

Figure 9.7.1 Plate Subjected to Axial Load

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%-----
% Example 9.7.1
% plane stress analysis of a solid using linear triangular elements
% (see Fig. 9.7.1 for the finite element mesh)
%
% Variable descriptions
% k = element matrix
% f = element vector
% kk = system matrix
% ff = system vector
% disp = system nodal displacement vector
% eldisp = element nodal displacement vector
% stress = matrix containing stresses
% strain = matrix containing strains
% gcoord = coordinate values of each node
% nodes = nodal connectivity of each element
% index = a vector containing system dofs associated with each element
% bcdof = a vector containing dofs associated with boundary conditions
% bcval = a vector containing boundary condition values associated with
%         the dofs in bcdof
%-----
%
%-----
% input data for control parameters
%-----
nel=8;                                % number of elements
nnel=3;                               % number of nodes per element
ndof=2;                               % number of dofs per node
nnode=10;                             % total number of nodes in system
sdof=nnode*ndof;                      % total system dofs
edof=nnel*ndof;                       % degrees of freedom per element
emodule=100000.0;                     % elastic modulus
poisson=0.3;                          % Poisson's ratio

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%
%-----
% input data for nodal coordinate values
% gcoord(i,j) where i-> node no. and j-> x or y
%-----
gcoord=[0.0 0.0; 0.0 1.0; 1.0 0.0; 1.0 1.0; 2.0 0.0;
2.0 1.0; 3.0 0.0; 3.0 1.0; 4.0 0.0; 4.0 1.0];
%
%-----
% input data for nodal connectivity for each element
% nodes(i,j) where i-> element no. and j-> connected nodes
%-----
nodes=[1 3 4; 1 4 2; 3 5 6; 3 6 4;
5 7 8; 5 8 6; 7 9 10; 7 10 8];
%
%-----
% input data for boundary conditions
%-----
bcdof=[1 2 3]; % first three dofs are constrained
bcval=[0 0 0]; % whose described values are 0
%
%-----
% initialization of matrices and vectors
%-----
ff=zeros(s dof,1); % system force vector
kk=zeros(s dof,s dof); % system matrix
disp=zeros(s dof,1); % system displacement vector
eldisp=zeros(edof,1); % element displacement vector
stress=zeros(nel,3); % matrix containing stress components
strain=zeros(nel,3); % matrix containing strain components
index=zeros(edof,1); % index vector
kinmtx=zeros(3,edof); % kinematic matrix
matmtx=zeros(3,3); % constitutive matrix
%
%-----
% force vector
%-----
ff(17)=500; % force applied at node 9 in x-axis
ff(19)=500; % force applied at node 10 in x-axis
%
%-----
% compute element matrices and vectors, and assemble
%-----
matmtx=fematiso(1,emodule,poisson); % constitutive matrix
%
for iel=1:nel % loop for the total number of elements
%
nd(1)=nodes(iel,1); % 1st connected node for (iel)-th element

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nd(2)=nodes(iel,2);           % 2nd connected node for (iel)-th element
nd(3)=nodes(iel,3);           % 3rd connected node for (iel)-th element
%
x1=gcoord(nd(1),1); y1=gcoord(nd(1),2);   % coord values of 1st node
x2=gcoord(nd(2),1); y2=gcoord(nd(2),2);   % coord values of 2nd node
x3=gcoord(nd(3),1); y3=gcoord(nd(3),2);   % coord values of 3rd node
%
index=feeldof(nd,nnel,ndof);   % extract system dofs for the element
%
%-----
% find the derivatives of shape functions
%-----
area=0.5*(x1*y2+x2*y3+x3*y1-x1*y3-x2*y1-x3*y2); % area of triangle
area2=area*2;
dhdx=(1/area2)*[(y2-y3) (y3-y1) (y1-y2)];    % derivatives w.r.t. x
dhdy=(1/area2)*[(x3-x2) (x1-x3) (x2-x1)];    % derivatives w.r.t. y
%
kinmtx2=fekine2d(nnel,dhdx,dhdy);             % kinematic matrix
%
k=kinmtx2'*matmtx*kinmtx2*area;               % element stiffness matrix
%
kk=feasmb1(kk,k,index);                      % assemble element matrices
%
end                                           % end of loop for the total number of elements
%
%-----
% apply boundary conditions
%-----
[kk,ff]=feaplyc2(kk,ff,bcdof,bcval);
%
%-----
% solve the matrix equation
%-----
disp=kk\ff;
%
%-----
% element stress computation (post computation)
%-----
for ielp=1:nel                               % loop for the total number of elements
%
nd(1)=nodes(ielp,1);           % 1st connected node for (iel)-th element
nd(2)=nodes(ielp,2);           % 2nd connected node for (iel)-th element
nd(3)=nodes(ielp,3);           % 3rd connected node for (iel)-th element
%
x1=gcoord(nd(1),1); y1=gcoord(nd(1),2);   % coord values of 1st node
x2=gcoord(nd(2),1); y2=gcoord(nd(2),2);   % coord values of 2nd node
x3=gcoord(nd(3),1); y3=gcoord(nd(3),2);   % coord values of 3rd node
%

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```

index=feeldof(nd,nnel,ndof);      % extract system dofs for the element
%
%-----
% extract element displacement vector
%-----
for i=1:edof
    eldisp(i)=disp(index(i));
end
%
area=0.5*(x1*y2+x2*y3+x3*y1-x1*y3-x2*y1-x3*y2); % area of triangle
area2=area*2;
dhdx=(1/area2)*[(y2-y3) (y3-y1) (y1-y2)];      % derivatives w.r.t. x
dhdy=(1/area2)*[(x3-x2) (x1-x3) (x2-x1)];      % derivatives w.r.t. y
%
kinmtx2=fekine2d(nnel,dhdx,dhdy);               % kinematic matrix
%
estrain=kinmtx2*eldisp;                        % compute strains
estress=matmtx*estrain;                        % compute stresses
%
for i=1:3
    strain(ielp,i)=estrain(i);                  % store for each element
    stress(ielp,i)=estress(i);                  % store for each element
end
%
end
%
%-----
% print fem solutions
%-----
num=1:1:sdof;
displace=[num' disp]                          % print nodal displacements
%
for i=1:nel
    stresses=[i stress(i,:)]                   % print stresses
end
%
%-----

```

```

function [kinmtx2]=fekine2d(nnel,dhdx,dhdy)
%-----
% Purpose:
% determine the kinematic equation between strains and displacements
% for two-dimensional solids
%
% Synopsis:
% [kinmtx2]=fekine2d(nnel,dhdx,dhdy)

```

```

%
% Variable Description:
% nnel - number of nodes per element
% dhdx - derivatives of shape functions with respect to x
% dhdy - derivatives of shape functions with respect to y
%-----
%
for i=1:nnel
    i1=(i-1)*2+1;
    i2=i1+1;
    kinmtx2(1,i1)=dhdx(i);
    kinmtx2(2,i2)=dhdy(i);
    kinmtx2(3,i1)=dhdy(i);
    kinmtx2(3,i2)=dhdx(i);
end
%
%-----

function [matmtx]=fematiso(iopt,elastic,poisson)
%-----
% Purpose:
% determine the constitutive equation for isotropic material
%
% Synopsis:
% [matmtx]=fematiso(iopt,elastic,poisson)
%
% Variable Description:
% elastic - elastic modulus
% poisson - Poisson's ratio
% iopt=1 - plane stress analysis
% iopt=2 - plane strain analysis
% iopt=3 - axisymmetric analysis
% iopt=4 - three dimensional analysis
%-----
%
if iopt==1 % plane stress
    matmtx= elastic/(1-poisson*poisson)* ...
    [1 poisson 0; ...
    poisson 1 0; ...
    0 0 (1-poisson)/2];
%
elseif iopt==2 % plane strain
    matmtx= elastic/((1+poisson)*(1-2*poisson))* ...
    [(1-poisson) poisson 0;
    poisson (1-poisson) 0;
    0 0 (1-2*poisson)/2];

```

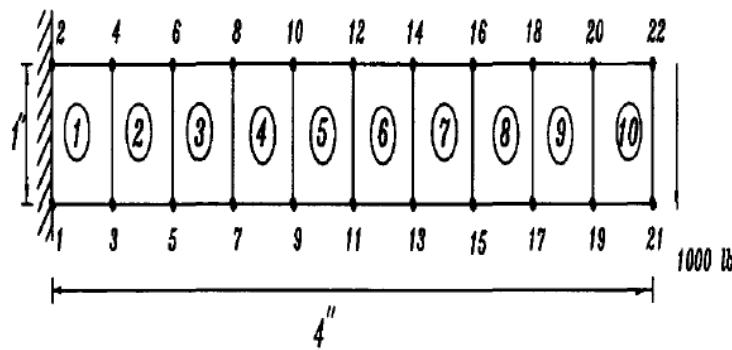
```

%
elseif iopt==3                                % axisymmetry
matmtrx= elastic/((1+poisson)*(1-2*poisson))* ...
[(1-poisson) poisson poisson 0;
poisson (1-poisson) poisson 0;
poisson poisson (1-poisson) 0;
0 0 0 (1-2*poisson)/2];
%
else                                            % three-dimension
matmtrx= elastic/((1+poisson)*(1-2*poisson))* ...
[(1-poisson) poisson poisson 0 0 0;
poisson (1-poisson) poisson 0 0 0;
poisson poisson (1-poisson) 0 0 0;
0 0 0 (1-2*poisson)/2 0 0;
0 0 0 0 (1-2*poisson)/2 0;
0 0 0 0 0 (1-2*poisson)/2];
%
end
%
%

```

The nodal displacements are listed below and they agree with the analytical solutions. On the other hand, the state of stress of each element is $\sigma_x = 1000$ and $\sigma_y = \tau_{xy} = 0$ as expected.

displace =		
d.o.f.	displ.	
1.0000	0.0000	% x-displacement of node 1
2.0000	0.0000	% y-displacement of node 1
3.0000	0.0000	% x-displacement of node 2
4.0000	-0.0030	% y-displacement of node 2
5.0000	0.0100	% x-displacement of node 3
6.0000	0.0000	% y-displacement of node 3
7.0000	0.0100	% x-displacement of node 4
8.0000	-0.0030	% y-displacement of node 4
9.0000	0.0200	% x-displacement of node 5
10.000	0.0000	% y-displacement of node 5
11.000	0.0200	% x-displacement of node 6
12.000	-0.0030	% y-displacement of node 6
13.000	0.0300	% x-displacement of node 7
14.000	0.0000	% y-displacement of node 7
15.000	0.0300	% x-displacement of node 8
16.000	-0.0030	% y-displacement of node 8
17.000	0.0400	% x-displacement of node 9
18.000	0.0000	% y-displacement of node 9
19.000	0.0400	% x-displacement of node 10
20.000	-0.0030	% y-displacement of node 10



$$E=10^6 \text{ psi}, \nu=0.3$$

Figure 9.7.2 Cantilever Beam Subjected to a Tip Load

♣ **Example 9.7.2** We want to analyze a short cantilever beam using two-dimensional isoparametric elements assuming plane stress condition. To this end, the beam is modeled using ten four-node quadrilateral elements as seen in Fig. 9.7.2.

```
%
%-----
% Example 9.7.2
% plane stress analysis of a cantilever beam using isoparametric
% four-node elements
% (see Fig. 9.7.2 for the finite element mesh)
%
% Variable descriptions
% k = element matrix
% f = element vector
% kk = system matrix
% ff = system vector
% disp = system nodal displacement vector
% eldisp = element nodal displacement vector
% stress = matrix containing stresses
% strain = matrix containing strains
% gcoord = coordinate values of each node
% nodes = nodal connectivity of each element
% index = a vector containing system dofs associated with each element
% point2 = matrix containing sampling points
% weight2 = matrix containing weighting coefficients
% bcdof = a vector containing dofs associated with boundary conditions
% bcval = a vector containing boundary condition values associated with
%         the dofs in bcdof
%
%-----
%
%-----
% input data for control parameters
```