

# Visual Inertial SLAM using Inertial Preintegration

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## Abstract

This document is a report on Visual Inertial SLAM using an efficient method of IMU pre-integration. The pre-integration method combines many IMU data as a single observation before fusion with camera images, resulting in a much reduced state and observation graph structure. An accurate map and robot path is hence obtainable in real-time. We present the pre-integration theory, including formulation of state, observation, covariance, observation model and Jacobians. We provide an implementation, obtained results of VIN SLAM with and without pre-integration. We also include a discussion of various methods of initialization along with their impact on linearization of the original problem. Based on our experimental results, we propose future research plans.

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# 1 Introduction

In this work, we firstly simulate a navigation system equipped with an IMU and an RGB camera.

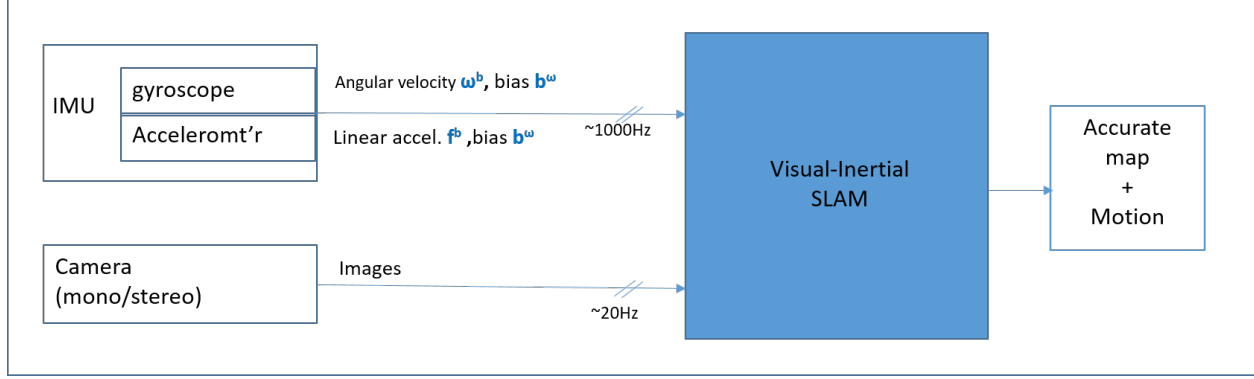


Figure 1: VIN SLAM

**States** The estimated state vector contains the 3-D vehicle position  $\mathbf{p}^n$ , velocity  $\mathbf{v}^n$  and Euler angles  $\mathbf{A}^n = [\alpha, \beta, \gamma]$ ; as well as the  $M$  feature locations  $(\mathbf{f}_i^n)$  in the environment where  $i = 1, \dots, N$ .

**Sensor data** The IMU readings include 3-D linear acceleration  $\mathbf{f}^b$  and angular rate  $\boldsymbol{\omega}^b$ , both given in body frame and come with non-zero bias :  $\mathbf{b}_f$  and  $\mathbf{b}_\omega$ .

Further, due to its design principal, the IMU can only measure acceleration with the gravity taken out, therefore the true vehicle's acceleration in the world frame should be

$$\mathbf{f}^n = R_b^n(\mathbf{f}^b - \mathbf{b}_f) + \mathbf{g}^n$$

$R_b^n$  and  $E_b^n$  are the rotation and rotation rate matrices. Superscript refers to the reference frame,  $^n$  is the global frame.

**The Original VIN model** The motion model based on IMU reading can be stated as

$$\begin{aligned}
 \Delta t &= t_{t+1} - t_t \\
 \mathbf{f}_t^n &= R_{bt}^n(\mathbf{f}_t^b - \mathbf{b}_f) \\
 \mathbf{v}_{t+1} &= \mathbf{v}_t + \mathbf{f}_t^n \Delta t + \mathbf{g}^n \Delta t \\
 \mathbf{p}_{t+1} &= \mathbf{p}_t + \mathbf{v}_t \Delta t \\
 \mathbf{A}_{t+1} &= \mathbf{A}_t + E_{bt}^n(\boldsymbol{\omega}_t^b - \mathbf{b}_\omega) \Delta t
 \end{aligned}$$

## 2 The original VIN problem

For a system composed of an IMU and a RGB-D camera navigating with  $N$  camera poses,  $K$  IMU sample per image and  $M$  features. The naive VIN problem includes all robot poses at IMU

samples.

**State Vector** the state vector  $\mathbf{X}$  is defined as:

$$\mathbf{x} = (\overbrace{\mathbf{A}_{10}, \mathbf{T}_{10}, \mathbf{A}_{20}, \mathbf{T}_{20}, \dots, \mathbf{A}_{K-1,0}, \mathbf{T}_{K-1,0}, \mathbf{A}_{0,1}, \mathbf{T}_{0,1}, \dots, \mathbf{A}_{K-1,1}, \mathbf{T}_{K-1,1}, \dots, \mathbf{A}_{K-1,N-1}, \mathbf{T}_{K-1,N-1}, \mathbf{A}_{0N}, \mathbf{T}_{0N}}^{K(N-1) \times 6}, \underbrace{\mathbf{F}_1, \mathbf{F}_2, \dots, \mathbf{F}_M}_{M \times 3}, \underbrace{\mathbf{v}_{00}, \mathbf{v}_{10}, \dots, \mathbf{v}_{K-1,0}, \dots, \mathbf{v}_{0,N-1}, \dots, \mathbf{v}_{K-1,N-1}, \mathbf{v}_{0N}}_{(K(N-1)+1) \times 3}, \mathbf{g}, \mathbf{A}_{u2c}, \mathbf{T}_{u2c}, \mathbf{b}_f, \mathbf{b}_w)'$$

**Observation Vector** The Observation vector  $\mathbf{Z}$  is defined as:

$$\begin{aligned} \mathbf{z}_{raw} &= (\mathbf{z}_{camera}, \mathbf{z}_{IMUraw}, \mathbf{z}_{Tv})' \\ &= (\underbrace{\mathbf{uv}_{11}, \mathbf{uv}_{21}, \dots, \mathbf{uv}_{M1}, \dots, \mathbf{uv}_{1N}, \mathbf{uv}_{2N}, \dots, \mathbf{uv}_{MN}}_{M \times N \times 2}, \underbrace{\omega \mathbf{a}_{01}, \omega \mathbf{a}_{11}, \dots, \omega \mathbf{a}_{(K-1)1}, \dots, \omega \mathbf{a}_{0(N-1)}, \omega \mathbf{a}_{1(N-1)}, \dots, \omega \mathbf{a}_{(K-1)(N-1)}}_{K \times (N-1) \times 6}, \end{aligned} \quad (1)$$

$$\underbrace{\mathbf{0}, \mathbf{0}, \dots, \mathbf{0}}_{K \times (N-1) \times 3})' \quad (2)$$

Clearly, such a large state space quickly becomes difficult to manage in practice. Further, each step of re-linearization, the integration from acceleration to velocity then to position has to be recomputed.

### 3 The Preintegration algorithm

Todd Lupton proposed the Preintegration method in 2012 [Lupton and Sukkarieh(2012)]: integrate a large number of high rate IMU observations into a single observation, making it faster and easier to deal with in a SLAM or navigation filter. IMU data are integrated in a body fixed frame that moves with the vehicle. Transformation to global frame only happens at end of integration, hence referred to as Pre-Integration.

**State Vector**  $\mathbf{X}$  is defined as:

$$\mathbf{x} = (\underbrace{\mathbf{A}_2^u, \mathbf{T}_2^u, \dots, \mathbf{A}_N^u, \mathbf{T}_N^u}_{(N-1) \times 6}, \underbrace{\mathbf{F}_1, \dots, \mathbf{F}_M}_{M \times 3}, \underbrace{\mathbf{v}_1, \dots, \mathbf{v}_N}_{N \times 3}, \mathbf{g}^n, \mathbf{A}_{u2c}, \mathbf{T}_{u2c}, \mathbf{b}_f, \mathbf{b}_w)'$$

where  $\mathbf{A}_i^u = (\alpha_i^u, \beta_i^u, \gamma_i^u)$ ,  $\mathbf{T}_i^u = (x_i^u, y_i^u, z_i^u)$ ,  $\mathbf{F}_i = (x_i, y_i, z_i)$ ,  $d\mathbf{P}_i = (dx_i, dy_i, dz_i)$ ,  $d\mathbf{v}_i = (dvx_i, dvy_i, dvz_i)$ , and  $d\mathbf{A}_i = (d\alpha_i, d\beta_i, d\gamma_i)$ .

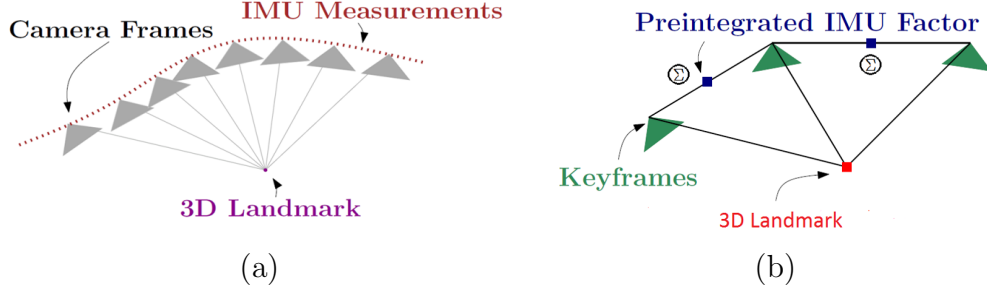


Figure 2: a) Samples: Camera+IMU b) Inertial-delta: preintegrated information [Forster and et al.(2015)]

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**Algorithm 1** The Pre-integration Method Based on Inertial Raw Data

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Inertial-delta observation =  $\begin{bmatrix} \Delta \mathbf{p}_t^+ \\ \Delta \mathbf{v}_t \\ \Delta \mathbf{A}_t \end{bmatrix}$ , initially set to  $\begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$

**for**  $t_1 < t < t_2$  **do**

$\Delta t = t_{t+1} - t_t$

$\mathbf{f}_t^{bt1} = R_{bt}^{bt1}(\mathbf{f}_t^b - \mathbf{b}_f)$

$\Delta \mathbf{v}_{t+1} = \Delta \mathbf{v}_t + \mathbf{f}_t^{bt1} \Delta t$

$\Delta \mathbf{p}_{t+1}^+ = \Delta \mathbf{p}_t^+ + \Delta \mathbf{v}_t \Delta t$

$\Delta \mathbf{A}_{t+1} = \Delta \mathbf{A}_t + E_{bt}^{bt1}(\omega_t^b - \mathbf{b}_\omega) \Delta t$

**end for**

---

**Observation vector** becomes:

$$\mathbf{z} = (\overbrace{\mathbf{u}\mathbf{v}\mathbf{d}_1, \dots, \mathbf{u}\mathbf{v}\mathbf{d}_N, \dots, \mathbf{u}\mathbf{v}\mathbf{d}_{1N}, \dots, \mathbf{u}\mathbf{v}\mathbf{d}_{MN}}^{M \times N \times 3}, \overbrace{d\mathbf{p}_2, d\mathbf{v}_2, d\mathbf{A}_2, \dots, d\mathbf{p}_N, d\mathbf{v}_N, d\mathbf{A}_N}^{(N-1) \times 9})'$$

where  $\mathbf{u}\mathbf{v}\mathbf{d}_{ij} = (u_{ij}, v_{ij}, d_{ij})$  represents the image of the  $i$ th feature point at the  $j$ th camera pose.

### 3.1 Bias-correction

Algorithm 1 gives the pre-integration process model, it is therefore possible to compute is uncertainty from that of IMU measurements. Also, the IMU readings contain biase values, so do not reflect the true motion's angular rate and acceleration. This is tackled in two steps. We first assume  $\mathbf{b}$  is known. Now let the difference between true bias and observed bias be  $\delta \mathbf{b} = \mathbf{b}^{obs} - \mathbf{b}^{est}$ ,

use first order expansion to get inertial delta's modified observation function.

$$\Delta \mathbf{p}^+(\mathbf{b}^{obs}) = \Delta \mathbf{p}^+(\mathbf{b}^{est}) - \frac{\partial \Delta \mathbf{p}^+(\mathbf{b}^{obs})}{\partial \mathbf{b}} * \delta \mathbf{b} \quad (3)$$

$$\Delta \mathbf{v}(\mathbf{b}^{obs}) = \Delta \mathbf{v}(\mathbf{b}^{est}) - \frac{\partial \Delta \mathbf{v}(\mathbf{b}^{obs})}{\partial \mathbf{b}} * \delta \mathbf{b} \quad (4)$$

$$\Delta \mathbf{A}(\mathbf{b}^{obs}) = \Delta \mathbf{A}(\mathbf{b}^{est}) - \frac{\partial \Delta \mathbf{A}(\mathbf{b}^{obs})}{\partial \mathbf{b}} * \delta \mathbf{b} \quad (5)$$

$$\mathbf{b}^{obs} = \mathbf{b}^{est} - I_3 * \delta \mathbf{b} \quad (6)$$

Note this  $\delta \mathbf{b}$  is exactly the delta increment we want to compute in each Gauss Newton iteration. Therefore an analytic formula of inertial delta to Jacobian to bias is needed.

### 3.2 Modified process model for Inertial-delta + Bias

To analyze the unknown bias term, a new process model is formed using Algorithm 1, it involves evolution of inertial delta and bias, as illustrated in algorithm 2 We will need Jacobian of this

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**Algorithm 2** The Pre-integration Method Based on Inertial Raw Data

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Inertial-delta observation =  $\begin{bmatrix} \Delta \mathbf{p}_t^+ \\ \Delta \mathbf{v}_t \\ \Delta \mathbf{A}_t \\ \mathbf{b}_a^{obs} \\ \mathbf{b}_\omega^{obs} \end{bmatrix}$ , initially set to  $\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$

**for**  $t_1 < t < t_2$  **do**

$\Delta t = t_{t+1} - t_t$

$\mathbf{f}_t^{bt1} = R_{bt}^{bt1}(\mathbf{f}_t^b - \mathbf{b}_f^{obs}) = R_{bt}^{bt1}(\mathbf{f}_t^b - \mathbf{b}_f^{est} + \delta \mathbf{b}_f)$

$\Delta \mathbf{v}_{t+1} = \Delta \mathbf{v}_t + \mathbf{f}_t^{bt1} \Delta t$

$\Delta \mathbf{p}_{t+1}^+ = \Delta \mathbf{p}_t^+ + \Delta \mathbf{v}_t \Delta t$

$\Delta \mathbf{A}_{t+1} = \Delta \mathbf{A}_t + E_{bt}^{bt1}(\omega_t^b - \mathbf{b}_\omega^{obs}) \Delta t = \Delta \mathbf{A}_t + E_{bt}^{bt1}(\omega_t^b - \mathbf{b}_\omega^{est} + \delta \mathbf{b}_\omega) \Delta t$

$\mathbf{b}_f^{obs} = \mathbf{b}_a^{est} - \delta \mathbf{b}_f$

$\mathbf{b}_\omega^{obs} = \mathbf{b}_\omega^{est} - \delta \mathbf{b}_\omega$

**end for**

---

modified process to its process vector to account for inertial delta's Jacobian on bias in later section.

### 3.3 Inertial delta $\Sigma$ and Jacobian for Bias

Now, it should be easy to compute inertial delta's uncertainty and Jacobian recursively based on definition of discrete integration process, see Figure 3.

The algorithm 1 is modified to include  $\mathbf{b}$  as part of process vector, as shown in Algorithm 2. The integration process is recursive, therefore the inertial delta's uncertainty  $\Sigma$  and Jacobian  $J$  (now against both inertial delta and Bias terms ) are computed recursively, starting from zero uncertainty and unity gain at the beginning. This process is listed in algorithm 3.

### Pre-integration in recursive form

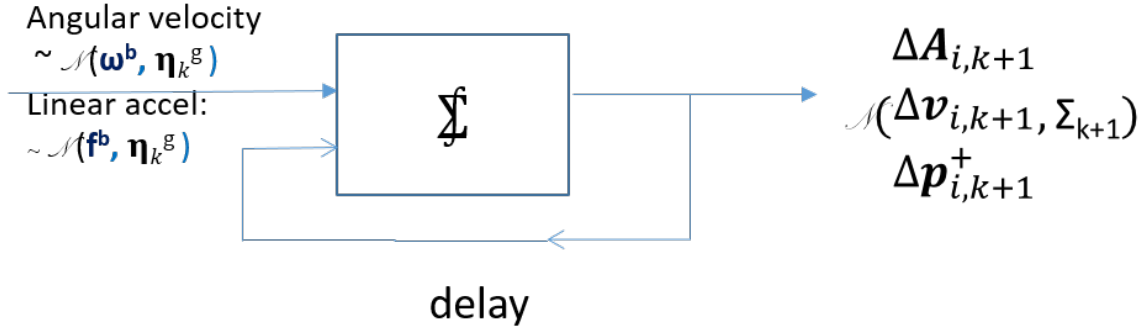


Figure 3: Pre-Integration

In each discrete summation step, state covariance  $\Sigma_t$  is related to the uncertainty at  $t - 1$   $\Sigma_t$  (Fig ??) and current measurement noise by  $F_t$  and  $G_t$ , where  $F_t$  and  $G_t$  are the Jacobians of the state transition function w.r.t the state vector inertial delta and the noise input  $\boldsymbol{\eta}_k$  respectively.

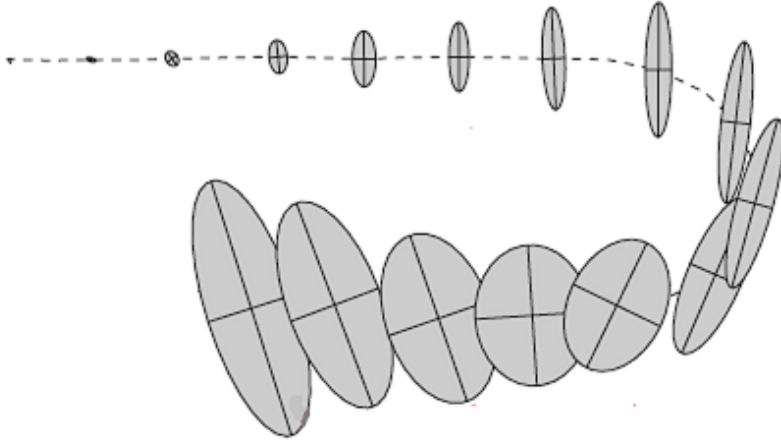


Figure 4: Evolution of uncertainty during Pre-Integration

The modified process's Jacobian  $J_t$  is a chain product of previous process's Jacobian  $J_{t-1}$  and state transition Jacobian  $F_{t-1}$ . The Jacobian's structure is shown in Equation 7.

$$[h!]J = \begin{bmatrix} \frac{\partial \Delta \mathbf{p}_{t2}^+}{\partial \mathbf{p}_{t1}^{t1}} & \frac{\partial \Delta \mathbf{p}_{t2}^+}{\partial \mathbf{v}_{t1}^{t1}} & \frac{\partial \Delta \mathbf{p}_{t2}^+}{\partial \mathbf{A}_{t1}^{t1}} & \frac{\partial \Delta \mathbf{p}_{t2}^+}{\partial \mathbf{b}_f} & \frac{\partial \Delta \mathbf{p}_{t2}^+}{\partial \mathbf{b}_\omega} \\ \mathbf{0}_3 & \frac{\partial \Delta \mathbf{v}_{t2}}{\partial \mathbf{v}_{t1}^{t1}} & \frac{\partial \Delta \mathbf{v}_{t2}}{\partial \mathbf{A}_{t1}^{t1}} & \frac{\partial \Delta \mathbf{v}_{t2}}{\partial \mathbf{b}_f} & \frac{\partial \Delta \mathbf{v}_{t2}}{\partial \mathbf{b}_\omega} \\ \mathbf{0}_3 & \mathbf{0}_3 & \frac{\partial \Delta \mathbf{A}_{t2}}{\partial \mathbf{A}_{t1}^{t1}} & \mathbf{0}_3 & \frac{\partial \Delta \mathbf{A}_{t2}}{\partial \mathbf{b}_\omega} \\ \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \frac{\partial \mathbf{b}_f^{obs}}{\partial \mathbf{b}_f} & \mathbf{0}_3 \\ \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \frac{\partial \mathbf{b}_\omega^{obs}}{\partial \mathbf{b}_\omega} \end{bmatrix} \quad (7)$$

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**Algorithm 3** The Covariance Matrix for the Pre-integration Method
 

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 $J_t = \mathbf{I}_{15}$ 
 $\Sigma_t = \mathbf{I}_{15}$ 
for  $t_1 < t < t_2$  do
   $\Delta t = t_{t+1} - t_t$ 
   $\alpha = \frac{dR_{bt}^{bt1}(\mathbf{f}_t - \mathbf{b}_f)}{d\mathbf{A}_t}$ 
   $\beta = \frac{dE_{bt}^{bt1}(\boldsymbol{\omega}_t - \mathbf{b}_\omega)}{d\mathbf{A}_t}$ 
   $F_t = \begin{bmatrix} \mathbf{I}_3 & \mathbf{I}_3 \Delta t & \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 \\ \mathbf{0}_3 & \mathbf{I}_3 & \alpha \Delta t & -R_{bt}^{bt1} \Delta t & \mathbf{0}_3 \\ \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{I}_3 + \beta \Delta t & \mathbf{0}_3 & -E_{bt}^{bt1} \Delta t \\ \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{I}_3 & \mathbf{0}_3 \\ \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{0}_3 & \mathbf{I}_3 \end{bmatrix}$ 
   $G_t = \begin{bmatrix} \mathbf{0}_3 & \mathbf{0}_3 \\ R_{bt}^{bt1} \Delta t & \mathbf{0}_3 \\ \mathbf{0}_3 & E_{bt}^{bt1} \Delta t \\ \mathbf{0}_3 & \mathbf{0}_3 \\ \mathbf{0}_3 & \mathbf{0}_3 \end{bmatrix}$ 
   $J_{t+1} = F_t J_t$ 
   $\Sigma_{t+1} = F_t \Sigma_t F_t' + G_t Q_t G_t'$ 
end for
 $J_{t1}^{t2} = J_t$ 
 $\Sigma_{t1}^{t2} = \Sigma_t$ 

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### 3.4 Pre-Integration observation model

Now the expanded Pre-Integration observation model (from Eq 3 5 )is:

$$d\mathbf{p}_i = R_i(\mathbf{T}_{i+1} - \mathbf{T}_i - \mathbf{v}_i \Delta t - \frac{1}{2} \mathbf{g}(\Delta t)^2) - \frac{\partial \Delta \mathbf{p}_t^+}{\partial \mathbf{b}_f}(\mathbf{b}_f - \mathbf{b}_{f0}) - \frac{\partial \Delta \mathbf{p}_t^+}{\partial \mathbf{b}_\omega}(\mathbf{b}_\omega - \mathbf{b}_{\omega0}) \quad (8)$$

$$d\mathbf{v}_i = R_i(\mathbf{v}_{i+1} - \mathbf{v}_i - \mathbf{g} \Delta t) - \frac{\partial \Delta \mathbf{v}_t}{\partial \mathbf{b}_f}(\mathbf{b}_f - \mathbf{b}_{f0}) - \frac{\partial \Delta \mathbf{v}_t}{\partial \mathbf{b}_\omega}(\mathbf{b}_\omega - \mathbf{b}_{\omega0}) \quad (9)$$

$$d\mathbf{A}_i = fn\_ABGFromR(R_{i+1} * R_i') - \frac{\partial \Delta \mathbf{A}_t}{\partial \mathbf{b}_\omega}(\mathbf{b}_\omega - \mathbf{b}_{\omega0}) \quad (10)$$

where  $i = 2, \dots, N$ ,  $fn\_ABGFromR$  is a function that can obtain Euler angles from a corresponding rotation matrix, and  $R_i, E_i$  correspond to the rotation matrix and rotation rate matrix for the IMU at the time step  $i$ . respectively.

#### 3.4.1 Feature observation model

From feature to its observation by the camera, [Hartley and Zisserman(2004)] tell us the following relationship holds:



$$\mathbf{F}_{ij} = (x_{ij}, y_{ij}, z_{ij}) = R_{cj}(\mathbf{F}_{fi} - \mathbf{T}_{c0j}) \quad (11)$$

$$u_{ij} = f * x_{ij}/z_{ij} + cx_0 \quad (12)$$

$$v_{ij} = f * y_{ij}/z_{ij} + cy_0 \quad (13)$$

$$d_{ij} = z_{ij} \quad (14)$$

where  $f$  is the focal length of the camera,  $(cx_0, cy_0)$  is the displacement of the origin of the camera.

### 3.4.2 Complete observation model

Putting all items together,  $H(\mathbf{x})$  can be written as:

$$\begin{aligned} H(\mathbf{x}) &= (H_{camera}(\mathbf{x}), H_{IMU_{int}}(\mathbf{x})) \\ &= (\overbrace{(u_{11}, v_{11}, \dots, u_{M1}, v_{M1}, \dots, u_{1N}, v_{1N}, \dots, u_{MN}, v_{MN})}^{M \times N \times 2}, \\ &\quad \overbrace{(d\mathbf{p}_2, d\mathbf{v}_2, d\mathbf{A}_2, \dots, d\mathbf{p}_N, d\mathbf{v}_N, d\mathbf{A}_N)}^{(N-1) \times 9}) \end{aligned} \quad (15)$$

## 3.5 Jacobian of Inertial Delta to X

Based on the composition of  $H(\mathbf{x})$ , the corresponding Jacobian matrix can be calculated.

For camera observations of  $(u_{ij}, v_{ij}, d_{ij})$  which represent the observation of the  $i$ th feature at the  $j$ th camera pose,

$$\frac{\partial u_{ij}}{\partial \mathbf{F}_{ij}} = [f/z_{ij}, 0, -fx_{ij}/z_{ij}^2] \quad (16)$$

$$\frac{\partial v_{ij}}{\partial \mathbf{F}_{ij}} = [0, f/z_{ij}, -fy_{ij}/z_{ij}^2] \quad (17)$$

$$\frac{\partial d_{ij}}{\partial \mathbf{F}_{ij}} = [0, 0, 1] \quad (18)$$

$$\frac{\partial \mathbf{F}_{ij}}{\partial \mathbf{A}_j} = R_{u2c} \frac{\partial R_j}{\partial \mathbf{A}_j} (\mathbf{F}_{i1} - \mathbf{T}_j) \quad (19)$$

$$\frac{\partial \mathbf{F}_{ij}}{\partial \mathbf{T}_j} = -R_{u2c} R_j \quad (20)$$

$$\frac{\partial \mathbf{F}_{ij}}{\partial \mathbf{A}_{u2c}} = \frac{\partial R_{u2c}}{\partial \mathbf{A}_{u2c}} R_j (\mathbf{F}_{i1} - R'_j \mathbf{T}_{u2c} - \mathbf{T}_j) \quad (21)$$

$$\frac{\partial \mathbf{F}_{ij}}{\partial \mathbf{T}_{u2c}} = -R_{u2c} \quad (22)$$

$$\frac{\partial \mathbf{F}_{ij}}{\partial \mathbf{F}_{i1}} = R_{u2c} R_j \quad (23)$$

For  $dp_i^+$ ,

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{A}_i} = \frac{\partial R_i}{\partial \mathbf{A}_i} (\mathbf{T}_{i+1} - \mathbf{T}_i - \mathbf{v}_i \Delta t - \frac{1}{2} \mathbf{g} (\Delta t)^2) \quad (24)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{T}_i} = -R_i \quad (25)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{T}_{i+1}} = R_i \quad (26)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{v}_i} = -R_i \Delta t \quad (27)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{g}} = -\frac{1}{2} R_i \Delta t^2 \quad (28)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{b}_f} = -\frac{\partial \Delta \mathbf{p}_t^+}{\partial \mathbf{b}_f} \quad (29)$$

$$\frac{\partial d\mathbf{p}_i^+}{\partial \mathbf{b}_\omega} = -\frac{\partial \Delta \mathbf{p}_t^+}{\partial \mathbf{b}_\omega} \quad (30)$$

For  $d\mathbf{v}_i$ ,

$$\frac{\partial d\mathbf{v}_i}{\partial R_i} = \frac{\partial R_i}{\partial \mathbf{A}_i} (\mathbf{v}_{i+1} - \mathbf{v}_i - \mathbf{g} \Delta t) \quad (31)$$

$$\frac{\partial d\mathbf{v}_i}{\partial \mathbf{v}_i} = -R_i \quad (32)$$

$$\frac{\partial d\mathbf{v}_i}{\partial \mathbf{v}_{i+1}} = R_i \quad (33)$$

$$\frac{\partial d\mathbf{v}_i}{\partial \mathbf{g}} = -R_i \Delta t \quad (34)$$

$$\frac{\partial d\mathbf{v}_i}{\partial \mathbf{b}_f} = -\frac{\partial \Delta \mathbf{v}_t}{\partial \mathbf{b}_f} \quad (35)$$

$$\frac{\partial d\mathbf{v}_i}{\partial \mathbf{b}_\omega} = -\frac{\partial \Delta \mathbf{v}_t}{\partial \mathbf{b}_\omega} \quad (36)$$

For  $d\mathbf{A}_i$ ,

$$\frac{\partial \Delta \mathbf{A}_i}{\partial \mathbf{A}_i} = \frac{\partial f n}{\partial R} R_{i+1} \frac{\partial R_i}{\partial \mathbf{A}_i} \quad (37)$$

$$\frac{\partial \Delta \mathbf{A}_i}{\partial \mathbf{A}_{i+1}} = \frac{\partial f n}{\partial R} \frac{\partial R_{i+1}}{\partial \mathbf{A}_{i+1}} R_1 \quad (38)$$

$$\frac{\partial \Delta \mathbf{A}_i}{\partial \mathbf{b}_\omega} = -\frac{\partial \Delta \mathbf{A}_t}{\partial \mathbf{b}_\omega} \quad (39)$$

### 3.5.1 Bias Jacobian

Table ?? shows the contents of inertial delta Jacobian. We will borrow the parts related to Bias, i.e. last 6 columns of  $J_{t1}^{t2}$  for inclusion in the pre-integration observation model.

## 4 Experimental results

### 4.1 Comparison of Naive VIN vs Pre-Integration

A matlab routine *Main\_simuNpose.m* was prepared to simulate VIN system and evaluate the performance of VIN with and without Pre-Integration. Table 1 shows performance results of Naive VIN vs Pre-integration. The later is much more efficient.

Table 1: Caption for the table.

Num image frames		Naive VIN	Pre-Integration
10	Total time	39.1 [sec]	4.4 [sec]
	$\delta X$	4.2	15.7
20	Total time	145.1 [sec]	9.1 [sec]
	$\delta X$	7.69	3.87
100	Total time	NIL	44.5 [sec]
	$\delta X$	NIL	12

A simulation run of Pre-integration is shown in Figure ??.

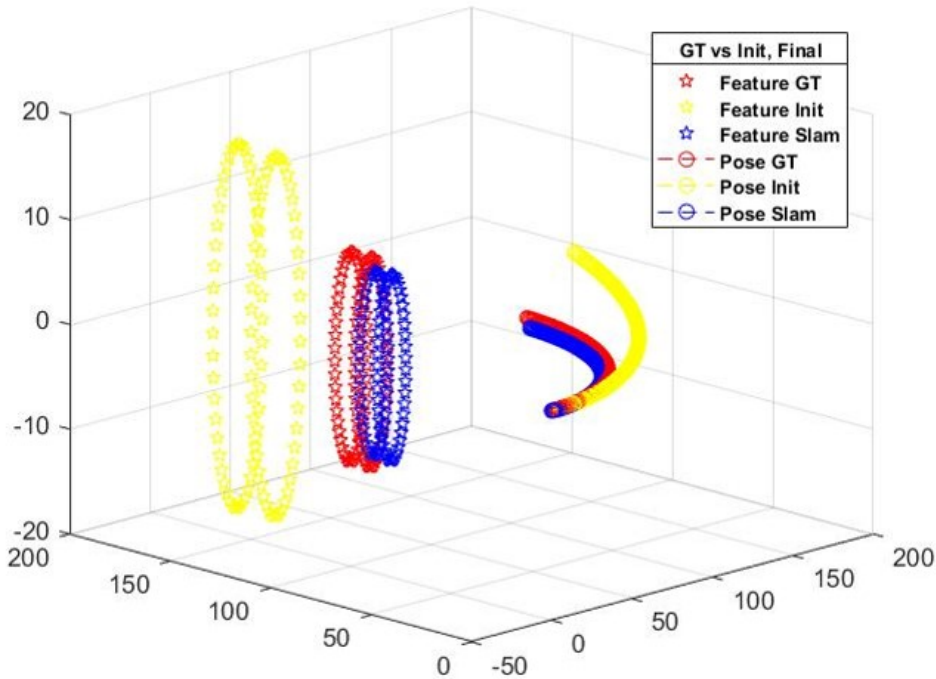


Figure 5: SimuNpose Naive vs Preintegration VIN

## 4.2 Incremental implementation of Pre-Integration

Direct initialization may lead to errors for long tests. This problem is solved by incremental introduction of new camera poses. Starting with limited number of frames, obtain optimized robot poses and features. Now introduce new observation, using previously obtained values as initial guess in new optimization, expand state vectors if necessary. Repeat process until all observations are covered. A matlab routine *Main.inc.m* was developed to simulate the process, see Fig 6 for illustration. Note: this is in effect similar to iSam2.

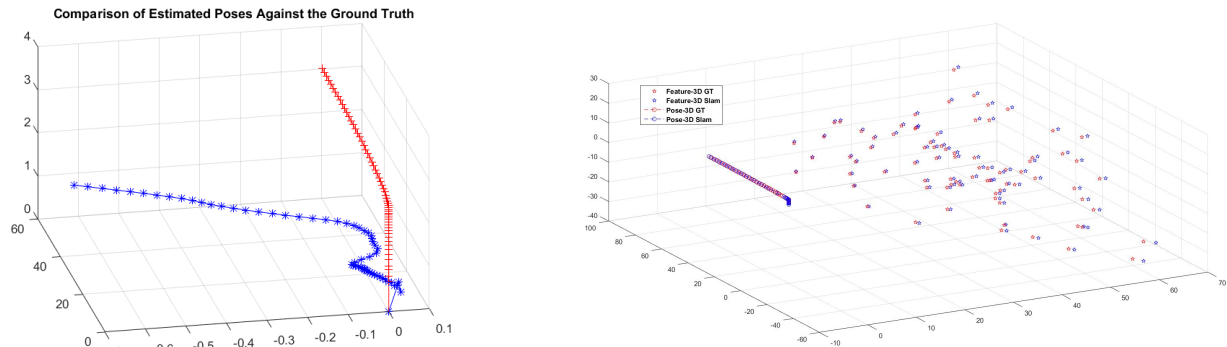


Figure 6: a) One off initialization , b) Incremental initialization

## 4.3 Future improvements

- Change parameterization with Manifold [Forster and et al.(2015)]
- Merge Parallax angles into feature representation [Zhao and Huang(2015)]

## A Rotation representation – Euler angles

### A.1 Rotation matrix

$$\begin{aligned}
 R &= R_x(\alpha)R_y(\beta)R_z(\gamma) \\
 &= \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos(\alpha) & \sin(\alpha) \\ 0 & -\sin(\alpha) & \cos(\alpha) \end{pmatrix} \begin{pmatrix} \cos(\beta) & 0 & -\sin(\beta) \\ 0 & 1 & 0 \\ \sin(\beta) & 0 & \cos(\beta) \end{pmatrix} \begin{pmatrix} \cos(\gamma) & \sin(\gamma) & 0 \\ -\sin(\gamma) & \cos(\gamma) & 0 \\ 0 & 0 & 1 \end{pmatrix}
 \end{aligned}$$

### A.2 Rotation Rate Matrix

$$E = \begin{pmatrix} 1 & 0 & -\sin(\beta) \\ 0 & \cos(\alpha) & \cos(\beta)\sin(\alpha) \\ 0 & -\sin(\alpha) & \cos(\beta)\cos(\alpha) \end{pmatrix}$$

### A.3 Camera frame to Global transform

Using the IMU's coordinates at the 1st pose as the global reference frame, the relative position of these two sensors at that time can be related by  $\mathbf{A}_{u2c}$  and  $\mathbf{T}_{u2c}$  :

$$\begin{aligned}
 \mathbf{A}_{u2c} &= (\alpha_{u2c}, \beta_{u2c}, \gamma_{u2c}), \\
 \mathbf{T}_{u2c} &= (x_{u2c}, y_{u2c}, z_{u2c})
 \end{aligned}$$

And at the following poses, given IMU's states ( $\mathbf{R}_i^u$  and  $\mathbf{T}_i^u$ ), the camera's states ( $\mathbf{R}_i^c$  and  $\mathbf{T}_i^c$ ) can be obtained according to this formula:

$$\begin{aligned}
 \mathbf{R}_i^c &= \mathbf{R}_{u2c} \mathbf{R}_i^u \\
 \mathbf{T}_i^c &= \mathbf{T}_i^u + \mathbf{R}_i^{u'} \mathbf{T}_{u2c}
 \end{aligned}$$

## B Naive VIN

The measurements model  $H(\mathbf{x})$  in Naive VIN can be broken into the following three parts:

$$\omega_{ij} = E_{ij}(\mathbf{A}_{(i+1)j} - \mathbf{A}_{ij})/\Delta t + \mathbf{b}_w \quad (40)$$

$$\mathbf{a}_{ij} = R_{ij}((\mathbf{v}_{(i+1)j} - \mathbf{v}_{ij})/\Delta t - \mathbf{g}) + \mathbf{b}_f \quad (41)$$

$$\mathbf{bZeros} = \mathbf{T}_{(i+1)j} - \mathbf{T}_{ij} - \mathbf{v}_{ij}\Delta t \quad (42)$$

where  $i = 0, \dots, K-1$ , and  $R_{ij}, E_{ij} (= \begin{pmatrix} 1 & 0 & -\sin(\beta_{ij}) \\ 0 & \cos(\alpha_{ij}) & \cos(\beta_{ij})\sin(\alpha_{ij}) \\ 0 & -\sin(\alpha_{ij}) & \cos(\beta_{ij})\cos(\alpha_{ij}) \end{pmatrix})$  correspond to the rotation matrix and rotation rate matrix for the IMU at the time step  $i$  since the  $j$ th key camera frame respectively.

Putting all items together,  $H(\mathbf{x})$  can be written as:

$$\begin{aligned}
H(\mathbf{x}) &= (H_{camera}(\mathbf{x}), H_{IMUraw}(\mathbf{x}), H_{Tv}(\mathbf{x})) \\
&= (\overbrace{u_{11}, v_{11}, \dots, u_{M1}, v_{M1}, \dots, u_{1N}, v_{1N}, \dots, u_{MN}, v_{MN}}^{M \times N \times 2}, \\
&\quad \overbrace{\omega \mathbf{a}_{01}, \omega \mathbf{a}_{11}, \dots, \omega \mathbf{a}_{(K-1)1}, \dots, \omega \mathbf{a}_{0(N-1)}, \omega \mathbf{a}_{1(N-1)}, \dots, \omega \mathbf{a}_{(K-1)(N-1)}}^{K \times (N-1) \times 6}, \\
&\quad \overbrace{\mathbf{T}_2 - \mathbf{T}_1 - \mathbf{v}_1 \Delta t, \mathbf{T}_3 - \mathbf{T}_2 - \mathbf{v}_2 \Delta t, \dots, \mathbf{T}_{(N-1)K+1} - \mathbf{T}_{(N-1)K} - \mathbf{v}_{(N-1)K} \Delta t}^{K \times (N-1) \times 3}) \\
&= (\overbrace{f * x_{11}/z_{11} + cx_0, f * y_{11}/z_{11} + cy_0, \dots, f * x_{MN}/z_{MN} + cx_0, f * y_{MN}/z_{MN} + cy_0,}^{M \times N \times 2}, \\
&\quad \overbrace{E_i * (\mathbf{A}_{11} - \mathbf{A}_{01})/\Delta t + \mathbf{b}_w, \dots, R_{(K-1)(N-1)} * ((\mathbf{v}_{0N} - \mathbf{v}_{(K-1)(N-1)})/\Delta t - \mathbf{g}) + \mathbf{b}_f,}^{K \times (N-1) \times 6}, \\
&\quad \overbrace{\mathbf{T}_2 - \mathbf{T}_1 - \mathbf{v}_1 \Delta t, \mathbf{T}_3 - \mathbf{T}_2 - \mathbf{v}_2 \Delta t, \dots, \mathbf{T}_{(N-1)K+1} - \mathbf{T}_{(N-1)K} - \mathbf{v}_{(N-1)K} \Delta t}^{K \times (N-1) \times 3}) \quad (43)
\end{aligned}$$

### B.0.1 Jacobian Matrix

Based on the composition of  $H(\mathbf{x})$ , the corresponding Jacobian matrix can be calculated.

For camera observations of  $(u_{ij}, v_{ij}, d_{ij})$  which represent the observation of the  $i$ th feature at

the  $j$ th camera pose,

$$\frac{\partial u_{ij}}{\partial \mathbf{P}_{ij}} = [f/z_{ij}, 0, -fx_{ij}/z_{ij}^2] \quad (44)$$

$$\frac{\partial v_{ij}}{\partial \mathbf{P}_{ij}} = [0, f/z_{ij}, -fy_{ij}/z_{ij}^2] \quad (45)$$

$$\frac{\partial d_{ij}}{\partial \mathbf{P}_{ij}} = [0, 0, 1] \quad (46)$$

$$\frac{\partial \mathbf{P}_{ij}}{\partial \mathbf{A}_{0j}} = R_{u2c} \frac{\partial R_{0j}}{\partial \mathbf{A}_{0j}} (\mathbf{P}_{i1} - \mathbf{T}_{0j}) \quad (47)$$

$$\frac{\partial \mathbf{P}_{ij}}{\partial \mathbf{T}_{0j}} = -R_{u2c} R_{0j} \quad (48)$$

$$\frac{\partial \mathbf{P}_{ij}}{\partial \mathbf{A}_{u2c}} = \frac{\partial R_{u2c}}{\partial \mathbf{A}_{u2c}} R_{0j} (\mathbf{P}_{i1} - R'_{0j} \mathbf{T}_{u2c} - \mathbf{T}_{0j}) \quad (49)$$

$$\frac{\partial \mathbf{P}_{ij}}{\partial \mathbf{T}_{u2c}} = -R_{u2c} \quad (50)$$

$$\frac{\partial \mathbf{P}_{ij}}{\partial \mathbf{P}_{fi}} = R_{u2c} R_{0j} \quad (51)$$

For  $\omega_{ij}$ ,

$$\begin{aligned} \frac{\partial \omega_{ij}}{\partial \mathbf{A}_{ij}} &= \frac{\partial E_{ij}}{\partial \mathbf{A}_{ij}} (\mathbf{A}_{(i+1)j} - \mathbf{A}_{ij}) / \Delta t + E_{ij} \left( -\frac{\partial \mathbf{A}_{ij}}{\partial \mathbf{A}_{ij}} \right) / \Delta t \\ &= \left( \frac{\partial E_{ij}}{\partial \mathbf{A}_{ij}} (\mathbf{A}_{(i+1)j} - \mathbf{A}_{ij}) - E_{ij} \right) / \Delta t \end{aligned} \quad (52)$$

$$\frac{\partial E_{ij}}{\partial \mathbf{A}_{ij}} = \left[ \frac{\partial E_{ij}}{\partial \alpha_{ij}}, \frac{\partial E_{ij}}{\partial \beta_{ij}}, \frac{\partial E_{ij}}{\partial \gamma_{ij}} \right] \quad (53)$$

$$\frac{\partial \omega_{ij}}{\partial \mathbf{A}_{(i+1)j}} = E_{ij} \frac{\partial \mathbf{A}_{(i+1)j}}{\partial \mathbf{A}_{(i+1)j}} / \Delta t \quad (54)$$

$$= E_{ij} / \Delta t \quad (55)$$

$$\frac{\partial \omega_{ij}}{\partial b_{\omega}} = I_{3 \times 3} \quad (56)$$

For  $\mathbf{a}_{ij}$ ,

$$\frac{\partial \mathbf{a}_{ij}}{\partial \mathbf{A}_{ij}} = \frac{\partial R_{ij}}{\mathbf{A}_{ij}} ((\mathbf{v}_{i+1} - \mathbf{v}_i)/\Delta t - \mathbf{g}) \quad (57)$$

$$\frac{\partial R_{ij}}{\partial \mathbf{A}_{ij}} = [\frac{\partial R_{ij}}{\partial \alpha_{ij}}, \frac{\partial R_{ij}}{\partial \beta_{ij}}, \frac{\partial R_{ij}}{\partial \gamma_{ij}}] \quad (58)$$

$$\frac{\partial \mathbf{a}_{ij}}{\partial \mathbf{v}_{(i+1)j}} = R_{ij}/\Delta t \quad (59)$$

$$\frac{\partial \mathbf{a}_{ij}}{\partial \mathbf{v}_{ij}} = -R_{ij}/\Delta t \quad (60)$$

$$\frac{\partial \mathbf{a}_{ij}}{\partial \mathbf{g}} = -R_{ij} \quad (61)$$

$$\frac{\partial \mathbf{a}_{ij}}{\partial b_f} = I_{3 \times 3} \quad (62)$$

For  $\mathbf{bZeros}_{ij}$ ,

$$\frac{\partial \mathbf{bZeros}_{ij}}{\partial \mathbf{T}_{(i+1)j}} = I_{3 \times 3} \quad (63)$$

$$\frac{\partial \mathbf{bZeros}_{ij}}{\partial \mathbf{T}_{ij}} = -I_{3 \times 3} \quad (64)$$

$$\frac{\partial \mathbf{bZeros}_{ij}}{\partial \mathbf{v}_{ij}} = -I_{3 \times 3} \Delta t \quad (65)$$



## 5 Bibliography

### References

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