

Lecture-18

On

INTRODUCTION TO ELECTRICAL ENGINEERING (ESO203)

- Impedance Parameters (Cont...)
- Admittance Parameters.

Impedance Parameters (Cont...)

- The relation between the terminal voltage and the terminal current can be established using the following equations:

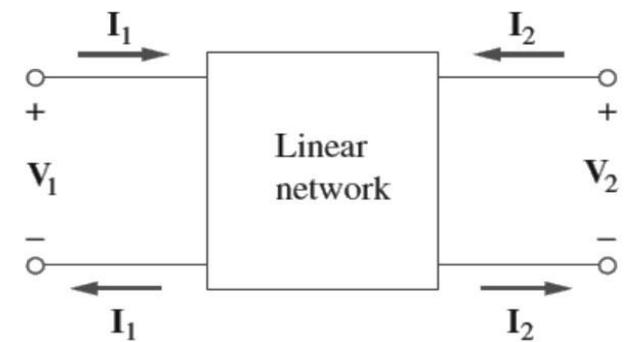
$$V_1 = z_{11}I_1 + z_{12}I_2$$

$$V_2 = z_{21}I_1 + z_{22}I_2$$

- This can alternatively be expressed in matrix form as,

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = [z] \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

- Here the **z** terms are known as the impedance parameters or the **z** parameters.
- Impedance parameters are expressed in ohms.



Impedance Parameters (Cont...)

- The values of the parameters can be evaluated by setting $\mathbf{I}_1 = \mathbf{0}$ (input port open-circuited) or $\mathbf{I}_2 = \mathbf{0}$ (output port open-circuited).
- Since the z parameters are obtained by open-circuiting the input or output port, they are also called the open-circuit impedance parameters.
- The individual parameters are evaluated as follows:

$$\mathbf{V}_1 = \mathbf{z}_{11}\mathbf{I}_1 + \mathbf{z}_{12}\mathbf{I}_2$$

$$\mathbf{V}_2 = \mathbf{z}_{21}\mathbf{I}_1 + \mathbf{z}_{22}\mathbf{I}_2$$

- If $\mathbf{I}_2 = \mathbf{0}$, then

$$\mathbf{z}_{11} = \frac{\mathbf{V}_1}{\mathbf{I}_1}, \mathbf{z}_{21} = \frac{\mathbf{V}_2}{\mathbf{I}_1}$$

- If $\mathbf{I}_1 = \mathbf{0}$, then

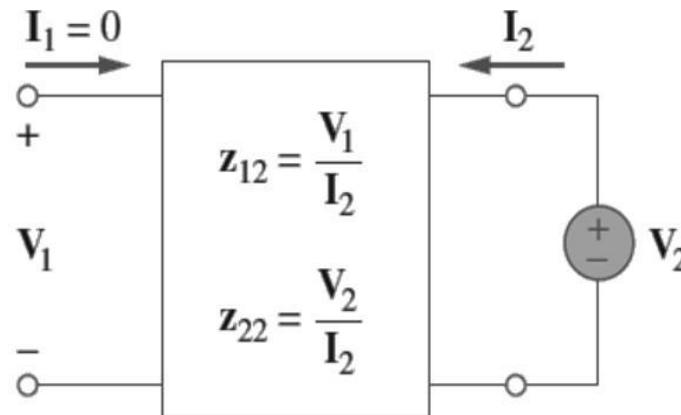
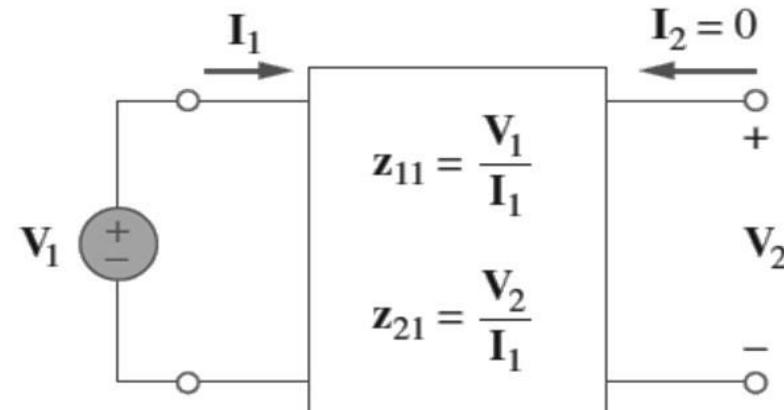
$$\mathbf{z}_{12} = \frac{\mathbf{V}_1}{\mathbf{I}_2}, \mathbf{z}_{22} = \frac{\mathbf{V}_2}{\mathbf{I}_2}$$

Impedance Parameters (Cont...)

- Specifically,
 - \mathbf{z}_{11} = Open-circuit input impedance
 - \mathbf{z}_{12} = Open-circuit transfer impedance from port 1 to port 2
 - \mathbf{z}_{21} = Open-circuit transfer impedance from port 2 to port 1
 - \mathbf{z}_{22} = Open-circuit output impedance
- The values of \mathbf{z}_{11} and \mathbf{z}_{21} can be obtained by connecting a voltage \mathbf{V}_1 (or current \mathbf{I}_1) to port 1 with port 2 open-circuited ($\mathbf{I}_2 = 0$).
- \mathbf{I}_1 , \mathbf{V}_1 and \mathbf{V}_2 are then obtained which can be used to evaluate $\mathbf{z}_{11} = \frac{\mathbf{V}_1}{\mathbf{I}_1}$ and $\mathbf{z}_{21} = \frac{\mathbf{V}_2}{\mathbf{I}_1}$
- Similarly, the values of \mathbf{z}_{12} and \mathbf{z}_{22} can be obtained by connecting a voltage \mathbf{V}_2 (or current \mathbf{I}_2) to port 2 with port 1 open-circuited ($\mathbf{I}_1 = 0$).
- \mathbf{I}_2 , \mathbf{V}_2 and \mathbf{V}_1 are then obtained which can be used to evaluate $\mathbf{z}_{12} = \frac{\mathbf{V}_1}{\mathbf{I}_2}$ and $\mathbf{z}_{22} = \frac{\mathbf{V}_2}{\mathbf{I}_2}$

Impedance Parameters (Cont...)

- The above procedure can be easily understood using the following Figure.

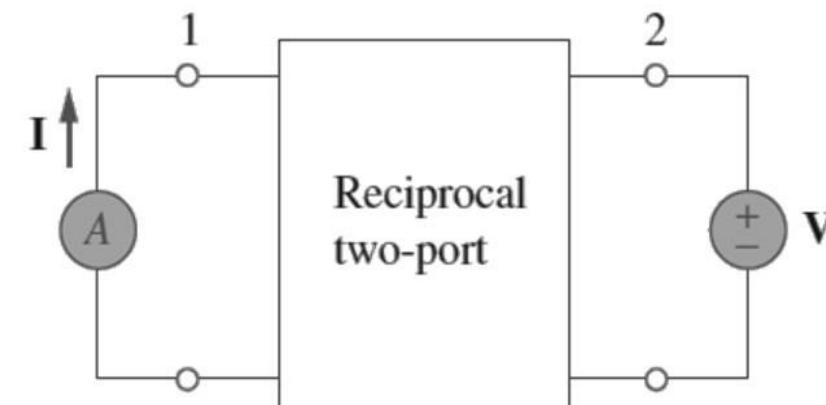
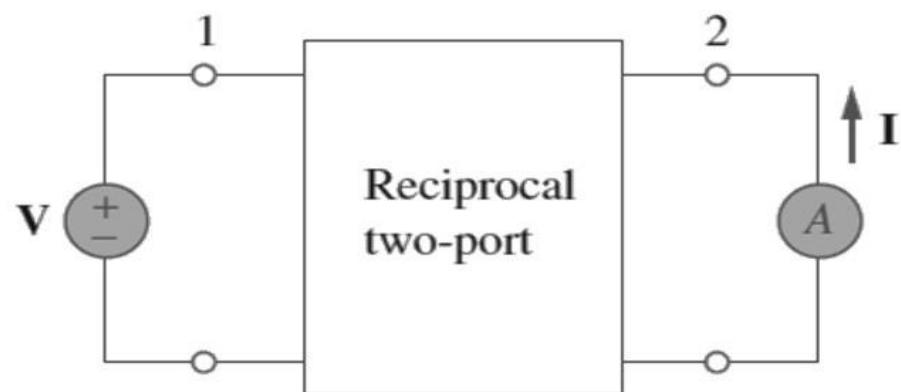


Impedance Parameters (Cont...)

- Sometimes \mathbf{z}_{11} and \mathbf{z}_{22} are called driving-point impedances, while \mathbf{z}_{12} and \mathbf{z}_{21} are called transfer impedances.
- A driving-point impedance is the input impedance of a two-terminal (one-port) device.
- Thus, \mathbf{z}_{11} is the input driving-point impedance with the output port open-circuited, while \mathbf{z}_{22} is the output driving-point impedance with the input port open-circuited.
- When $\mathbf{z}_{11} = \mathbf{z}_{22}$, the two-port network is said to be symmetrical.
- This implies that the network has mirror-like symmetry about some center line; that is, a line can be found that divides the network into two similar halves.
- In other words, a two port network is said to be symmetrical if the input and output ports can be interchanged without altering the port voltages and currents.

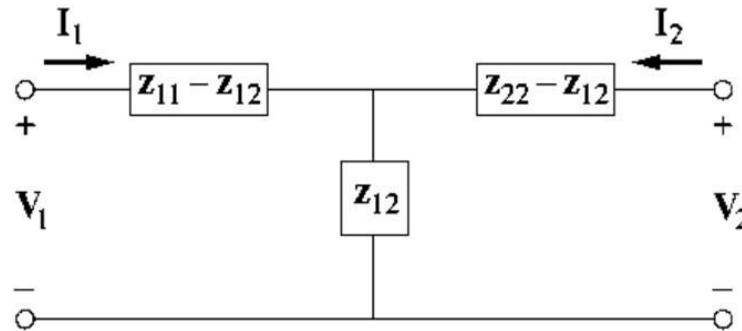
Impedance Parameters (Cont...)

- When the two-port network is linear and has no dependent sources, and the transfer impedances are equal ($\mathbf{Z}_{12} = \mathbf{Z}_{21}$), then the two-port is said to be reciprocal.
- This means that if the points of excitation and response are interchanged, the transfer impedances remain the same.
- As shown in the figure below, a two-port is reciprocal if interchanging an ideal voltage source at one port with an ideal ammeter at the other port gives the same ammeter reading.

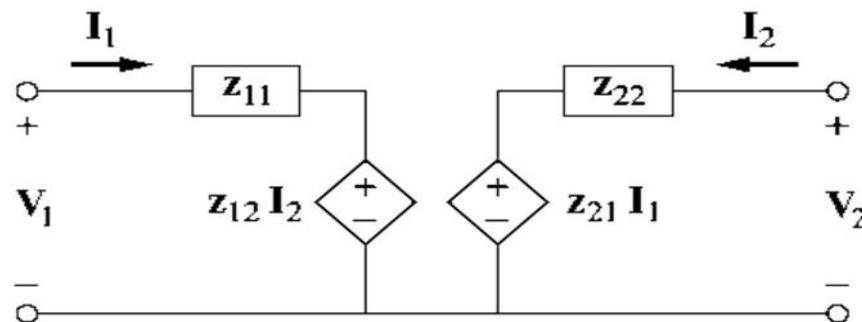


Impedance Parameters (Cont...)

- Any two-port that is made entirely of resistors, capacitors, and inductors must be reciprocal.
- A reciprocal network can be replaced by the T-equivalent circuit as shown in the below figure.



- If the network is not reciprocal, a more general equivalent network as shown below can be used.

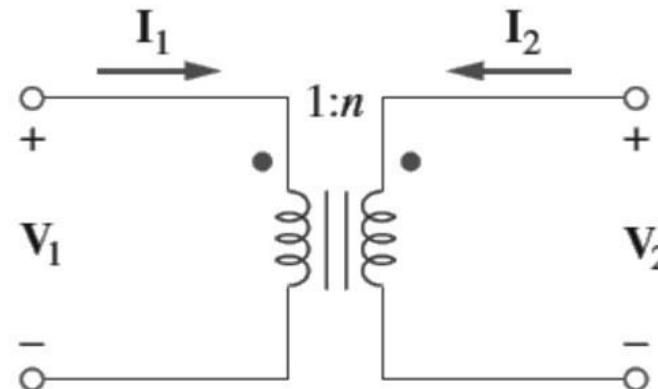


Impedance Parameters (Cont...)

- It should be mentioned that for some two-port networks, the **z**-parameters do not exist because they cannot be described by the **z**-parameter equations.
- As an example, consider the ideal transformer shown in the figure.
- The defining equations for the two-port network are:

$$\mathbf{V}_1 = \frac{1}{n} \mathbf{V}_2, \mathbf{I}_1 = -n \mathbf{I}_2$$

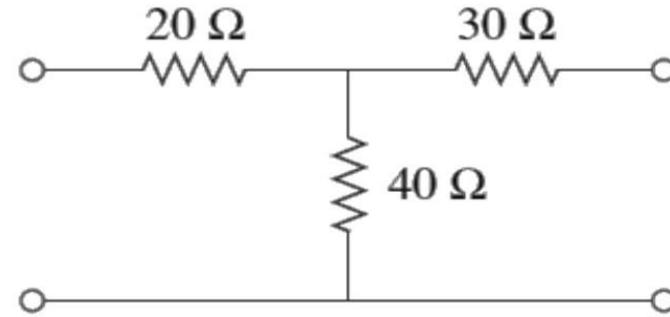
- Observe that it is impossible to express the voltages in terms of the currents, and vice versa.
- Thus, the ideal transformer has no **z**-parameters.
- However, it does have hybrid parameter as will be discussed in the upcoming lectures.



Impedance Parameters (Cont...)

□ Example:

- ❖ Determine the **z**-parameters for the below circuit?



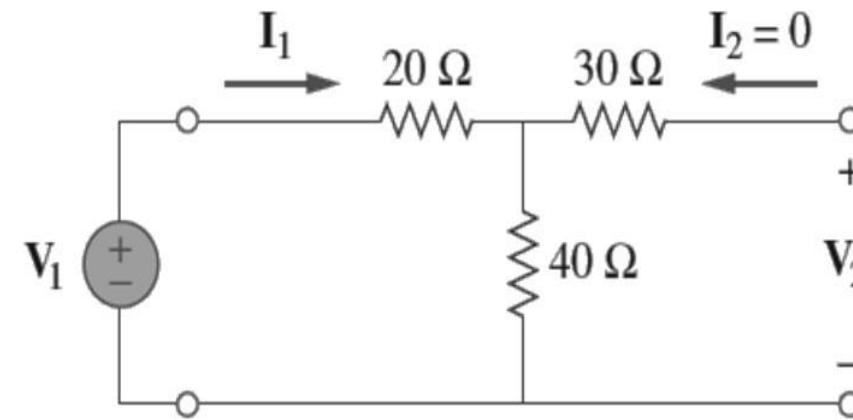
□ Solution:

The parameters are determined using the equations discussed earlier in the lecture

Impedance Parameters (Cont...)

□ Solution:

To determine \mathbf{z}_{11} and \mathbf{z}_{21} , we apply a voltage source \mathbf{V}_1 to the input port and leave the output port open as in the following figure.



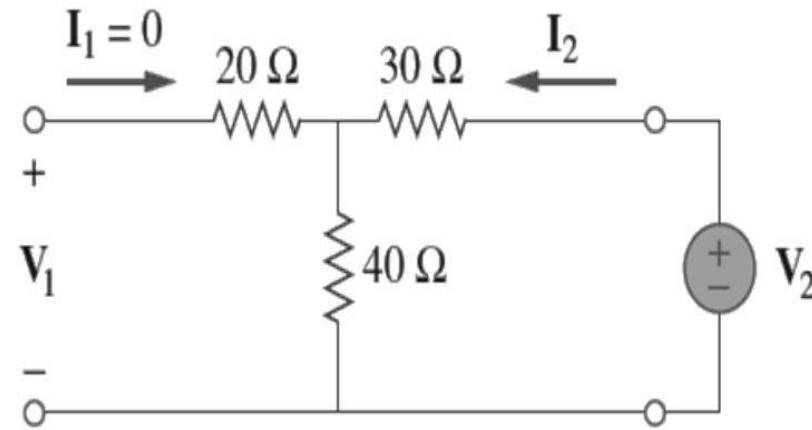
$$\mathbf{z}_{11} = \frac{\mathbf{V}_1}{\mathbf{I}_1} = \frac{(20 + 40)\mathbf{I}_1}{\mathbf{I}_1} = 60\ \Omega$$

$$\mathbf{z}_{21} = \frac{\mathbf{V}_2}{\mathbf{I}_1} = \frac{40\mathbf{I}_1}{\mathbf{I}_1} = 40\ \Omega$$

Impedance Parameters (Cont...)

□ Solution:

To determine \mathbf{z}_{12} and \mathbf{z}_{22} , we apply a voltage source \mathbf{V}_2 to the output port and leave the input port open as in the following figure.



$$\mathbf{z}_{12} = \frac{\mathbf{V}_1}{\mathbf{I}_2} = \frac{40\mathbf{I}_2}{\mathbf{I}_2} = 40 \Omega$$

$$\mathbf{z}_{22} = \frac{\mathbf{V}_2}{\mathbf{I}_2} = \frac{(40 + 30)\mathbf{I}_2}{\mathbf{I}_2} = 70 \Omega$$

Impedance Parameters (Cont...)

□ Solution:

- This can alternatively be expressed in matrix form as,

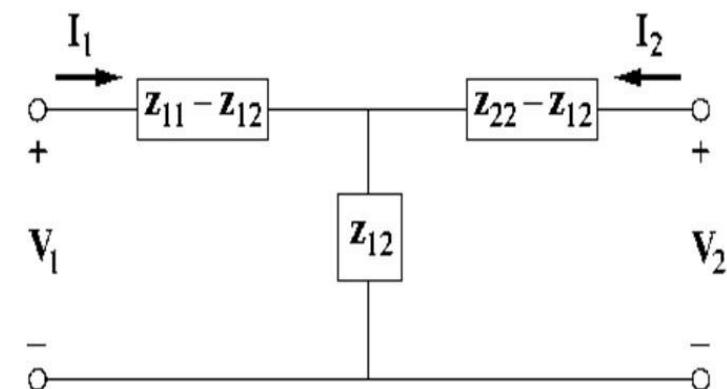
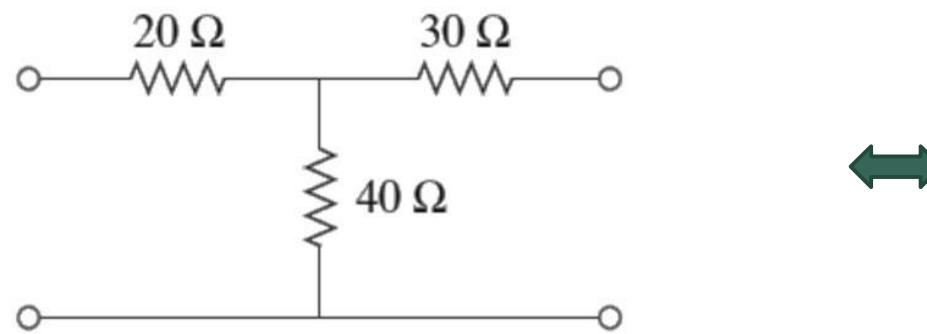
$$[z] = \begin{bmatrix} 60\Omega & 40\Omega \\ 40\Omega & 70\Omega \end{bmatrix}$$

- Alternatively, since there is no dependent source in the circuit, $z_{12} = z_{21}$, we can use the T-equivalent circuit. Comparing the circuit in the question to the equivalent circuit,

$$z_{12} = 40 \Omega = z_{21}$$

$$z_{11} - z_{12} = 20 \Rightarrow z_{11} = 20 + z_{12} = 60 \Omega$$

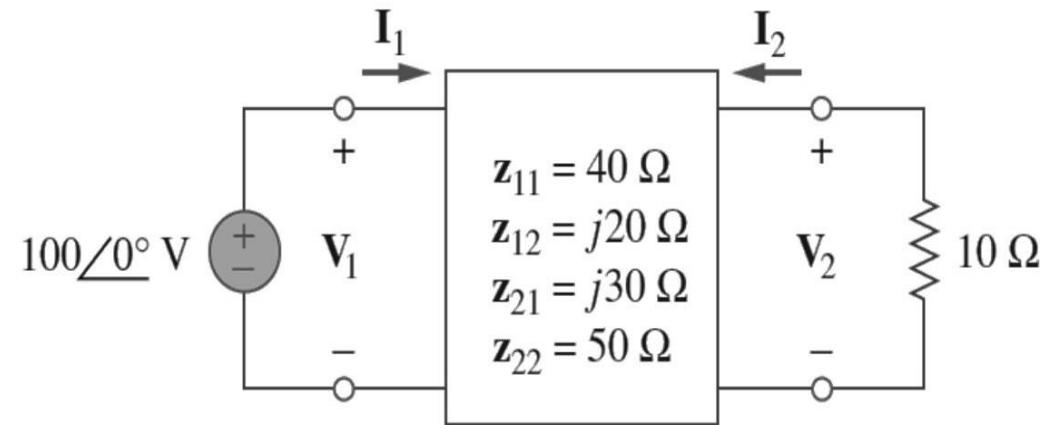
$$z_{22} - z_{12} = 30 \Rightarrow z_{22} = 30 + z_{12} = 70 \Omega$$



Impedance Parameters (Cont...)

□ Example:

- ❖ Find \mathbf{I}_1 and \mathbf{I}_2 in the circuit given below?



□ Solution:

This is not a reciprocal circuit. The equivalent circuit discussed previously can be used to solve the problem. However, the z -parameter equations can be used directly in this scenario.

Impedance Parameters (Cont...)

□ Solution:

- The relation between the terminal voltage and the terminal current can be established using the following equations, as discussed previously:

$$\mathbf{V}_1 = 40\mathbf{I}_1 + j20\mathbf{I}_2$$

$$\mathbf{V}_2 = j30\mathbf{I}_1 + 50\mathbf{I}_2$$

- But $\mathbf{V}_1 = 100\angle 0^\circ$ and $\mathbf{V}_2 = -10\mathbf{I}_2$

- Therefore,

$$100 = 40\mathbf{I}_1 + j20\mathbf{I}_2 \quad (1)$$

$$-10\mathbf{I}_2 = j30\mathbf{I}_1 + 50\mathbf{I}_2 \Rightarrow \mathbf{I}_1 = j2\mathbf{I}_2 \quad (2)$$

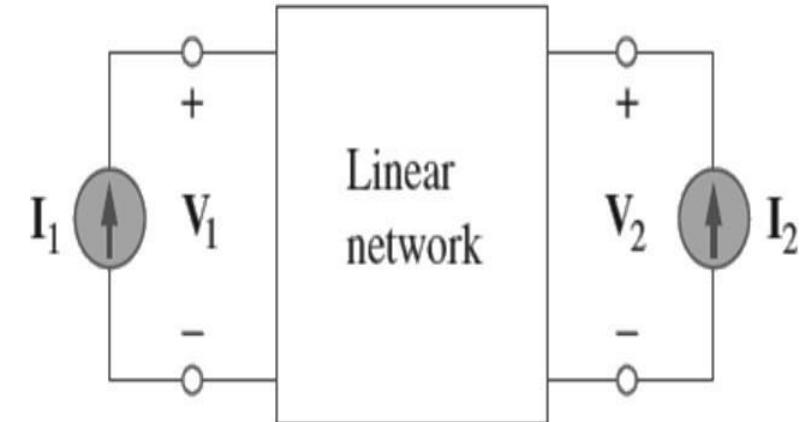
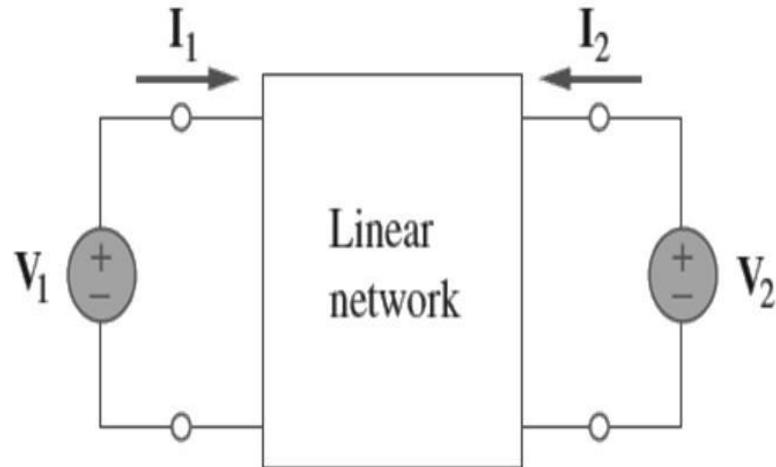
- Substituting the (2) in (1)

- As $\mathbf{I}_1 = j2\mathbf{I}_2 = j2(-j) = 2$. Thus,

$$\mathbf{I}_1 = 2\angle 0^\circ \text{A} \quad \text{and} \quad \mathbf{I}_2 = 1\angle -90^\circ \text{A}$$

Admittance Parameters

- A two-port network may be voltage driven or current driven as illustrated in the figure below.
- To determine the admittance parameters the terminal currents are expressed in terms of the terminal voltages.



Admittance Parameters (Cont..)

- The relation between the terminal voltage and the terminal current can be established using following equations:

$$\begin{aligned}\mathbf{I}_1 &= \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2 \\ \mathbf{I}_2 &= \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2\end{aligned}$$

- This can alternatively be expressed in matrix form as,

$$\begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix} \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix} = [\mathbf{y}] \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix}$$

- Here the \mathbf{y} terms are known as the admittance parameters or the y parameters.
- Admittance parameters are expressed in siemens.

Admittance Parameters (Cont..)

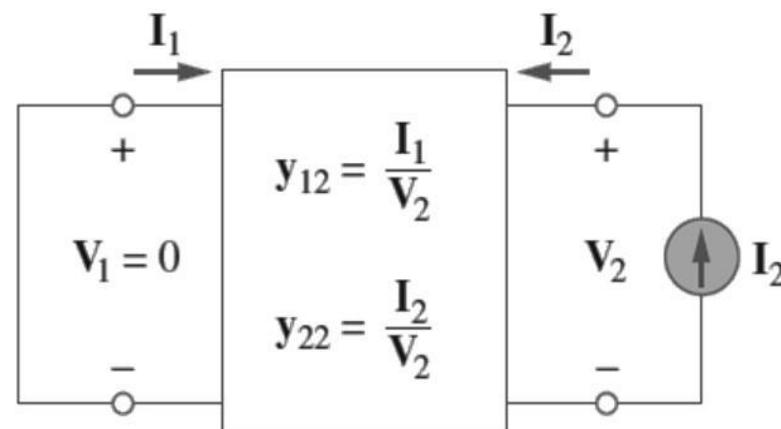
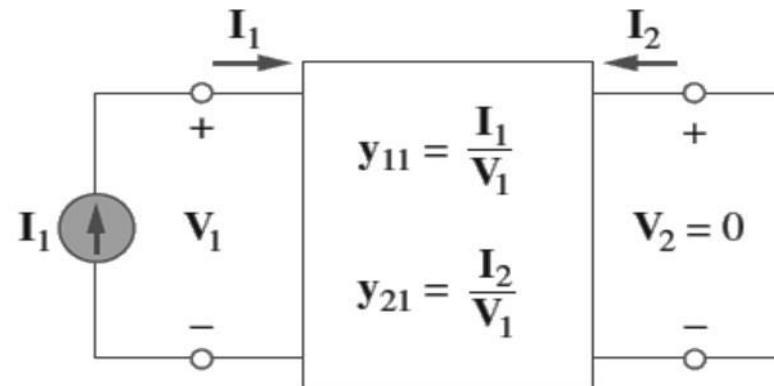
- The values of the parameters can be evaluated by setting $\mathbf{V}_1 = \mathbf{0}$ (input port short-circuited) or (output port short-circuited). $\mathbf{V}_2 = \mathbf{0}$
- Since the y parameters are obtained by short-circuiting the input or output port, they are also called the short-circuit admittance parameters.
- The individual parameters are evaluated as follows:
 - If $\mathbf{V}_2 = 0$, then
$$\mathbf{y}_{11} = \frac{\mathbf{I}_1}{\mathbf{V}_1}, \mathbf{y}_{21} = \frac{\mathbf{I}_2}{\mathbf{V}_1}$$
 - If $\mathbf{V}_1 = 0$, then
$$\mathbf{y}_{12} = \frac{\mathbf{I}_1}{\mathbf{V}_2}, \mathbf{y}_{22} = \frac{\mathbf{I}_2}{\mathbf{V}_2}$$

Admittance Parameters (Cont..)

- Specifically,
 - y_{11} = Short-circuit input admittance
 - y_{12} = Short-circuit transfer admittance from port 1 to port 2
 - y_{21} = Short-circuit transfer admittance from port 2 to port 1
 - y_{22} = Short-circuit output admittance
 - The values of y_{11} and y_{21} can be obtained by connecting a current I_1 to port 1 with port 2 short-circuited.
 - V_1, I_1 , and I_2 are then obtained which can be used to evaluate $y_{11} = \frac{I_1}{V_1}$ and $y_{21} = \frac{I_2}{V_1}$.
 - Similarly, the values of y_{12} and y_{22} can be obtained by connecting a current I_2 to port 2 with port 1 short-circuited.
 - V_2, I_2 , and I_1 are then obtained which can be used to evaluate $y_{12} = \frac{I_1}{V_2}$ and $y_{22} = \frac{I_2}{V_2}$.

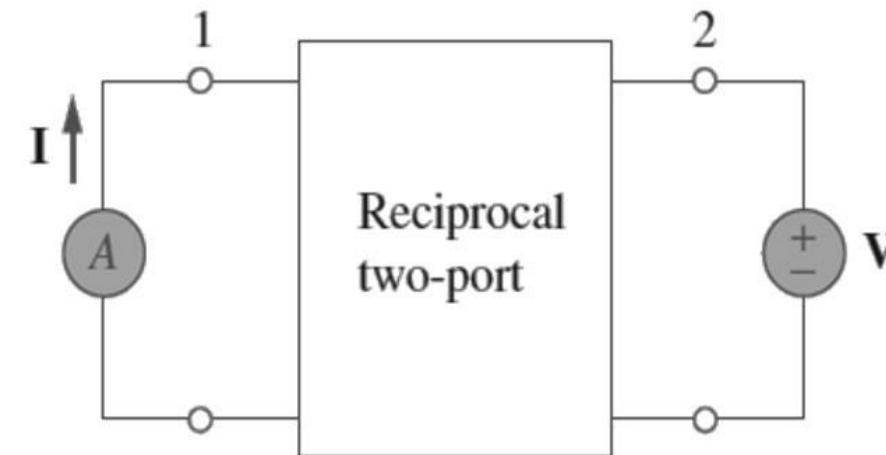
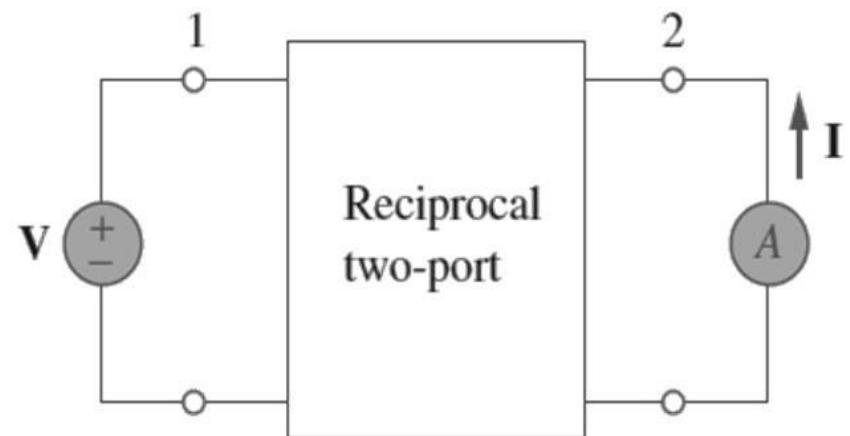
Admittance Parameters (Cont..)

- The above procedure can be easily understood using the following Figures.



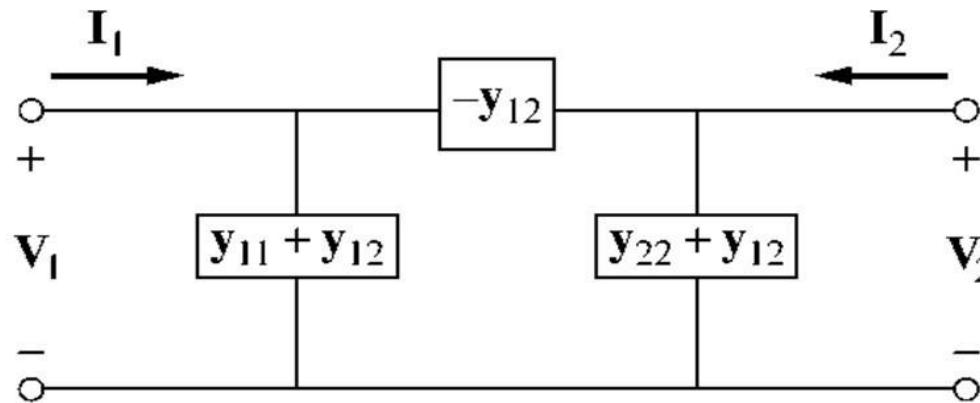
Admittance Parameters (Cont..)

- When the two-port network is linear and has no dependent sources, the transfer admittances are equal ($y_{12} = y_{21}$) , and the two-port is said to be reciprocal.
- This can be proven the same way as in case of the **z**-parameters.
- As shown in the figure below, a two-port is reciprocal if interchanging an ideal voltage source at one port with an ideal ammeter at the other port gives the same ammeter reading.

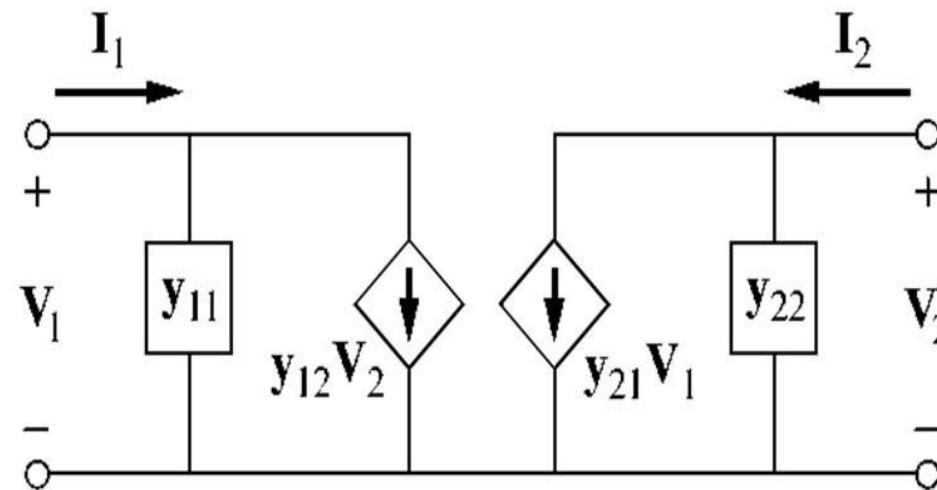


Admittance Parameters (Cont..)

- In this case, the reciprocal network can be replaced by the π -equivalent circuit as shown in the below figure.

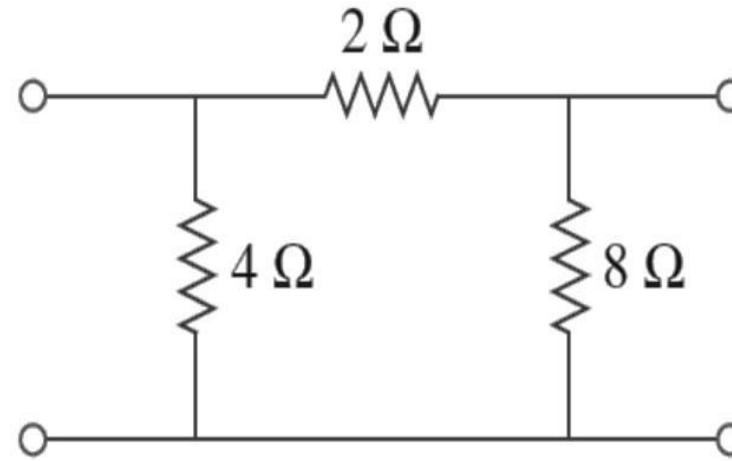


- If the network is not reciprocal, a more general equivalent network as shown below can be used.



Admittance Parameters (Cont..)

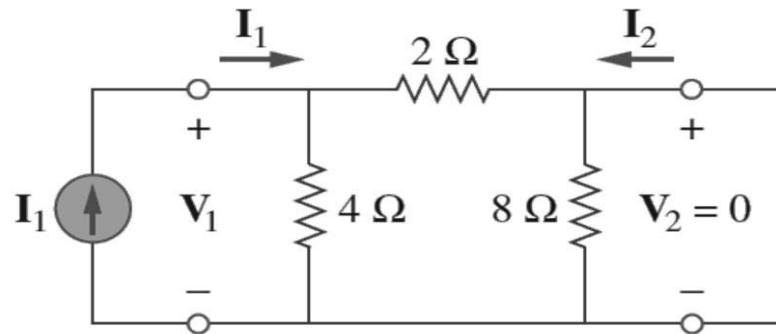
Example: Determine the y-parameters for the below circuit?



Solution: The parameters are determined using the equations discussed earlier in the lecture.

Admittance Parameters (Cont..)

- To determine y_{11} and y_{21} , we connect a current source I_1 to the input port and short the output port as in the following figure.
- Since the 8 ohm resistor is shorted, 2 and 4 ohm resistors are in parallel.



$$V_1 = I_1(4||2) = \frac{4}{3}I_1$$

$$y_{11} = \frac{I_1}{V_1} = \frac{I_1}{\frac{4}{3}I_1} = 0.75 \text{ S}$$

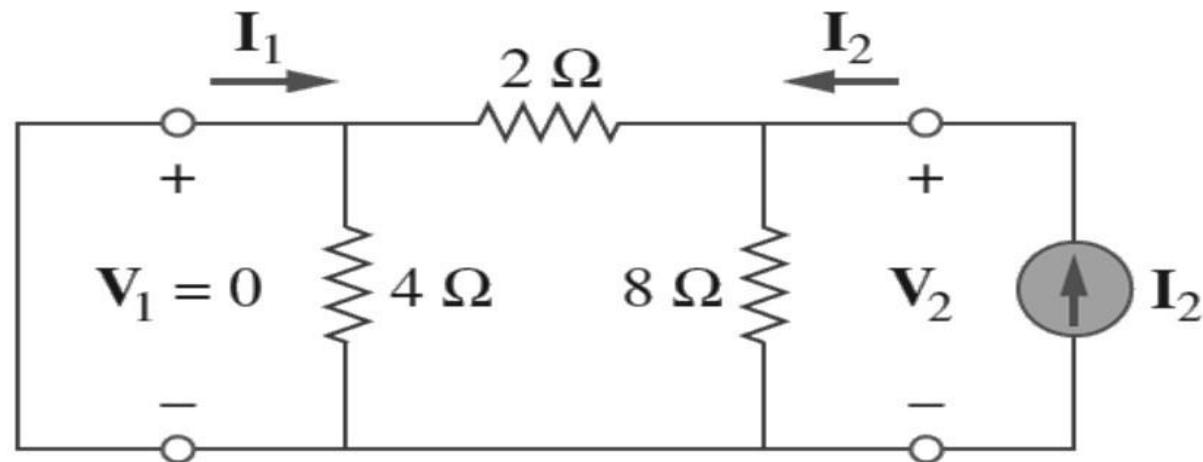
Admittance Parameters (Cont..)

- By current division,

$$-\mathbf{I}_2 = \frac{4}{4+2} \mathbf{I}_1 = \frac{2}{3} \mathbf{I}_1$$

$$\mathbf{y}_{21} = \frac{\mathbf{I}_2}{\mathbf{V}_1} = \frac{-\frac{2}{3}\mathbf{I}_1}{\frac{4}{3}\mathbf{I}_1} = -0.5 \text{ S}$$

- To determine \mathbf{y}_{12} and \mathbf{y}_{22} , we connect a current source \mathbf{I}_2 to the output port and short circuit the input port as in the following figure.



Admittance Parameters (Cont..)

- The 4 ohm resistor is shorted so that the 2 and 8 ohm resistors are in parallel.

$$V_2 = I_2(8\parallel 2) = \frac{8}{5}I_2$$

$$y_{22} = \frac{I_2}{V_2} = \frac{I_2}{\frac{8}{5}I_2} = 0.625 \text{ S}$$

- By current division,

$$-I_1 = \frac{8}{8+2}I_2 = \frac{4}{5}I_2$$

$$y_{12} = \frac{I_1}{V_2} = \frac{-\frac{4}{5}I_2}{\frac{8}{5}I_2} = -0.5 \text{ S}$$

Admittance Parameters (Cont..)

- This can alternatively be expressed in matrix form as,

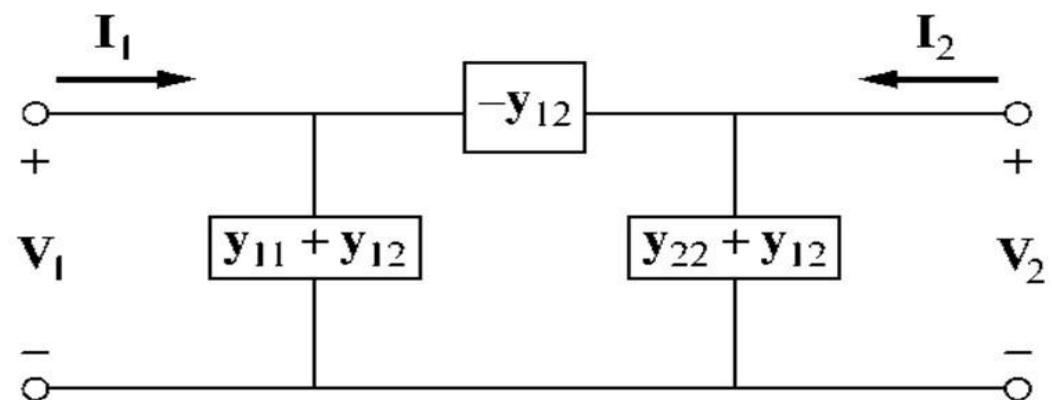
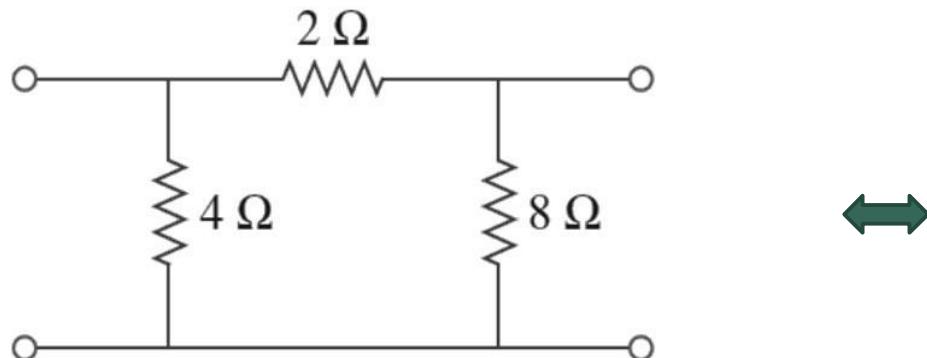
$$[y] = \begin{bmatrix} 0.75 \text{ S} & -0.5 \text{ S} \\ -0.5 \text{ S} & 0.625 \text{ S} \end{bmatrix}$$

- Alternatively, since there is no dependent source in the circuit, and $\mathbf{y}_{12} = \mathbf{y}_{21}$, we can use the following π equivalent circuit to find parameters. Comparing the circuit in the question to the π equivalent circuit,

$$\mathbf{y}_{12} = -0.5 \text{ S} = \mathbf{y}_{21}$$

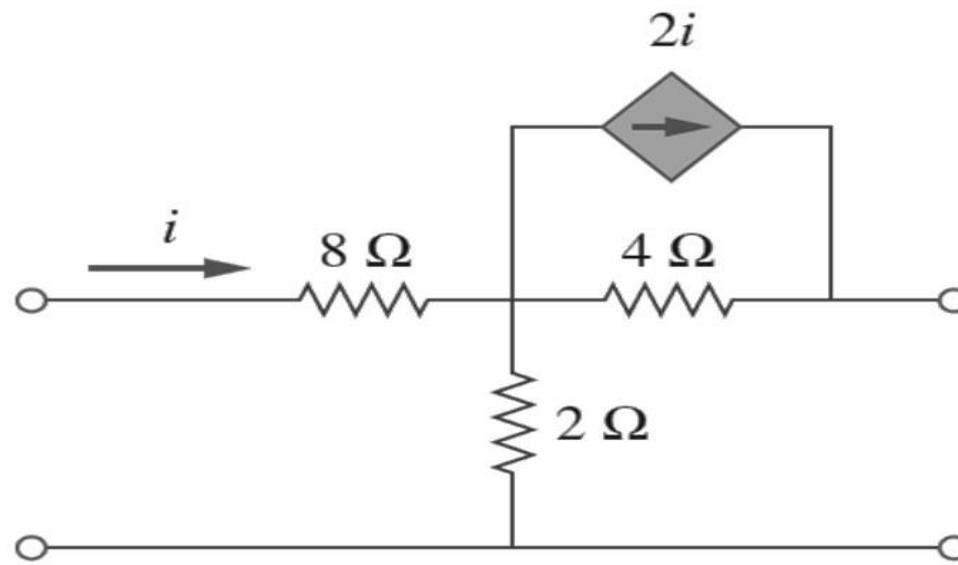
$$\mathbf{y}_{11} + \mathbf{y}_{12} = 0.25 \Rightarrow \mathbf{y}_{11} = 0.25 - \mathbf{y}_{12} = 0.75 \text{ S}$$

$$\mathbf{y}_{22} + \mathbf{y}_{12} = 0.125 \Rightarrow \mathbf{y}_{22} = 0.125 - \mathbf{y}_{12} = 0.625 \text{ S}$$



Admittance Parameters (Cont..)

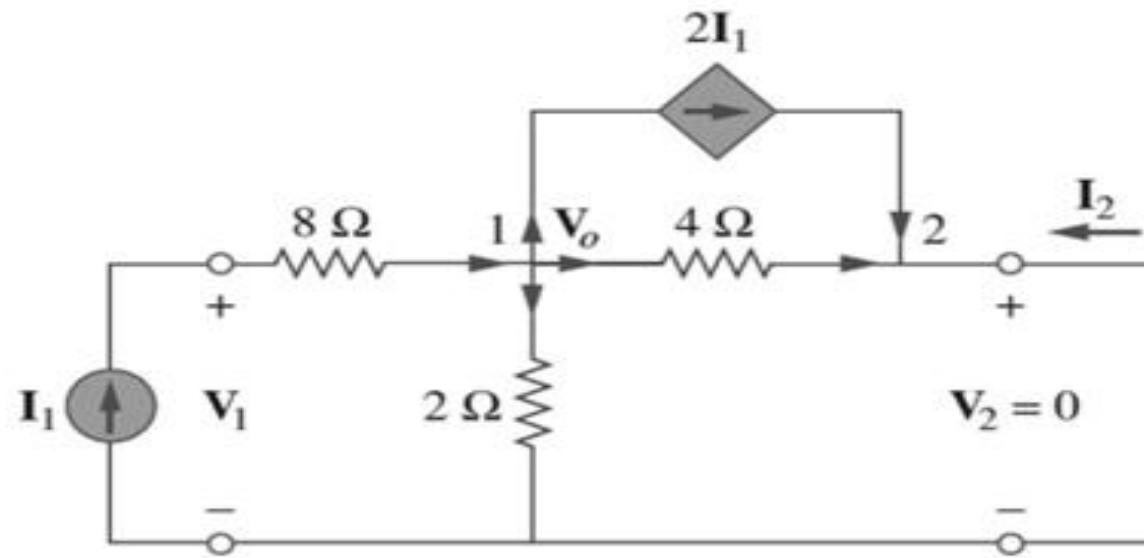
Example: Determine y-parameters for the following circuit?



Solution: The above circuit can be solved using the same procedure discussed in the previous example.

Admittance Parameters (Cont..)

- To determine y_{11} and y_{21} , we connect a current source \mathbf{I}_1 to the input port and short the output port as in the following figure.



- At node 1,

$$\frac{\mathbf{V}_1 - \mathbf{V}_0}{8} = 2\mathbf{I}_1 + \frac{\mathbf{V}_0}{2} + \frac{\mathbf{V}_0 - 0}{4}$$

Admittance Parameters (Cont..)

- But $I_1 = (V_1 - V_0)/8$, therefore

$$0 = \frac{V_1 - V_0}{8} + \frac{3V_0}{4}$$

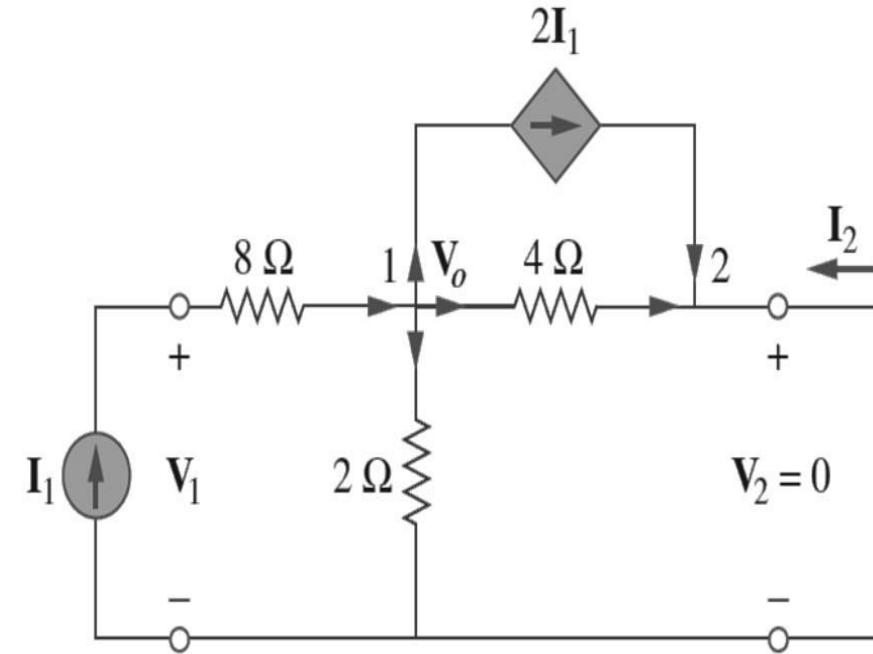
$$0 = V_1 - V_0 + 6V_0 \Rightarrow V_1 = -5V_0$$

- Hence,

$$I_1 = \frac{-5V_0 - V_0}{8} = -0.75V_0$$

and,

$$y_{11} = \frac{I_1}{V_1} = \frac{-0.75V_0}{-5V_0} = 0.15 \text{ S}$$



Admittance Parameters (Cont..)

- At node 2,

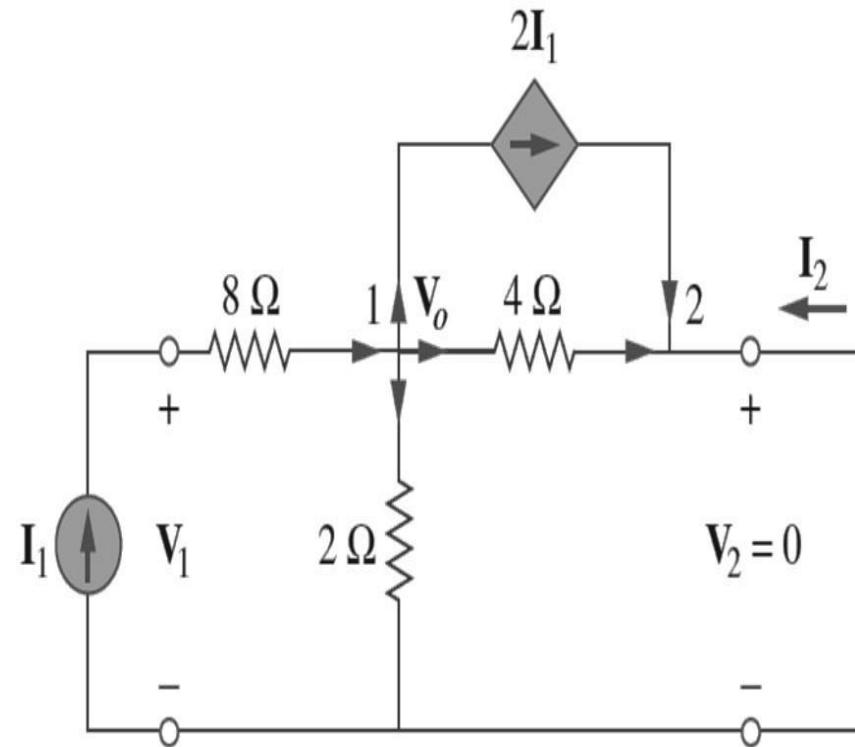
$$0 = \frac{V_0 - 0}{4} + 2I_1 + I_2$$

or

$$-I_2 = 0.25V_0 - 1.5V_0 = -1.25V_0$$

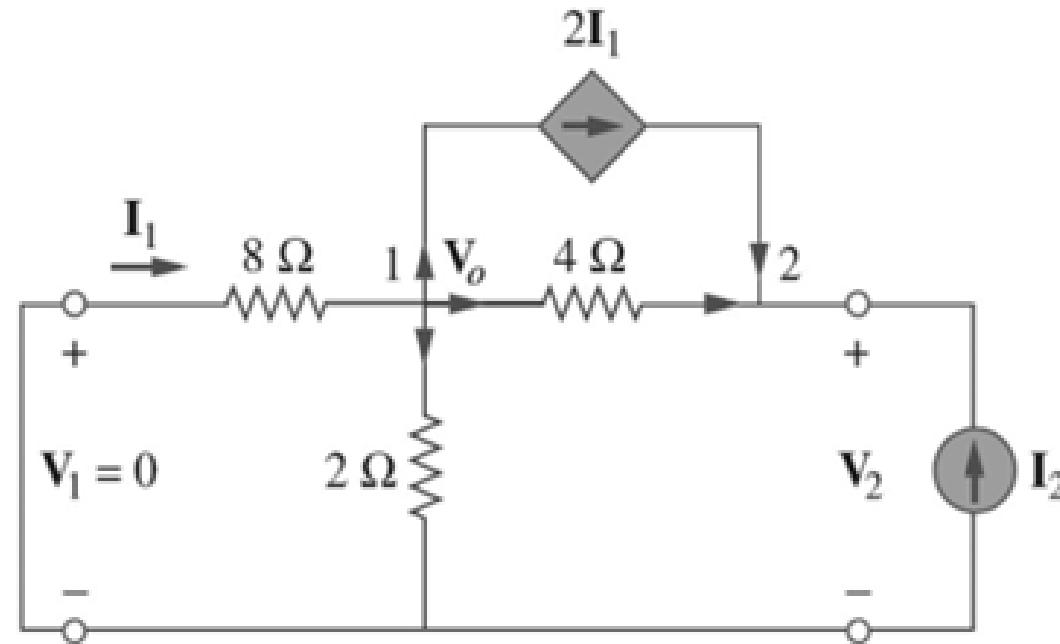
- Hence,

$$y_{21} = \frac{I_2}{V_1} = \frac{1.25V_0}{-5V_0} = -0.25 \text{ S}$$



Admittance Parameters (Cont..)

- To determine y_{12} and y_{22} , we connect a current source I_2 to the output port and short the input port as in the following figure.



- At node 1,

$$\frac{0 - V_o}{8} = 2I_1 + \frac{V_o}{2} + \frac{V_o - V_2}{4}$$

Admittance Parameters (Cont..)

- But $\mathbf{I}_1 = (0 - \mathbf{V}_0)/8$, therefore

$$0 = \frac{0 - \mathbf{V}_0}{8} + \frac{\mathbf{V}_0}{2} + \frac{\mathbf{V}_0 - \mathbf{V}_2}{4}$$
$$0 = -\mathbf{V}_0 + 4\mathbf{V}_0 + 2\mathbf{V}_0 - 2\mathbf{V}_2 \Rightarrow \mathbf{V}_2 = 2.5\mathbf{V}_0$$

- Hence,

$$\mathbf{y}_{12} = \frac{\mathbf{I}_1}{\mathbf{V}_2} = \frac{-\mathbf{V}_0/8}{2.5\mathbf{V}_0} = -0.05 \text{ S}$$

Admittance Parameters (Cont..)

- At node 2,

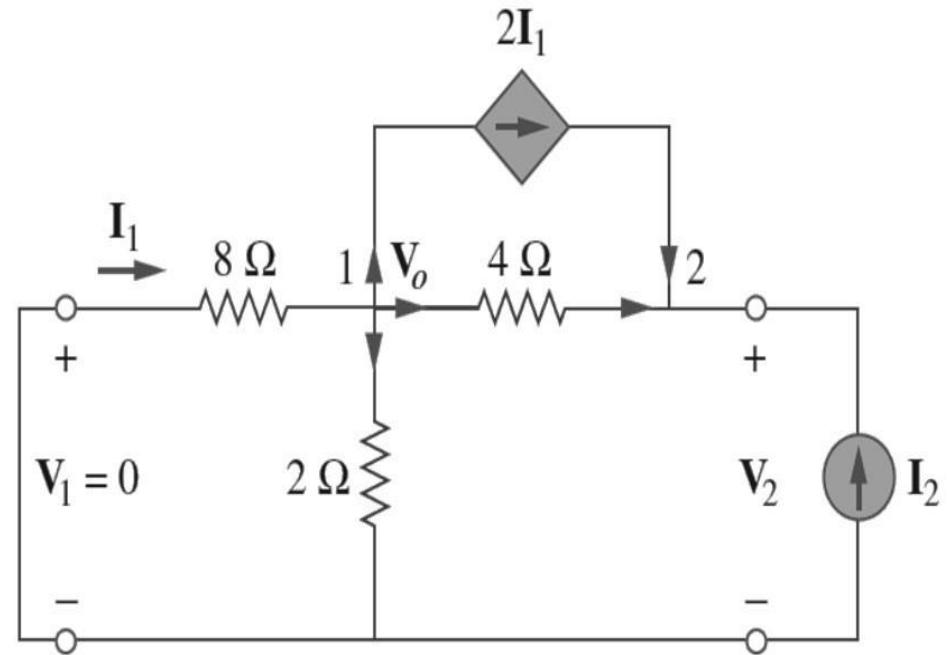
$$0 = \frac{V_0 - V_2}{4} + 2I_1 + I_2$$

or

$$\begin{aligned}-I_2 &= 0.25V_0 - \frac{1}{4}(2.5V_0) - \frac{2V_0}{8} \\ &= -0.625V_0\end{aligned}$$

- Hence,

$$y_{22} = \frac{I_2}{V_2} = \frac{0.625V_0}{2.5V_0} = 0.25 \text{ S}$$



- Here, $y_{12} \neq y_{21}$, hence the network is not reciprocal.

