

- For *inversion channel* to exist at the *D end*,
 V_{GD} must be $> V_{TN}$
 - V_{DS} must be $< V_{GT}$
- When $V_{DS} = V_{GT}$, the *channel* is said to be *pinched-off* at the *D end*, and I_D does not increase any more
- This value of V_{DS} is known as the *drain-to-source saturation voltage* $V_{DS,sat}$
 - $V_{DS,sat} = V_{GT}$

- For $V_{DS} > V_{DS,sat}$, the ***mode of operation*** is known as ***saturation***
- ***Drain current in saturation:***

$$I_D = \frac{k_N}{2} V_{GT}^2$$

- ***Obtained from the non-saturation I_D expression by substituting $V_{DS} = V_{GT}$***
- ***Note that I_D is independent of V_{DS}***
- ***Above equations are valid for $V_{GT} > 3V_T$***
 $(\sim 80 \text{ mV at room temperature})$

The Complete LEVEL 0 Model

$$I_D = k_N \left(V_{GT} V_{DS} - V_{DS}^2 / 2 \right)$$

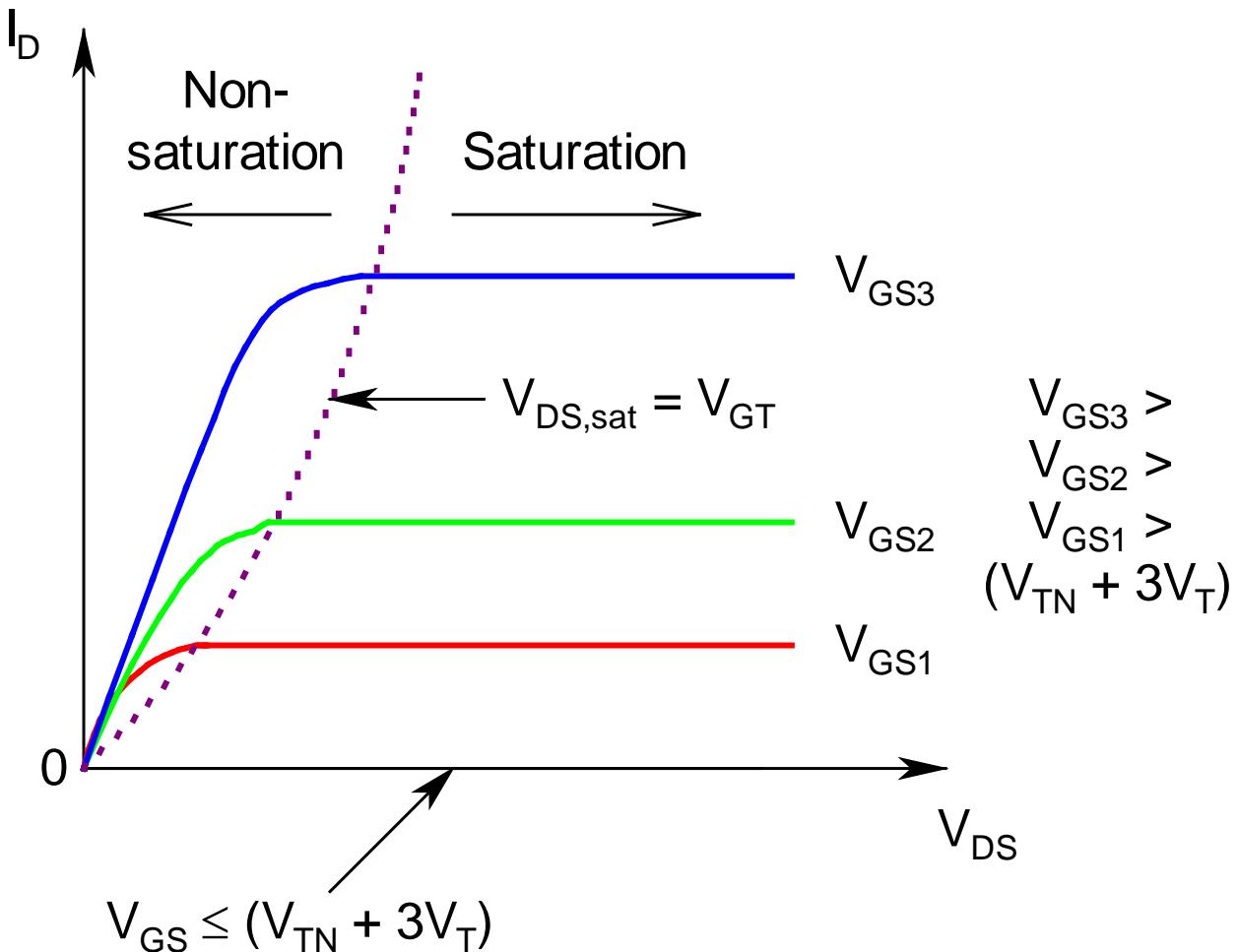
(linear region - $V_{GT} > 3V_T, V_{DS} < V_{GT}$)

$$= \left(k_N / 2 \right) V_{GT}^2$$

(saturation region - $V_{GT} > 3V_T, V_{DS} \geq V_{GT}$)

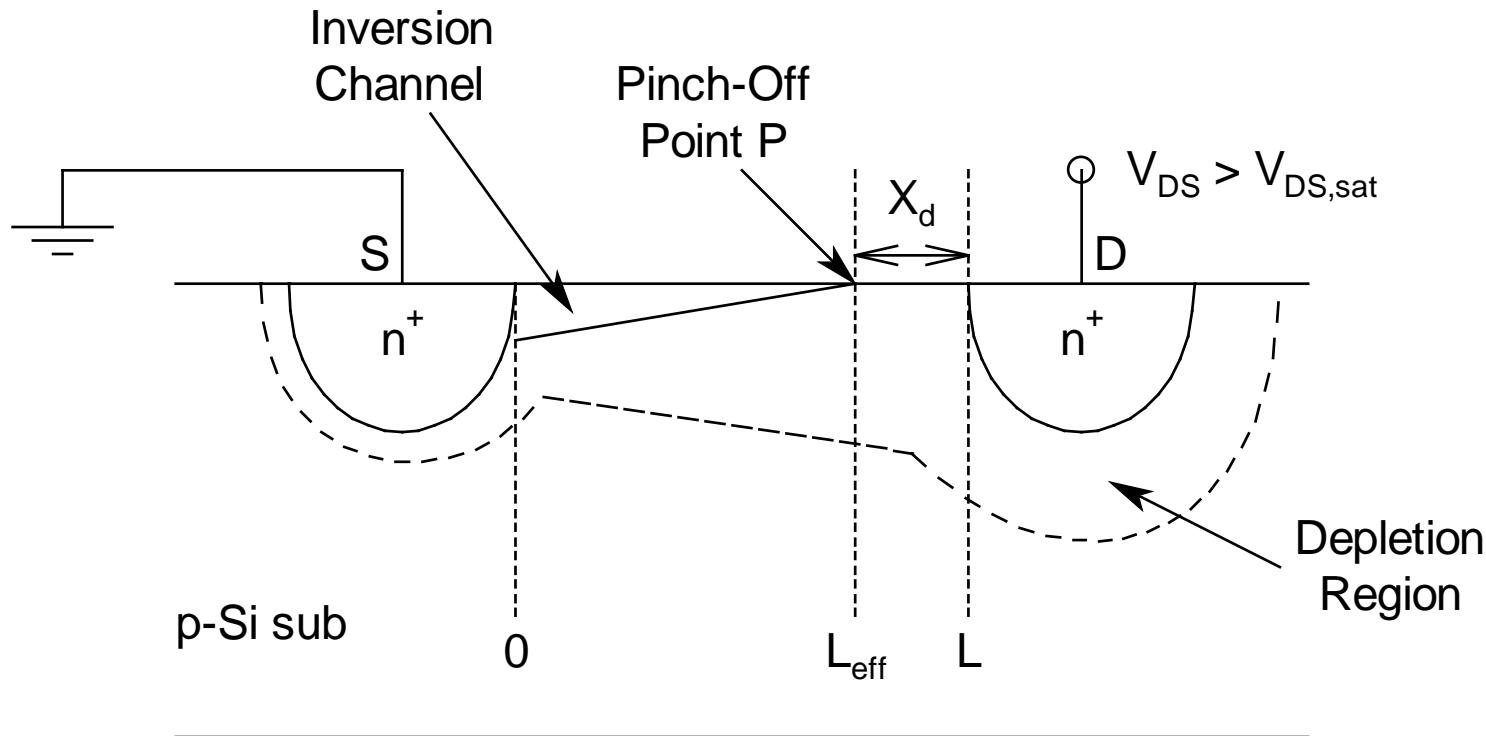
$$= 0$$

(cutoff region - $V_{GT} \leq 3V_T, \text{ any } V_{DS}$)



I_D - V_{DS} Characteristics

Channel-Length Modulation (CLM)



$X_d \rightarrow$ length of the pinched-off region

- For $V_{DS} = V_{DS,sat}$, ***pinch-off point P at D end***
- For $V_{DS} > V_{DS,sat}$, ***P moves towards source***
- ***Effective channel length reduces*** from L to $L_{eff} = L - X_d$
 - $X_d =$ ***pinch-off region/drain region/saturation region length***
- ***Excess voltage*** ($V_{DS} - V_{DS,sat}$) ***drops across*** ***X_d***

- *Reduction of effective channel length causes an increase in current*
 - *Channel length modulation*
- With $V_{DS} \uparrow$, $X_d \uparrow$, $L_{eff} \downarrow$, and $I_D \uparrow$
 - *No real current saturation*
- Thus, *saturated drain current*:

$$\begin{aligned}
 I_{D,sat} &= \left(k'_N / 2 \right) \left(W / L_{eff} \right) V_{GT}^2 \\
 &= \left(k_N / 2 \right) V_{GT}^2 \left(1 + \lambda V_{DS} \right)
 \end{aligned}$$

- $\lambda = \text{Channel length modulation parameter}$

$$= \frac{1}{L} \frac{dX_d}{dV_{DS}}$$

- *Function of L and N_A*
- *Higher L and N_A => Lower λ*
- *Typical values of λ* may range from *close to 0* to *as high as 0.1-0.3 V⁻¹*
- *Very similar to V_A inverse for BJTs*

- This gives ***LEVEL 1 model*** (also known as ***Shichman-Hodges model***) for MOSFETs:

$$I_D = k_N \left[V_{GT} V_{DS} - V_{DS}^2 / 2 \right] (1 + \lambda V_{DS})$$

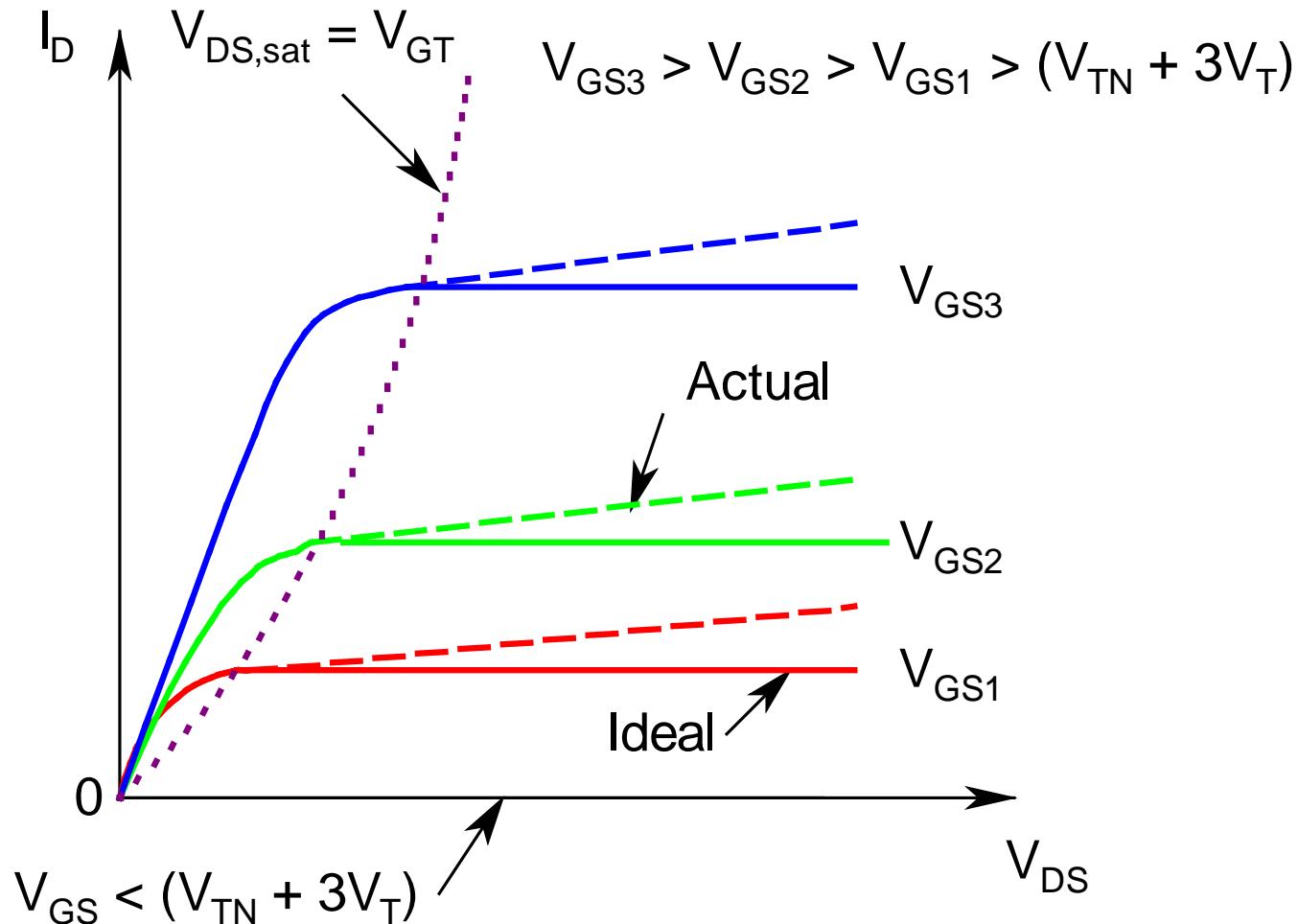
(linear region - $V_{GT} > 3V_T$, $V_{DS} < V_{GT}$)

$$= (k_N / 2) V_{GT}^2 (1 + \lambda V_{DS})$$

(saturation region - $V_{GT} > 3V_T$, $V_{DS} \geq V_{GT}$)

$$= 0$$

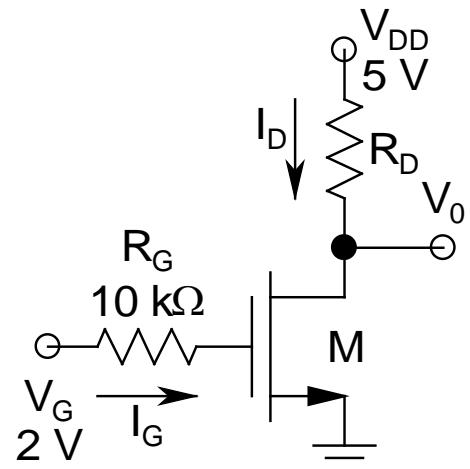
(cutoff region - $V_{GT} \leq 3V_T$, any V_{DS})



I_D - V_{DS} Characteristics in presence of CLM

DC Bias Point Calculation

- *To find R_D for BB*
 - $V_{TN0} = 1 \text{ V}$, $k'_N = 40 \mu\text{A/V}^2$,
 $W/L = 10$
- *Body terminal not shown*
 - *Implies that it is connected to the most negative potential available in the circuit (ground in this case)*
 $\Rightarrow V_{SB} = 0 \Rightarrow V_{TN} = V_{TN0}$
- $I_G = 0 \Rightarrow V_{GS} = V_G = 2 \text{ V}$



- $V_{GT} = V_{GS} - V_{TN} = 1 \text{ V}$
- *Assuming saturation mode of operation and neglecting CLM:*

$$I_D = (k_N/2)V_{GT}^2 = 200 \mu\text{A}$$

- *For BB, $V_{DS} = V_{DD}/2 = 2.5 \text{ V}$ (**2-element output branch**):*

$$R_D = (V_{DD} - V_{DS})/I_D = 12.5 \text{ k}\Omega$$

- $V_{DS} > V_{GT} \Rightarrow$ *Assumption of saturation mode of operation validated*

- $P_D = V_{DS} \times I_D = 0.5 \text{ mW}$