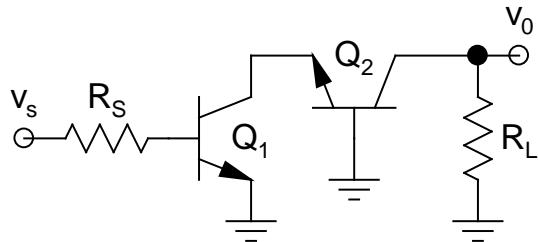
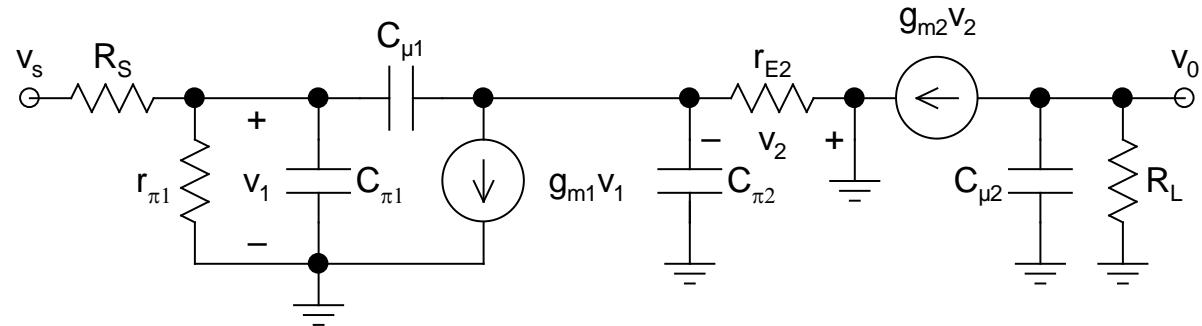


- *npn Cascode:*



ac Schematic



High-Frequency Equivalent

- *Looks intimidating*, but *extremely easy to solve (just by inspection)*
- Also known as *Wideband* (or *Broadband*) *Amplifier* due to its *superb frequency response*

➤ ***Reason:***

- *The circuit does have an input-output coupling capacitor ($C_{\mu 1}$)*
- *Miller Effect Multiplication Factor* (MEMF) of $C_{\mu 1} = (1 - A_{v1})$
 $A_{v1} = \text{voltage gain of } Q_1 = -r_{E2}/r_{E1} = -1$
(since Q_1 and Q_2 are biased with the same I_C)
⇒ Thus, the *MEMF of $C_{\mu 1}$ is only 2*
- For *NMOS Cascode* stage, the *MEMF of C_{gd1}* of M_1 (*CS stage*) will be $[1 + 1/(1 + \chi_2)]$ (*verify this expression*), which is *even less than 2*

➤ $C_{\pi l}$:

- *By inspection:*

$$R_{\pi 1}^0 = R_S \parallel r_{\pi 1} \Rightarrow \tau_1 = R_{\pi 1}^0 C_{\pi 1}$$

➤ $C_{\mu l}$:

- Can be easily identified as the ***Three-Legged Creature***

$$\Rightarrow R_{\mu 1}^0 = R_{\pi 1}^0 + r_{E2} + g_{m1} R_{\pi 1}^0 r_{E2}$$

$$\Rightarrow \tau_2 = R_{\mu 1}^0 C_{\mu 1}$$

➤ $C_{\pi 2}$:

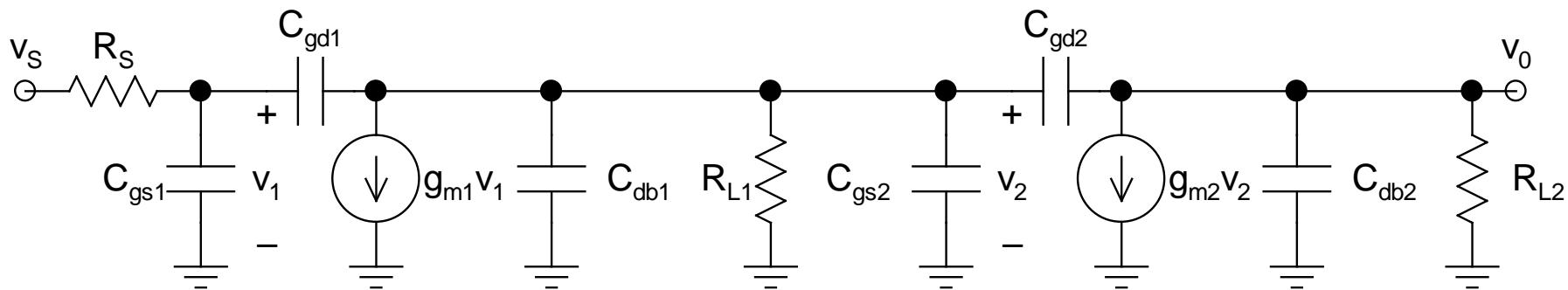
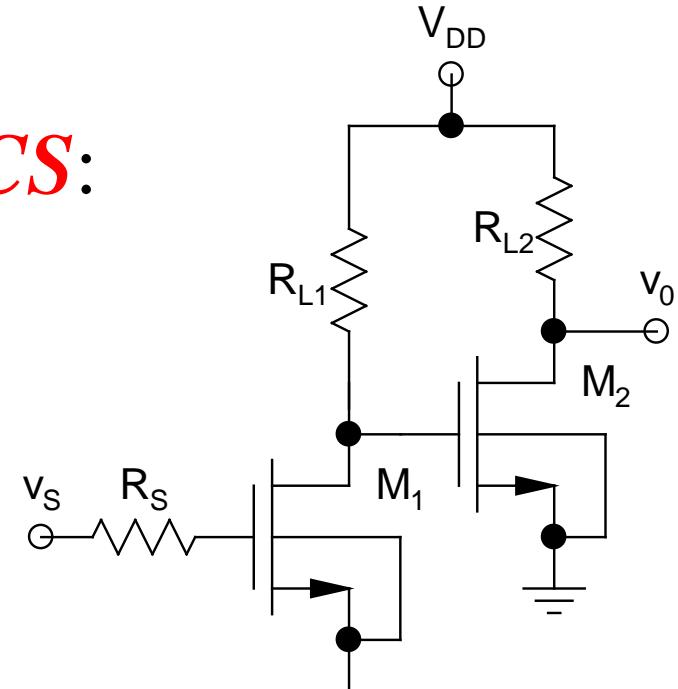
- *By inspection:*

$$R_{\pi 2}^0 = r_{E2} \Rightarrow \tau_3 = R_{\pi 2}^0 C_{\pi 2}$$

- $C_{\mu 2}$:
 - *By inspection:*
$$R_{\mu 2}^0 = R_L \Rightarrow \tau_4 = R_{\mu 2}^0 C_{\mu 2}$$
- Generally, for this circuit, $C_{\pi 1}$ is the *dominant capacitor* that determines f_H , since it sees the *largest resistance*
- The *resistance seen by $C_{\mu 1}$* , which is the *largest for CE stage, becomes quite small here, due to the low gain of Q_1*
- Note how *simple* it is to use this *technique* even for *multi-stage amplifiers!*

- **NMOS 2-Stage Cascaded CS:**

- *Except C_{sb} , all other capacitors will be present for both devices*
- *6 capacitors*
 \Rightarrow *6 time constants*



High-Frequency Equivalent

- **Note**: An *exact analysis* would have required *solving a 6th-order equation in ω !*
- Let's perform a *quantitative analysis* of this circuit
- **Data**: $g_{m1} = 3 \text{ mA/V}$, $g_{m2} = 6 \text{ mA/V}$, $C_{gs1} = 5 \text{ pF}$, $C_{gs2} = 10 \text{ pF}$, $C_{gd1} = C_{gd2} = 1 \text{ pF}$, $C_{db1} = C_{db2} = 2 \text{ pF}$, $R_S = 10 \text{ k}\Omega$, $R_{L1} = 10 \text{ k}\Omega$, and $R_{L2} = 5 \text{ k}\Omega$.

■ *C_{gs1}* :

$$R_{gs1}^0 = R_S = 10 \text{ k}\Omega \quad \Rightarrow \tau_1 = R_{gs1}^0 C_{gs1} = 50 \text{ ns}$$

- C_{gd1} :

$$R_{gd1}^0 = R_S + R_{L1} + g_{m1} R_S R_{L1} = 320 \text{ k}\Omega$$

$$\Rightarrow \tau_2 = R_{gd1}^0 C_{gd1} = 320 \text{ ns}$$

- C_{db1} and C_{gs2} in parallel

$$\Rightarrow \text{Club them to a single capacitor } C_3 = C_{db1} + C_{gs2} \\ = 12 \text{ pF}$$

$$R_3^0 = R_{L1} = 10 \text{ k}\Omega$$

$$\Rightarrow \tau_3 = R_3^0 C_3 = 120 \text{ ns}$$

- ***C_{gd2}*:**

$$R_{gd2}^0 = R_{L1} + R_{L2} + g_{m2} R_{L1} R_{L2} = 315 \text{ k}\Omega$$

$$\Rightarrow \tau_4 = R_{gd2}^0 C_{gd2} = 315 \text{ ns}$$

- ***C_{db2}*:**

$$R_{db2}^0 = R_{L2} = 5 \text{ k}\Omega$$

$$\Rightarrow \tau_5 = R_3^0 C_3 = 10 \text{ ns}$$

- Thus:

$$\tau_{\text{net}} = 815 \text{ ns} \text{ and } f_H = 195.3 \text{ kHz}$$

- Such a *low value* of f_H is the *result* of the *presence* of a *large number of capacitors* in the circuit

- ***Limitations of the ZVTC Technique:***
 - *One obvious limitation is the suppression of information of all other poles and zeros of the system except the DP*
 - *This limitation is not that acute since we are actually interested in only the DP, which gives the information about f_H*
 - ***The other limitation is the error, which can reach as high as 22%***
 - However, *this error is negative*, i.e., *underestimation* (far better than *overestimation*)

- The **maximum error** of 22% occurs if the **actual circuit** has **two overlapping poles**
- In **real situations**, this is **highly unlikely**, due to the effect of **pole splitting** caused by **compensation** (*to be discussed in the next chapter*)
- **The resulting circuit after compensation would have a single DP**

➤ *Proof that the maximum error is 22%*

- Consider a circuit having **2 negative real poles** at the **same angular frequency** ω_x
- The **Transfer Function**:

$$A(j\omega) = A_0 / (1 + j\omega/\omega_x)^2$$

A_0 : **Midband gain**

$$\Rightarrow |A(j\omega)| = A_0 / [1 + (\omega/\omega_x)^2]$$

- At the **upper cutoff frequency** ω_H , the **gain would drop to $1/\sqrt{2}$ of its maximum value**

$$\Rightarrow 1 + (\omega_H/\omega_x)^2 = \sqrt{2}$$

$$\Rightarrow \omega_H = [\sqrt{\sqrt{2} - 1}] \omega_x = 0.64 \omega_x$$

- Now, using the **ZVTC technique**, the ***net time constant***

$$\tau = \sum_{i=1}^n (-1/p_i)$$

i = ***number of poles***

p_i = ***individual poles***

- For the ***given problem***, $i = 2$ and $p_i = -\omega_x$ (***for both***)
- Thus:

$$\tau_{\text{net}} = 2/\omega_x \text{ and } \omega_H = 1/\tau_{\text{net}} = 0.5\omega_x$$

- Therefore, the ***maximum error is about -22%***
- This being an ***underestimation***, is ***not that dangerous*** :)

- **Rise/Fall Time:**
 - *Recall: f_L caused tilt/sag in the output for square-wave input*
 - *On the other side of the frequency spectrum, f_H causes rise/fall time of the output for square-wave input*
 - *These two phenomena can be thought of as an interlinking between the analog and digital domains*
 - Assume that a circuit has some ω_H , with the **corresponding pole** at $p_1 (= -\omega_H)$

- The ***Transfer Function*** is *single-pole*:

$$v_0(s)/v_i(s) = A_0/(1 - s/p_1)$$

A_0 : ***Midband gain***

- Now, consider v_i to be ***step input*** of *amplitude*

$$V_A \ (\Rightarrow v_i = V_A/s)$$

$$\begin{aligned} \Rightarrow v_0(s) &= (A_0 V_A / s) / (1 - s/p_1) \\ &= A_0 V_A [1/s - 1/(s - p_1)] \end{aligned}$$

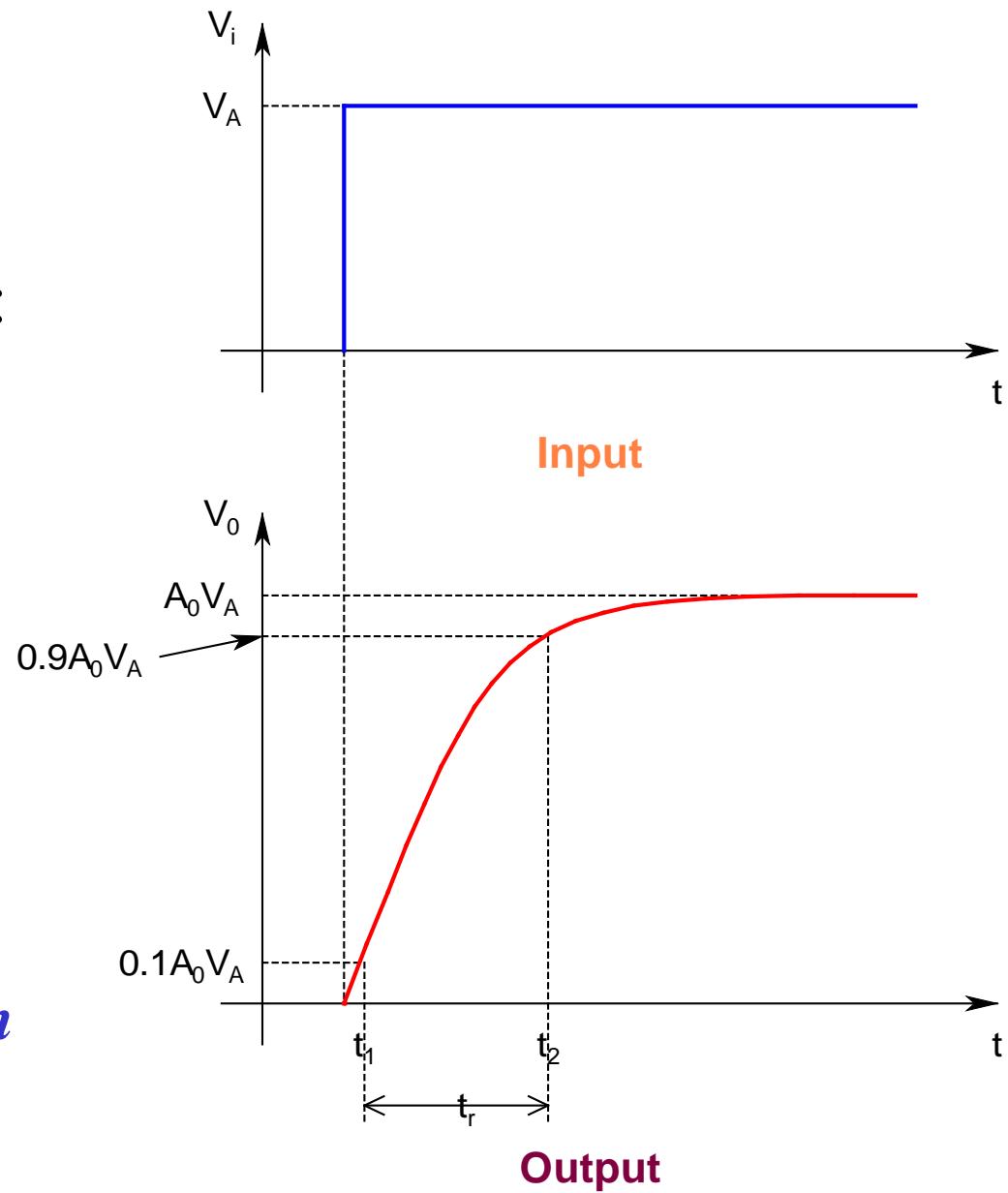
- Taking ***inverse Laplace Transform***:

$$v_0(t) = A_0 V_A [1 - \exp(|p_1|t)]$$

\Rightarrow ***Output approaches its maximum value of $A_0 V_A$ with a time constant $1/|p_1|$ (p_1 negative)***

➤ *Calculation of Rise/Fall Time:*

- *Time taken for the output to rise (fall) from 10% (90%) to 90% (10%)*
- *Can be calculated from the figure*



- *At $t = t_1$:*

$$0.1A_0V_A = A_0V_A[1 - \exp(p_1 t_1)]$$

$$\Rightarrow t_1 = \ln(0.9)/p_1$$

- *At $t = t_2$:*

$$0.9A_0V_A = A_0V_A[1 - \exp(p_1 t_2)]$$

$$\Rightarrow t_2 = \ln(0.1)/p_1$$

- Thus, the *rise time*:

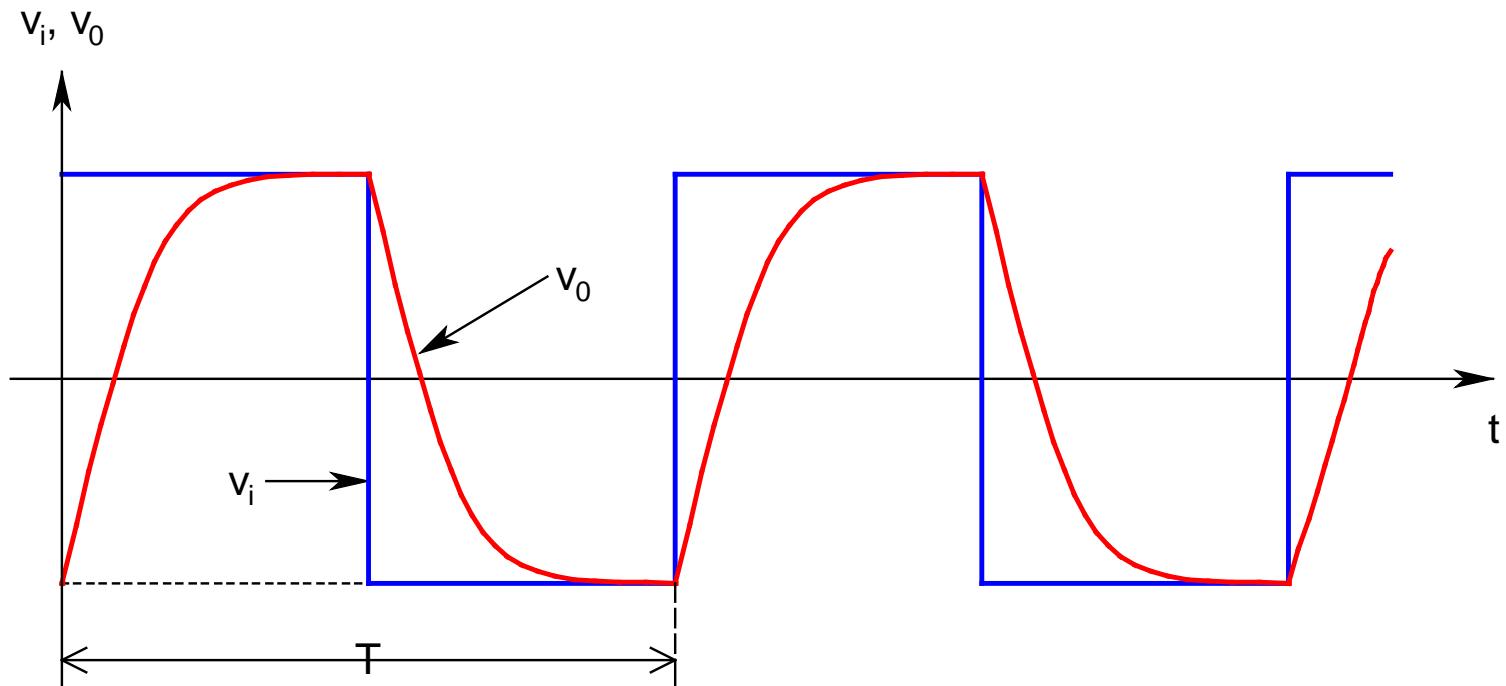
$$t_r = t_2 - t_1 = -2.2/p_1 = 2.2/\omega_H = 0.35/f_H$$

- Hence, *higher the f_H , smaller the t_r*

- *The same expression holds for the fall time (t_f) as well*

- Thus, circuits having ***high bandwidth*** under ***sinusoidal excitation (analog domain)***, will also have ***superb switching characteristics*** under ***square-wave excitation (digital domain)***
- Under ***square-wave excitation, due to t_r/t_f ,*** ***enough time should be provided for the transient in the output to get completed***
- ***Rule of Thumb:***
 - ***At least 5 time constants should be allowed for each rising and falling transient***
 - This determines the ***maximum allowable frequency*** of the ***input pulse train:***

$$f_{\max} = 1/T_{\min} \approx 1/(10\tau) = \omega_H/10 = |p_1|/10$$



Effect of t_r/t_f on the Output for Square-Wave Excitation

- As $f \uparrow$, $T \downarrow$, V_0 first starts to become triangular (*incomplete transient*), then the amplitude starts to drop, and eventually drops to zero (*no output at all!*)

FEEDBACK, STABILITY, & COMPENSATION

Feedback

- *Connection between input and output - either directly through a wire, or through some circuit elements*
 - ⇒ *Input and output gets coupled*
 - ⇒ *Any change in either of them, affects the overall behavior*
- *2 Types:*
 - *Negative*
 - *Positive*

- **Negative Feedback:**
 - *Output fed back to input in such a way that it reduces net input*
⇒ *Causes a reduction in the output*
 - Known as **Degenerative Feedback**
- **Positive Feedback:**
 - *Output fed back to input in such a way that it increases net input*
⇒ *Causes an increase in the output*
 - Known as **Regenerative Feedback**