

M Earth = 0.39860-106

b) 
$$F: na$$
,  $\frac{F}{C} = a$ 

evisor from lecture:

$$\alpha_{T} = \frac{1}{2} \frac{J(v^{1})}{ds} + \frac{Jv}{r^{1}} \frac{dr}{ds} \left\{ \left( \frac{dr}{ds} + \frac{dr}{ds} \right) \right\} \left( \frac{dr}{ds} + \frac{dr}{ds} + \frac{dr}{ds} \right)$$

$$2v \frac{dv}{ds} \qquad Sin V$$

C) Given The equation:

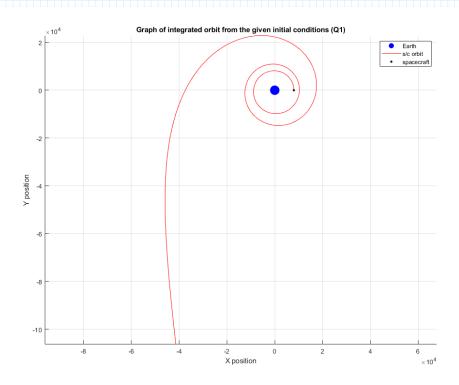
$$\psi_{esc} = \psi_{o} = \frac{V_{o}}{\alpha_{T}} \left( \left[ -\left( \frac{20 \, \alpha_{T}^{2} \, \Gamma_{o}^{2}}{V_{o}^{4}} \right)^{1/3} \right) \right]$$

 $\frac{1}{1 + c_{sc}} = \frac{\left\| \frac{s/c_{vel_{in}y}}{\omega_{T}} \right\|}{\left(1 - \left( \frac{20 \left\| \frac{s}{vel_{in}y} \right\|^{2}}{\left\| \frac{s}{vel_{in}y} \right\|^{2}} \right)^{\frac{1}{2}} \right)^{\frac{1}{2}}}{\left\| \frac{s}{vel_{in}y} \right\|^{2}} \right)^{\frac{1}{2}}$ 

$$= \frac{7.0587}{0.0001} \left( 1 - \left( \frac{20(0.001)^2 (3000)^2}{(7.0587)^4} \right)^{1/4} \right)$$

= 3. +0+728 6187 · 10 + seconds

7)



e) given that Cosc can be lowed
$$C_{esc} = \frac{\|s/c_{perint}\|\|s/c_{volint}\|}{(20 \circ c_v^2 \|s/c_{perint}\|^2)^{1/4}}$$

$$C_{esc} = \frac{(8000)(7.0587)}{(20(0.0001)^2(8000)^2)^{1/4}}$$

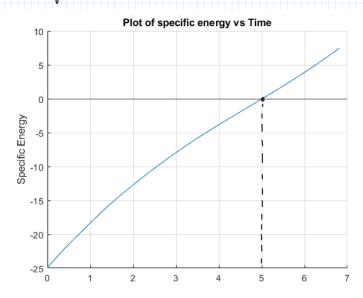
$$C_{esc} = \frac{29855}{(8000)^2} \text{ km}$$

from inspection of integrated data, Sesc. Is reached at 36413 seconds

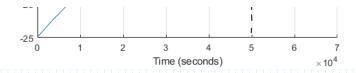
different from our analytical 34047 seconds by 2366 seconds! a little less lime I have

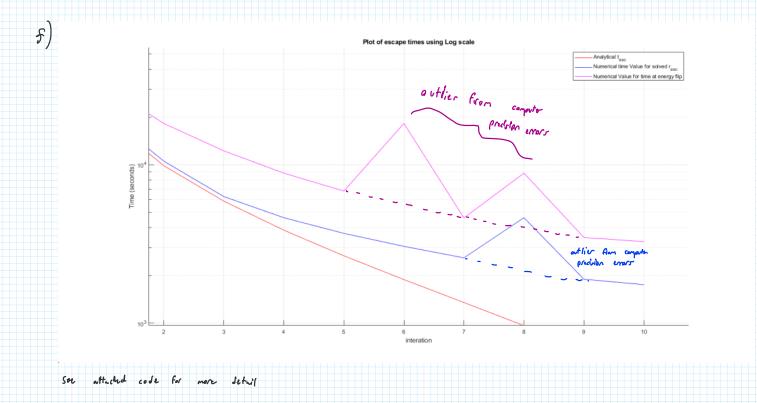
- · However, inspection of the change in energy sign, i.e. when & (specific energy) good from regative to partitle, occur roughly at 50130 seconds!
- Both numerically found escape times are greater than the analytical answer. I think the analytical answer is conservative with it's output because it really doesn't take into account the force of gravity on the spacecraft the same way that the numerical integrated does. Since it's only going off of

$$U_{sing}$$
  $e = \frac{V^{2}}{2} - \frac{\mu}{r} = \frac{||\vec{v}||^{2}}{2} - \frac{\mu}{||\vec{r}||}$ 



output because it really doesn't take into account the force of gravity on the spacecraft the same way that the numerical integrated does. Since it's only going off of the kinematics of the problem (other than the acceleration due to thrust being a nonkinematic term since it is a force), it does not account for the extra time it might take for the spacecraft to break from the planets gravity well, giving us a conservative value. TL:DR - The exclusion of the gravity term from the t\_esc equation leads to a faster escape time being found. Since the t\_esc equation is only influenced by a single force (and not the accounting for the gravitiational force being applied to the craft), it will find a escape time.





From the plot, it is clear that the analytical method is lacking in it's accuracy. As the acceleration due to thrust is increased, we see a larger separation of numerical vs analytical values of the escape time. However, there are two key things to note: the analytical method produces a smooth, continuous curve of solutions, because it gives you exactly one solution. The integration method requires that you find the value at which either the energy changes or the time at which you reach your analytically solved for r\_esc. Disregarding the outliers of data in the provided plot, and assuming they are smooth curves, we can still see the growing gap between the analytical solution and the numerical integration soltuion. The main limitation, I believe of the analytical method is that it does not incorporate gravity into the equation at all, and only relies on the input thrust as it's only force. I think this limitation is what causes the analytical method to undershoot, as it requires less time to escape if there is no modeled force of gravity "hold you back" (resisting the spacecrafts power to escape orbit)