

CADi

ROS as a Development Platform

Kinematic Lateral Control

Renato Galluzzi

renato.galluzzi@tec.mx

July 2020

Types of Lateral Control

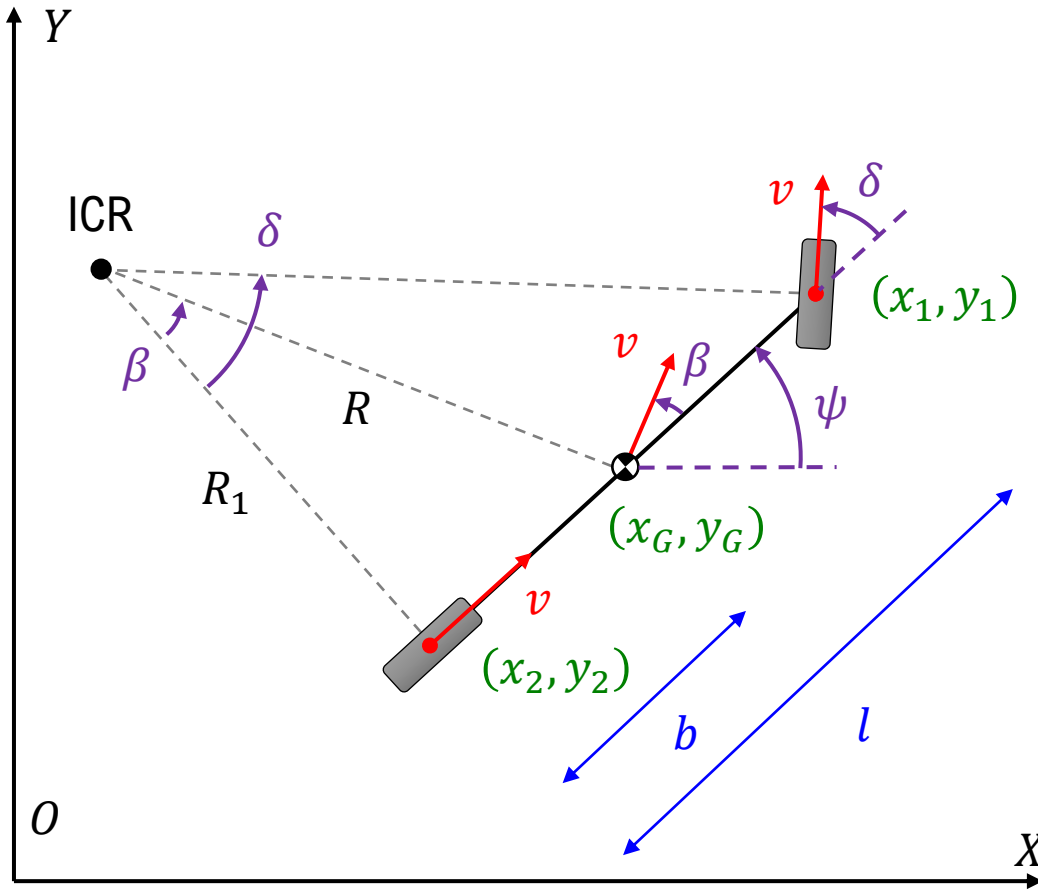
- **Kinematic or geometric control:**

- It exploits geometric relationships between the vehicle and the path.
- Simple and effective control laws.
- Could potentially fall in the presence of heavy dynamic content.
- **Examples:** pure pursuit (carrot following) and Stanley.

- **Dynamic control:**

- It considers the nonlinear model of lateral dynamics.
- More accurate results than the kinematic variant.
- Computationally expensive.
- **Examples:** model predictive control, feedback linearization, sliding mode control.

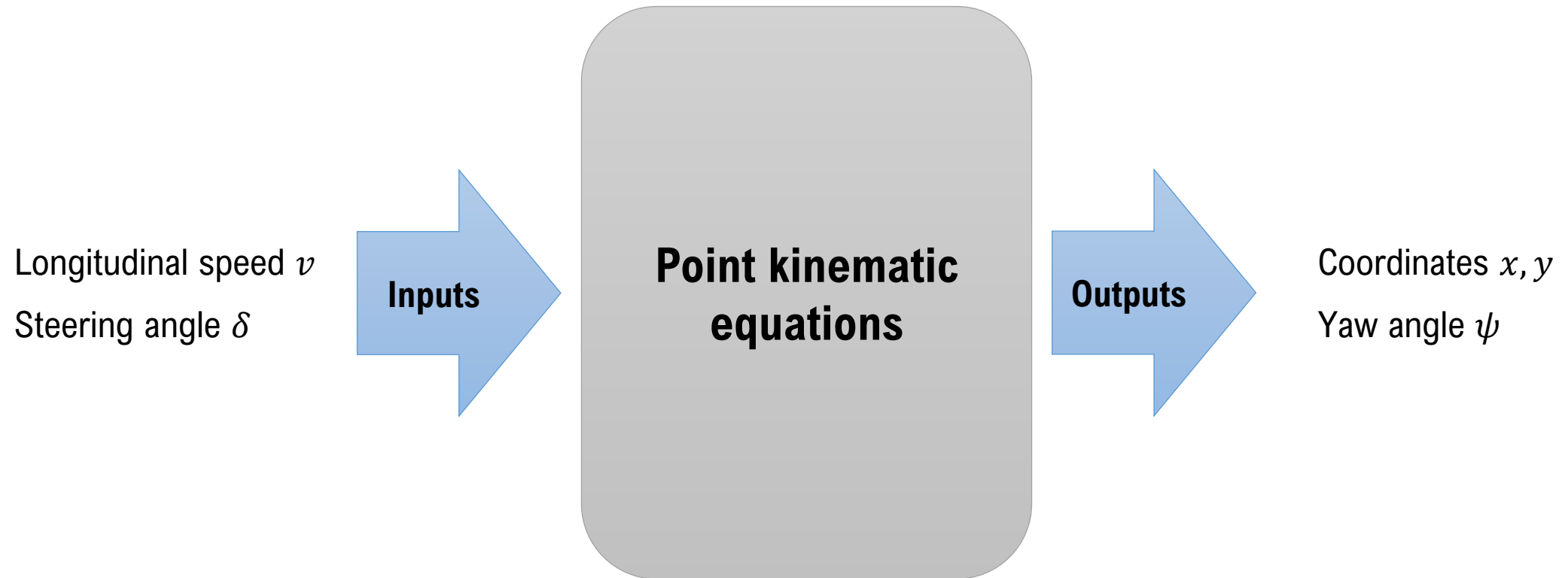
Kinematic Bicycle Model



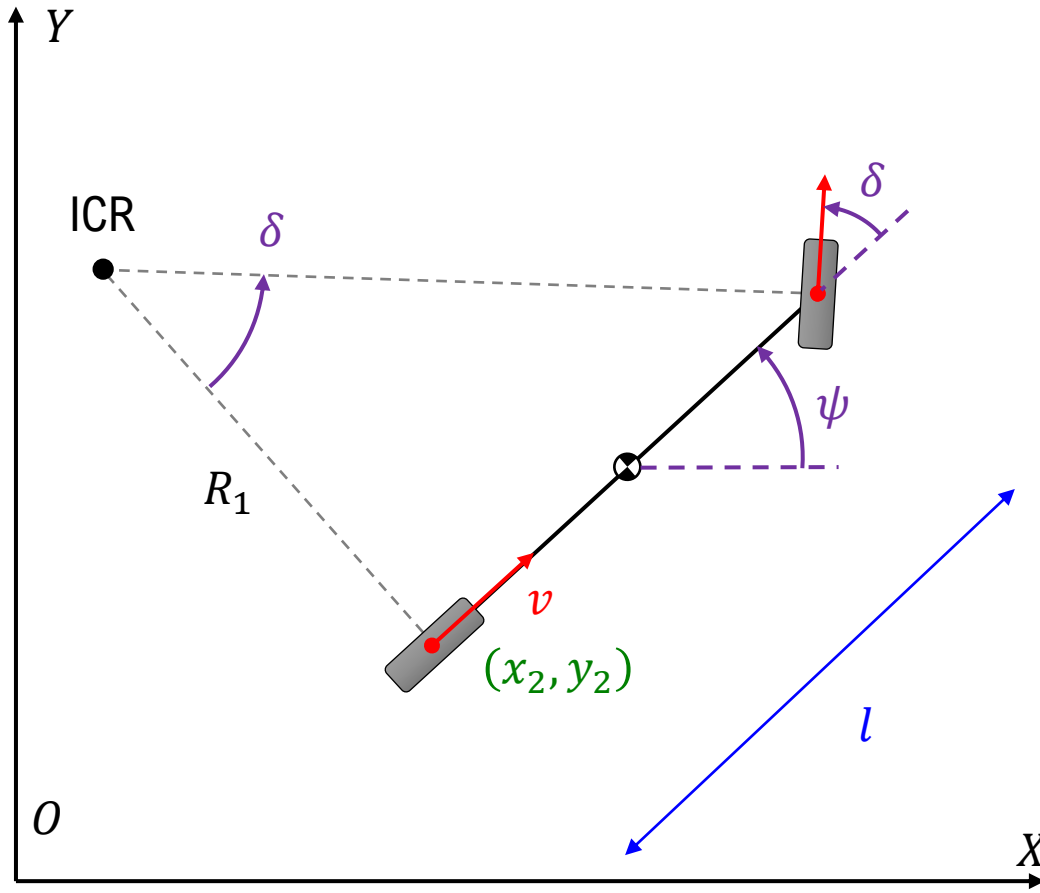
- **Motion in three possible points of interest:**
 - **rear axle** (x_2, y_2)
 - **front axle** (x_1, y_1)
 - **center of gravity (COG)** (x_G, y_G)
- We determine the instantaneous center of rotation (ICR).
- All points experience the same longitudinal speed v .

*Vehicle geometry denoted by wheelbase l and distance between rear axle and COG b

Approach



Rear Axle Kinematics



$$\dot{x}_2 = v \cos \psi$$

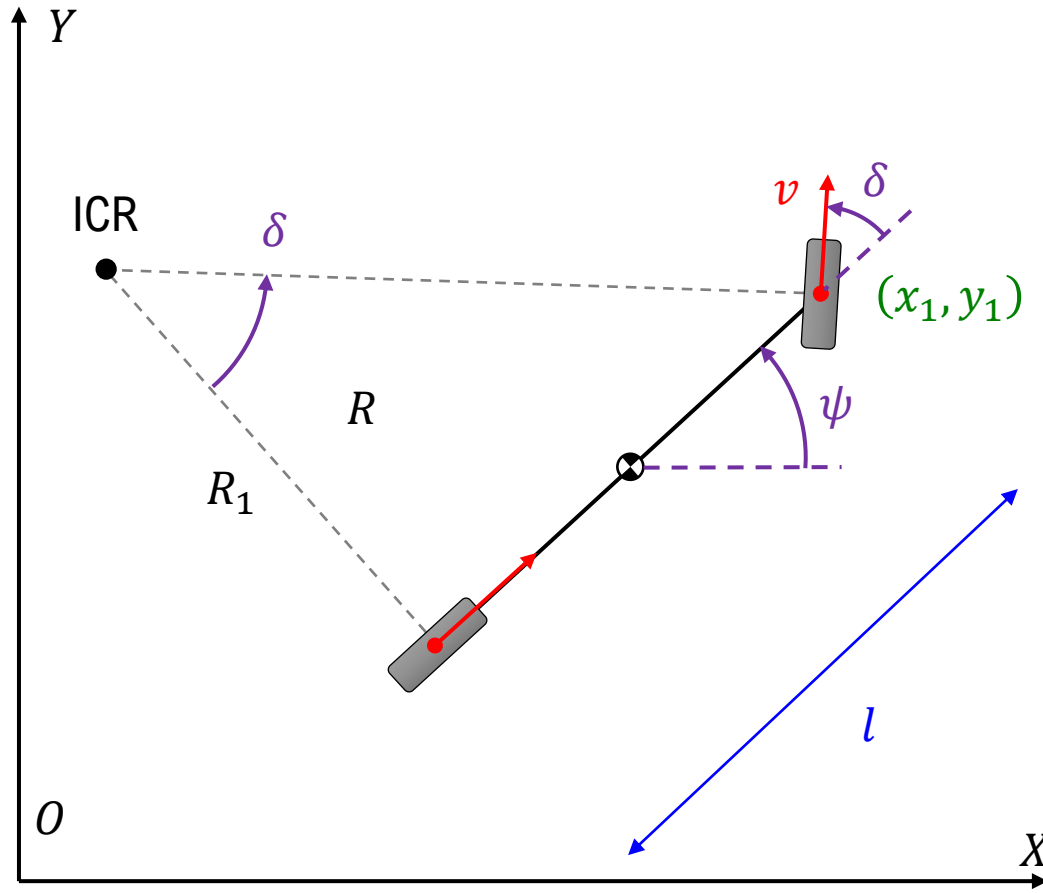
$$\dot{y}_2 = v \sin \psi$$

$$\dot{\psi} = \frac{v}{R_1}$$

$$\tan \delta = \frac{l}{R_1}$$

$$\dot{\psi} = \frac{v \tan \delta}{l}$$

Front Axle Kinematics



$$\dot{x}_1 = v \cos(\psi + \delta)$$

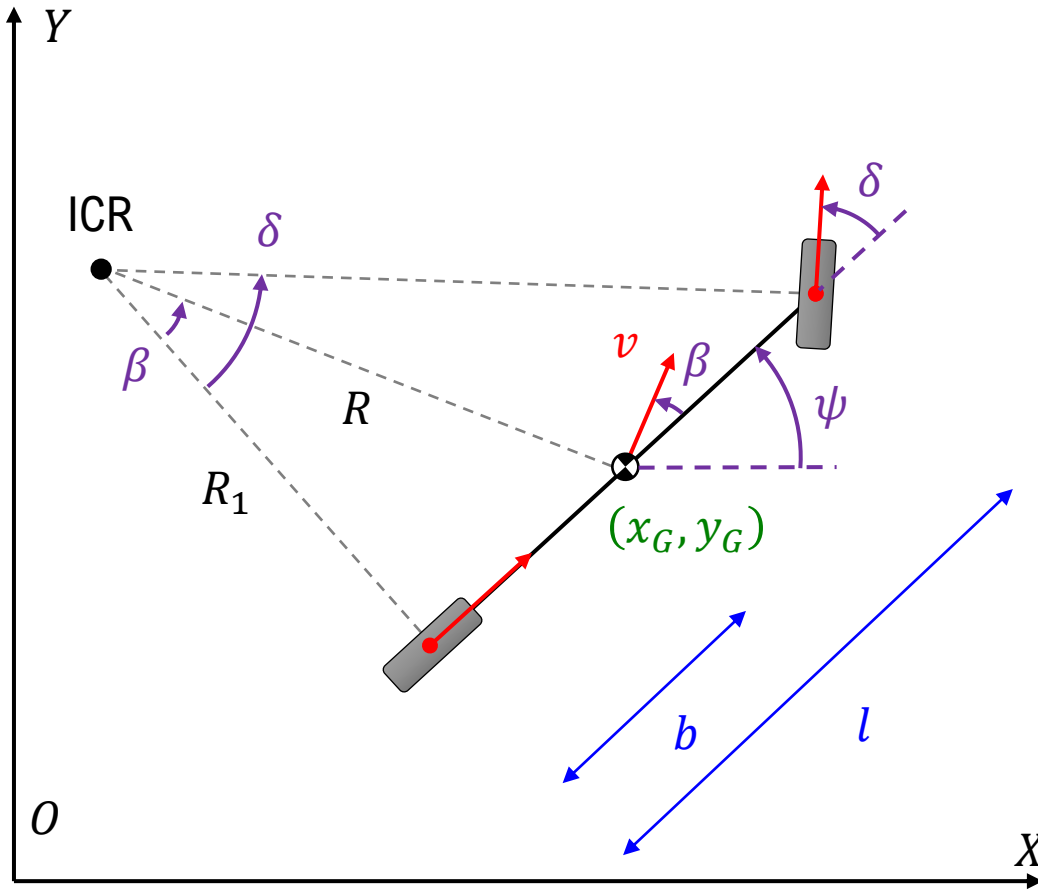
$$\dot{y}_1 = v \sin(\psi + \delta)$$

$$\dot{\psi} = \frac{v \cos \delta}{R_1}$$

$$\tan \delta = \frac{l}{R_1}$$

$$\dot{\psi} = \frac{v \cos \delta \tan \delta}{l} = \frac{v \sin \delta}{l}$$

COG Kinematics



$$\dot{x}_G = v \cos(\psi + \beta)$$

$$\dot{y}_G = v \sin(\psi + \beta)$$

$$\dot{\psi} = \frac{v \cos \beta}{R_1}$$

$$\tan \delta = \frac{l}{R_1}$$

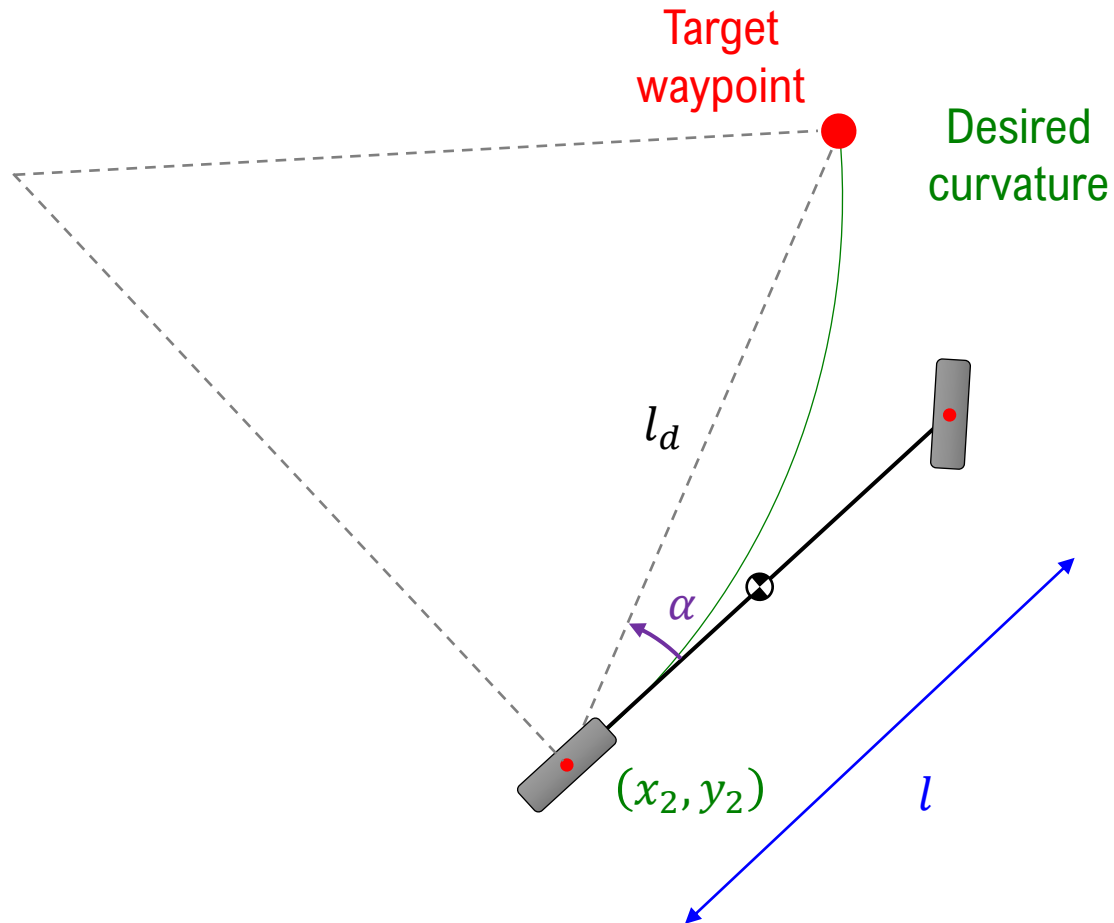
$$\dot{\psi} = \frac{v \cos \beta \tan \delta}{l}$$

$$\beta = \arctan\left(\frac{b}{R_1}\right) = \arctan\left(\frac{b \tan \delta}{l}\right)$$

Pure Pursuit Control

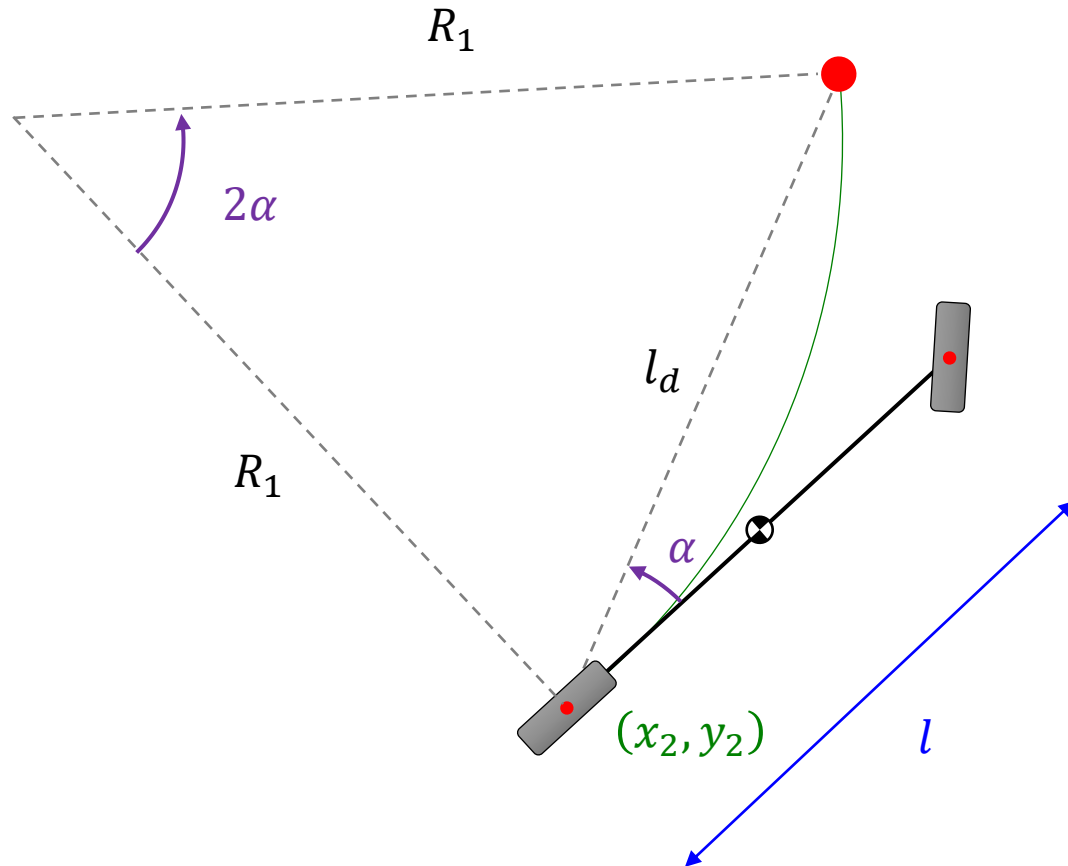
Kinematic Steering Technique

Overview



- The **pure pursuit algorithm** connects the rear axle of the vehicle with a given target waypoint by means of a lookahead distance l_d .
- The goal is to calculate the trajectory curvature among these points.
- The steering angle δ is obtained from:
 - Target point location
 - Angle α between the vehicle heading and the lookahead direction

Approach



Sines law

$$\frac{l_d}{\sin(2\alpha)} = \frac{R_1}{\sin\left(\frac{\pi}{2} - \alpha\right)}$$

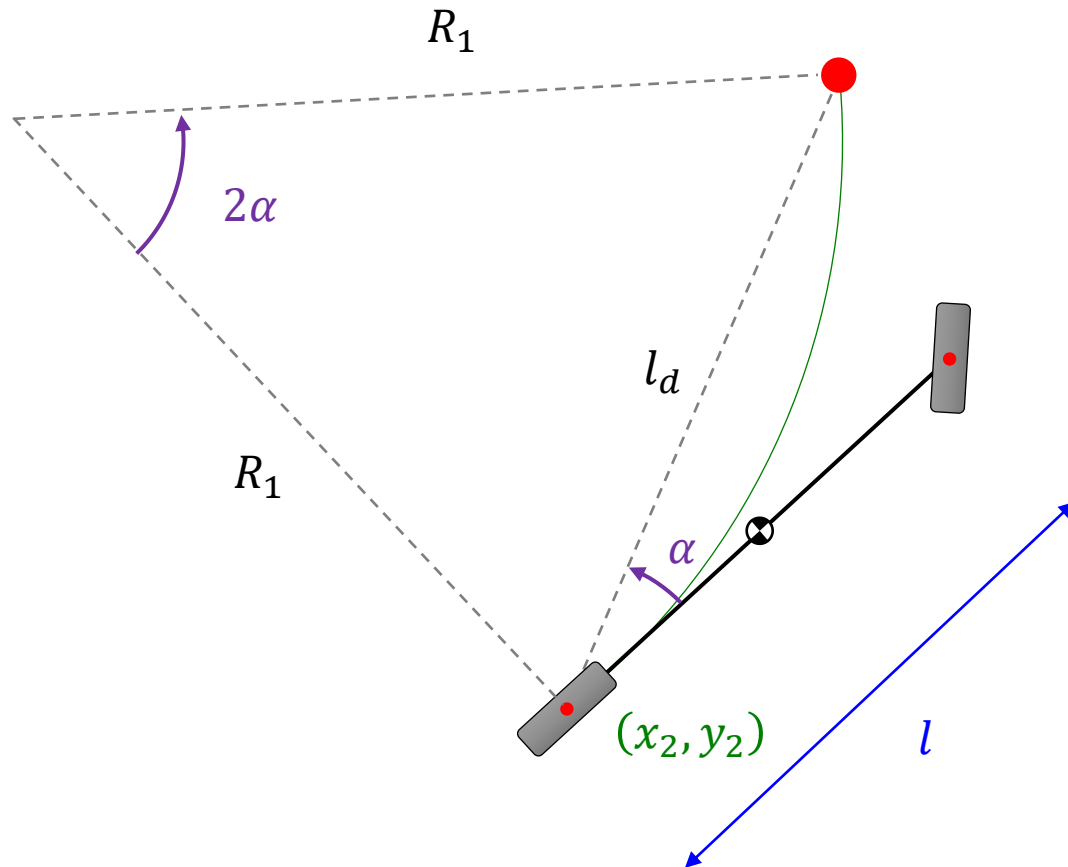
$$\frac{l_d}{2 \sin \alpha \cos \alpha} = \frac{R_1}{\cos \alpha}$$

$$\frac{l_d}{2 \sin \alpha} = R_1$$

Path curvature

$$\kappa = \frac{1}{R_1} = \frac{2 \sin \alpha}{l_d}$$

Approach



Path curvature

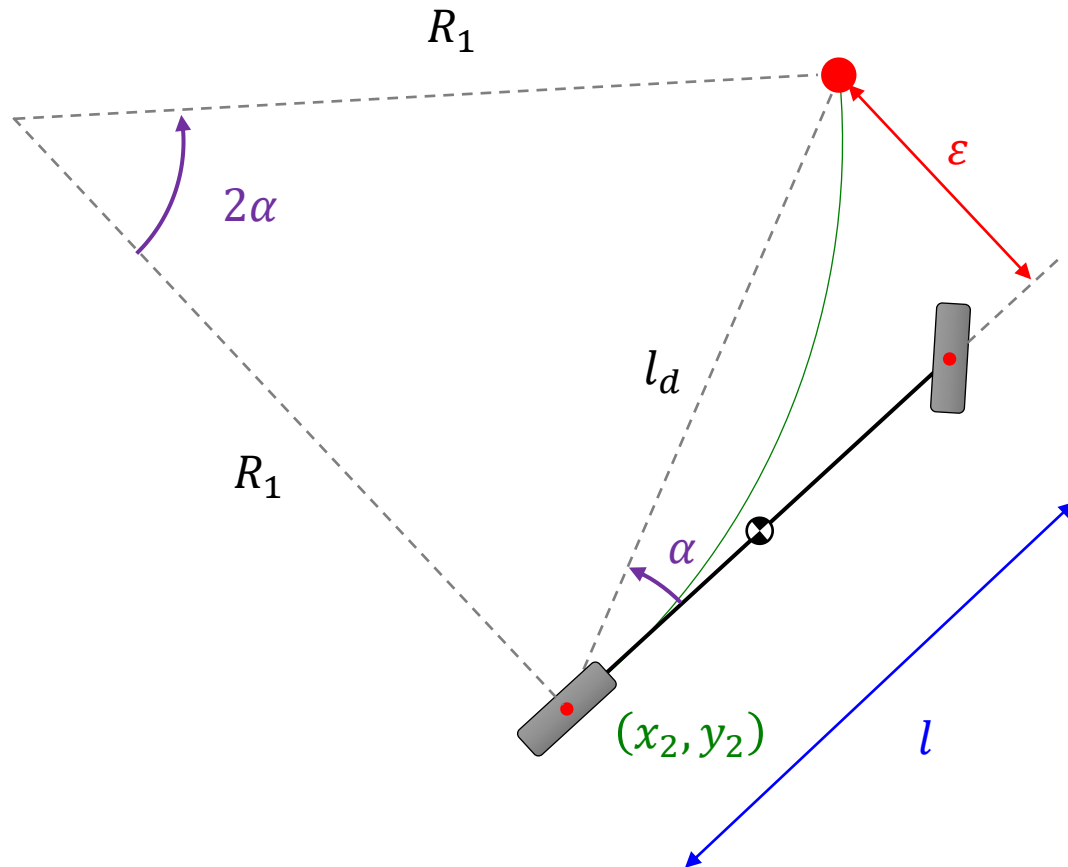
$$\kappa = \frac{1}{R_1} = \frac{2 \sin \alpha}{l_d}$$

Bicycle model (rear axle)

$$\tan \delta = \frac{l}{R_1} \rightarrow \delta = \arctan(\kappa l)$$

$$\delta = \arctan\left(\frac{2l \sin \alpha}{l_d}\right)$$

Cross-Track Error

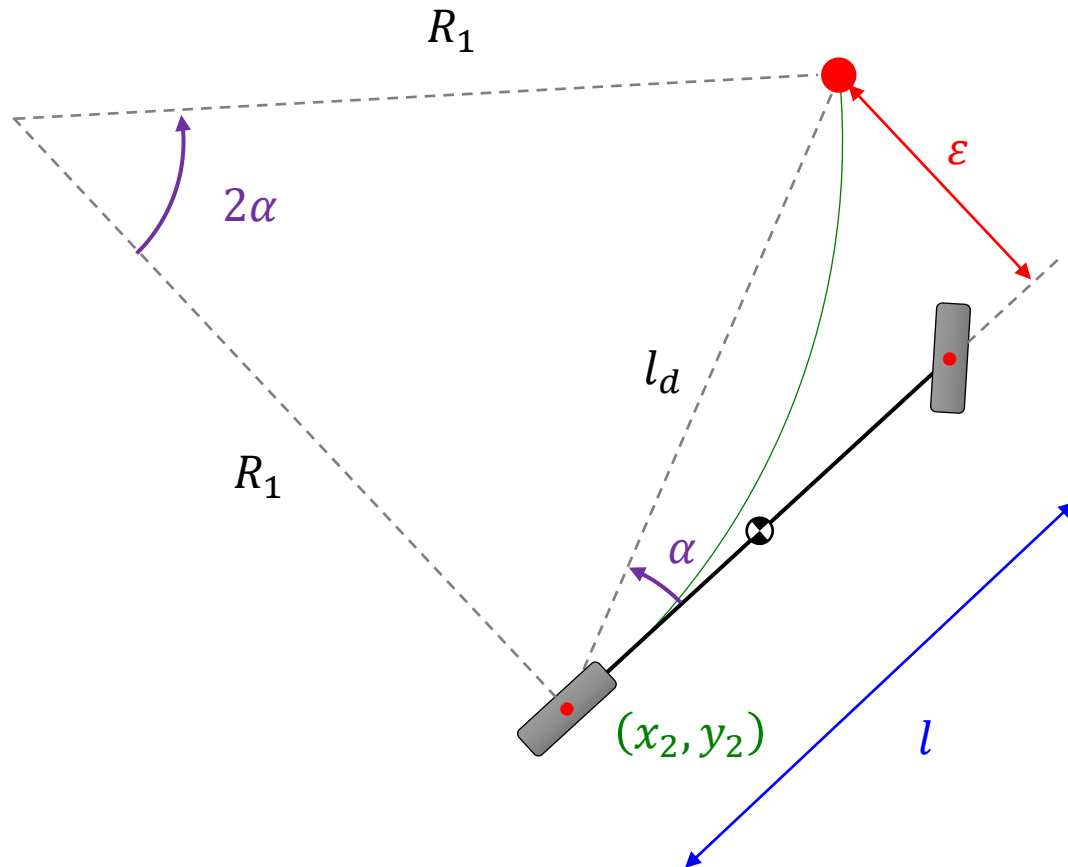


- The cross-track error ε is defined as the lateral distance between the vehicle heading and the target waypoint.

$$\sin \alpha = \frac{\varepsilon}{l_d}$$
$$\kappa = \frac{2 \sin \alpha}{l_d} = \frac{2}{l_d^2} \varepsilon$$

- Remember that $\delta = f(\kappa)$. Hence, the steering input depends on the cross-track error and a proportionality constant $2/l_d^2$.

Setting the Lookahead Distance



- The lookahead distance l_d plays a fundamental role in selecting a proper steering input δ .
- The faster the vehicle travels, the further this distance must be set to yield effective commands to follow the target path.
- **Idea:** Set l_d proportional to the vehicle longitudinal speed v .

$$l_d = K_d v$$

$$\delta = \arctan\left(\frac{2l \sin \alpha}{K_d v}\right)$$

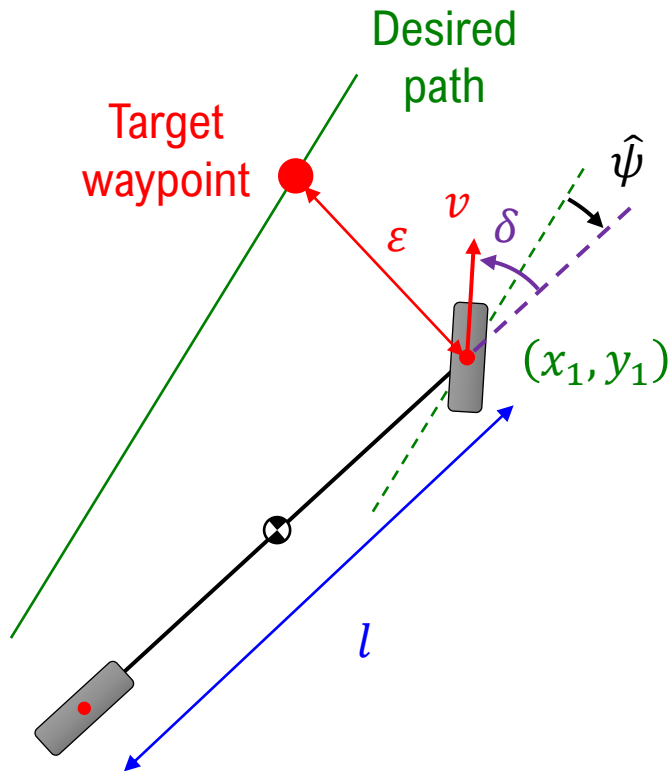
Stanley Control

Kinematic Steering Technique

Overview

- The **Stanley algorithm** defines a steering law to
 - Correct the heading error
 - Correct the position error
 - Constrain δ to feasible bounds
- The control approach is referred to the front axle.
- The Stanley algorithm was developed by Stanford University for the 2005 DARPA Grand Challenge.

Heading Control Requirements



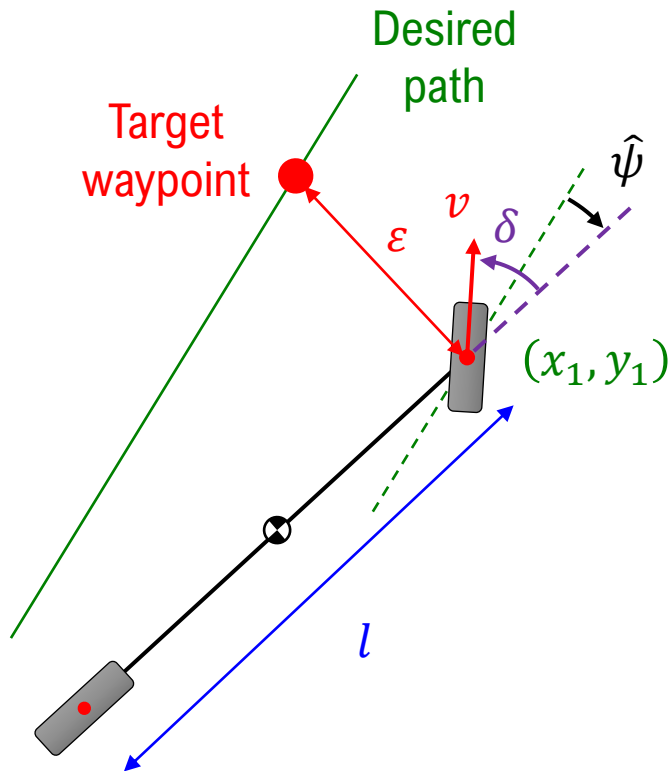
Alignment contribution

- Apply a steering input to align heading with desired heading.

$$\delta(t) = -\hat{\psi}(t)$$

- *Remark 1: $\hat{\psi}$ is the yaw angle with respect to the desired path.*
- *Remark 2: Notice that the sense of δ and $\hat{\psi}$ are opposite.*

Heading Control Requirements



Cross-track error elimination

- Apply a steering input

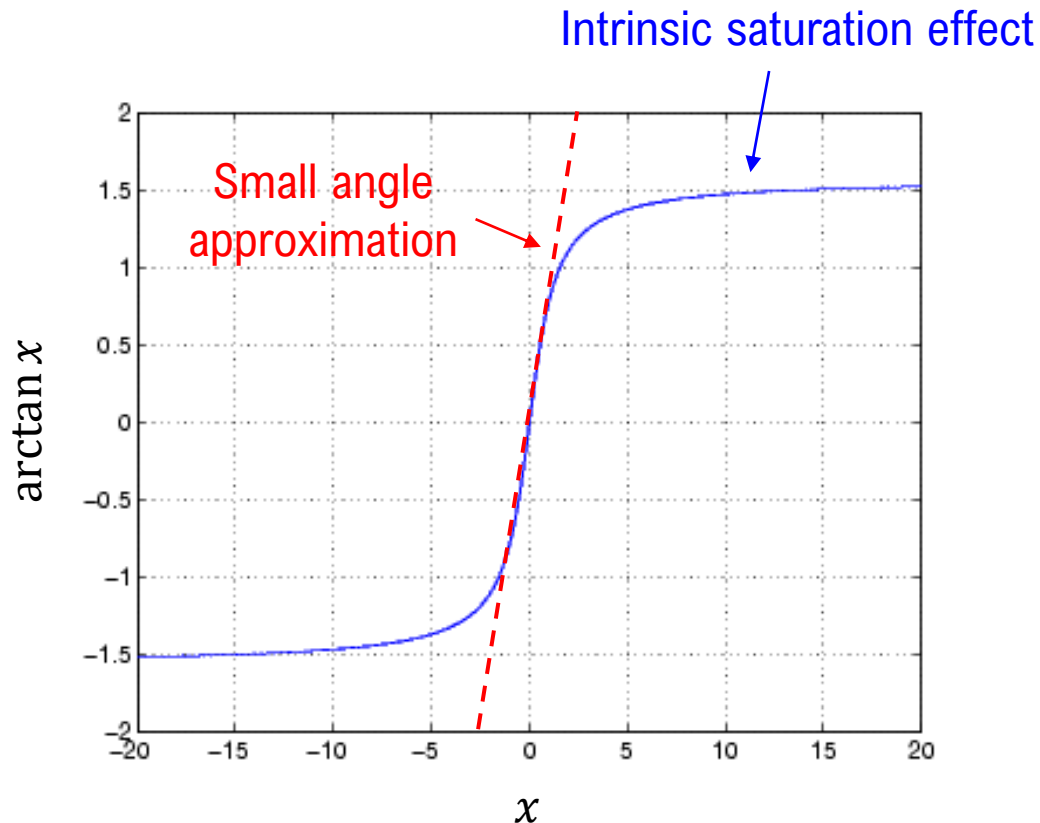
$$\delta(t) = \arctan\left(\frac{K\varepsilon(t)}{v(t)}\right)$$

For small arguments: $\delta(t) \approx \frac{K\varepsilon(t)}{v(t)}$

- Directly proportional to the cross-track error ε
- Inversely proportional to longitudinal speed v
- Gain K is tuned heuristically

Command bounds $\delta(t) \in [\delta_{min}, \delta_{max}]$

Cross-Track Elimination



Stanley

$$\delta(t) = \arctan \left(\frac{K\varepsilon(t)}{v(t)} \right)$$

Pure pursuit

$$\delta = \arctan \left(\frac{2l\varepsilon(t)}{K_d^2 v(t)^2} \right)$$

Steering Law

Command combination

$$\delta(t) = \hat{\psi}(t) + \arctan\left(\frac{K\varepsilon(t)}{K_s + v(t)}\right)$$

$$\delta(t) \in [\delta_{min}, \delta_{max}]$$

- The cross-track error control law can be modified with:
 - Softening constant K_s to improve numerical stability when $v \approx 0$
 - Control law enhancement by adding integral and derivative terms

Example

Stanley Control in Python

Parameters

Stanley Control Tuning

- Proportional constant $K = 2.5$

Vehicle / Inputs

- Wheelbase $l = 1$ m
- Maximum steering angle of 25 deg in both directions.
- Constant longitudinal speed v . Try 2, 5 and 10 m/s.

Trajectory

- Move along x axis only. At 20 meters, introduce a step variation towards 5 meters in the y axis
- Initial yaw angle $\psi = 20$ deg
- Initial cross track error $\varepsilon = 0$

Euler discretization

$$\frac{x_k - x_{k-1}}{\Delta t} \cong \dot{x} = f(x, u)$$

$$x_k = x_{k-1} + \Delta t f(x, u)$$

*Implement front-axle kinematics