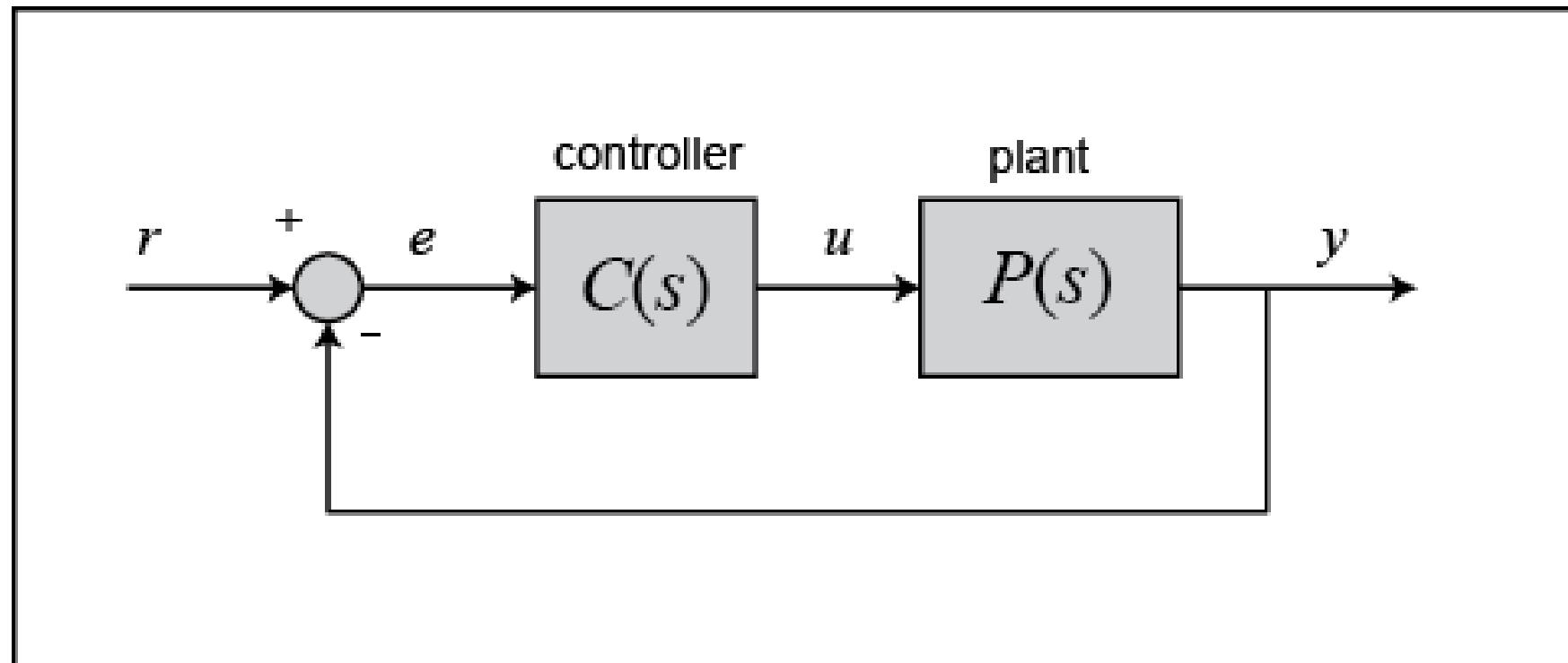




# Dynamics and Control - II

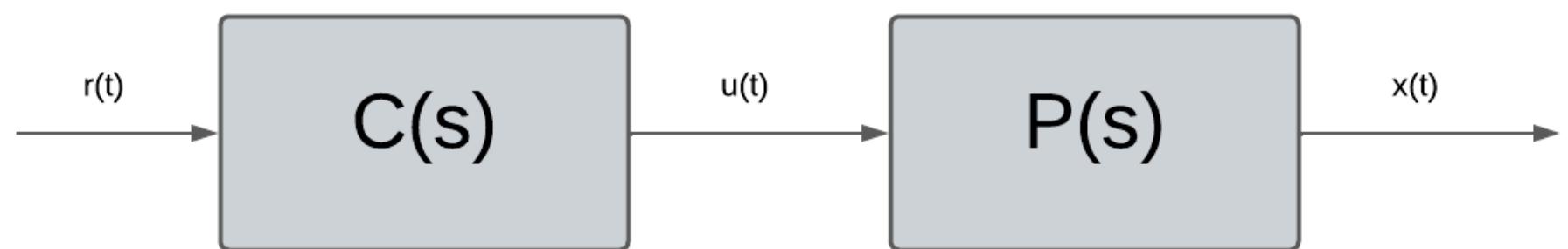
Astik Srivastava

# Plant and Controller



- Plant refers to any process that takes in an input and produces an output
- Relation between input and output is governed by the plant dynamics
- A controller is a plant which is designed to influence the (main) plant to obtain desirable results

# Open Loop Controller

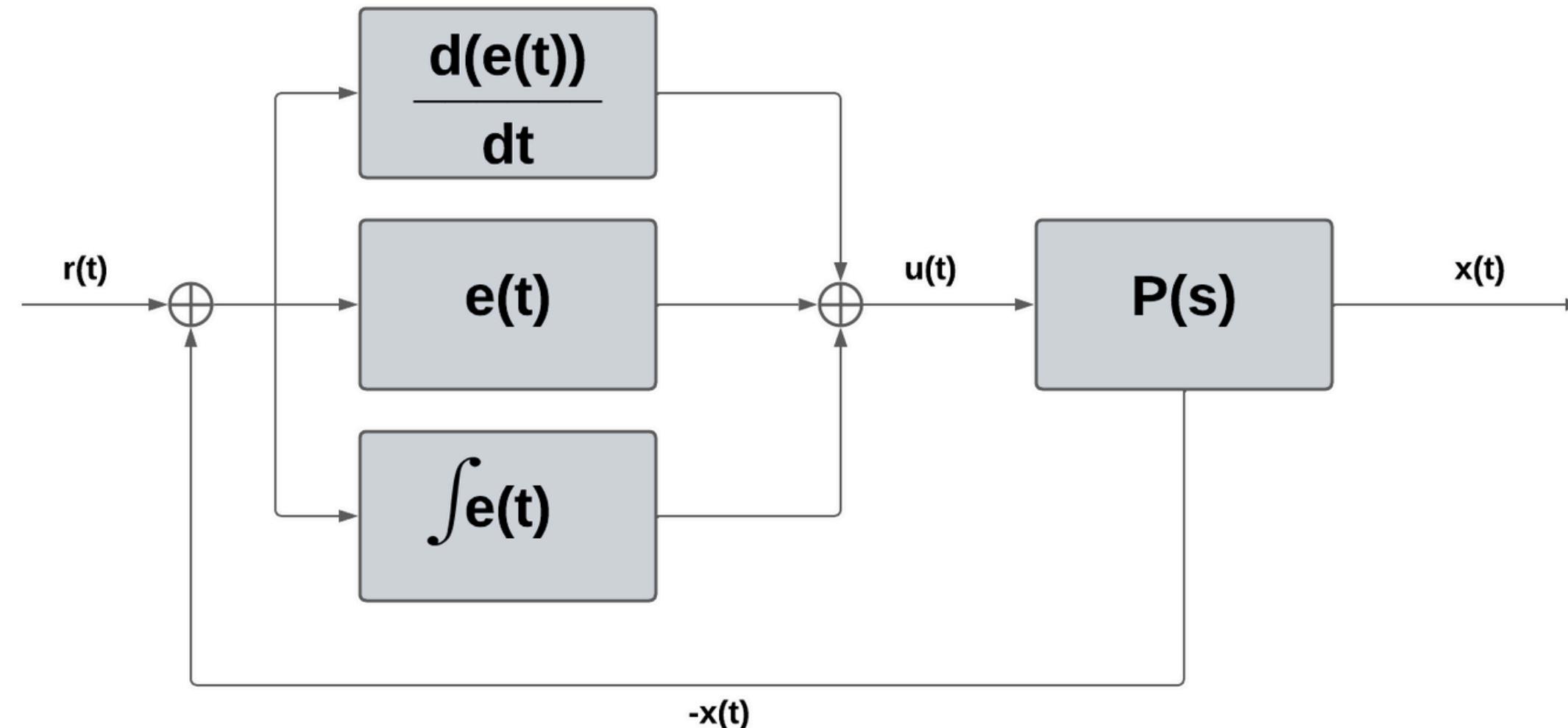


- A controller without any feedback from the plant
- Generally uses information about plant dynamics to compute  $u(t)$

# Passively stable system



# PID Controller



$$u(t) = kp * e(t) + kd * \frac{d(e(t))}{dt} + ki * \int e(t)$$

# PID Controller

## Proportional

- Responsible for making the system reach desired reference “asymptotically”
- Small values lead to a slower rise time and sluggish response.
- Large values lead to overshoot

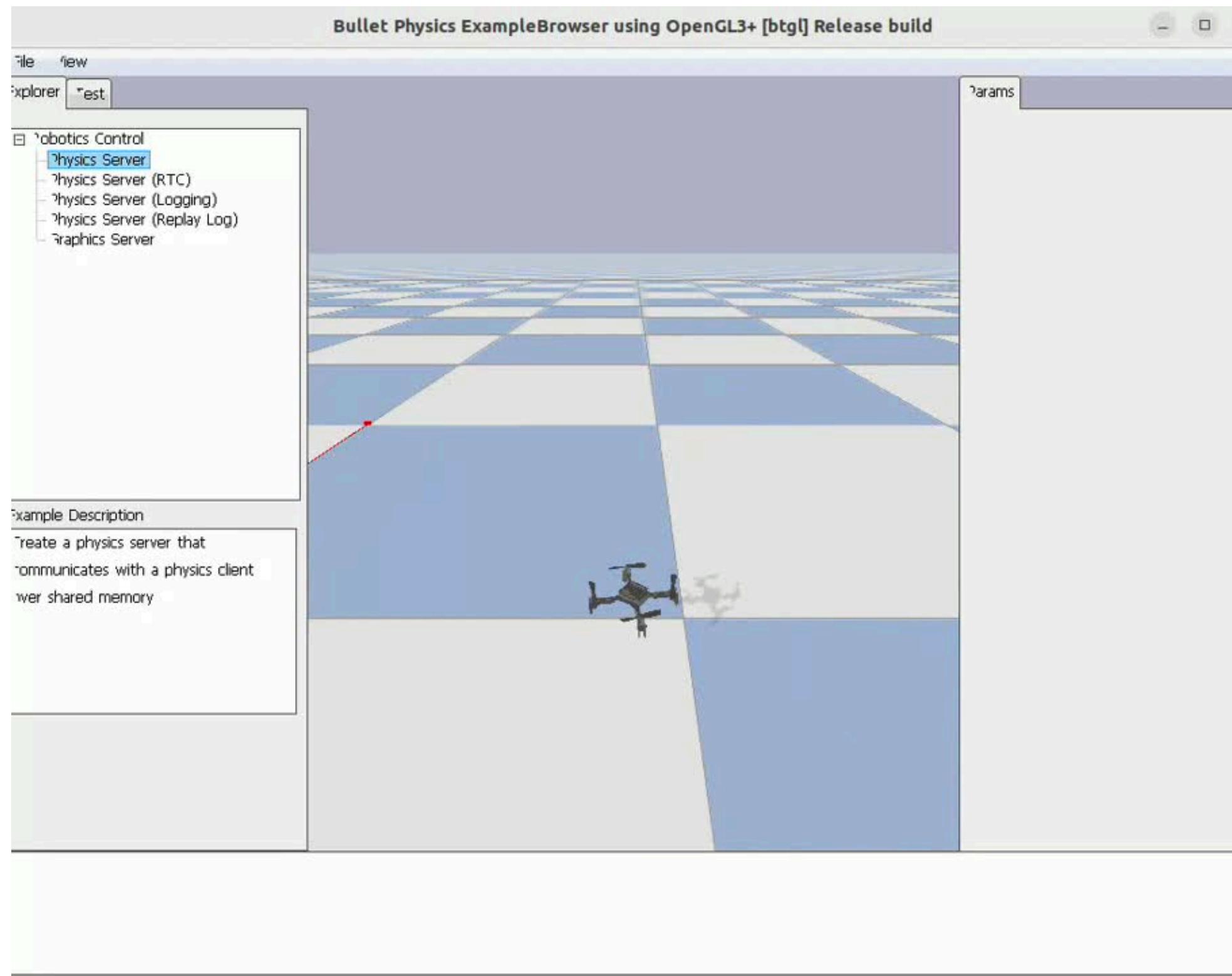
## Integral

- Eliminates the steady state error present in the system.
- Small values lead to a slower removal of steady state error, generally safer
- Large values might lead to “integral windup”, causing overshoot and oscillations, also saturations

## Derivative

- Dampens the system by reacting to rate of error.
- Small values lead to under-damped behavior.
- Large values might lead to noisy and over-damped behavior, reducing rise time and performance

# PID Controller

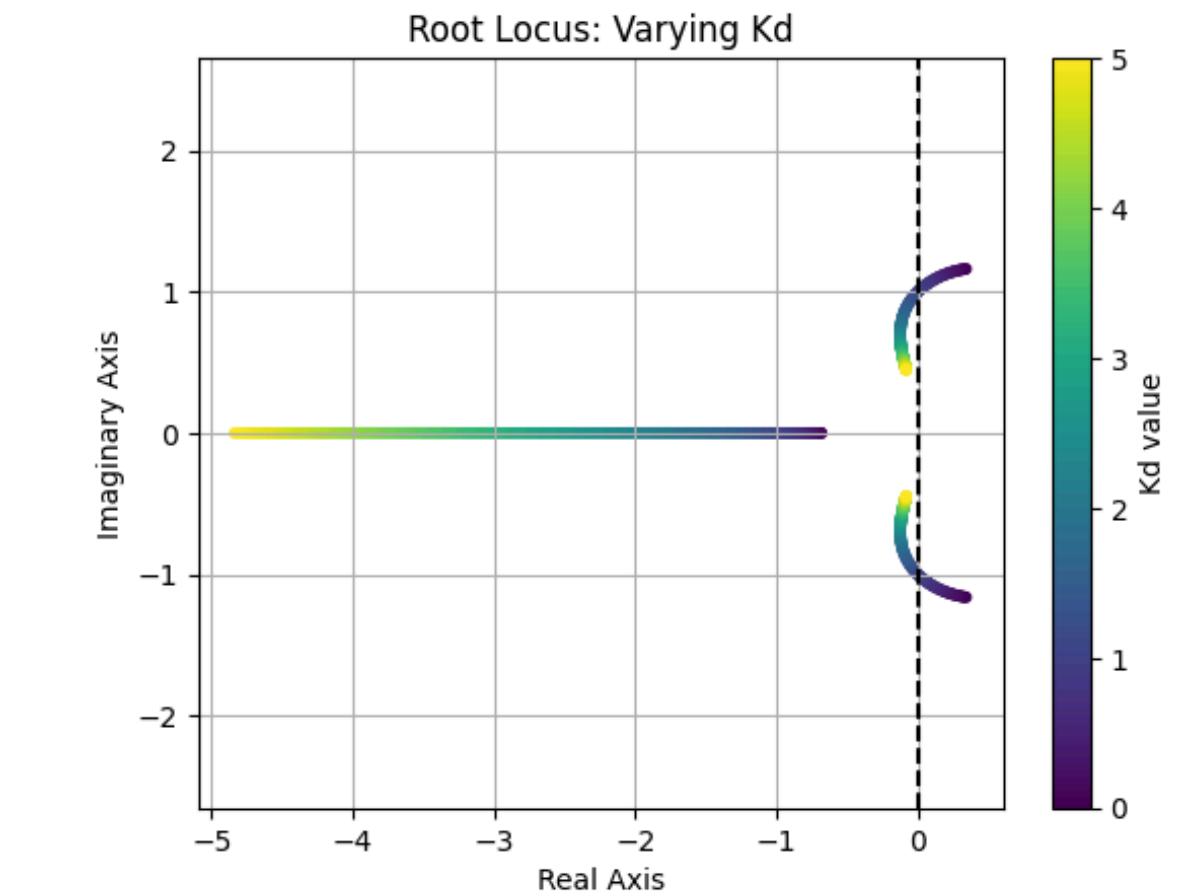
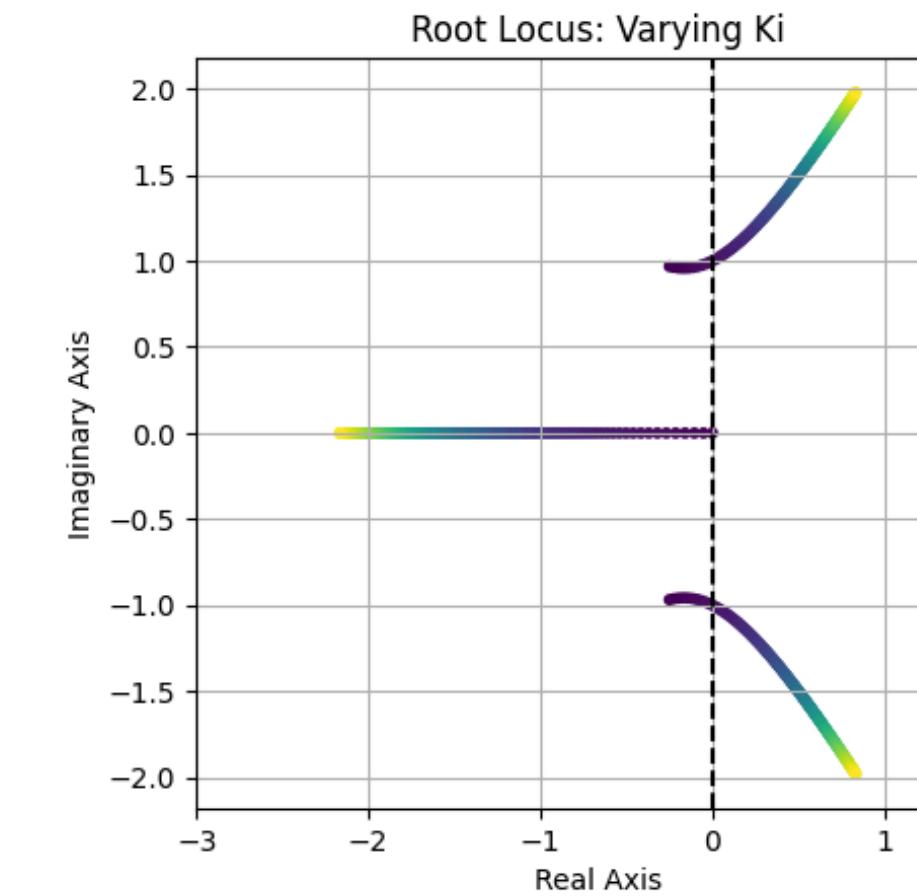
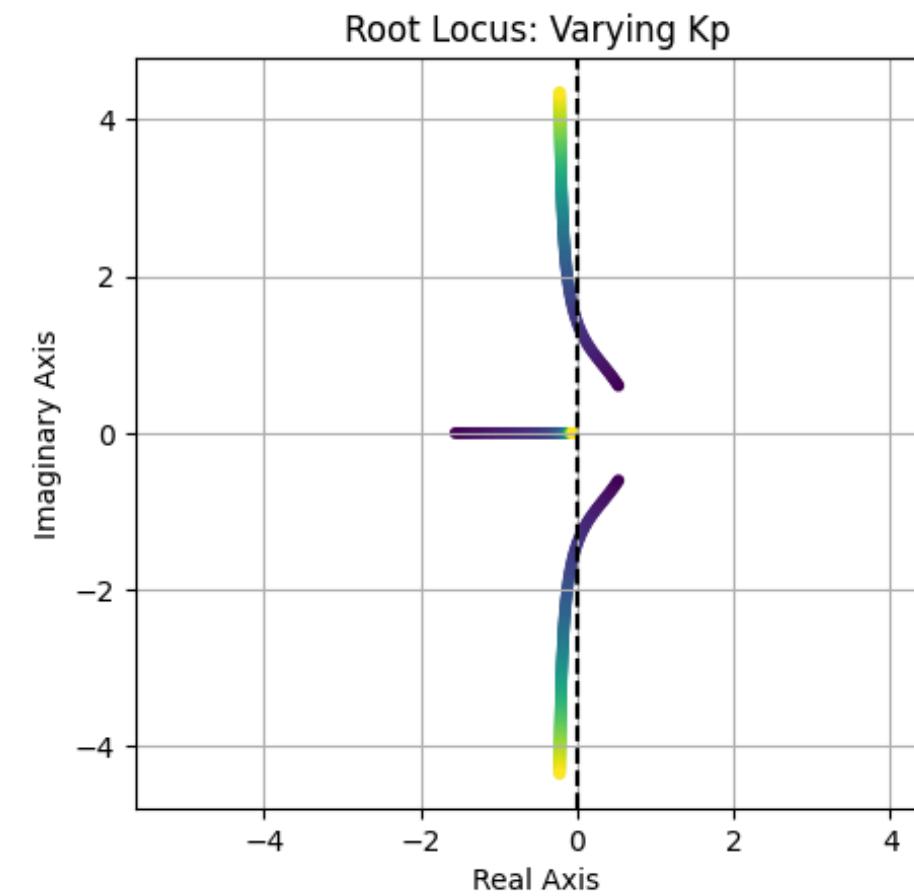


# Control theory recap

$$H(s) = \frac{N(s)}{D(s)} = K \frac{(s - z_1)(s - z_2) \dots (s - z_{m-1})(s - z_m)}{(s - p_1)(s - p_2) \dots (s - p_{n-1})(s - p_n)}$$

- Poles: Values of s that make the denominator D(s)=0
- Zeros: Values of s that make the numerator N(s) = 0
- Poles determine the system stability, natural frequencies, and response speed
- Zeros influence the shape and overshoot of the response

# PID Controller: Cautionary tale about tuning gains



# PID Controller: Cautionary tale about tuning gains



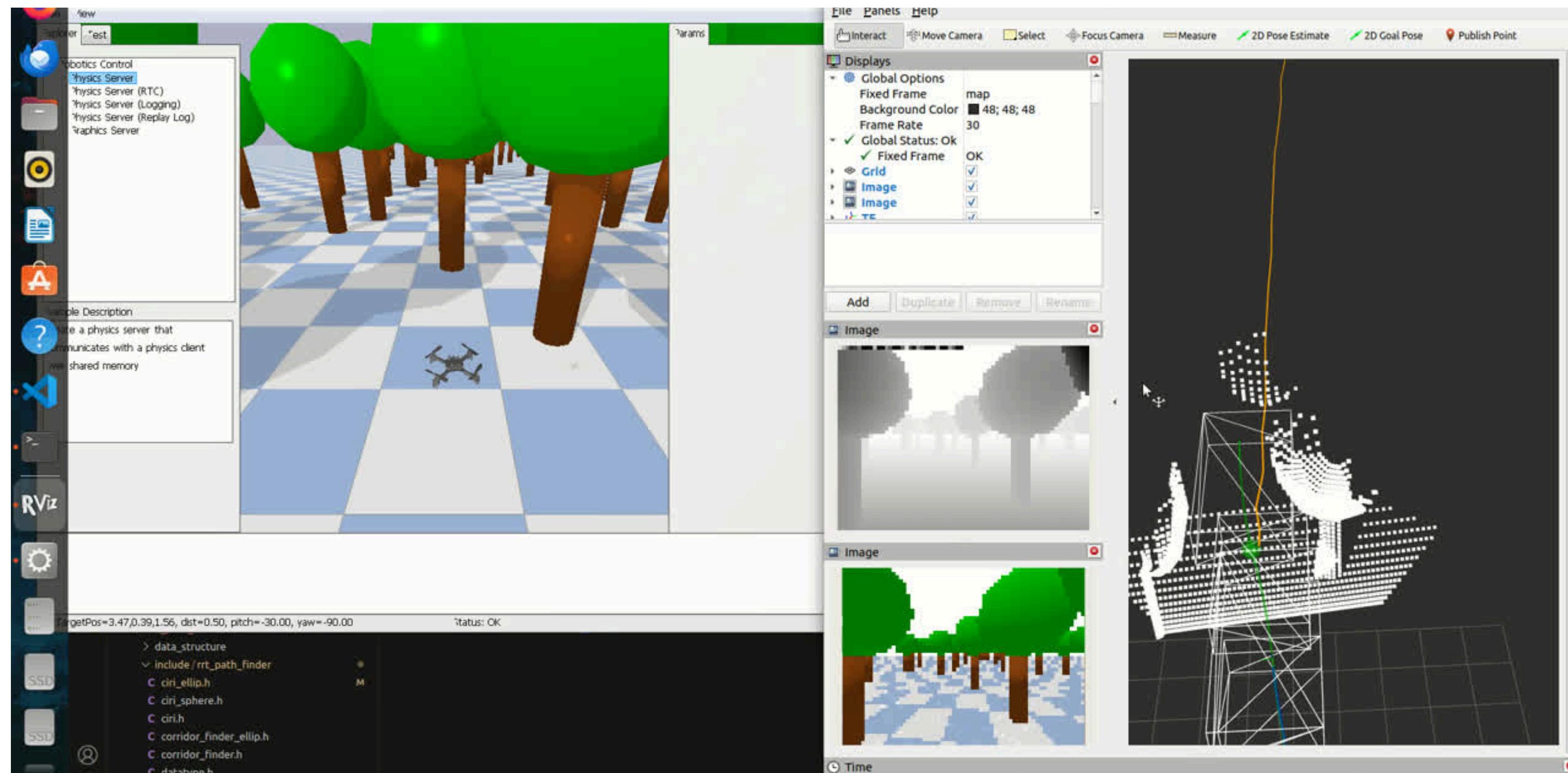
**Before**

# PID Controller: Cautionary tale about tuning gains

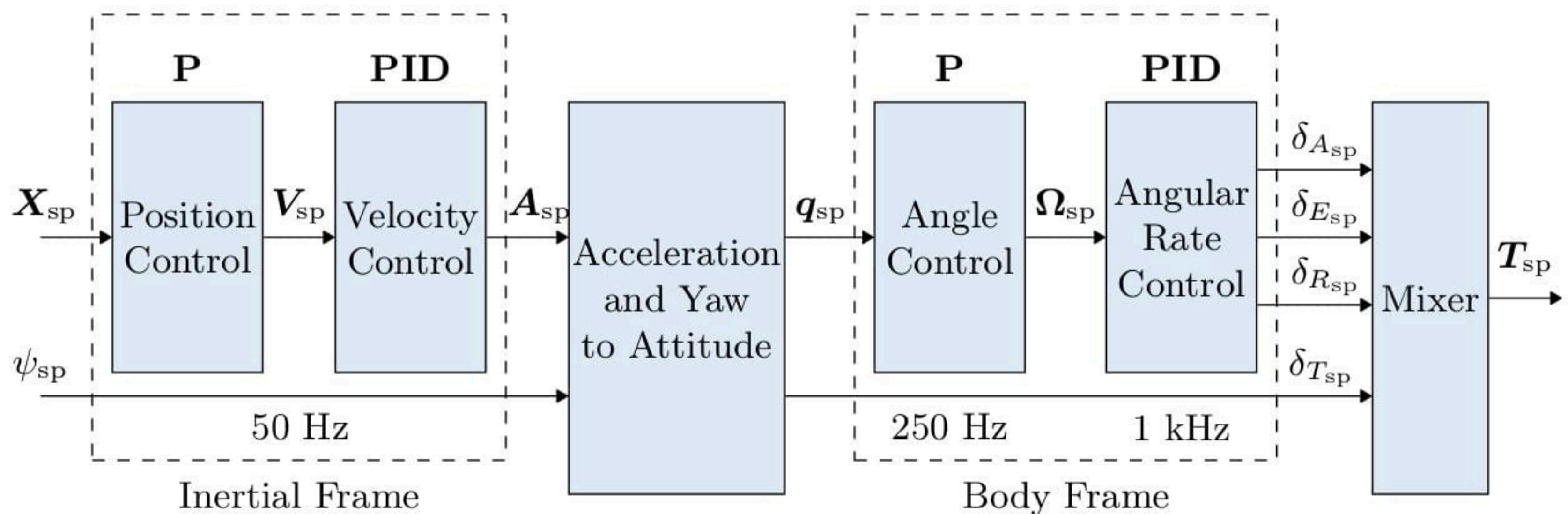


After

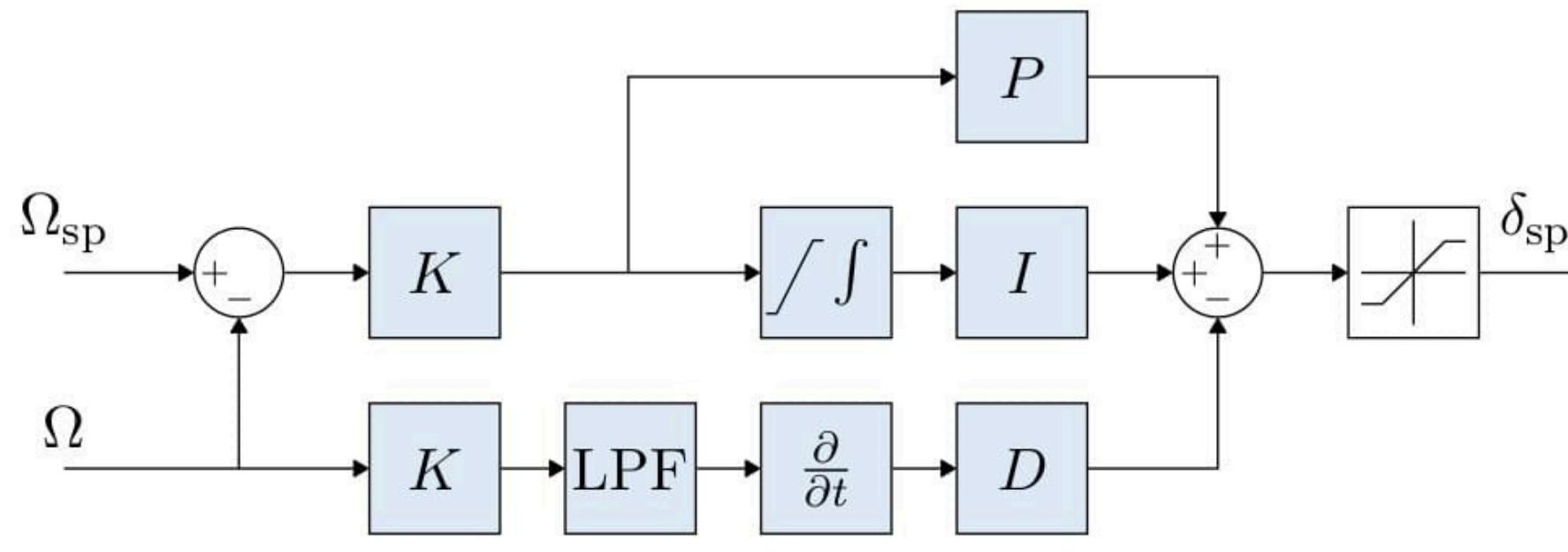
# Multirotor Controller



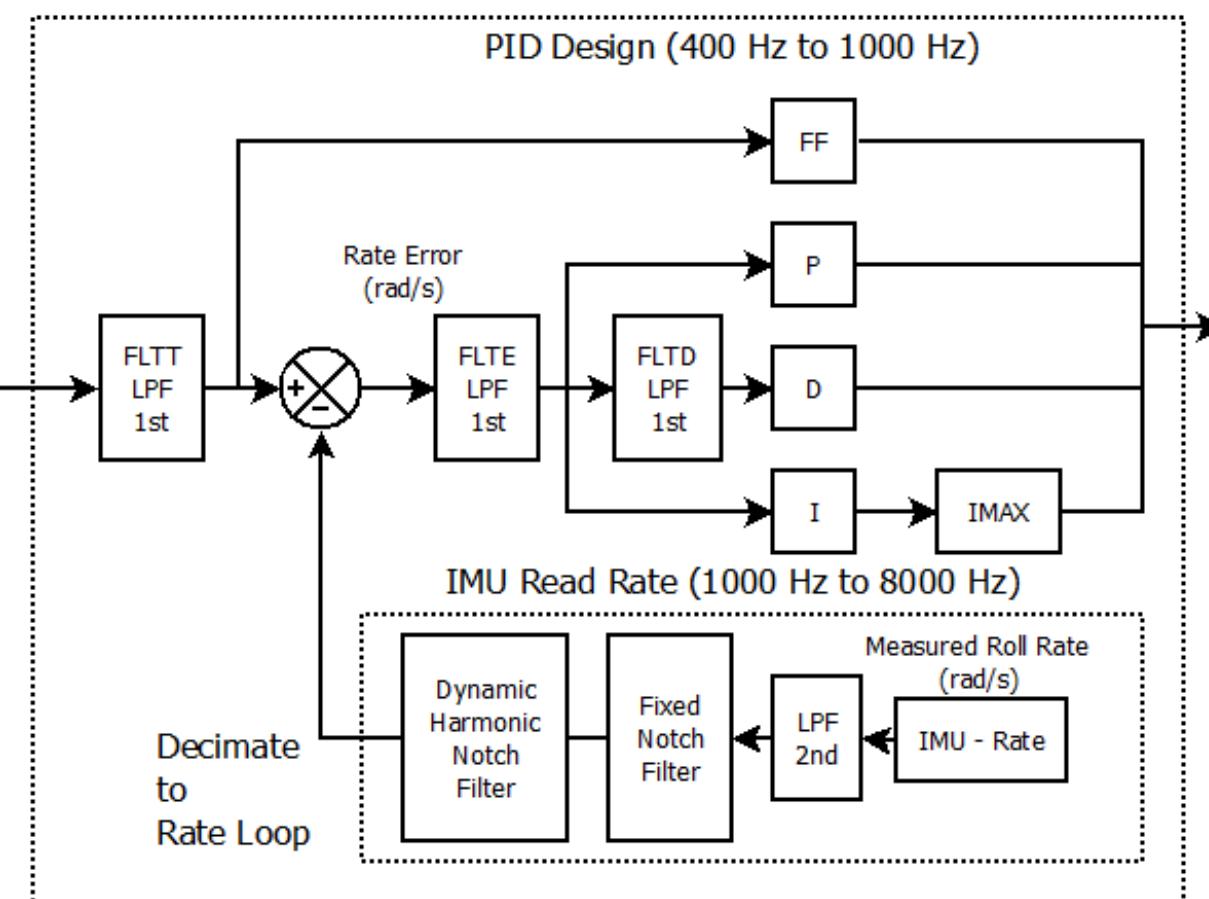
# Multirotor Controller



# Multirotor Controller: Inner loop rate tracking



**Discrepancy:** Angular rate derivative gain applied on sensor measurement rather than error between reference and measurement



# Multirotor Controller: Acceleration and Yaw to quaternion reference

$$\mathbf{z}_b = \frac{-\mathbf{a}_{des}}{\|\mathbf{a}_{des}\|}$$

$$\mathbf{x}_c = \begin{bmatrix} \cos \psi_{des} \\ \sin \psi_{des} \\ 0 \end{bmatrix}$$

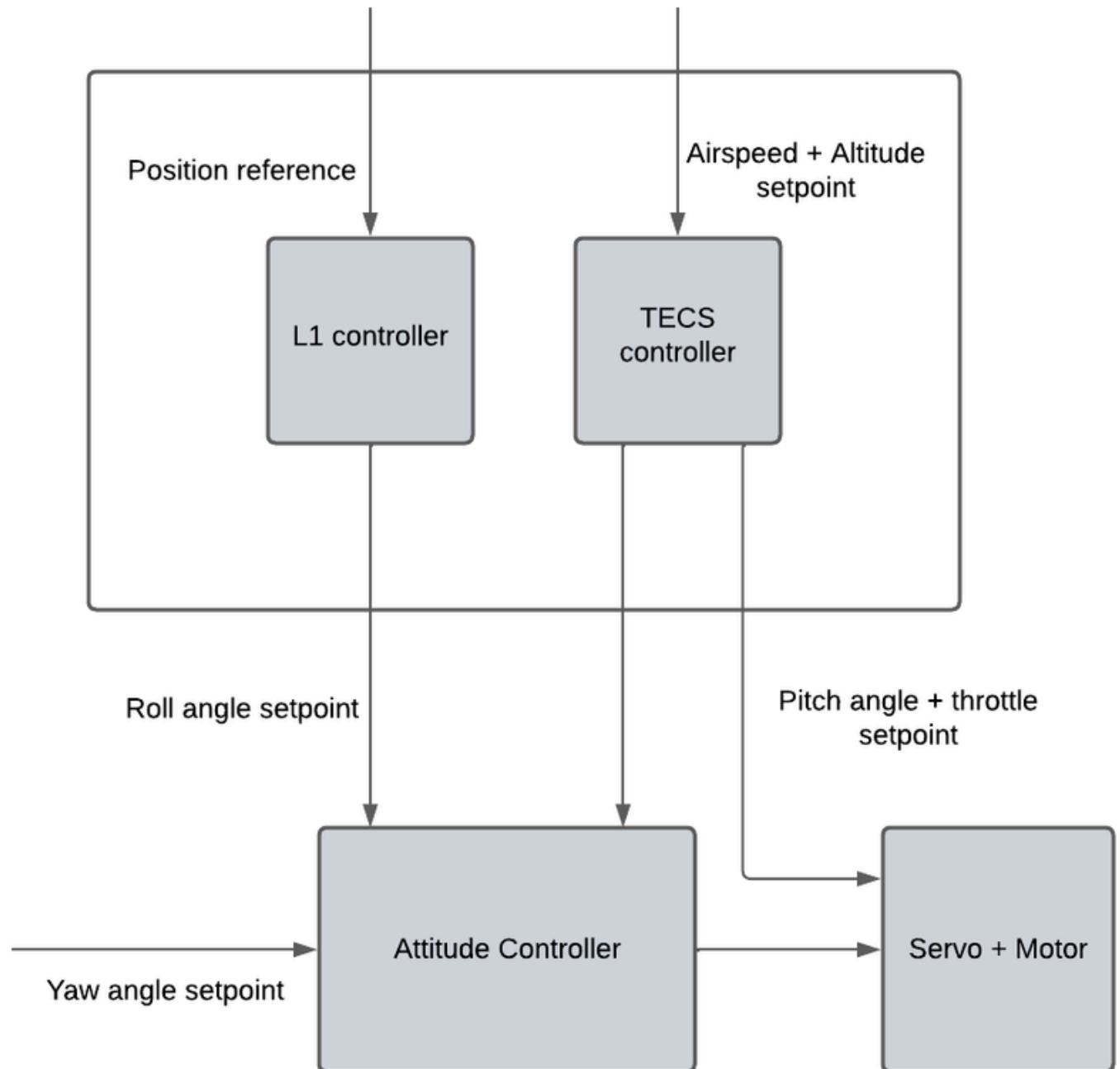
$$\mathbf{y}_b = \frac{\mathbf{z}_b \times \mathbf{x}_c}{\|\mathbf{z}_b \times \mathbf{x}_c\|}$$

$$\mathbf{x}_b = \mathbf{y}_b \times \mathbf{z}_b$$

$$\mathbf{R}_{des} = [\mathbf{x}_b \quad \mathbf{y}_b \quad \mathbf{z}_b]$$

**Note:** Implementation present in Ardupilot  
AC\_PosControl.cpp

# Fixed Wing Controller

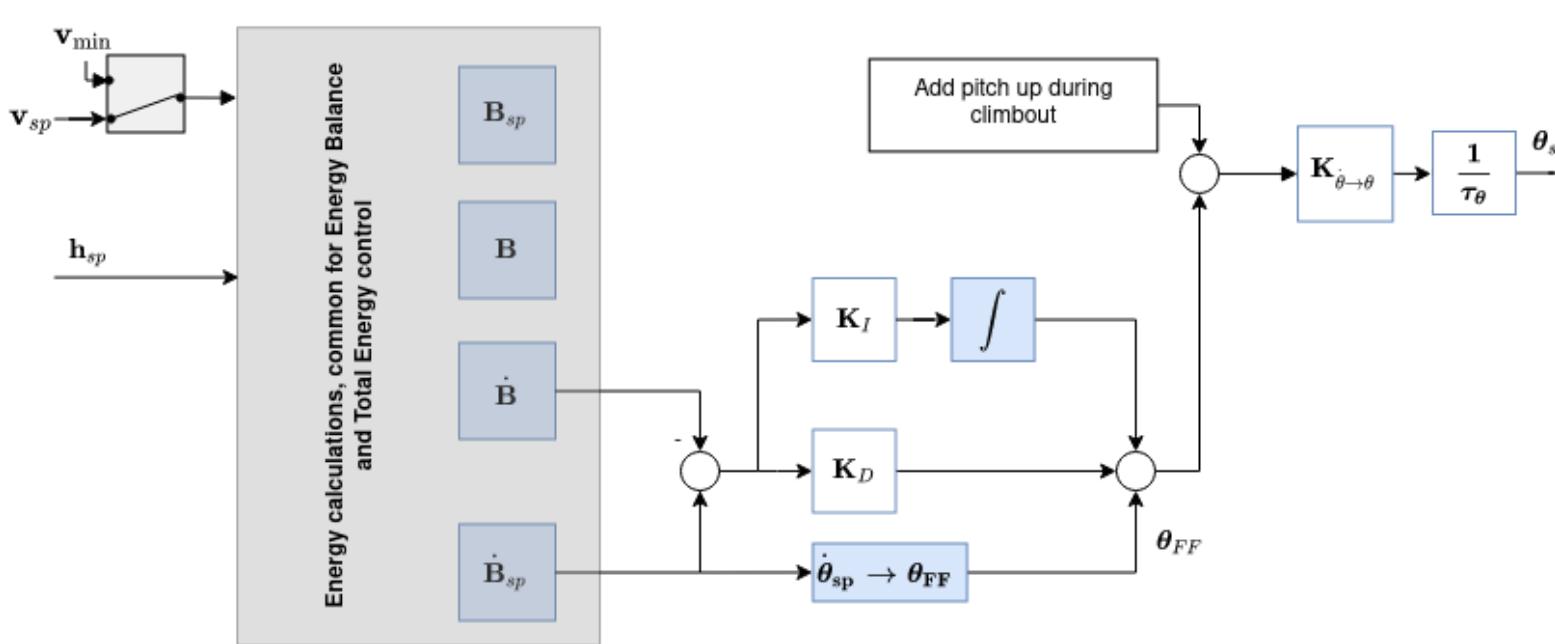


- Position controller consisting of TECS and L1 controller for controlling longitudinal and lateral motion respectively
- Attitude references obtained are tracked via a cascaded PID, similar to multirotor

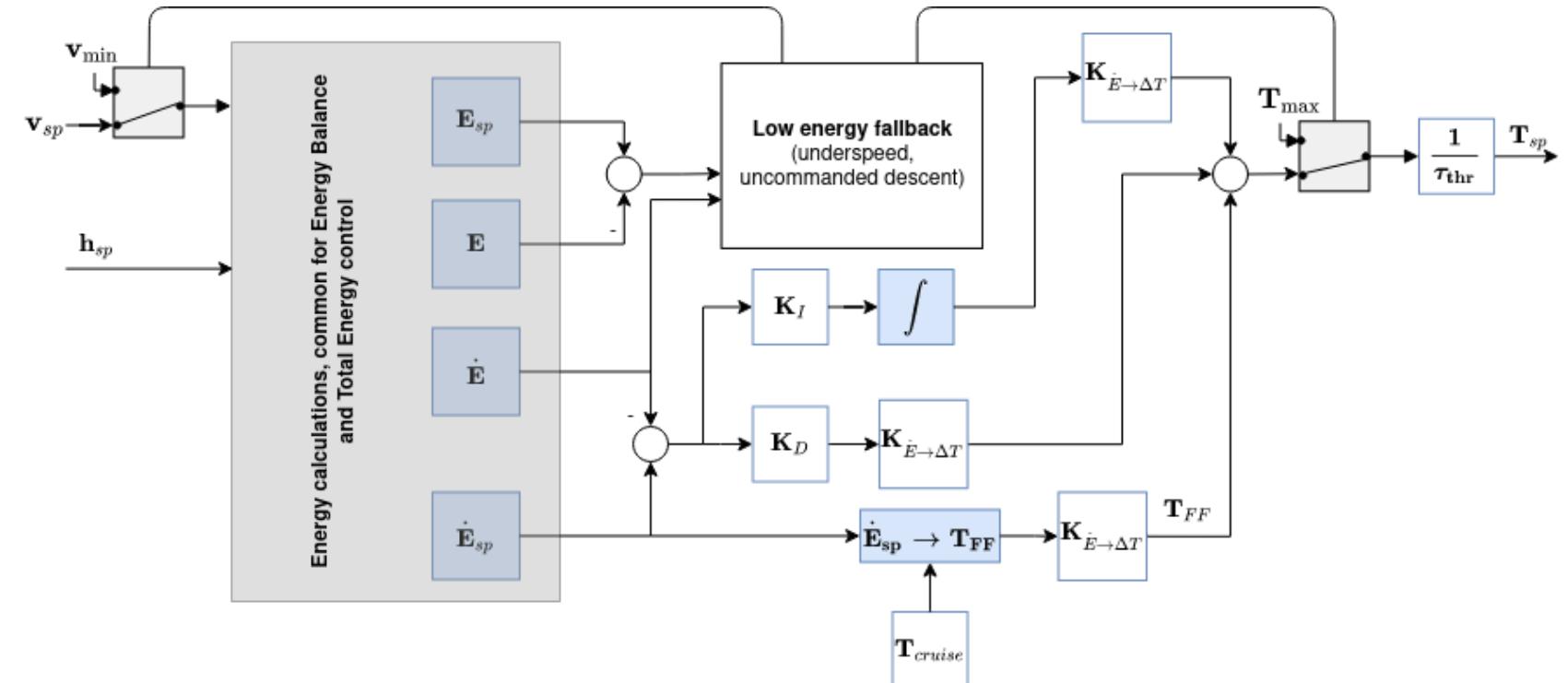
# Fixed Wing Controller: In Action



# Fixed Wing Controller: TECS



$h_{sp}$	height setpoint (a.m.s.l) [m]	$B_{sp}$	energy balance setpoint [ $m^2/s^2$ ]	$K_I$	pitch integrator gain	$\tau_\theta$	pitch time constant
$V_{sp}$	TAS airspeed setpoint [m/s]	$B$	energy balance [ $m^2/s^2$ ]	$K_D$	pitch damping gain	$\theta_{FF}$	balance rate feedforward
		$\dot{B}_{sp}$	energy balance rate setpoint	$K_{\dot{B} \rightarrow \theta}$	energy balance rate to pitch gain	$\theta_{sp}$	pitch setpoint
		$\dot{B}$	energy balance rate [ $m^2/s^3$ ]				

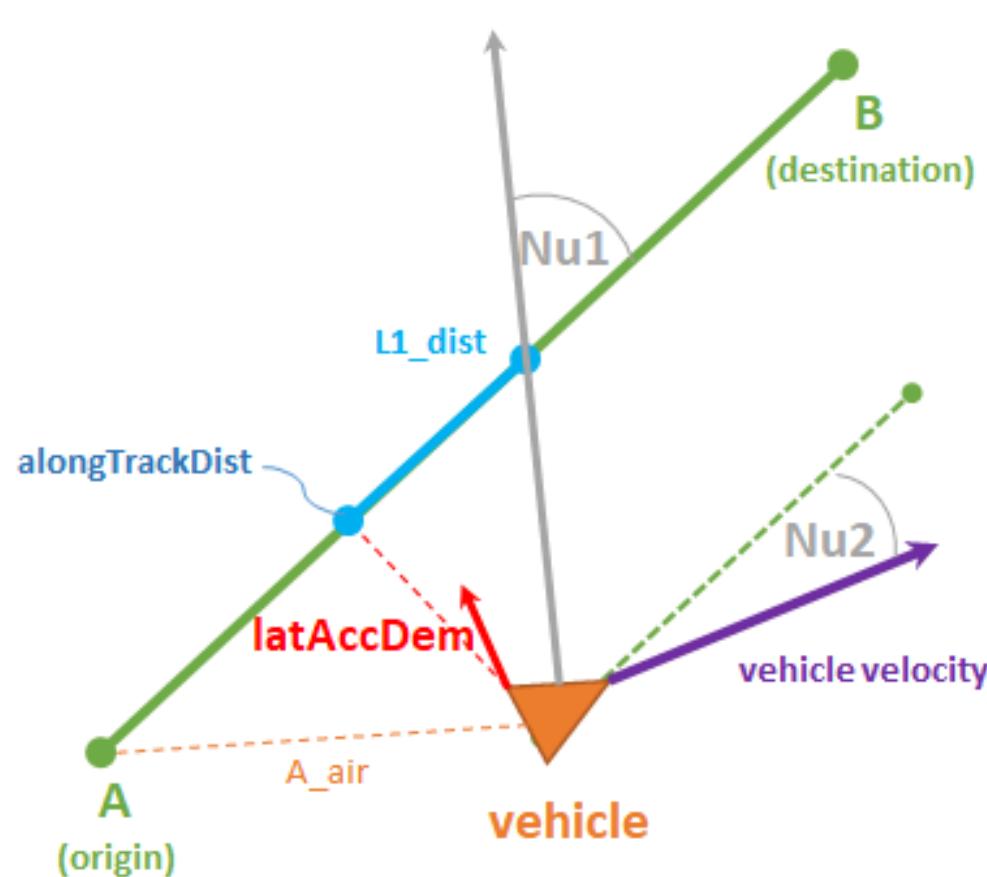


$h_{sp}$	height setpoint (a.m.s.l) [m]	$E_{sp}$	energy setpoint [ $m^2/s^2$ ]	$K_I$	throttle integrator gain	$\tau_{thr}$	throttle time constant
$V_{sp}$	TAS airspeed setpoint [m/s]	$E$	energy [ $m^2/s^2$ ]	$K_D$	throttle damping gain	$T_{FF}$	Feedforward throttle
		$\dot{E}_{sp}$	energy rate setpoint	$K_{\dot{E} \rightarrow \Delta T}$	energy rate to throttle	$T_{FF}$	Feedforward throttle
		$\dot{E}$	energy rate [ $m^2/s^3$ ]	$K_{\dot{E} \rightarrow \Delta T}$	energy rate to throttle	$T_{cruise}$	cruise throttle
						$T_{sp}$	throttle setpoint

Pitch controller (Energy balancing)

Throttle controller (Energy Addition)

# Fixed Wing Controller: L1

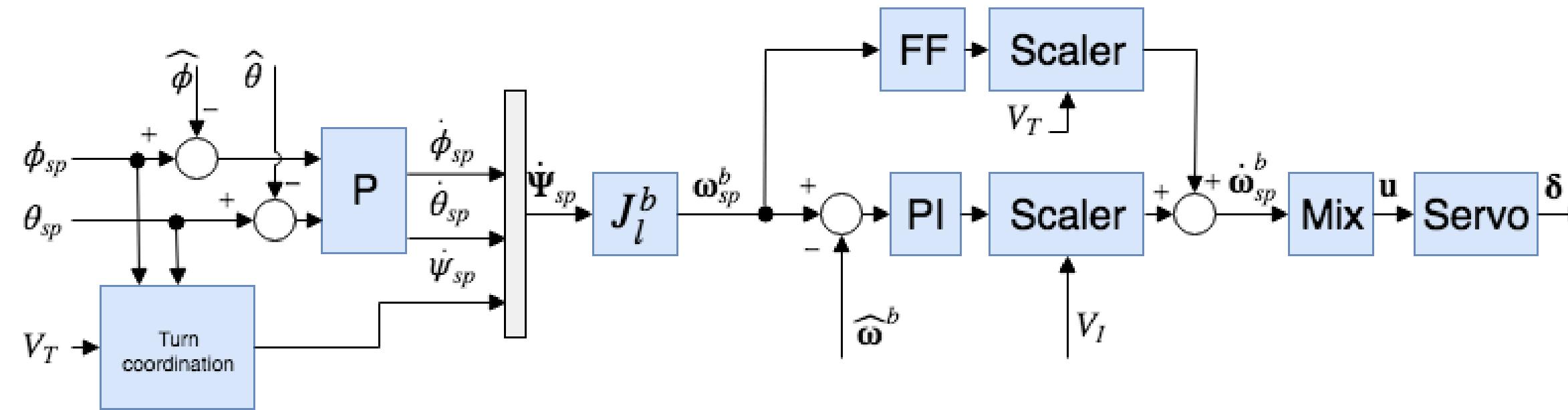


- L1 distance is a hyperparameter, defined as a look ahead distance for the UAV.
- Angle between LOS between L1 point and UAV and the UAV ground velocity is referred as  $\eta$ .

$$a_{\text{lat}} = 2 \frac{V^2}{L_1} \sin(\eta)$$

$$\phi_{\text{cmd}} = \arctan \left( \frac{a_{\text{lat}}}{g} \right)$$

# Fixed Wing Controller: Attitude Controller



$\Psi = [\phi \ \theta \ \psi]^T$  - attitude vector (NED)

$\omega^b$  - body rate vector (FRD)

$\mathbf{u}$  - actuators output

$V_T$  - true airspeed

$V_I$  - indicated airspeed

$J_l^b$  - Jacobian matrix from local to body

$\delta$  - actuator deflection

P - proportional gain

PI - proportional + integral controller

FF - feed-forward gain

Mix - mixer (control allocation)

Scaler - Scales controllers outputs using airspeed

$(\dot{x})$  - derivative of  $x$

$(\widehat{x})$  - estimated value of  $x$  (EKF)

$(x)_{sp}$  - setpoint of  $x$

# LQR control