

# Project 2

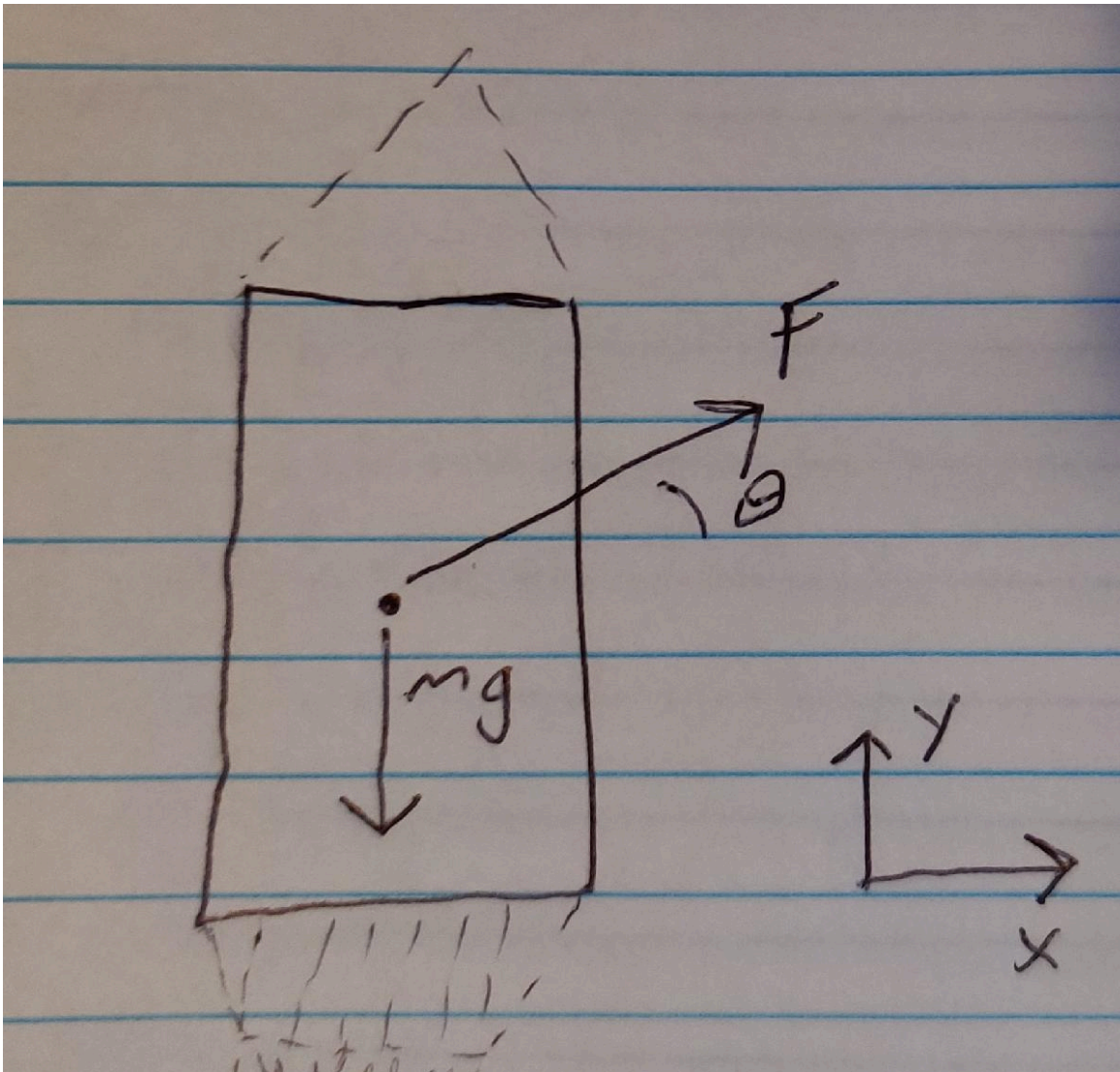
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## Summary

This report will go over Project 2 from MEEM 4730. This project aims at developing a model of a simple rocket in Simulink using base Simulink structures, and a model using Simscape structures, verifying them, and then comparing the results for more complicated situations. The following steps were followed:

1. Develop differential equation model
2. Implement Simulink model of differential equations
3. Implement Simscape model
4. Find closed form solution of simple situation at burn out for verification
5. Simulate more complicated situation without closed-form solution, compare two models

## Derivation



The rocket is assumed to be a point mass, and air resistance is assumed to be negligible.

From the free-body diagram above, the following force expressions can be developed:

$$m a_x = F(t) \cos(\theta(t))$$

$$a_x = \frac{F(t)}{m} \cos(\theta(t))$$

$$m a_y = F(t) \sin(\theta(t)) - m g$$

$$a_y = \frac{F(t)}{m} \sin(\theta(t)) - g$$

Afterwards, the states for the model can be set:

$$x_1 = x$$

$$x_2 = y$$

$$x_3 = \dot{x}$$

$$x_4 = \dot{y}$$

Then the derivatives can be inserted from the force expressions to get the state-variables representation.

$$\dot{x}_1 = x_3$$

$$\dot{x}_2 = x_4$$

$$\dot{x}_3 = \frac{F}{m} \cos(\theta(t))$$

$$\dot{x}_4 = \frac{F}{m} \sin(\theta(t)) - g$$

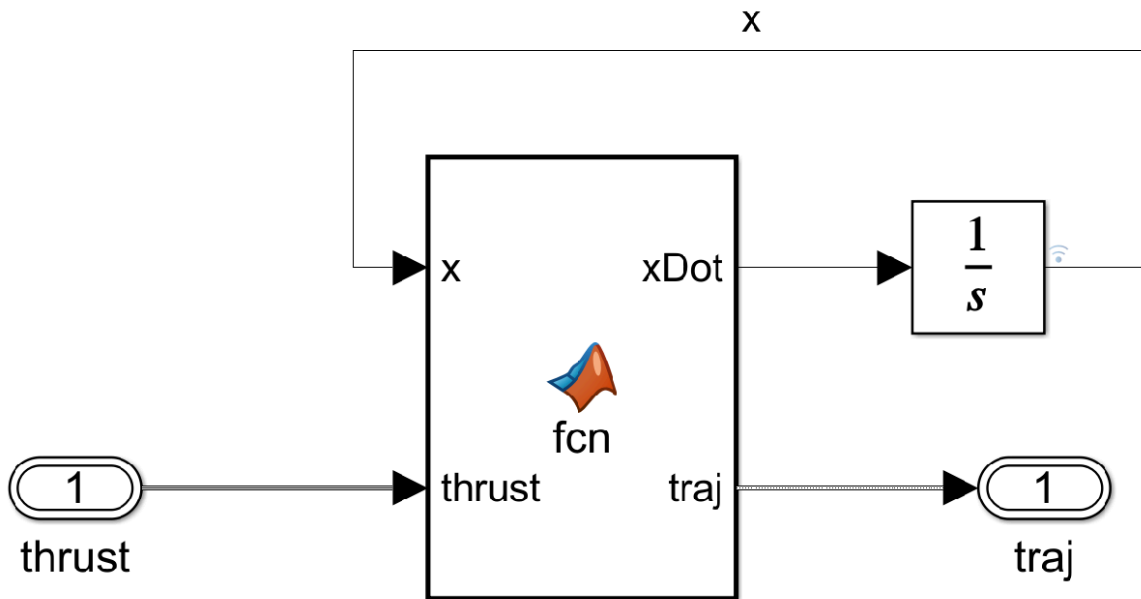
If represented in a more traditional matrix-like form:

$$\dot{\vec{x}} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \vec{x} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{\cos(\theta(t))}{m} & 0 \\ \frac{\sin(\theta(t))}{m} & -1 \end{bmatrix} \begin{bmatrix} F \\ g \end{bmatrix}$$

## Simulink Models

### Base Simulink

This model directly implements the above derivation into a Simulink construct. This was done by creating a Matlab function in the model that took in the states of the mode, calculated the derivatives from the states using the above differential equations, then integrated the output.

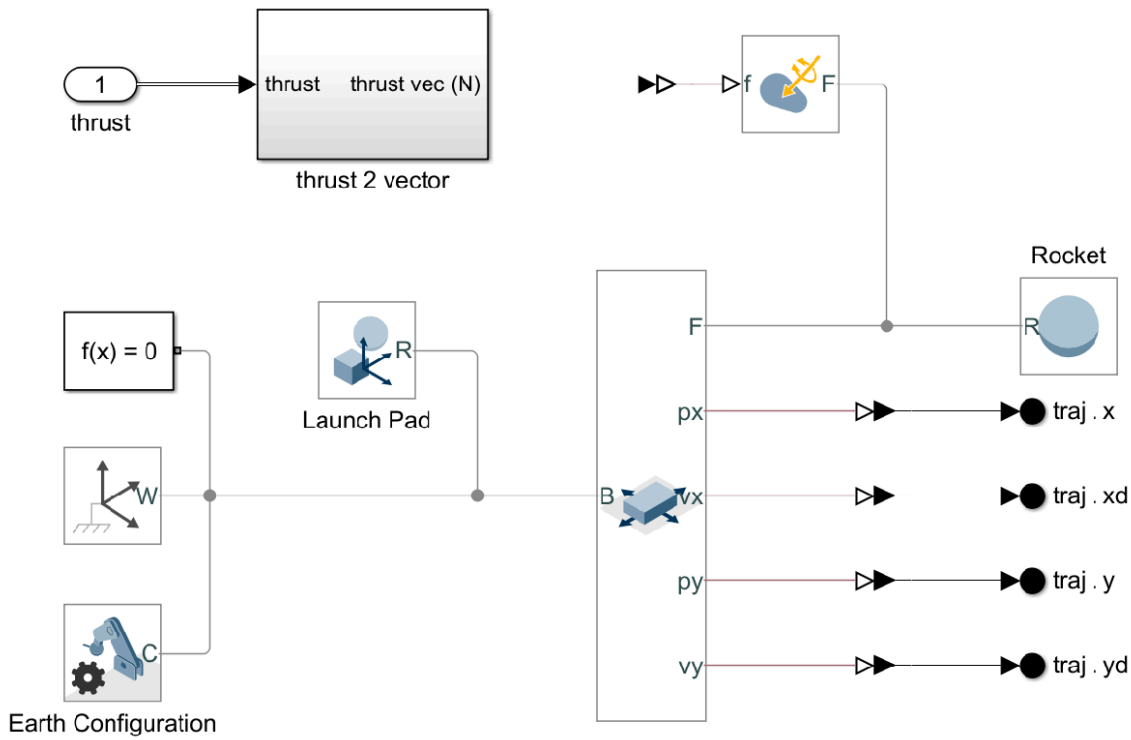


## Simscape

This model indirectly implements the derived model. It more of a graphical way of thinking, rather than a mathematical way. Reference frames are defined, then constraints and joints are placed between them. In this case there are two frames:

1. The Earth
2. The rocket

The frames are joined with a rectangular joint, which has two prismatic portions to it that are orthogonal to each other. This joint does not have rotation as the rocket is assumed a point mass. A force vector from the thrust is applied to the rocket, and gravity is a part of the simulation.



## Closed-form

For the closed form solution, the following parameters were used:

- Thrust = 15000N
- Thrust Angle = 56 Degrees
- Mass = 1000 kg
- Initial conditions =  $\vec{0}$
- Burn time = 5 seconds
- Gravity = 10 m/s/s

From this conditions, a closed-form solution can be developed. All that is done is the above equations are integrated from zero to five seconds.

$$\vec{x} = \int_0^5 \dot{\vec{x}}$$

$$\dot{y}(5) = \left( \frac{15000}{1000} \sin(56) - 10 \right) t = 12.17781 \frac{m}{s}$$

$$y(5) = \frac{1}{2} \left( \frac{15000}{1000} \sin(56) - 10 \right) t^2 = 30.44454 m$$

$$\dot{x}(5) = \left( \frac{15000}{1000} \cos(56) \right) t = 41.93946 \frac{m}{s}$$

$$x(5) = \frac{1}{2} \left( \frac{15000}{1000} \cos(56) \right) t^2 = 104.84866 \text{ m}$$

## Verification

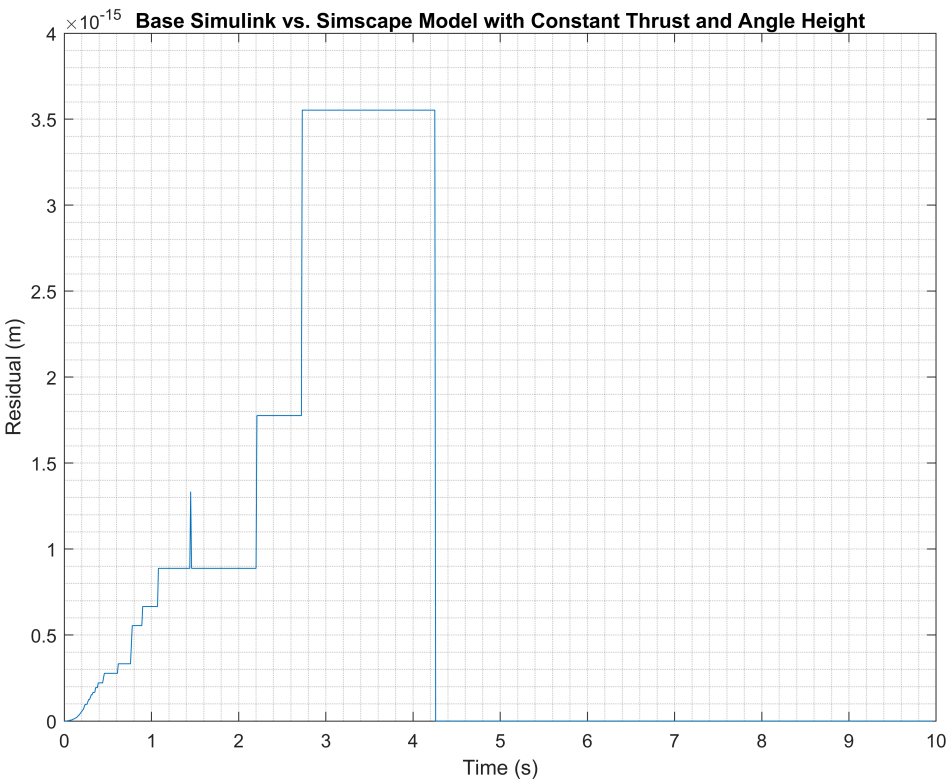
After the closed form solutions were found above, they were compared with the output from the base Simulink model. Another form of verification used was ensuring that after burnout of the rocket energy was conserved. The closed form solution was also used to find an acceptable integration technique. Finally, the models were verified via energy conservation and against each other with a time-varying thrust scenario.

## Closed-form Comparison

\*\*\* BURNOUT STATE COMPARISON \*\*\*

State	Unit	Closed Form	Simulated	Error
-----				
x	m	+104.85	+104.85	1.279e-13
y	m	+30.44	+30.44	5.684e-14
xd	m/s	+41.94	+41.94	2.416e-13
yd	m/s	+12.18	+12.18	1.208e-13

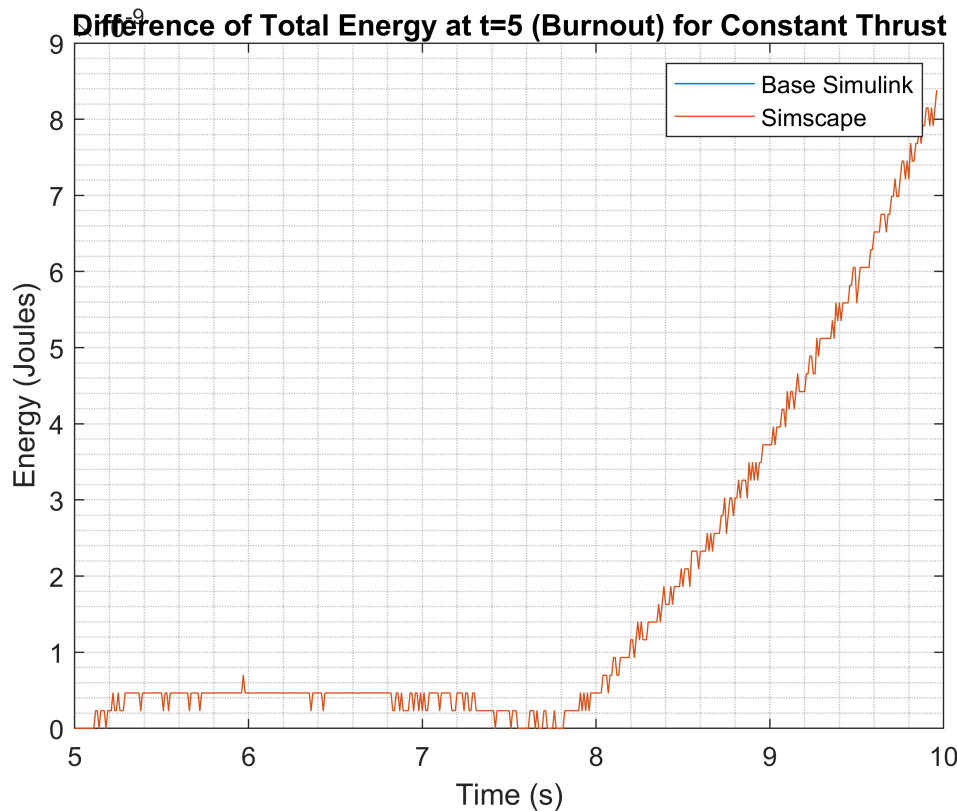
As can be seen above, the error between the closed form solutions and the model is very low. This is between the closed-form and the base Simulink model. Below shows the difference between the base Simulink and the Simscape models' y coordinate with time.



As can be seen, the error between the two models is extremely small, much smaler than the error of the base Simulink model, meaning that both models have less than  $\times 10^{-10}$  meters of error to the closed-form solution.

## Energy Conservation

Below shows the energy vs time for both models post-burnout.



As can be seen above, after the burnout of the rocket the energy change by a maximum of approximately  $9 \times 10^{-9}$  Joules. This is minimal, and is within a reasonable amount of error for this simulation. The cumulative RSS error of the energy with the energy at burnout can be seen below for both models:

```
base_simulink_cumulative_energy_error_constant = 6.3909e-08
```

```
simscape_cumulative_energy_error_constant = 6.3909e-08
```

## Integration Tuning

After verification, the Simulink integrator used was adjusted to be more accurate for this dynamic system. In a lecture of MEEM 4730 it was mentioned that for this dynamic system, third-order Runge-Kutta integrator will most likely work better than the typically used ode4 Runge-Kutta integration method. After inspection, this was found to be true. The maximum error in the states with the closed form solutions is shown below for each method. All timesteps are 0.01 seconds. ODE-14x has Newton iterations set to 4 (arbitrarily).

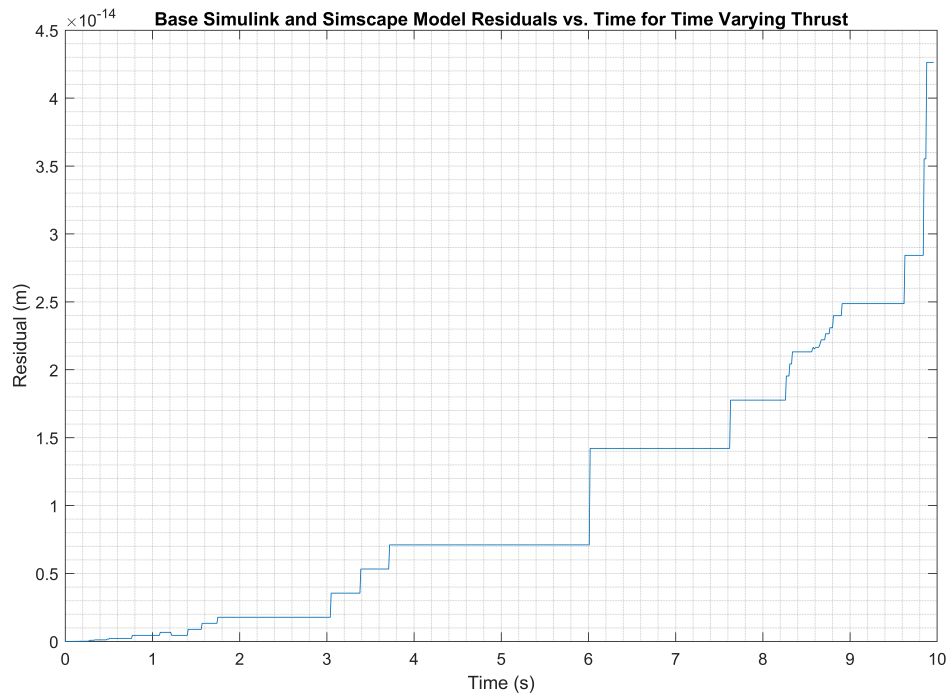
- Backward Euler integration:  $2.089 \times 10^{-1}$
- ODE-1 integration:  $2.097 \times 10^{-1}$
- ODE-2 integration:  $6.218 \times 10^{-2}$
- ODE-3 integration:  $2.416 \times 10^{-13}$
- ODE-4 integration:  $2.073 \times 10^{-2}$

- ODE-5 integration:  $1.628 \times 10^{-2}$
- ODE-8 integration:  $1.479 \times 10^{-3}$
- ODE-14x integration:  $3.171 \times 10^{-12}$

The fact that ODE3 is significantly better than any of the others is very interesting. It is even better than the Mathworks recommended ode14x, which is recommended as the "best global fixed-step choice for physical systems." While the comparison above is for the base Simulink model and not the Simscape model, it is still an interesting comparison. Because of these results ODE-3 with a timestep of 0.01 is used.

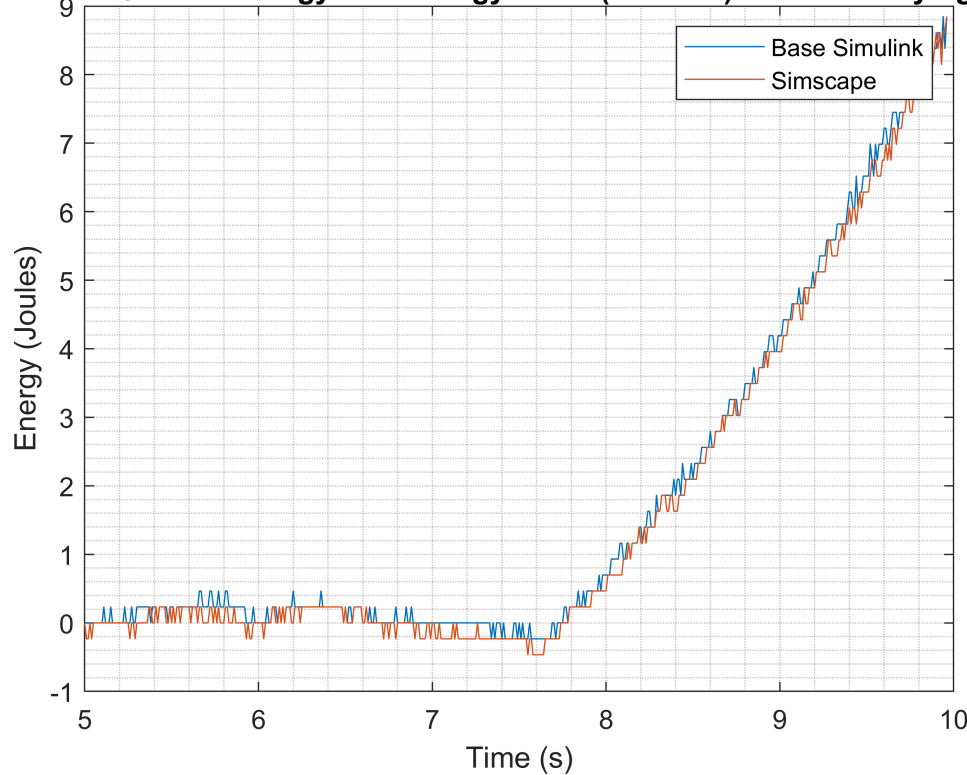
## Time-Varying Thrust Verification

Because of the above verification, the models are known to work with constant thrust scenarios as they were compared with a closed-form solution. Time-varying thrusts are often used on rockets, so verification of those models was done as well. This verification process was to first verify the models against each other, then verify that energy remained conserved with time-varying thrust. Below shows the residuals between the two models.



The above residuals between the two models is promising. The maximum residual between the two models is approximately  $10 \times 10^{-13}$  which is very reasonable for model. Next a look at the energy conservation.

**Difference of Total Energy with Energy at t=5 (Burnout) for Time Varying Thrus**



This shows that the total error between the energy at burnout and the maximum deviation afterwards is near  $9 \times 10^{-9}$ . This is very small, and is an acceptable result. The cumulative RSS errors are shown below.

```
base_simulink_cumulative_energy_error_constant = 6.9830e-08
simscape_cumulative_energy_error_constant = 6.7961e-08
```

Unlike the case with constant thrust there is a slight variation between the two models, but it is minimal. This is most likely due to more moving parts accentuating the internal differences of the Simscape model. But with these figures, it is safe to say that these models are verified for both constant thrust, and time-varying thrust. This does not necessarily mean they are accurate to the real world, but it does mean they are consistent with theoretical results and with each other. The next step to take would be to validate the models with real-world data.