

- For *inversion channel* to exist at the *D end*,  
 $V_{GD}$  must be  $> V_{TN}$ 
  - $V_{DS}$  must be  $< V_{GT}$
- When  $V_{DS} = V_{GT}$ , the *channel* is said to be *pinched-off* at the *D end*, and  $I_D$  does not increase any more
- This value of  $V_{DS}$  is known as the *drain-to-source saturation voltage*  $V_{DS,sat}$ 
  - $V_{DS,sat} = V_{GT}$



- For  $V_{DS} > V_{DS,sat}$ , the *mode of operation* is known as *saturation*

- *Drain current in saturation:*

$$I_D = \frac{k_N}{2} V_{GT}^2$$

➤ *Obtained from the non-saturation  $I_D$  expression by substituting  $V_{DS} = V_{GT}$*

➤ *Note that  $I_D$  is independent of  $V_{DS}$*

- *Above equations are valid for  $V_{GT} > 3V_T$   
(*~ 80 mV at room temperature*)*



# The Complete LEVEL 0 Model

$$I_D = k_N \left( V_{GT} V_{DS} - V_{DS}^2 / 2 \right)$$

*(linear region -  $V_{GT} > 3V_T, V_{DS} < V_{GT}$ )*

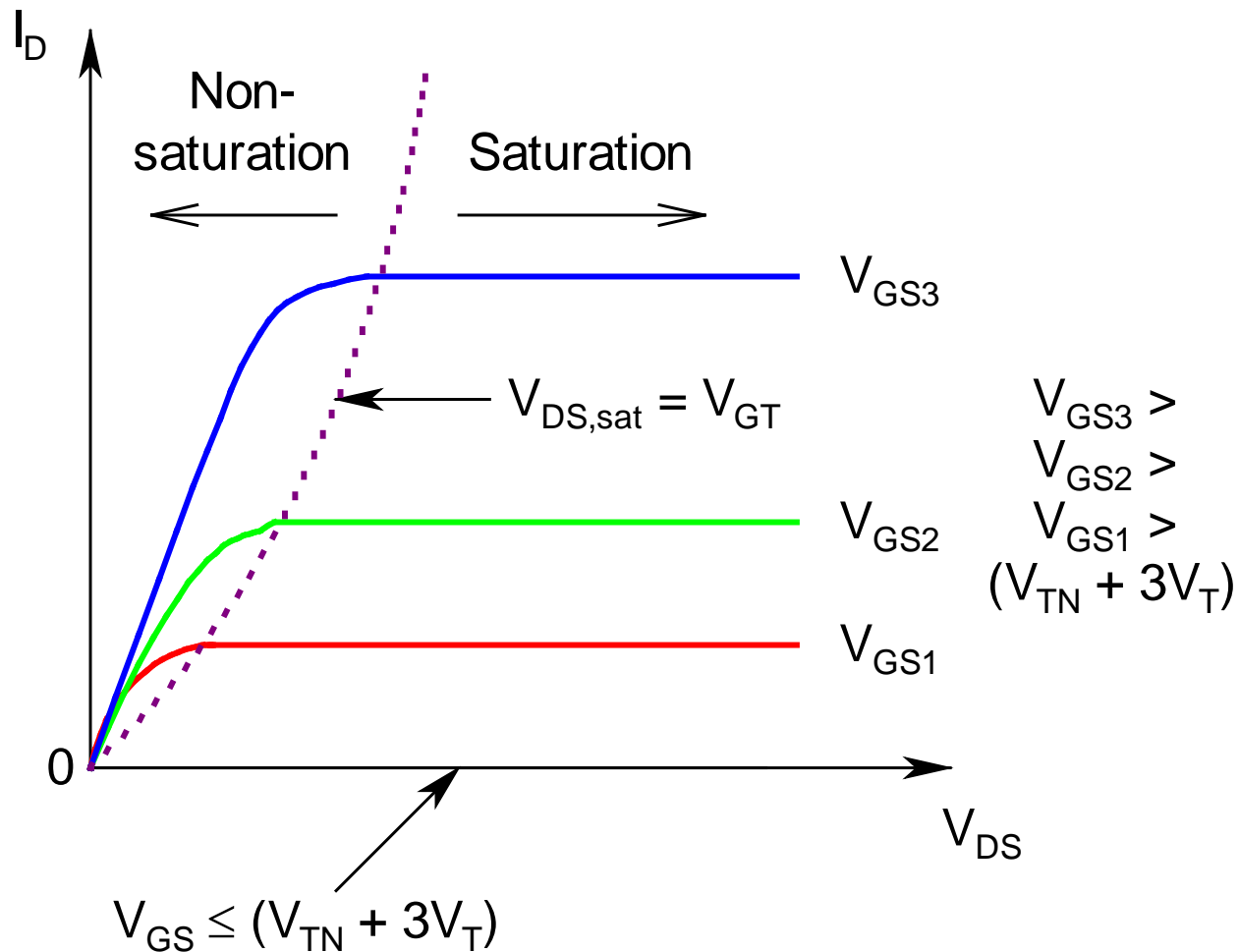
$$= (k_N / 2) V_{GT}^2$$

*(saturation region -  $V_{GT} > 3V_T, V_{DS} \geq V_{GT}$ )*

$$= 0$$

*(cutoff region -  $V_{GT} \leq 3V_T, \text{ any } V_{DS}$ )*

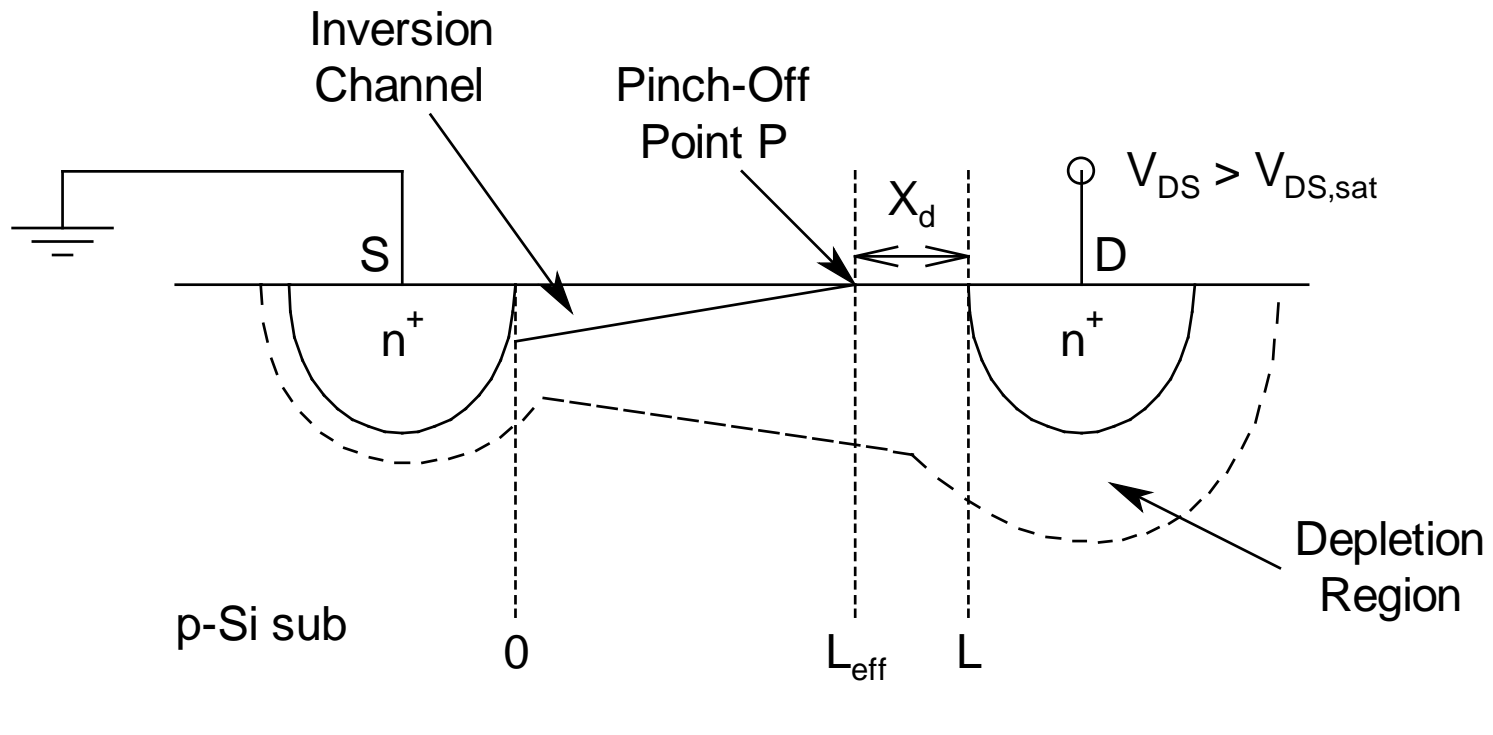




## $I_D$ - $V_{DS}$ Characteristics



# Channel-Length Modulation (CLM)



**$X_d \rightarrow$  length of the pinched-off region**



- For  $V_{DS} = V_{DS,sat}$ , *pinch-off point P at D end*
- For  $V_{DS} > V_{DS,sat}$ , *P moves towards source*
- *Effective channel length reduces* from L to  $L_{eff} = L - X_d$ 
  - $X_d =$  *pinch-off region/drain region/saturation region length*
- *Excess voltage*  $(V_{DS} - V_{DS,sat})$  *drops across*  $X_d$



- *Reduction of effective channel length causes an increase in current*

- *Channel length modulation*

- With  $V_{DS} \uparrow$ ,  $X_d \uparrow$ ,  $L_{eff} \downarrow$ , and  $I_D \uparrow$

- *No real current saturation*

- Thus, *saturated drain current*:

$$\begin{aligned} I_{D,sat} &= (k'_N/2)(W/L_{eff}) V_{GT}^2 \\ &= (k_N/2) V_{GT}^2 (1 + \lambda V_{DS}) \end{aligned}$$



- $\lambda =$  *Channel length modulation parameter*

$$= \frac{1}{L} \frac{dX_d}{dV_{DS}}$$

- *Function of  $L$  and  $N_A$*
- *Higher  $L$  and  $N_A \Rightarrow$  Lower  $\lambda$*
- *Typical values of  $\lambda$  may range from close to 0 to as high as 0.1-0.3  $V^{-1}$*
- *Very similar to  $V_A$  inverse for BJTs*



- This gives **LEVEL 1 model** (also known as **Shichman-Hodges model**) for MOSFETs:

$$I_D = k_N \left[ V_{GT} V_{DS} - V_{DS}^2 / 2 \right] (1 + \lambda V_{DS})$$

*(linear region -  $V_{GT} > 3V_T$ ,  $V_{DS} < V_{GT}$ )*

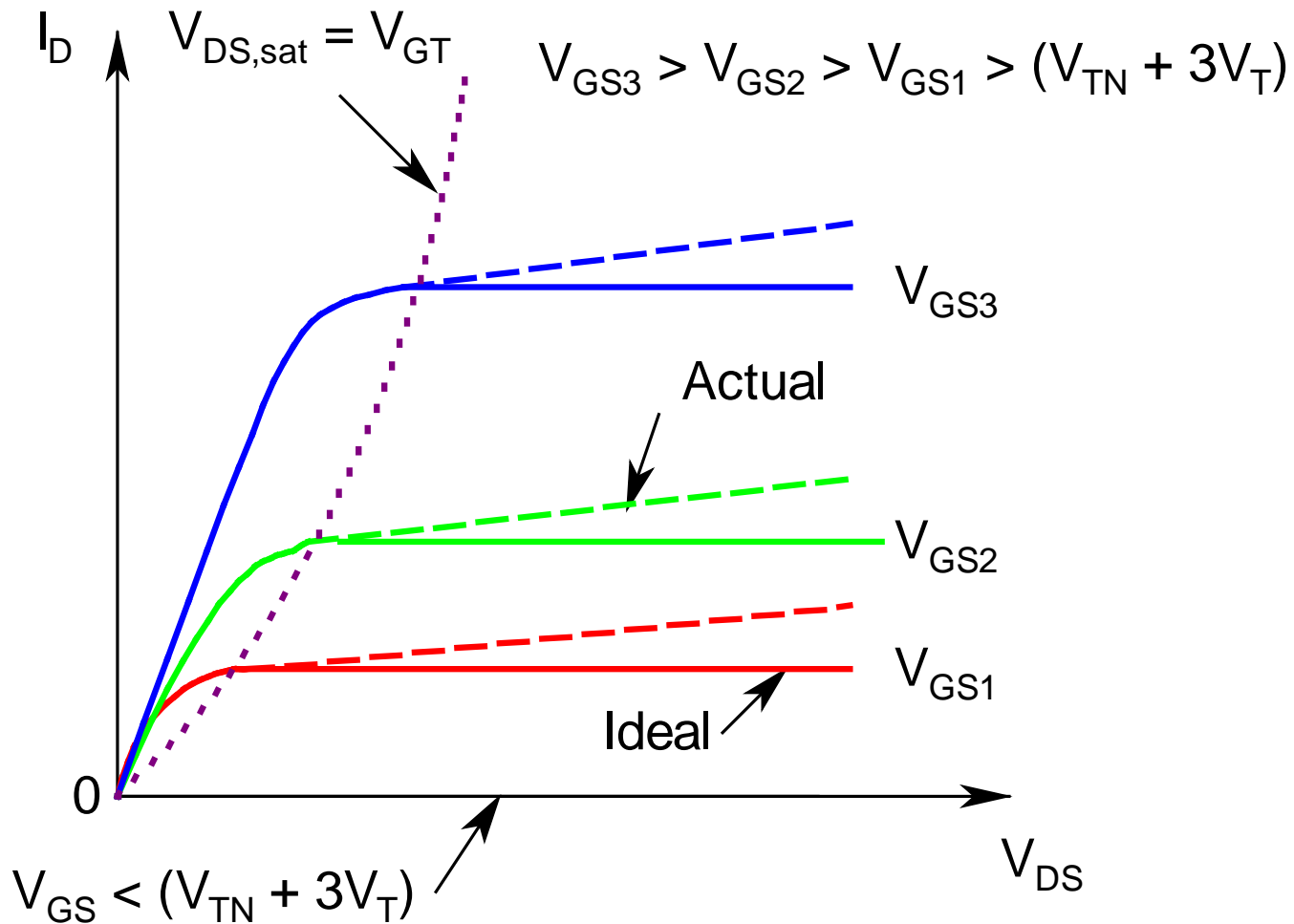
$$= (k_N / 2) V_{GT}^2 (1 + \lambda V_{DS})$$

*(saturation region -  $V_{GT} > 3V_T$ ,  $V_{DS} \geq V_{GT}$ )*

$$= 0$$

*(cutoff region -  $V_{GT} \leq 3V_T$ , any  $V_{DS}$ )*





## $I_D$ - $V_{DS}$ Characteristics in presence of CLM



# DC Bias Point Calculation

- *To find  $R_D$  for BB*

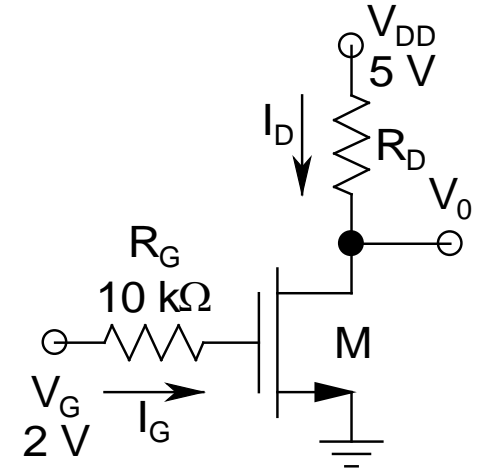
- $V_{TN0} = 1 \text{ V}$ ,  $k'_N = 40 \mu\text{A/V}^2$ ,  
 $W/L = 10$

- *Body terminal not shown*

➤ *Implies that it is connected  
to the most negative potential available in the  
circuit (**ground in this case**)*

$$\Rightarrow V_{SB} = 0 \Rightarrow V_{TN} = V_{TN0}$$

- $I_G = 0 \Rightarrow V_{GS} = V_G = 2 \text{ V}$





- $V_{GT} = V_{GS} - V_{TN} = 1 \text{ V}$
- *Assuming saturation mode of operation and neglecting CLM:*

$$I_D = (k_N/2) V_{GT}^2 = 200 \text{ } \mu\text{A}$$

- *For BB,  $V_{DS} = V_{DD}/2 = 2.5 \text{ V}$  (2-element output branch):*

$$R_D = (V_{DD} - V_{DS})/I_D = 12.5 \text{ k}\Omega$$

- $V_{DS} > V_{GT} \Rightarrow$  *Assumption of saturation mode of operation validated*
- $P_D = V_{DS} \times I_D = 0.5 \text{ mW}$