Vortexy fluid dynamics simulator

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Software documentation

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1 Introduction

Vortexy is a computational fluid dynamics (CFD) simulation package. It is written in C and uses the finite volume method with the SIMPLE algorithm to calculate flow of incompressible fluids, namely liquids.

The simulator is based on irregular tetrahedral meshes. These meshes can be computed from surfaces using the program Tetgen. The simulator takes a configuration file as input that contains paths to the simulation mesh and boundary conditions in addition to other settings. The state of the system is periodically written to an output file specified in the config. Included is also a renderer that uses OpenGL to visualize results.

2 Background

2.1 Navier-Stokes equations

The Navier-Stokes equations form the basis for all of fluid dynamics. The momentum equation is typically written as

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\frac{1}{\rho}\nabla p + \nu \nabla^2 \mathbf{u} + g, \tag{1}$$

where $\mathbf{u} = (u, v, w)$ is velocity in m s⁻¹, t time in s, ρ density in kg m⁻³, p pressure in Pa, $\nu = \frac{\mu}{\rho}$ kinematic viscosity in m² s⁻¹, g gravity in m s⁻².

The continuity equation must be satisfied for incompressible fluids that have no sinks of sources

$$\nabla \cdot \mathbf{u} = 0, \tag{2}$$

where $\mathbf{u} = (u, v, w)$ is velocity in m s⁻¹.

2.2 Turbulence

A simple way of predicting onset of turbulence is the Reynolds number:

$$Re = \frac{\mu uL}{\rho} = \frac{uL}{\nu}$$

Turbulence models in simulations include RANS (Reynolds Averaged), LES (Large Eddy) and DNS (Direct).

2.3 Finite volume method

The *finite volume method* (FVM) is based on a simulation mesh with volume elements. This enables evaluation of partial differential equations (PDEs) prevalent in physics. The divergence theorem allows us to convert volume integrals to surface integrals

$$\int_{V} \nabla \cdot \mathbf{F} \, dV = \oint_{S} \mathbf{F} \cdot d\mathbf{S},$$

so volume terms can be computed from fluxes at element faces.

2.4 Discretization

The momentum equation is written in a form conducive for discretization:

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u} \otimes \mathbf{u}) = -\frac{\nabla p}{\rho} + \frac{\mu}{\rho} \nabla \cdot (\nabla u) + \nabla \cdot (\nabla u)^T + \mathbf{f}_b$$

transient + convective = diffusive + sources

Continuity equation:

$$\nabla \cdot \mathbf{u} = 0$$

This saddle-point problem can be represented in matrix form as:

$$A\mathbf{u} = \begin{pmatrix} F & B^T \\ B & 0 \end{pmatrix} \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} = \begin{pmatrix} \mathbf{f}_b \\ 0 \end{pmatrix}$$

In practice, the velocity and pressure fields are calculated using 4 matrices (vx, vy, vz, p).

Discretization for the one-dimensional momentum equation [1]:

$$a_v u_v + \sum_{f \in f_{nb}} a_f u_f = b_v, \tag{3}$$

where a_v refers to a volume element and a_f to a face element coefficient. This can be represented in matrix form as:

$$\begin{pmatrix} a_{00} & a_{01} & 0 & \dots & 0 \\ \vdots & \ddots & & & \vdots \\ a_f & a_f & a_v & a_f & a_f \\ \vdots & & \ddots & \vdots \\ 0 & \dots & 0 & a_{n(n-1)} & a_{0n} \end{pmatrix} \begin{pmatrix} u_0 \\ \vdots \\ u_n \end{pmatrix} = \begin{pmatrix} b_0 \\ \vdots \\ b_n \end{pmatrix},$$

where $u_0 \dots u_n$ represents volume element velocities. In the pressure calculation these are referred to as u^* , i.e. momentum conserving. The coefficients a and b are calculated for each volume element and assembled into a matrix. Components X, Y and Z are calculated one after another.

Face fluxes:

$$\phi_f = \max(\dot{m}_f, 0) + \mu \frac{E_f}{d_{vf}} \tag{4}$$

$$\Phi_f = -\max(-\dot{m}_f, 0) - \mu \frac{E_f}{d_{vf}}$$
 (5)

$$\vec{\psi}_f = -\mu(\nabla \mathbf{u}_f) \cdot \mathbf{T}_f + \dot{m}_f(\mathbf{u}_f^{\text{hr}} - \mathbf{u}_f^{\text{uw}}), \tag{6}$$

where $\mathbf{S}_f = A_f \hat{n}_f = \mathbf{E}_f + \mathbf{T}_f$ and $\dot{m}_f = \rho \mathbf{u}_f \cdot \mathbf{S}_f$. High-resolution model velocity $\mathbf{u}_f^{\text{hr}} = \mathbf{u}_f$ and upwind velocity $\mathbf{u}_f^{\mathrm{uw}}$.

Volume fluxes:

$$\phi_v = \frac{\rho V}{\Delta t} \tag{7}$$

$$\phi_v = \frac{\rho V}{\Delta t} \tag{7}$$

$$\vec{\psi}_v = \frac{\rho V}{\Delta t} \mathbf{u}_v - \mathbf{f}_b V \tag{8}$$

Coefficients:

$$a_v = \phi_v + \sum_{f \in f_{nb}} \phi_f = \frac{\rho V}{\Delta t} + \sum_{f \in f_{nb}} \left(\max(\dot{m}_f, 0) + \mu \frac{E_f}{d_{vf}} \right)$$
 (9)

$$a_f = \Phi_f = -\max(-\dot{m}_f, 0) - \mu \frac{E_f}{d_{v_f}}$$
 (10)

$$\mathbf{b}_v = -\vec{\psi}_v - \sum_{f \in f_{nb}} \vec{\psi}_f + \sum_{f \in f_{nb}} \left(\mu(\nabla \mathbf{u}_f)^T \cdot \mathbf{S}_f \right) - V \nabla p_v$$
 (11)

$$= -\frac{\rho V}{\Delta t} \mathbf{u}_v - \mathbf{f}_b V - \sum_{f \in f_{nb}} \left(-\mu(\nabla \mathbf{u}_f) \cdot \mathbf{T}_f + \dot{m}_f (\mathbf{u}_f - \mathbf{u}_f^{\text{uw}}) \right) + \sum_{f \in f_{nb}} \left(\mu(\nabla \mathbf{u}_f)^T \cdot \mathbf{S}_f \right) - V \nabla p_v$$

Pressure equation:

$$u_v^* + \sum_{f \in f_{-k}} \frac{a_f}{f_v} \mathbf{u}_f^* = -\frac{V}{a_v} \nabla p_v + \frac{b_v + V \nabla p_v}{a_v}$$

$$\tag{12}$$

Similarly, the pressure correction equation can be discretized [1]:

$$a_v p_v' + \sum_{f \in f_{nb}} a_f p_f' = b_v$$
 (13)

With coefficients:

$$a_f = -\rho \frac{E_f}{d_{vf}} \tag{14}$$

$$a_v = \sum_{f \in f_{nb}} \rho \frac{E_f}{d_{vf}} \tag{15}$$

$$b_v = -\sum_{f \in f_{nb}} \dot{m}_f^* = -\sum_{f \in f_{nb}} \rho \mathbf{u}_f^* \cdot \mathbf{S}_f$$
 (16)

All of these are $n \times n$ diagonally dominant matrices which can be solved using a numerical matrix solver, such as Gauss-Seidel. The off-diagonal coefficients represent neighbouring elements, so they will be mostly zero.

2.5 Gauss-Seidel method

2.6 SIMPLE algorithm

- 1. Set boundary conditions, set u and p
- 2. Compute gradients ∇u and ∇p
- 3. Compute mass fluxes j_m , flow rate $\dot{m} = j_m \cdot A$
- 4. Solve momentum equation using velocity guess u^0
- 5. Solve pressure correction equation to get p'

- 6. Correct pressure p = p + p' and velocity
- 7. Increment time $t^{n+1} = t^n + \Delta t$
- 8. Repeat

2.7 Boundary conditions

```
No-slip wall
```

Slip wall

Inlet (velocity / pressure)

Outlet (mass flow rate / pressure)

3 Implementation

3.1 Simulation mesh

Triangular/tetrahedral, closed, connected, Delaunay tetrahedralization with spatial Hilbert curve sorting

3.2 Solver

Gauss-Seidel with some sparse matrix optimizations

3.3 Rendering

OpenGL 3.1, GLSL 150

4 Software

4.1 Compilation

The software is compiled using CMake. The CMakeLists.txt file is found in the root directory. There are two main ways to configure the simulator: with rendering and without. This is achieved by passing the -DSIMONLY=ON flag to CMake. The non-graphical version is linked entirely statically. The graphical version has its RPATH set to ./lib/, so required dynamically linked libraries can be placed there.

The root directory contains shell scripts that can be used for compilation. To build the simulator, renderer and libraries use the script buildall.sh. To build the simulator without the renderer use the script buildsim.h and set RENDER_ENABLED to 0 in sim.h.

Dependencies: libc, libm, (OpenGL, GLEW, GLFW)

Building using default options:

```
cmake .
```

4.2 Configuration

- 4.2.1 Simulation config
- 4.2.2 Fluid config
- 4.3 Output data

Format:

```
s <sim tick>
o <object id> t <time in s> f <face id> x <face centroid x in m> <y> <z>
v <face velocity x in m/s> <y> <z> p <face pressure in Pa>
e
```

- 4.4 Examples
- 4.4.1 Lid-driven cavity
- 4.4.2 Pipe flow
- 4.5 Problems

References

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