so that it is not possible for this axis to align with the magnetic field.

In fact, this is the reason a distinct definition of front, back and side is even possible. Since the front is always pointing to the north pole of the magnetic field, we also call it the north face, or north edge in two dimensions, and all the other faces can also be called by their corresponding cardinal direction. For each face we define a vector  $\vec{e} \in \{\vec{N}, \vec{E}, \vec{S}, \vec{W}\}$  with  $\|\vec{e}\| = 1$  pointing the the cardinal direction of the magnetic field. For simplification we call magnets by their outwards pointing pole in further sections.

Furthermore, two different cube types are defined: Either both side magnets point out their north pole, these cubes are called red cubes, or they point out their south pole, which is then called a blue cube. Figure 2.1 shows a top-down view of the two cube types with all the outwards pointing magnet poles. A compass always shows the orientation of the magnetic field in our illustrations.

Magnetic Modular Cubes can be constructed in different sizes and ways. For more technical details and length measurements, we refer to the original [5]. Two important lengths that we use for planning and simulating are the cube radius  $r_C$  and the magnet radius  $r_M$  (also illustrated in Figure 2.1).  $r_C$  is one half-length of a cube face and  $r_M$  is the distance from the center of the cube to the center of the magnet.



Figure 2.2: Rectangular workspace with a configuration of four magnetic modular cubes. All cubes have the same orientation as the magnetic field, indicated by the compass in the top-left corner.

## 2.2 Workspace and Configuration

Magnetic modular cubes could theoretical be placed and maneuvered on any 2-dimensional plane with numerous obstacles, as long as you can surround the workspace with a time varying magnetic field. The magnetic field should be able to point in any direction specified by angles of latitude and longitude, so that the cubes can operate in all desired motion modes. Because the motion planning problem of self-assembling target shapes in the special Euclidean group is hard enough without considering obstacles and arbitrary workspace shapes, we only work in a rectangular workspace with no internal obstacles. The workspace is limited by surrounding walls, which are the only objects that could be considered as obstacles in classical motion planning. However, we do not assume a fixed size, as long as the workspace stays finite and rectangular.

For planning we work in the configuration space of the 2-dimensional special Euclidean group  $SE(2) = \mathbb{R}^2 \times \mathbb{S}^1$ . When only considering one cube, the group consists of the position in  $\mathbb{R}^2$  and an orientation  $\mathbb{S} = [0, 2\pi)$  [8]. When working with  $n$  cubes, the dimension of our configuration space increases to  $\mathbb{R}^{2n} \times \mathbb{S}^1$ . Note that we can still assume only one orientation for  $n$  cubes, because we are working with a global magnetic field orienting all cubes the same way. Figure 2.2 shows a configuration with four cubes in the workspace. It is irrelevant which exact physical cube is at which position as long as they are the same type, so switching the positions of the two red cubes in Figure 2.2 would lead to the same configuration as before.



Figure 2.3: Examples of polyominoes and their equality. a) and d) are equal, only the magnetic field changed its orientation. a) and c) are not equal, they have the same shape but rotated. a) and c) are also not equal because of different cube types in the same shape. e) shows an invalid polyomino in its grid representation (top) and how it behaves in the simulation (bottom).

## 2.3 Polyominoes

The embedded magnets not only align the cube with the magnetic field, they also allow cubes to self-assemble into polyominoes. Two cube faces can connect if their magnets have opposite polarities. Because of this and the alignment with the magnetic field, cubes can either be connected at north and south faces, or east and west faces, if the cubes are not the same type. A polyomino is a set of uniformly sized cubes on a 2-dimensional grid. Because we work with arbitrary positions and orientations the grid alignment does not hold true for multiple polyominoes in the workspace, but for each polyomino on its own the cubes can be represented in a local coordinate system with position  $(x, y)$ ,  $x, y \in \mathbb{Z}$  [11].

We consider fixed polyominoes, meaning that two polyominoes are distinct if their shape or orientation are different [11]. The magnetic field always provides an orientation, so in Figure 2.3 a) and d) the polyominoes are equal, just the magnetic field is rotated. Conversely, the polyominoes in Figure 2.3 a) and c) are the same shape but with a different rotation under the same magnetic field orientation, so they are not equal. Furthermore, two polyominoes are only equal if all the cubes at equal positions are the same type. The polyominoes in Figure 2.3 a) and b) are not equal because the cube types differ. It is possible that a workspace contains multiple equal polyominoes. In that case, we refer to them as being the same polyomino-type, instead of calling them equal, since it is important to differentiate between physical polyominoes with different positions.

The size of a polyomino is the number of cubes it consists of. Because it is easier to view all structures in the workspace as a polyomino, single cubes are often referred to



Figure 2.4: This figure describes the pivot walking motion in detail. a) shows the six pivot walking steps for a single red cube. You can see the orientation of the magnetic field (bigger arrow indicates elevation). In b) an example polyomino with its pivot axis, edges and points is shown. c) illustrates the rotation of the pivot axis labeled with all the pivot walking parameters.

as trivial polyominoes with size 1. Although it is not possible to connect cubes of same type at east and west faces, the magnetic modular cubes can assemble structures like the one shown in Figure 2.3 e). The connection of the bottom two cubes is strong enough to hold the structure together, even though the four blue cubes on the top repel each other. The resulting polyomino in its grid representation has two east-west connections between cubes the same type and is therefore marked as an invalid polyomino.

## 2.4 Motion Modes

In [5] three motion modes are presented. Rotation, pivot walking and rolling.

If the magnetic field orientation lays in the plane of the workspace and rotates without any inclination the rotation is performed around the center of mass for all polyominoes and we consider this motion a normal rotation.

Rotating the magnetic field perpendicular to the workspace plane, cubes can roll forwards or backwards. This rolling motion becomes problematic for self-assembly, because the top and bottom face of the cube, which contain no magnets, can become a side face.

## 2 Preliminaries

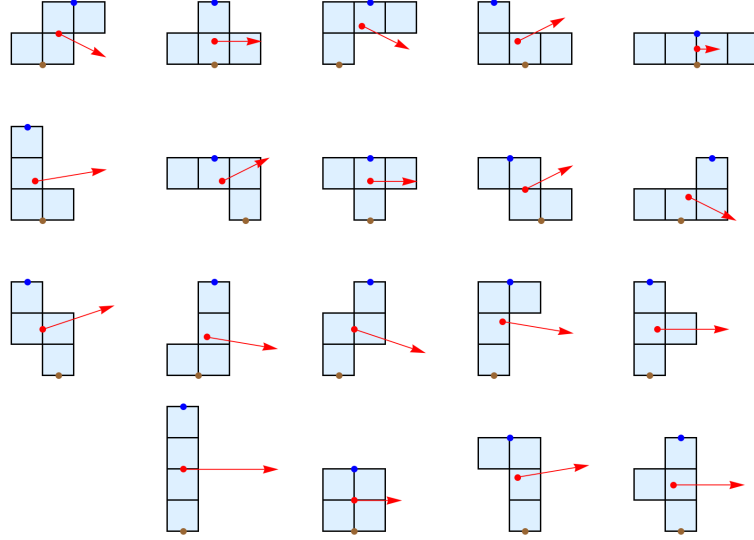


Figure 2.5: All 19 four-cube polyomino shapes with their displacement vector  $\vec{d}$  for one pivot walking cycle with  $\alpha = \frac{\pi}{4}$ .  $\vec{d}$  is drawn from the center of mass (red dot). North and south pivot point are drawn as blue and brown dots.

Because rotation and pivot walking are sufficient to reach any position in the workspace, we do not consider rolling in our simulation and planning algorithms.

When elevating the magnetic field orientation by lifting up the south pole slightly, all polyominoes will pivot on the north face bottom edges of their most north-placed cubes. Pulling up the north pole does the opposite. The polyominoes will pivot on the south face bottom edges of their most south-placed cubes. The sum of all these cube edges is called the north or south pivot-edge and by keeping the magnetic field elevated and rotating around the normal vector of the workspace plane, the polyominoes will rotate around the center point of their pivot-edge. This point is called the north or south pivot-point. All these edges and points are illustrated in Figure 2.4 b).

**pivot walking:** Not rotating around the center of mass is important for pivot walking. In the first step of a pivot walking cycle, the magnetic field is elevated to let the polyomino pivot on its north pivot edge. As a second step a rotation of  $-\frac{1}{2} \cdot \alpha$  is performed around the north pivot point.  $-\pi \leq \alpha \leq \pi$  is the pivot walking angle. For step 3 and 4 the elevation changes to its opposite to perform a rotation of  $\alpha$  around the south pivot point. Step 5 and 6 are equal to 1 and 2 and will bring the polyomino back to its original orientation. You can see the pivot walking cycle steps in Figure 2.4 a) and have a closer look at its parameters in Figure 2.4 c).

After one pivot walking cycle, the polyomino has moved by a displacement vector  $\vec{d}$  with  $\|\vec{d}\| = d_p$ , so  $d_p$  is the distance the polyomino moved. The direction and length of  $\vec{d}$  changes with the shape of the polyomino. The movement is always perpendicular to

the pivot walking axis  $\vec{a}$  with  $\|\vec{a}\| = a_p$ , which is the vector between the north and the south pivot point, visualized in Figure 2.4 b).  $d_p$  can be calculated as

$$d_p = 2 \cdot \sin\left(\frac{1}{2} \cdot \alpha\right) \cdot a_p. \quad (2.1)$$

To calculate  $\vec{d}$  you can take the perpendicular of  $\vec{a}$  and scale it to the length  $d_p$ .

When a big  $\alpha$  is chosen according to amount,  $d_p$  becomes also bigger, but the polyomino needs more space to the north and south to perform the rotations. For better maneuvering smaller values of  $\alpha$  are preferable. There is a strong deviation of length and direction of the displacement for different polyomino shapes. So doing a pivot walking motion might not move two polyominoes in the same direction. Figure 2.5 shows all 19 four-cube polyomino shapes with their displacement vectors. There are still two options for pivot walking, depending on a negative or positive value of  $\alpha$ . You can walk left, in the direction of the west-faces, or right, in the direction of the east-faces. Although the polyomino actually moves in the direction of  $\vec{d}$ , we can still say that for instance a pivot walk right moves to the east, because  $\left|\angle\left(\vec{E}, \vec{d}\right)\right| < \frac{\pi}{2}$ . We call these two options the pivot walking direction  $\vec{w} \in \{\vec{E}, \vec{W}\}$ .





## 3 Local Planner

This chapter is about the local planner that will be used for motion planning on a global scale in Chapter 4. Local planning means that the planner only focuses on simple motion task. The task could be to develop a plan that moves a polyomino from position  $a$  to position  $b$ , or even simpler, to develop a plan for one pivot walk. Since on a global scale we consider the problem of self-assembly, we are not interested in changing positions alone. To work efficiently with local plans in the global planner, the initial and goal configuration of those plans should differ in the set of polyominoes they contain. The local planner takes two cubes  $c_A$  and  $c_B$  out of different polyominoes  $A$  and  $B$  and attempts to establish a connection at a valid edge-pair  $(e_A, e_B)$ . If a local plan was successful, this guaranties a change of polyominoes in the workspace.

For this, the local planner makes use of our simulator from Chapter 5 in a closed-loop manner, meaning that the state of the simulation can be observed at any time and the actions can be adjusted accordingly. The local planner observes the position of cubes and polyominoes and works with the distance between them. It also works with the orientation of cube faces. In a real application of Magnetic Modular Cubes a camera, able to track cubes in the workspace, could be used to retrieve the necessary information.

The following Sections 3.1 to 3.4 explain the techniques used in the local planning algorithm of Section 3.5.

### 3.1 Connecting Polyominoes

The two main rules that have to be considered when connecting two polyominoes  $A$  and  $B$  are: First, cubes can only be connected in the way described in Section 2.3, so we can distinguish between east-west and north-south connections. Second, pivot walking (Section 2.4) only allows the polyominoes to move left or right with  $\vec{w}$ . Keep in mind that a pivot walking motion is actually performed in the direction of the displacement  $\vec{d}$  and not directly in direction of  $\vec{w}$ . To move in any arbitrary direction it is necessary to rotate the polyomino  $A$ , so that  $\vec{d}_A$  points into the desired direction.

East-west connections are generally easier to handle. If we want to connect an east face of polyomino  $A$  to a west face of polyomino  $B$ ,  $A$  has to walk into the east direction towards  $B$ , or the other way around. When  $A$  should be connected at a south face of  $B$ ,  $A$  can now walk into east or west direction towards  $B$ , or  $B$  could again do the opposite. A closer look on why these two options differ and how both can be established at any position is taken in Section 3.2. We call this the slide-in direction  $\vec{m} \in \{\vec{E}, \vec{W}\}$ , which states that  $B$  is positioned in direction  $\vec{m}$  of  $A$ .



Figure 3.1: The figure shows examples for straight- and offset-aligning. The edges to be connected are marked yellow. a) shows two not aligned polyominoes (top) and the result of a straight-align (bottom). In b) you can see the two approaches for an offset-align. The cubes were aligned with their west edge (top) and with their east edge (bottom).

## 3.2 Aligning Cubes

To establish a connection between two polyominoes  $A$  and  $B$ , the connection-cubes  $c_A$  and  $c_B$  with their connection-edges  $e_A$  and  $e_B$  need to be aligned in the right way. When  $A$  is rotated without magnetic field elevation, a cube with position  $P_{c_A}$  rotates in a circle around the center of mass of its polyomino  $C_A$ . The vector  $\vec{r}_A = P_{c_A} - C_A$  is the radius of this rotation-circle. When also considering  $B$ , a rotation of the magnetic field rotates  $\vec{r}_A$  and  $\vec{r}_B$  by the same angle  $\beta$ . The goal is to find this angular difference  $\beta$ , so that the cubes are aligned. There are two different approaches for alignment: Straight-align and offset-align.

**Straight-Align:** For straight aligning, we define a vector  $\overrightarrow{AB} = P_{c_B} - P_{c_A}$  pointing from  $c_A$  to  $c_B$ . The aligning is done when  $\vec{e}_A$  points in the same direction as  $\overrightarrow{AB}$ , so  $\angle(\vec{e}_A, \overrightarrow{AB}) = 0$ . Consequently  $\angle(\vec{e}_B, \overrightarrow{AB}) = \pi$ , since  $e_A$  and  $e_B$  have to be opposite edges for a connection.

Figure 3.1 a) illustrates a straight-align for an east-west connection with all the parameters. The two polyominoes could now theoretically pivot walk together and connect the desired edges. Straight-aligning is always used for east-west connections, but we also use it for north-south connection in one special case. More on that in Section 3.4.

**Offset-Align:** When considering north-south connections we need to align with an offset, so that the cubes can be moved together from east or west direction. We again define  $\overrightarrow{AB} = \hat{P}_{c_B} - P_{c_A}$  with  $\hat{P}_{c_B} = d_o \cdot \vec{e}_B + P_{c_B}$ . We add an offset  $d_o$  to  $P_{c_B}$  in the direction of  $e_B$ , so  $\overrightarrow{AB}$  points from  $P_{c_A}$  to a position above or below  $P_{c_B}$ . In a perfect world  $d_o = 2 \cdot r_C$  is exactly one cube length, but to avoid failures when moving together, we give the alignment a bigger offset. Instead of pointing  $e_A$  in the same direction as  $\overrightarrow{AB}$  we now have two options: Either solving  $\angle(\vec{E}, \overrightarrow{AB}) = 0$  or  $\angle(\vec{W}, \overrightarrow{AB}) = 0$ , depending on if we want to move  $A$  in east direction, or in the west direction towards  $B$ .

You can see the two options for offset-aligning in Figure 3.1 b). For the two polyominoes you can also see that aligning with east or west edge can make a difference when moving together. Establishing a connection by letting  $A$  move towards  $B$  in west direction is possible, but by moving in east direction other cubes of the polyominoes are blocking the way. In Section 3.4 we present a method for checking if moving in from east or west is possible.

**Solving Alignment:** For calculating angular difference we use the dot-product

$$\angle(a, b) = \frac{a \cdot b}{\|a\| \|b\|},$$

with  $a, b \in \mathbb{R}^2$ . This way the difference is always positive, which is beneficial in the case of alignment. We define a function for straight-aligning based on the rotation angle  $\beta$ ,

### 3 Local Planner

where both  $\vec{e}_A$  and  $\overrightarrow{AB}$  change according to  $\beta$ .

$$a(\beta) = \angle(R_\beta \vec{e}_A, (R_\beta r_B + C_B) - (R_\beta r_A + C_A)) . \quad (3.1)$$

$R_\beta$  is a rotation matrix used for rotating vectors by  $\beta$ . For an offset-align the function would be

$$a(\beta) = \angle(R_\beta \vec{e}, (R_\beta \hat{r}_B + C_B) - (R_\beta r_A + C_A)) , \quad (3.2)$$

with  $\vec{e} \in \{\vec{E}, \vec{W}\}$  and  $\hat{r}_B = \hat{P}_{c_B} - C_B$

Alignment is not always possible, so instead of solving  $a(\beta) = 0$ , we are minimizing  $a(\beta)$ . Because  $-\pi < \beta \leq \pi$  we can iterate through increasing values of  $\beta$ . If we encounter a value close enough to zero we can return it. If not we return the minimum of all the calculated values. This way we at least get as close to an alignment as possible.

### 3.3 Moving Polyominoes Together

Since both polyominoes  $A$  and  $B$  perform pivot walking motions simultaneously, due to global control, a connection will most likely happen when one polyomino walks into a wall of the workspace boundary. Connection can only happen in the middle of the workspace when one polyomino is faster than the other, meaning it was a greater pivot walking distance  $d_P$ . At a first glance it seems easy to move polyominoes together, after the connection-cubes are aligned as described in Section 3.2. The two options of walking left and right determine if either  $A$  is chasing  $B$ , or if  $B$  is chasing  $A$ , which is of course also dependent on their initial position and orientation. In the end one option might be shorter or better in terms of other polyominoes interfering with  $A$  and  $B$ , but theoretically both are able to establish the connection.

In reality it becomes more difficult. When a polyomino is continuously walking against a wall in more or less than a 90 degree angle, the polyomino will move alongside the wall. In [16] research is done on how friction with boundary-walls under global control forces can be used to calculate the necessary motions for reaching a desired goal configuration, but friction forces depend greatly on material choices and are stochastic. Another difficulty are different orientations of displacement vectors. It is mathematically possible to calculate the right orientation of the magnetic field to result in a collision after  $n$  pivot walking cycle for both polyominoes, even at desired edges, but it is not guaranteed that this collision-point is within the workspace boundaries. In that case the calculation of friction and displacement have to be combined together with other factors like polyominoes blocking each other or changing their shape during movement. This seems fairly complex and recalculating would be necessary in many situations, so we choose a simpler dynamic approach.

We estimate the pivot walking cycles necessary until  $c_A$  moved to the position of  $c_B$  with

$$n = \left\lceil \frac{\|P_{c_A} - P_{c_B}\|}{d_{p,A}} \right\rceil . \quad (3.3)$$

We then only walk a portion of  $n$  and re-align the cubes. When  $c_A$  and  $c_B$  are near enough for magnetic forces to act we frequently wait a short period to let magnetic

attraction pull  $e_A$  and  $e_B$  together. This will automatically adjust the alignment, but for even more precision we decreased the pivot walking angle  $\alpha$ , when in close proximity.

### 3.4 Plan and Failures

A plan is a sequence of actions  $A = a_1, \dots, a_n$  that when applied to an initial configuration  $g_{init}$ , leads to a goal configuration  $g_{goal}$ . Two plans can be concatenated when the goal of the first matches with the initial configuration of the second. That way multiple local plans can be connected to form a global plan. We define a metric to compare and evaluate plans based on rotational cost of its actions only considering magnetic field rotations, not elevation. Let  $a_i$  be a normal rotation of angle  $\beta$ , then  $\text{cost}(a_i) = |\beta|$ . If it is a pivot walking motion, then  $\text{cost}(a_i) = |2\alpha|$ . The cost for the plan is the sum of the costs of all its actions

$$\sum_{i=1}^n \text{cost}(a_i). \quad (3.4)$$

A local plan is successful if  $g_{goal}$  contains a polyomino with the desired connection of  $c_A$  and  $c_B$  at  $(e_A, e_B)$ . If a plan is successful or not is described by the plan-state  $s$ . There are several reasons the local planner might fail to develop a plan:

**Impossible Connection:** Most reasons of failure resolves around the fact, that it is not possible to connect the polyominoes. First of all,  $e_A$  and  $e_B$  need to be free, so no other cube is already connected to them, but even if that is the case other cubes then  $c_A$  and  $c_B$  can prevent a connection. By connecting two polyominoes in one local discrete coordinate-system, for all cubes  $c_1, c_2$  with coordinates  $(x_1, y_1), (x_2, y_2)$ :  $(x_1, y_1) \neq (x_2, y_2)$  should hold true. If two positions are equal, we call this an overlap, which prevents the connection. Of course, a connection is also not possible, if  $e_A$  and  $e_B$  are part of the same polyomino and not already connected.

All that conditions are easy to check in a discrete way before even starting to plan, but that is not enough. Connection with other polyominoes during planning can invalidate those pre-checked conditions, so we need to frequently re-check them.

**Impossible Slide-In:** Even if a connection in a common local coordinate-system is possible you can only connect by moving in from east or west. Other cubes can again prevent this by blocking the way for an easy slide-in. We can also verify both east and west slide-in in a common local coordinate system. This discrete check assumes exact movement from east or west direction. Because of different displacement directions, we know this is not true, but it is a reasonable approximation. Research on assembling a polyomino out of two parts by moving one part towards the other without collision, was done by Agarwal et al. [1].

When pre-checking this condition, we can state failure, if both directions are not possible. Otherwise, we can align with respect to the valid slide-in direction, or try out

### 3 Local Planner

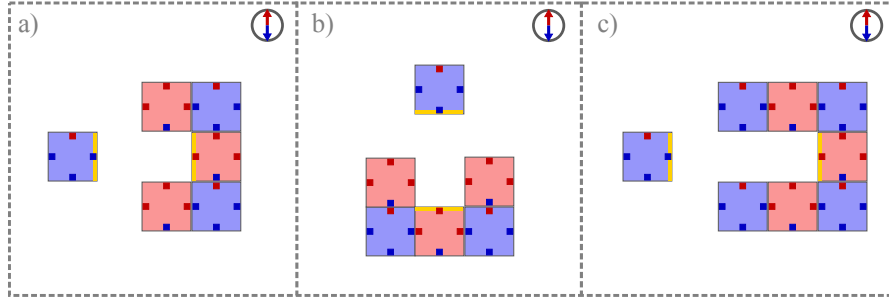


Figure 3.2: Three different examples for connecting polyominoes into caves. a) and b) show one-cube-deep caves (a) east-west and b) north-south). c) illustrates a two-cube-deep east-west cave. The edges to be connected are marked yellow.

both, if both are possible. Again, the condition needs to be re-checked frequently, due to changing polyominoes.

**Polyominoes being Stuck:** Polyominoes can get stuck in corners or on walls of the workspace. In this state it is not possible anymore to decrease the distance of  $A$  and  $B$  by pivot walking. We can identify this state when the position of both cubes  $c_A$  and  $c_B$  did not change after a certain amount of pivot walking motions.

When stuck while trying to establish a north-south connection, a straight-align instead of an offset-align can solve the problem. It depends on the distance of the cubes after straight-aligning. If the distance is too big for magnetic forces to act, failure is reported, but if they are close enough the local planner waits until magnetic attraction connected  $e_A$  and  $e_B$ .

**Connecting in Caves:** Connecting two polyominoes where one of the connection-faces is located inside a cave is a difficult task in the continuous world. We differentiate between east-west and north-south located caves. Furthermore a cave can be of a certain depth measured in multiples of  $2r_C$ . Figure 3.2 shows examples for different caves and different depths.

Connecting into a cave with a depth of more than  $2r_C$  is not possible. For instance, when inserting the blue single cube into the polyomino in Figure 3.2 c), the blue cube would connect with north and south faces of the polyomino before even reaching the full depth of the cave. But even caves with depth  $2r_C$  are hard to handle. Inserting into a cave can be done by pivot walking, this would only work for east-west caves, or by letting magnetic forces attract the connection-faces. Relying on magnetic forces alone seem promising, since it would work for both cave types, but in reality not only the forces of the connection-faces are present. All the forces between other magnets prevent an easy slide-in. In our simulator the connection-face will be more attracted or repelled by faces outside the cave, then the once inside. Pivot walking into east-west caves, even with small values for  $\alpha$ , has also a high failure rate because of other magnets. The

local planner states failure immediately when polyominoes should be connected in any cave-type.

**Invalid Polyominoes:** Because construction of invalid polyominoes is hard to handle on a global scale, we already omit plans containing them in our local planner. We state failure if any invalid polyominoes is created at any point during planning. We also pre-check and frequently re-check, if the polyomino that will be created by establishing the connection would itself be invalid.

**Maximum Movement Capacity:** As a worst-case failure, we limit the amount of movement  $A$  and  $B$  are able to do. Whenever a pivot walking motion is done, we sum up the distances  $c_A$  and  $c_B$  moved together. Let  $(w, h)$  be the size of the workspace. We define a maximum movement capacity of  $2 \cdot (w + h)$ . This capacity gives the polyominoes enough movement, so that both can move along a horizontal and vertical workspace boundary, which should definitely be sufficient to establish a connection.

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**Algorithm 1** ALIGN-WALK-REALIGN

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**Input:**  $c_A, c_B, e_A, e_B, \vec{w}, \vec{m}, g_{init}$ **Output:**  $s, g_{goal}, A$  $s \leftarrow \text{undefined}$  $g_{goal} \leftarrow g_{init}$  $A \leftarrow \{\}$  $\text{wait} \leftarrow \text{true}$ **loop**  **if**  $e_A \in \{E, W\}$  **then**     $a \leftarrow \text{ALIGN-STRAIGHT}(c_A, c_B, e_A)$   **else**     $a \leftarrow \text{ALIGN-OFFSET}(c_A, c_B, \vec{m}, e_B)$   **end if**   $g_{goal} \leftarrow \text{SIMULATE}(g_{goal}, a)$    $A \leftarrow \text{APPEND}(A, a)$    $s \leftarrow \text{UPDATE-STATE}(g_{goal}, c_A, c_B, e_A, \vec{m})$   **if**  $s \neq \text{undefined}$  **then**    **return**  $s, g_{goal}, A$   **end if**  **if**  $\text{CRITICAL-DISTANCE}(c_A, c_B)$  **and**  $\text{wait}$  **then**     $a \leftarrow \text{WAIT}()$      $\text{wait} \leftarrow \text{false}$   **else**     $a \leftarrow \text{WALK}(c_A, c_B, \vec{w})$      $\text{wait} \leftarrow \text{true}$   **end if**   $g_{goal} \leftarrow \text{SIMULATE}(g_{goal}, a)$    $A \leftarrow \text{APPEND}(A, a)$   **if**  $\text{STUCK}(c_A, c_B)$  **then**     $a \leftarrow \text{ALIGN-STRAIGHT}(c_A, c_B, e_A)$      $g_{goal} \leftarrow \text{SIMULATE}(g_{goal}, a)$      $A \leftarrow \text{APPEND}(A, a)$     **while not**  $\text{STUCK}(c_A, c_B)$  **do**       $a \leftarrow \text{WAIT}()$        $g_{goal} \leftarrow \text{SIMULATE}(g_{goal}, a)$        $A \leftarrow \text{APPEND}(A, a)$     **end while**  **end if**   $s \leftarrow \text{UPDATE-STATE}(g_{goal}, c_A, c_B, e_A, \vec{m})$   **if**  $s \neq \text{undefined}$  **then**    **return**  $s, g_{goal}, A$   **end if****end loop**

---



### 3.5 Local Planning Algorithm

Before executing the algorithm presented in Algorithm 1 we evaluate all the failure conditions that can be checked in advance, so no simulation-time is wasted on a plan that is bound to fail from the start. While doing so, the possible slide-in directions are also determined and Algorithm 1 is executed with both pivot walking directions  $\vec{w}$  for each possible  $\vec{m}$ . This means for an east-west connection, we always develop two plans and for a north-south connection two or four, depending on the slide-in directions.

In the end, the successful plan with the lowest costs is returned. Even if all plans fail, we still determine the best failure. Again, plans with lower costs are preferable, but we favor impossible connection and slide-in failures. These failures just state that we can not establish a specific connection, but a global planner could continue to plan based on the goal configuration the local planner ended in. A configuration when the polyominoes are stuck, or the maximum movement capacity is reached, is not good for further planning, but invalid polyominoes or polyominoes with gaps will definitely be omitted on a global scale.

The different plans are developed in parallel and if one process finishes with a successful plan, the execution of all other plans can be canceled. This saves a lot of computation time, although we might not return the optimal plan, since fastest computation does not automatically mean lowest costs. Generally speaking a low computation time can be linked with low rotational cost, because the local planner spends the majority of time, about 98%, on simulating the actions.

**Align-Walk-Realign:** Algorithm 1 takes the connection-cubes and edges  $c_A, c_B, e_A, e_B$  along with  $\vec{w}, \vec{m}$  and an initial configuration  $g_{init}$  as inputs and returns a plan-state  $s$  along with the configuration  $g_{goal}$  the algorithm ended in after applying the sequence of actions  $A$ . The algorithm runs in a loop until  $s$  changes to success or one of the failure condition. The failure and success conditions are evaluated twice per iteration with UPDATE-STATE. Once after aligning, and once at the end of the loop. That way, the planner avoids simulating unnecessary actions.  $g_{goal}$  is updated by simulating the determined actions with SIMULATE. The actions are appended to  $A$  after simulation. We perform either a straight or offset-align, depending on  $e_A$  and  $e_B$ . The offset-align is done with the direction of  $\vec{m}$ . After aligning we walk the estimated amount of pivot walking cycles (Section 3.3) in direction  $\vec{w}$  with WALK, or we wait with WAIT, if  $c_A$  and  $c_B$  are in close proximity, determined by CRITICAL-DISTANCE. If we waited in the previous iteration, we walk in the current one and oppositely. This behavior is toggled by the variable *wait*. The stuck condition is evaluated with STUCK and does not state failure immediately, since a straight-align might be able to fix the situation. When the polyominoes are stuck, the algorithm performs a straight-align and waits as long as this changes the stuck condition.



## 4 Global Planner

The task of the global planner is to assemble a specified target polyomino  $T$  given an initial configuration  $g_{init}$ . The configuration-space is explored by executing local plans developed by the local planner from Chapter 3. That way, the part of the configuration-space we can actually explore, is limited to configurations where a connection attempt between two cubes was made. Compared to  $SE(2)$  this part is manageable in size and only contains configurations which are interesting for self-assembly.

The question still remains, how these configurations are explored. Using rapidly-exploring random trees (RRTs) [9] yields good results in a lot of cases, since the space gets evenly explored without the problematic of determining what decisions are promising for the end goal. But, it also means the exploration of many configurations, which are not necessary for reaching the goal. For us this approach is not reasonable. Because of the high fidelity simulation we are working with, the computation time for a local plan is huge, so planning the assembly of  $T$  with as less local plans as possible is the aim for our global planner.

We need to make well thought-through connection decisions, that are valid for assembling  $T$ , meaning some sort of building plan for a polyomino is needed. Creating a building sequences by removing one tile at a time from the target was done by Becker et al. [4]. However, this does not consider sub-assemblies, so all cubes that are not to be connected, have to stay separated at any time and occurring sub-assemblies would lead to immediate failure.

It is hard to prevent sub-assemblies, so our approach uses an enumeration of cutting a polyomino into two pieces (Section 4.1), which will be used for generating a so called two-cut-sub-assembly graph (Section 4.2). In Section 4.3 that graph will be used as a building instruction along side the exploration of the configuration-space. For this technique the number of cubes in the workspace is limited to the size of  $T$ . A take on why is this done and why the problem becomes more complex when working with extra cubes, is done in Section 4.4.

### 4.1 Two-Cutting Polyominoes

### 4.2 Two-Cut-Sub-Assembly Graph

#### Building TCSA-Graph

#### Complexity

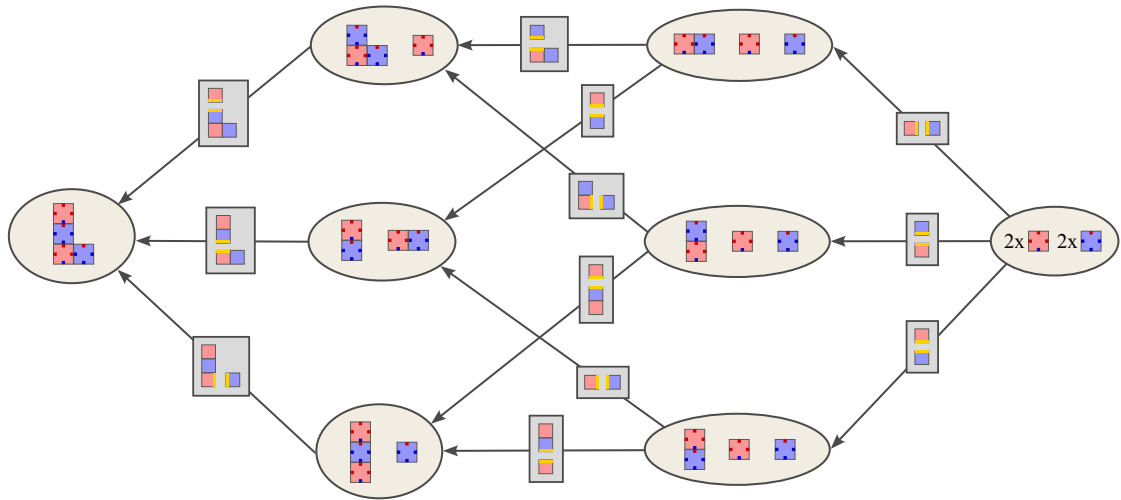


Figure 4.1: long caption...

## 4.3 Global Planning Algorithm

### 4.3.1 Connection Options

### 4.3.2 Option Sorting

Minimal Distance

Grow Largest Component

Grow Smallest Component

### 4.3.3 Graph Traversal

Complexity

Discretize Configurations

## 4.4 More Cubes than Target

## 5 Simulator



# Bibliography

- [1] P. K. Agarwal, B. Aronov, T. Geft, and D. Halperin. On two-handed planar assembly partitioning with connectivity constraints. In *Proceedings of the 2021 ACM-SIAM Symposium on Discrete Algorithms (SODA)*, pages 1740–1756. SIAM, 2021.
- [2] A. Becker, E. D. Demaine, S. P. Fekete, G. Habibi, and J. McLurkin. Reconfiguring massive particle swarms with limited, global control. In P. Flocchini, J. Gao, E. Kranakis, and F. Meyer auf der Heide, editors, *Algorithms for Sensor Systems*, pages 51–66, Berlin, Heidelberg, 2014. Springer Berlin Heidelberg.
- [3] A. Becker, E. D. Demaine, S. P. Fekete, and J. McLurkin. Particle computation: Designing worlds to control robot swarms with only global signals. In *2014 IEEE International Conference on Robotics and Automation (ICRA)*, pages 6751–6756, 2014.
- [4] A. T. Becker, S. P. Fekete, P. Keldenich, D. Krupke, C. Rieck, C. Scheffer, and A. Schmidt. Tilt assembly: Algorithms for micro-factories that build objects with uniform external forces. *Algorithmica*, 82(2):165–187, Feb 2020.
- [5] A. Bhattacharjee, Y. Lu, A. T. Becker, and M. Kim. Magnetically controlled modular cubes with reconfigurable self-assembly and disassembly. *IEEE Transactions on Robotics*, 38(3):1793–1805, 2022.
- [6] J. Bishop, S. Burden, E. Klavins, R. Kreisberg, W. Malone, N. Napp, and T. Nguyen. Programmable parts: A demonstration of the grammatical approach to self-organization. In *2005 IEEE/RSJ International Conference on Intelligent Robots and Systems*, pages 3684–3691. IEEE, 2005.
- [7] D. Caballero, A. A. Cantu, T. Gomez, A. Luchsinger, R. Schweller, and T. Wylie. Hardness of reconfiguring robot swarms with uniform external control in limited directions. *Journal of Information Processing*, 28:782–790, 2020.
- [8] S. M. LaValle. *Planning Algorithms*. Cambridge University Press, Cambridge, U.K., 2006. Available at <http://planning.cs.uiuc.edu/>.
- [9] S. M. LaValle et al. Rapidly-exploring random trees: A new tool for path planning. 1998.
- [10] S. M. LaValle and J. J. Kuffner. Rapidly-exploring random trees: Progress and prospects: Steven m. lavalley, iowa state university, a james j. kuffner, jr., university of tokyo, tokyo, japan. *Algorithmic and computational robotics*, pages 303–307, 2001.

## Bibliography

- [11] Y. Lu, A. Bhattacharjee, D. Biediger, M. Kim, and A. T. Becker. Enumeration of polyominoes and polycubes composed of magnetic cubes. In *2021 IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS)*, pages 6977–6982, 2021.
- [12] A. Mueller. Modern robotics: Mechanics, planning, and control [bookshelf]. *IEEE Control Systems Magazine*, 39(6):100–102, 2019.
- [13] A. T. B. Patrick Blumenberg, Arne Schmidt. Computing motion plans for assembling particles with global control. In *Under Review*. IEEE, 2023.
- [14] R. Pelrine, A. Wong-Foy, A. Hsu, and B. McCoy. Self-assembly of milli-scale robotic manipulators: A path to highly adaptive, robust automation systems. In *2016 International Conference on Manipulation, Automation and Robotics at Small Scales (MARSS)*, pages 1–6. IEEE, 2016.
- [15] W. Saab, P. Racioppo, and P. Ben-Tzvi. A review of coupling mechanism designs for modular reconfigurable robots. *Robotica*, 37(2):378–403, 2019.
- [16] A. Schmidt, V. M. Baez, A. T. Becker, and S. P. Fekete. Coordinated particle relocation using finite static friction with boundary walls. *IEEE Robotics and Automation Letters*, 5(2):985–992, 2020.
- [17] A. Schmidt, S. Manzoor, L. Huang, A. T. Becker, and S. P. Fekete. Efficient parallel self-assembly under uniform control inputs. *IEEE Robotics and Automation Letters*, 3(4):3521–3528, 2018.
- [18] M. Sitti, H. Ceylan, W. Hu, J. Giltinan, M. Turan, S. Yim, and E. Diller. Biomedical applications of untethered mobile milli/microrobots. *Proceedings of the IEEE*, 103(2):205–224, 2015.
- [19] P. J. White and M. Yim. Scalable modular self-reconfigurable robots using external actuation. In *2007 IEEE/RSJ International Conference on Intelligent Robots and Systems*, pages 2773–2778. IEEE, 2007.
- [20] E. Winfree. *Algorithmic self-assembly of DNA*. California Institute of Technology, 1998.