

- *However, there may be situations when they may become unstable and break out into spontaneous oscillations*
- *Potentially dangerous situation*, and the *system should be protected against it*
- *How does a negative feedback system become unstable?*
  - Write the *loop gain* expression in *polar form*:  
$$L(j\omega) = f(j\omega)A(j\omega) = |f(j\omega)A(j\omega)|\exp[j\phi(\omega)]$$
 $\phi(\omega)$ : *Frequency dependent phase of the system*

- Consider a *particular frequency*  $\omega_x$ , at which  $\phi(\omega_x) = 180^\circ$
- At  $\omega_x$ , L would be a *real number* with *negative sign*
  - ⇒ *The feedback turns positive at this frequency*
- *3 conditions may arise at  $\omega_x$ :*
  - $|L| < 1$ :
    - ❖  $A_f(j\omega_x) > A(j\omega_x)$ , but the *system will be stable*
  - $|L| = 1$ :
    - ❖  $A_f(j\omega_x) \rightarrow \infty$ , and *output will appear without any input*  
⇒ *Oscillator*

- $|L| > 1$ :
  - ❖  $A_f(j\omega_x) < A(j\omega_x)$ , but the *output will oscillate with gradually increasing amplitude*, and will *eventually get limited by the nonlinearities present in the system*
- Thus, for a *negative feedback system* to turn into a *positive feedback one*, the *loop gain* ( $L = fA$ ) being *equal to or less than  $-1$*  is a *sufficient and necessary condition*
- *For this to happen*, the *magnitude of the loop gain* ( $L$ ) *should be equal to or greater than unity*, and the *total phase around the loop should be  $180^\circ$*

# Transfer Function & Stability

- There is a *strong correlation* between the *transfer function* and *stability* of a system
- *Single-Pole System:*
  - *Transfer function* with a *negative real pole* at  $\omega_p$ :

$$A(j\omega) = \frac{A_0}{1 + j\omega/\omega_p}$$

$A_0$ : *Low-Frequency Gain*

- Now, assume that the *system* is *connected* in a *feedback loop*, with the *feedback network* having *feedback factor* f  
 $\Rightarrow$  The *closed-loop transfer function*:

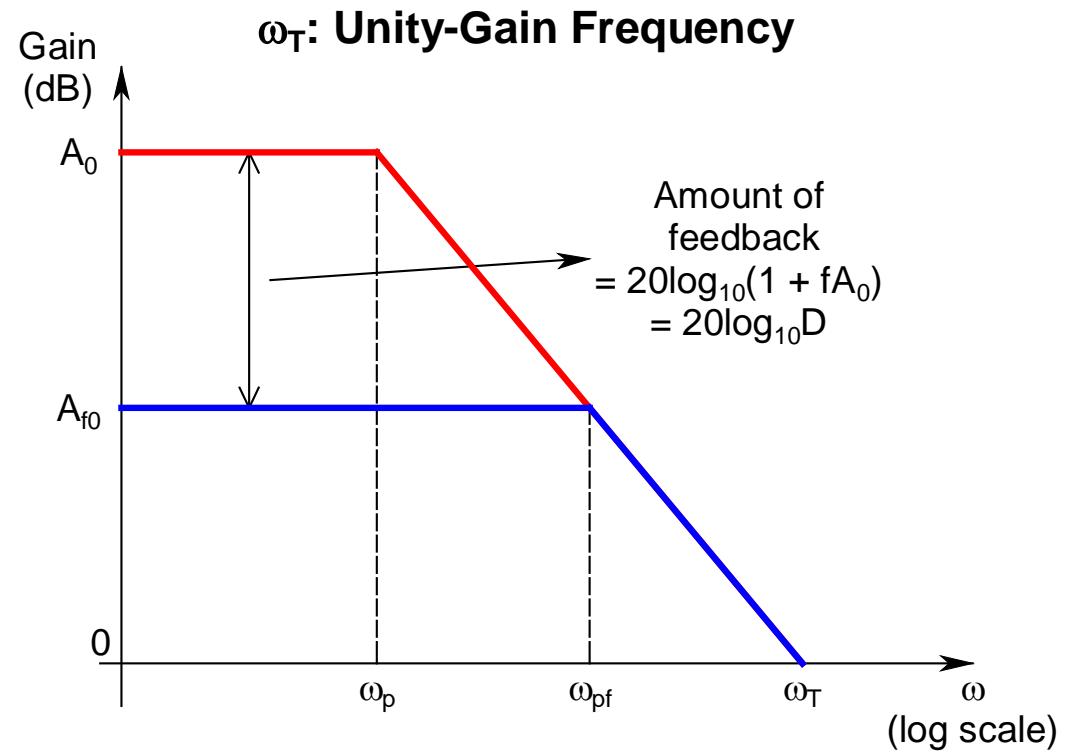
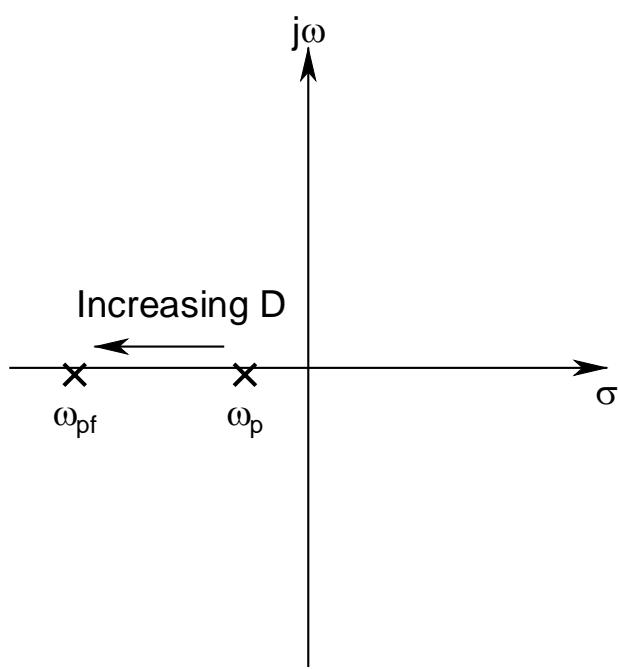
$$A_f = \frac{A_{f0}}{1 + j\omega/\omega_{pf}}$$

$$A_{f0} = A_0/(1 + fA_0) \text{ and } \omega_{pf} = \omega_p(1 + fA_0)$$

- The *gain with feedback reduces by the same amount as the bandwidth gets increased, keeping the GBP constant*

- Thus, the *new pole frequency* is D (the *return difference*) times the *old pole frequency*
  - ⇒ It shifts *left* along the  *$\sigma$ axis* in the *s-plane*, and *remains on the LHP without any imaginary component*
  - ⇒ *The system remains stable even with feedback*
- Also, the *phase* of the system *can never fall below  $-90^\circ$*
- Here, of course we are assuming a *passive feedback network*, i.e., *f is a real number*

- Thus, *f does not add any phase to the system*
- Hence, *Barkhausen's criteria can never be satisfied for this case*
- Also, the *pole can never enter the RHP*
- Thus, we *conclude*:
  - A system with *single-pole transfer function* is *Unconditionally Stable*, i.e., it will *remain stable* for *values of f* all the way *up to unity* (i.e., *the entire output fed back to the input*)



**Movement of the Pole for a Single-Pole System Under Negative Feedback and the Bode Plot of the Gain**

- **Two-Pole System:**

- **Transfer Function:**

$$A(s) = \frac{A_0}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$

$A_0$ : **Low-Frequency Gain**

$\omega_{p1}, \omega_{p2}$ : **Two negative real poles, lying on the  $\sigma$  axis, with  $\omega_{p2} > \omega_{p1}$**

- Now, with **passive feedback** with **feedback factor** f, the **locations** of the **closed-loop poles** can be found from:  $1 + fA(s) = 0$

➤ Thus:

$$s^2 + (\omega_{p1} + \omega_{p2})s + (1 + fA_0)\omega_{p1}\omega_{p2} = 0$$

➤ **Solution** gives the **locations** of the **two closed-loop poles**:

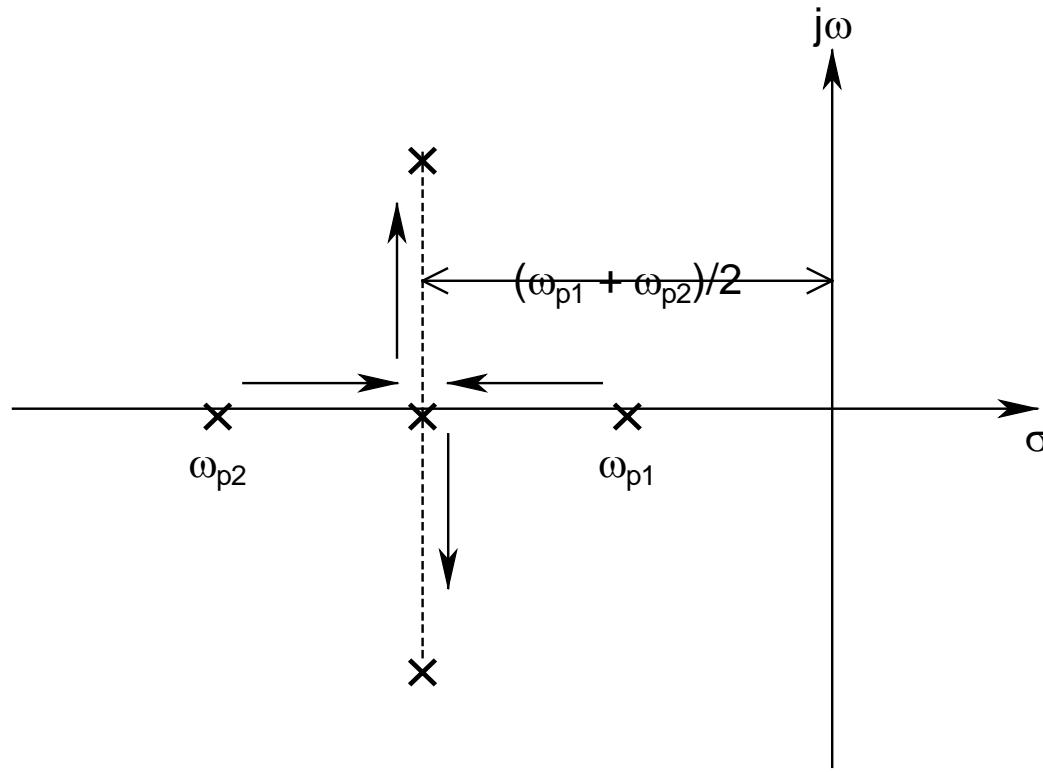
$$s_1, s_2 = -\frac{\omega_{p1} + \omega_{p2}}{2} \pm \frac{1}{2} \sqrt{(\omega_{p1} + \omega_{p2})^2 - 4(1 + fA_0)\omega_{p1}\omega_{p2}}$$

➤ With **increase in feedback**, the **second term reduces**

⇒ **s<sub>1</sub> and s<sub>2</sub> start to move towards each other along the σ axis**

➤ Eventually, at a **particular feedback**, the **second term would vanish**

- At this point, the two poles will merge at  $(\omega_{p1} + \omega_{p2})/2$
- With further increase in feedback, the second term becomes imaginary, while the first term remains constant
  - ⇒ The poles remain complex conjugates
- Even for all the way up to unity, when the entire output is fed back to the input, the poles remain in the LHP and can never enter RHP
  - ⇒ The system remains unconditionally stable



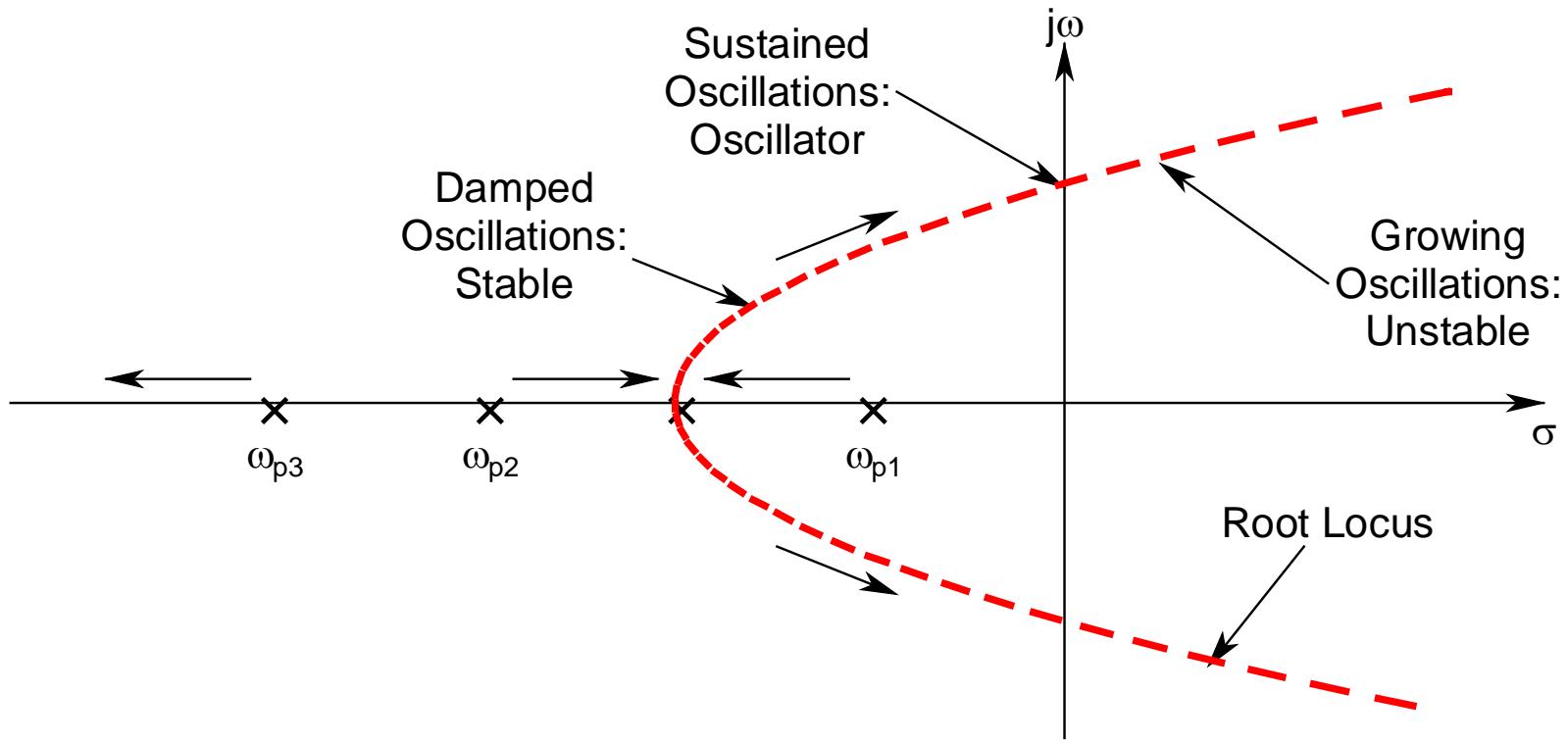
**Movement of the Poles for a Two-Pole System  
Under Negative Feedback With Increasing D**

- Also, for a ***two-pole system***, the ***phase reaches  $-180^\circ$  only when the frequency becomes infinite (mathematically)***
  - ⇒ ***There is no physically achievable frequency when this can happen***
  - ⇒ ***Unconditional Stability***
- ***System With Three (or More) Poles:***
  - ***Actual mathematical analysis quite tedious***
  - It can be shown that as the ***amount of feedback ( $D$ ) is increased:***
    - ***The highest frequency pole ( $\omega_{p3}$ ) moves outward along the  $-\sigma$ -axis***

- *The other two poles ( $\omega_{p1}$  and  $\omega_{p2}$ ) move towards each other (similar to a two-pole system)*
- As  $D$  is increased further, these *two poles eventually merge*, and then start having *imaginary components*
- Their *real part* also *keeps on changing with D, keeping the nature of complex conjugacy intact*, and *moves right in the s-plane*
- *The path traced out by these poles is known as the root locus*
- *For a particular value of D, this root locus intersects the imaginary axis of the s-plane at two symmetric points*

- *Under this condition, sustained sinusoidal oscillation can be achieved, since it now has a complex conjugate pair of poles without any real part ( $\omega_{p3}$  will be so large that it will be inconsequential)*
- *With further increase in D, the root locus enters the RHP with the poles now having positive real part*  
 $\Rightarrow$  *Potentially dangerous situation in terms of stability*
- *In terms of phase, the total can be  $-270^\circ$*   
 $\Rightarrow$  *There exists a particular value of f, for which the phase will become  $-180^\circ$*

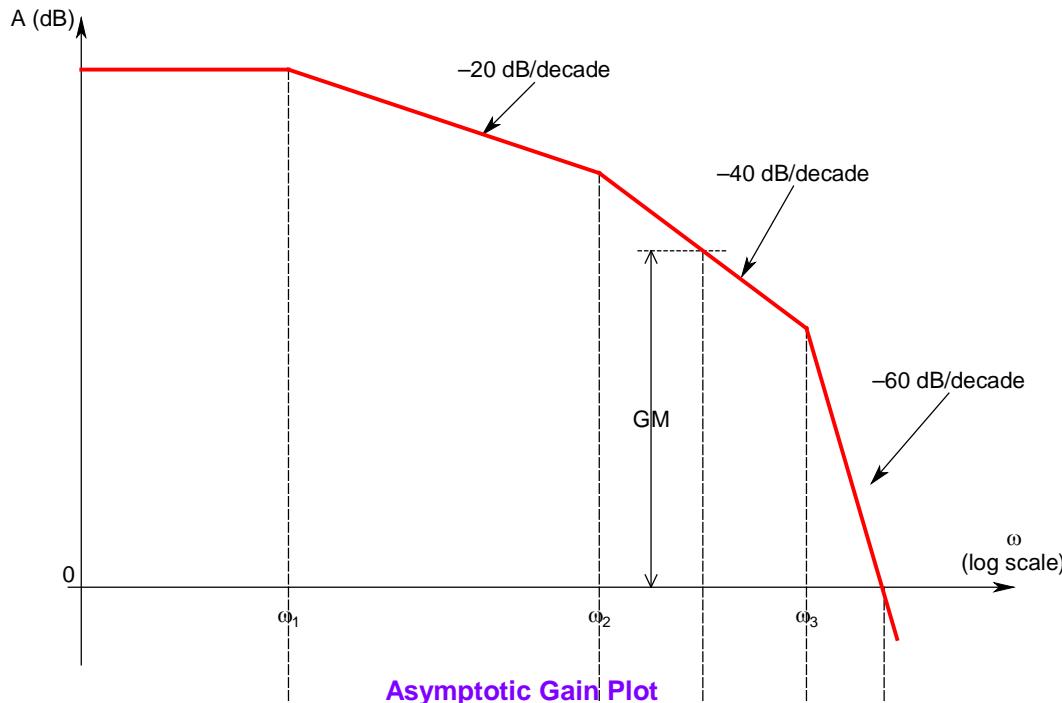
- *Under this condition, if the magnitude of the loop gain is exactly unity, then the system will break out into spontaneous oscillation, however, the amplitude will be controlled*  
⇒ *Sustained sinusoidal oscillation*
- *This particular value of  $f$  is known as the critical feedback factor ( $f_{crit}$ ) for oscillation*
  - ❖ For  $f < f_{crit}$ , the *system will be stable*
  - ❖ For  $f > f_{crit}$ , the *system will be unstable*
- Thus, the system is *NOT Unconditionally Stable*, but *stable only till a specific value of  $f$* 
  - ❖ Known as *Conditionally Stable System*



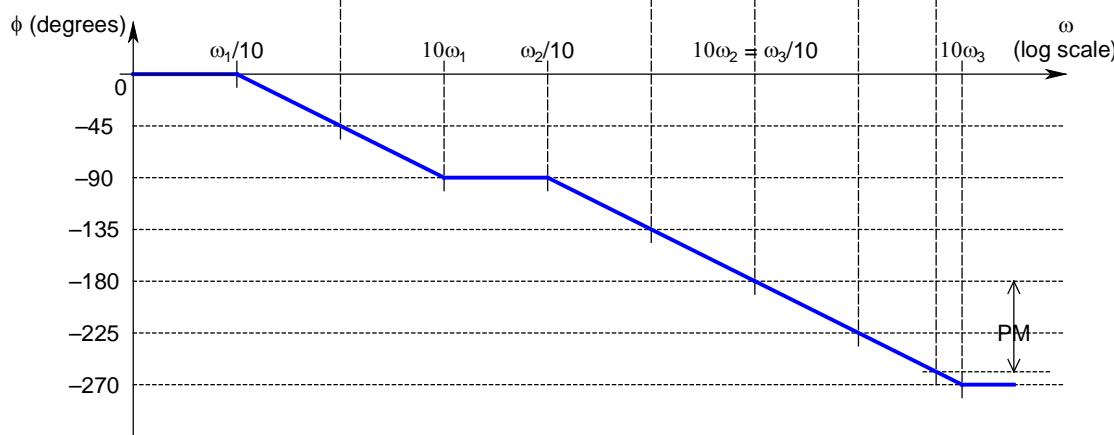
## Root Locus of the Poles of a Three-Pole System as D is Increased

# Stability Study Using Bode Plot

- The *most convenient* and the *most useful*
- *Recall: Single- and Two-Pole Systems are unconditionally stable*
- Consider a *Three-Pole System*, with the *pole frequencies* at  $\omega_1$ ,  $\omega_2$ , and  $\omega_3$ , with  $\omega_3 = 100\omega_2$ , and  $\omega_2 > 100\omega_1$
- *Note:  $A = L$  iff  $= 1$  (100% feedback)*
- Refer to the next slide (*Bode Plot*)



Asymptotic Gain Plot



Asymptotic Phase Plot

- *Profile of A:*
  - *Remains constant at its low-frequency value for  $\omega \leq \omega_1$*
  - *Then drops @ 20 dB/decade till  $\omega_2$*
  - *Followed by a drop @ 40 dB/decade till  $\omega_3$*
  - *Then drops @ 60 dB/decade*
  - *Finally crosses 0 dB at  $\omega$  slightly less than  $10\omega_3$*
- *Profile of  $\phi$ :*
  - *Remains zero till  $\omega_1/10$*
  - *Then drops @ 45 %decade*

- **Reaches  $-90^\circ$  at  $10\omega_1$**
- **Stays constant at  $-90^\circ$  till  $\omega_2/10$**
- **Then starts to drop again @ 45%decade till  $10\omega_3$**
- **Reaches  $-180^\circ$  at  $10\omega_2$  ( $= \omega_3/10$ ) and  $-270^\circ$  at  $10\omega_3$**
- ***Gain Margin (GM) and Phase Margin (PM):***
  - ***Extremely important terms with regard to stability of a system***
  - ***From the sign and magnitude of these terms, the stability of the system can be predicted***

- $GM = A(dB)$  (*when  $\phi = -180^\circ$* )
- $PM = 180^\circ - |\phi|$  (*when  $A = 0 \text{ dB}$* )
- In our example,  $GM$  is positive (as shown in the figure)
- This is *potentially a dangerous situation*, and characterizes a *highly unstable system*
  - For *positive GM*, with each pass around the loop, the *output amplitude will keep on growing*
- On the contrary, if *GM were negative*, with each pass around the loop, the *output amplitude would have decreased*

- *The system would have come out of any unwanted oscillations*
- *The GM dictates the maximum amount of feedback that can be allowed for the system to remain stable*
- *For an unconditionally stable system, GM must be negative*  
⇒ *A must be negative when  $\phi = -180^\circ$*
- *With regard to phase, when A crossed 0 dB,  $\phi$  is close to  $-270^\circ$*   
⇒ *PM is negative, with a value of  $\sim -90^\circ$*

- *This also implies that when  $\phi$  crossed  $-180^\circ$ , A of the system was greater than unity (0 dB)*
  - *A potentially dangerous situation in terms of stability*
- Therefore, *for an unconditionally stable system, PM must be positive*
- *The two conditions with regard to GM and PM are actually correlated*
- *Rule of Thumb:*
  - *For a stable system,  $GM \sim -10 \text{ dB}$  and  $PM \sim 45^\circ$  are generally good enough*