## Chapter 6

# How can marine biologists track sperm whales in the oceans?

Hear they are!

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Whale watching has become a trendy occupation these last years. It is carried on in the waters of some 40 countries, plus Antarctica. Far beyond its touristic aspects, being able to spot the position of whales in real time has several important scientific applications, such as censusing (estimation of animal population), behavior studies and mitigation efforts concerning fatal collisions between marine mammals and ships and exposure of marine mammals to loud sounds of anthropogenic origin (seismic surveys, oil and gas exploitation and drilling, naval and other uses of sonar).

When whales do not appear on the surface of water, one way of detecting their position is to listen to the sounds they emit through several fixed *hydrophones* (i.e., microphones specially designed for underwater use).

Hydrophone signals are then processed with a SOund Navigation And Ranging (*sonar*) technique, which uses sound propagation under water to detect and spot objects. In this Chapter, we thus plunge deep into underwater acoustics, by examining a proof of concept for sperm whale tracking

using *passive acoustics*<sup>1</sup>, and based on the estimation of the cross-correlation between hydrophone signals to spot whales on a 2D map.

## 6.1 Background – Source localization

We start by examining sperm whale sounds (Section 6.1.1), and show how the Teager-Kaiser operator efficiently increases the signal-to-noise ratio of hydrophone signals (Section 6.1.2).

Sperm whale sounds are actually received by hydrophones at slightly different times, due to the various distances between the animal and the hydrophones. Knowing the location of the hydrophones, the *time difference of arrival* (TDOA) between pairs of hydrophones can be obtained, using various techniques (Sections 6.1.3 and 6.1.4), and provided to a *multilateration* algorithm (Section 6.1.5) for determining the position of the animal.

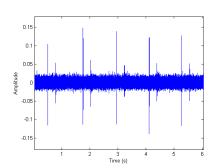
## 6.1.1 Sperm whale sounds

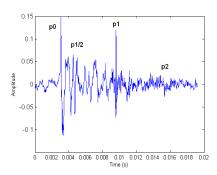
Sperm whales are highly vocal active animals. An adult sperm whale produces some 25000 clicks a day. If we consider that the heart rate of such a large whale is around 15 beats per minute (i.e., 20000 beats a day), sperm whale produces more clicks than heart beats (Madsen 2002). Their repertoire is made up almost entirely of a number of click types with different properties.

Usual (or regular) clicks (Fig. 6.1) are the most commonly heard click type during deep foraging dives, and are therefore used to locate the animals using passive acoustic methods. They are impulsive broadband sounds of multi-pulse structure with inter-click interval (ICI) between 0.5s-1s. Usual clicks are highly directional sounds with source levels up to 235 dB rms re  $1\mu Pa^2$ . It is believed that these properties represent adaptations for long-range echolocation.

Sonars can be *active* or *passive*. Passive sonars only listen to their surrounding, while active sonars emit sounds and detect echoes from their surrounding. Whales and dolphins use echolocation systems similar to active sonars to locate predators and preys; marine biologists listen to the resulting sounds and echoes (hence, in a passive set-up) to detect cetaceans.

 $<sup>^2</sup>$  For underwater sound, 1  $\mu$ Pa is the reference pressure level. Since the measured pressure level from a particular sound source decreases with distance from the source, the convention is to use one meter as a reference distance. Thus, the





**Fig. 6.1** Left: Sequence of usual sperm whale clicks. Each click is followed by an echo, due to surface reflection<sup>3</sup>. Right: zoom on a single click, showing the multipulse structure of the signal. The notation on pulses follows that of (Møhl et al. 2000, Zimmer et al. 2005)

*Creak clicks* (Fig. 6.2) are burst of mono-pulsed clicks with high repetition rate (up to 200 clicks per second). They are highly directional sounds with source level between 180-205 dB rms re 1μPa. They are produced during foraging dives and it is believed that they have a function analogous to the terminal buzzes produced by bats during echolocation <sup>4</sup>.

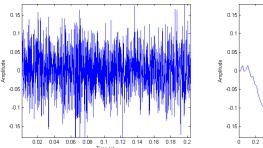
Several other types of sounds are also encountered, such as *coda clicks*, *chirrup clicks*, *slow clicks*, *squeals*, and *trumpets*, most of which have a social communicative role. <sup>5</sup>

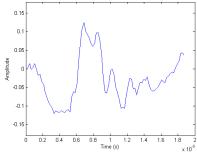
pressure level from a sound source is measured in "dB rms re  $1\mu$ Pa at 1m" (and the "at 1m" is usually omitted).

<sup>&</sup>lt;sup>3</sup> Hydrophones are mounted at roughly 5m off the bottom, so that reflection from the bottom comes with a ∼7ms delay, i.e. inside the direct path click itself. Furthermore, the hydrophones have an upward directed beam pattern.

<sup>&</sup>lt;sup>4</sup> After detecting a potential prey using low rate echolocation calls, bats emit a characteristic series of calls at a high repetition rate (a *terminal buzz*) to localize the prey.

<sup>&</sup>lt;sup>5</sup> For more information on sperm whale sounds, please refer to Madsen 2002, Drouot 2003, Teloni *et al.* 2005.





**Fig. 6.2** Left: Segment of a creak, composed of several clicks (and their echoes) in high amplitude noise. Right: zoom on a single click of the segment, which shows the mono-pulse nature of the sound.

As shown in Fig. 6.1 and Fig. 6.2, hydrophone signals exhibit very low signal-to-noise ratios. In particular they are often contaminated by low-frequency noise, mostly due to human activity. Shipping indeed, which accounts for more of 75% of all human sound in the sea (ICES 2005), produces low-frequency sounds (rumble of engines, propellers). Commercial shipping traffic is growing as does the tonnage (cargo capacity) of ships, adding more noise in the low frequency band.

## 6.1.2 The Teager-Kaiser energy operator

The Teager–Kaiser (TK) energy operator is defined in the continuous domain as:

$$TK[x(t)] = \dot{x}(t)^2 - x(t)\ddot{x}(t)$$
 (6.1)

where  $\dot{x}$  and  $\ddot{x}$  denote the first and second derivative over time, respectively. For a discrete time signal, it is shown in (Kaiser 1990) that the TK energy operator is given by:

$$TK[x(n)] = x^{2}(n) - x(n+1)x(n-1)$$
(6.2)

The TK operator is referred to as *energy operator* because it is related to the concept of energy in the generation of acoustic waves (Kaiser 1990).

This operator can be seen as a special case of *quadratic filters* defined by:

$$y(n) = \sum_{i_1 = -\infty}^{\infty} \sum_{i_2 = -\infty}^{\infty} h(i_1, i_2) x(n - i_1) x(n - i_2)$$
(6.3)

where  $h(i_1,i_2)$  is known as the second order *Volterra kernel* <sup>6</sup>. As a matter of fact, the TK energy operator is obtained from (6.2) when:

$$h(i_1, i_2) = \begin{cases} 1 & i_1 = i_2 = 0\\ -1/2 & (i_1, i_2) = (1, -1) \text{ or } (-1, 1)\\ 0 & \text{otherwise} \end{cases}$$
 (6.4)

The analysis of such non-linear filters is not trivial. Since their output to a sum of inputs is not the sum of their outputs to isolated inputs, the classical notions of impulse and frequency responses no longer have the usual reach. When the input is composed of a sum of sinusoids, for instance, cross-product terms appear in the output. In the case of the TK operator, it is easy to check from (6.2) that the response of this filter to  $\delta(n)$  is  $\delta(n)$ , and that its response to an isolated cosine  $A\cos(n\varphi_0)$  is a constant signal  $A^2\sin^2(\varphi_0)$ . This response, however, cannot be interpreted as a frequency response, and is not the Fourier transform of the impulse response.

In the specific case of noisy impulsive signals, the TK operator has interesting properties. Let us assume that the signal x(n) recorded by a hydrophone is composed of the sum of a low frequency interference signal i(n), of the impulsive click signal s(n) produced by a sperm whale, and of some background wideband noise u(n):

$$x(n) = s(n) + i(n) + u(n)$$
 (6.5)

$$y(n) = \sum_{i_1 = -\infty}^{\infty} h(i_1)x(n - i_1)$$

$$+ \sum_{i_1 = -\infty}^{\infty} \sum_{i_2 = -\infty}^{\infty} h(i_1, i_2)x(n - i_1)x(n - i_2)$$

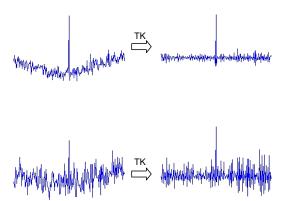
$$+ \dots$$

$$+ \sum_{i_1 = -\infty}^{\infty} \dots \sum_{i_N = -\infty}^{\infty} h(i_1, \dots, i_N)x(n - i_1)\dots x(n - i_N)$$

<sup>&</sup>lt;sup>6</sup> Quadratic filters are themselves a simple case of the more general *polynomial* or *Volterra filters* (Sicuranza 1992):

If the interference frequency is low and the signal-to-noise ratio (SNR) between the impulsive clicks and the background noise is sufficient, it is shown in (Kandia and Stylianou 2005) that the TK operator has the very interesting property of ignoring the interference component while increasing the SNR (Fig. 6.3). Moreover, it does not smear input pulses in time (Fang and Atlas 1995). As a matter of fact, if we neglect the influence of the noise u(n) and identify x(n) to a Dirac pulse  $\delta(n)$  and i(n) in the vicinity of this pulse to a constant value K, it is easy to show from (6.2) that the output y(n) of the TK filter only has three non zero samples:

$$y(n) = \begin{cases} -K & n = -1\\ 1 - 2K & n = 0\\ -K & n = 1 \end{cases}$$
 (6.6)



**Fig. 6.3** Applying the Teager-Kaiser operator to simulated clicks corrupted by low-frequency interference and background noise with various SNR efficiently pre-processes the data for later click detection or TDOA estimation (Kandia and Stylianou 2007).

The application of the TK operator to sperm whale sounds therefore provides a good example of the efficient use of a non-linear filter for making the data more amenable to further TDOA estimation.

## 6.1.3 TDOA estimation based on the generalized cross correlation

Let us assume that signals  $x_1(t)$  and  $x_2(t)$  result from the propagation of signal s(t) through different paths that are identified to a simple attenuation and a delay:

$$x_i(t) = a_i s(t - \tau_i) + b_i(t)$$
 (6.7)

where  $b_i(t)$  (i=1,2) are zero-mean, uncorrelated stationary random processes, which are also non-correlated with s(t).

The *cross* power spectrum density (PSD)  $S_{x_1x_2}(f)$  between  $x_1$  and  $x_2$  is given by:

$$S_{x_{1}x_{2}}(f) = \int_{-\infty}^{\infty} \phi_{x_{1}x_{2}}(t)e^{-j2\pi ft}dt$$

$$= a_{1}a_{2}e^{-j2\pi f\tau_{12}} \int_{-\infty}^{\infty} \phi_{ss}(t)e^{-j2\pi ft}dt$$

$$= a_{1}a_{2}e^{-j2\pi f\tau_{12}}S_{ss}(f)$$
(6.8)

in which  $\phi_{x_1x_2}(t)$  is the cross correlation between  $x_1(t)$  and  $x_2(t)$ ,  $\phi_{ss}(t)$  is the autocorrelation of s(t), and  $S_{ss}(f)$  is therefore the PSD of s(t).

Knapp and Carter (1976) have proposed to estimate the *time difference* of arrival TDOA  $\tau_{12} = \tau_1 - \tau_2$  between  $x_1(t)$  and  $x_2(t)$ , as the position of the maximum of the generalized cross correlation function, defined as:

$$\psi_{x_1 x_2}(\tau) = \int_{-\infty}^{+\infty} \Phi(f) S_{x_1 x_2}(f) e^{j2\pi f \tau} df$$
 (6.9)

in which  $\Phi(f)$  is a weighting function.

In particular, when  $\Phi(f)$  is set to 1,  $\psi_{x_1x_2}(\tau)$  is the inverse Fourier Transform of the cross PSD, i.e., the standard cross-correlation function. For signals verifying (6.8), this leads to have:

$$\psi_{x_1 x_2}(\tau) = a_1 a_2 \phi_{ss}(\tau - \tau_{12}) \tag{6.10}$$

in which  $\phi_{ss}(\tau)$  is the autocorrelation function of s(t). Since the maximum of  $\phi_{ss}(\tau)$  is always found at  $\tau = 0$ ,  $\tau_{I2}$  can be estimated as the position of

the maximum of (6.10). However, if  $b_1(t)$  and  $b_2(t)$  exhibit some cross-correlation, (6.10) becomes:

$$\psi_{x_1x_2}(\tau) = a_1 a_2 \phi_{ss}(\tau - \tau_{12}) + \phi_{bb_2}(\tau) \tag{6.11}$$

whose maximum may not correspond to  $\tau_{12}$ . In particular, if  $b_i(t)$  are sinusoidal components with the same frequency, a sinusoidal term will appear in (6.11), due to a spectral line in  $S_{x_ix_2}(f)$ .

When  $\Phi(f)$  is set to  $1/|S_{x_1x_2}(f)|$ , we obtain the so-called *phase transform*, which computes the generalized cross correlation from the phase of the cross PSD. For signals verifying (6.8), the phase transform still provides a perfect estimate of  $\tau_{12}$ , since:

$$\Phi(f)S_{x_1x_2}(f) = \frac{S_{x_1x_2}(f)}{|S_{x_1x_2}(f)|} = e^{-j2\pi f \tau_{12}}$$
(6.12)

which leads to:

$$\psi_{x_1 x_2}(\tau) = \delta(\tau - \tau_{12})$$
 (6.13)

Now if  $b_i(t)$  are sinusoidal components with the same frequency, their contributions to  $\psi_{x_1x_2}(\tau)$  will be much lower than in (6.11), since the spectral line in  $S_{x_1x_2}(f)$  will be canceled in (6.12). This makes the phase transform an interesting estimator, provided  $S_{x_1x_2}(f)$  can itself be correctly estimated.

In practice,  $S_{x_1x_2}(f)$  is estimated in  $[0, F_s]$  from a finite number of samples of  $x_1(n)$  and  $x_2(n)$ , as (Fig. 6.4):

$$S_{x_1x_2}(k\frac{F_s}{N}) \cong X_1(k)X_2^*(k) \quad (k=0,...,N-1)$$
 (6.14)

where  $X_i(k)$  (i=1,2) is the N-point Discrete Fourier Transform of the sequence  $[x_i(n), x_i(n-1), \cdots, x_i(n-N+1)]$ . This is known to give a biased but consistent estimation of  $S_{x_i,x_j}(f)$ .

TDOA estimation from *real* signals is not so easy. As mentioned above, hydrophone signals are polluted with interference signals and additive noise due to surrounding sources other than the one we want to spot. More annoyingly, several propagation paths may exist to each hydrophone: typically a direct path with lowest attenuation plus many secondary paths,

which create echoes (one of which being due to surface reflection) and reverberations. As a result, a more realistic model for hydrophone signals  $x_1$  and  $x_2$  receiving a click s(t) after propagation is given by:

$$x_i(t) = h_i(t) * s(t) + b_i(t)$$
 (6.15)

where \* denotes convolution,  $h_i(t)$  is the acoustic impulse response of the channel between the whale and the  $i^{th}$  hydrophone (including reverberation), and  $b_i(t)$  is the additive noise received by this hydrophone. Consequently, applying the phase transform to real signals does not always lead to efficient estimates of TDOAs. Several other weighting functions have been proposed for the estimation of the general cross-correlation in (6.9), and proved to provide interesting results in specific cases (Knapp and Carter 1976).

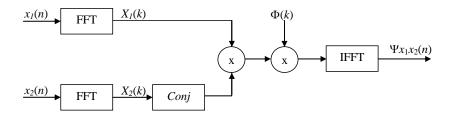


Fig. 6.4 Practical computation of the generalized cross correlation function

## 6.1.4 Adaptive TDOA estimation

A radically different approach was proposed in (Benesty 2000), which leads to a simple and elegant adaptive filtering implementation, in the framework of the Least Means Squares (LMS) algorithm. This approach is based on the estimation of the impulse responses from the source to the receivers.

If we neglect the noise components in (6.15), we have (Fig. 6.5):

$$x_{1}(n) * h_{2}(n) = s(n) * h_{1}(n) * h_{2}(n)$$

$$= s(n) * h_{2}(n) * h_{1}(n)$$

$$= x_{2}(n) * h_{1}(n)$$
(6.16)

which can be written in vector notation as:

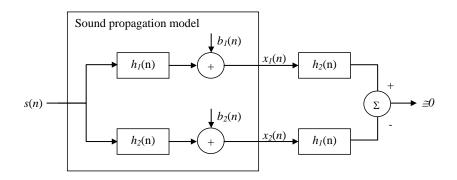
$$\mathbf{x}_{1}^{T}(n)\mathbf{h}_{2} = \mathbf{x}_{2}^{T}(n)\mathbf{h}_{1} \qquad \text{for all } n$$
 (6.17)

where

$$\mathbf{x}_{i}(n) = [x_{i}(n), x_{i}(n-1), \dots, x_{i}(n-M+1)]^{T} \quad (i=1,2)$$
(6.18)

and

$$\mathbf{h}_{i} = [h_{i}(0), h_{i}(1), \dots, h_{i}(M-1)]^{T} \quad (i = 1, 2)$$
(6.19)



**Fig. 6.5** If additive noise is neglected, passing  $x_l(n)$  through  $h_2$  gives the same result as passing  $x_2(n)$  through  $h_1$ .

If we stack  $\mathbf{x}_1(n)$  and  $\mathbf{x}_2(n)$  as:

$$\mathbf{x}(n) = \begin{bmatrix} \mathbf{x}_1(n) \\ \mathbf{x}_2(n) \end{bmatrix} \tag{6.20}$$

then the covariance matrix of  $\mathbf{x}(n)$  is given by:

$$\mathbf{R}_{\mathbf{x}\mathbf{x}} = \begin{bmatrix} \mathbf{R}_{\mathbf{x}_1 \mathbf{x}_1} & \mathbf{R}_{\mathbf{x}_1 \mathbf{x}_2} \\ \mathbf{R}_{\mathbf{x}_2 \mathbf{x}_1} & \mathbf{R}_{\mathbf{x}_2 \mathbf{x}_2} \end{bmatrix}$$
(6.21)

with:

$$\mathbf{R}_{\mathbf{x}_{i},\mathbf{x}_{j}} = E\left[\mathbf{x}_{i}(n)\mathbf{x}_{j}^{T}(n)\right] \quad (i, j = 1, 2)$$
(6.22)

It then follows from (6.17) and (6.21) that:

$$\mathbf{R}\mathbf{u} = 0 \quad \text{with } \mathbf{u} = \begin{bmatrix} \mathbf{h}_2 \\ -\mathbf{h}_1 \end{bmatrix}$$
 (6.23)

This remarkably simple result provides a simple means of estimating the impulse responses  $h_1$  and  $h_2$  from the estimation of  $\mathbf{R}_{xx}$ .

In practice, though, accurate estimation of  $\mathbf{u}$  is not trivial, as the impulse responses may be long, and background noise may falsify (6.23). Benesty (2000) has therefore proposed an adaptive estimation of  $\mathbf{u}$ , based on a Least Means Squares (LMS) principle. The idea is to find an error function e(n) such that the expectation  $\mathrm{E}[e^2(n)]$  is minimized when (6.23) is verified, and such that the gradient of  $\mathrm{E}[e^2(n)]$  with respect to  $\mathbf{u}$  has a simple analytical form. Clearly,  $e(n) = \mathbf{u}^T \mathbf{x}$  meets these requirements, as  $\mathrm{E}(e^2(n)) = \mathbf{u}^T \mathbf{R} \mathbf{u}$  and  $\nabla_{\mathbf{u}}(\mathbf{u}^T \mathbf{R} \mathbf{u}) = 2\mathbf{R} \mathbf{u}$ . Minimizing it on  $\mathbf{u}$  can then be achieved by the *gradient descent* approach (Fig. 6.6): by starting from an initial guess and updating it in the direction of the steepest descent, i.e., in the direction of the negative gradient of the cost function with respect to the  $\mathbf{u}$ :

$$\mathbf{u}^{new} = \mathbf{u}^{old} - \frac{\mu}{2} \nabla_{\mathbf{u}} (\mathbf{u}^T \mathbf{R} \mathbf{u}) \Big|_{\mathbf{u} = \mathbf{u}^{old}}$$

$$= \mathbf{u}^{old} - \mu \mathbf{R} \mathbf{u}^{old}$$
(6.24)

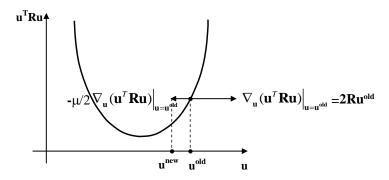


Fig. 6.6 A schematic 2D view of the gradient descent approach

The classical simplification of the LMS approach (Widrow and Stearns 1985) is then to replace  $\mathbf{R}$  in (6.24) by its very short term estimate

 $E(\mathbf{x}\mathbf{x}^T) \approx \mathbf{x}\mathbf{x}^T$ , and to update **u** every sample, leading to the following update equation for  $\mathbf{u}(n)$ :

$$\mathbf{u}(n+1) = \mathbf{u}(n) - \mu \mathbf{x}(n) \mathbf{x}^{T}(n) \mathbf{u}(n)$$

$$= \mathbf{u}(n) - \mu \mathbf{x}(n) e(n)$$
(6.25)

It is also suggested by Benesty (2000) to constrain  $\mathbf{u}(n)$  to unitary norm, in order to avoid round-off error propagation, and to avoid selecting the obvious  $\mathbf{u}$ =0 solution in (6.23). This is achieved by changing (6.25) into:

$$\mathbf{u}(n+1) = \frac{\mathbf{u}(n) - \mu \mathbf{x}(n)e(n)}{\|\mathbf{u}(n) - \mu \mathbf{x}(n)e(n)\|}$$
(6.26)

Additionally, as only the TDOA is required, one only needs to estimate the direct paths in  $\mathbf{h}_1$  and  $\mathbf{h}_2$  (as opposed to the complete impulse responses). A simple solution is to initialize  $\mathbf{h}_2$  (the first half of  $\mathbf{u}$ ) to a single Dirac pulse. A "mirror" effect follows from (6.23) in the estimate of  $\mathbf{h}_1$  (the second half of  $\mathbf{u}$ ): a negative dominant peak appears, which is an estimation of the direct path of  $\mathbf{h}_1$ . The expected TDOA can then be computed as time difference between these peaks within their respective impulse responses. Since the TDOA can *a priori* be positive or negative, the initial Dirac pulse is positioned at the center of  $\mathbf{h}_2$ , and the value of M is set to twice the maximum value of the TDOA.

Provided the adaptation step  $\mu$  is correctly set (not too high to avoid instability, but not too low to be able to track the TDOA as a function of time), this simple algorithm provides remarkably stable results. Moreover, applied to sperm whale spotting, it does not require a preliminary detection of clicks.

## 6.1.5 Multilateration

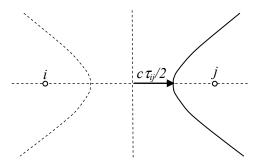
Given two hydrophone locations  $(x_1y_1)$  and  $(x_2y_2)$  and a known TDOA  $\tau_{12}$ , the loci of possible whale positions (x,y) on a 2D map is obtained easily. The travel time of a click to each hydrophone is given by:

$$\tau_i = \frac{1}{c} \left( \sqrt{(x - x_i)^2 + (y - y_i)^2} \right)$$
 (6.27)

where c is the propagation speed of sound in water (typically 1510 m/s). The locus is thus defined by:

$$\tau_{ij} = \tau_i - \tau_j = \frac{1}{c} \left( \sqrt{(x - x_i)^2 + (y - y_i)^2} - \sqrt{(x - x_j)^2 + (y - y_j)^2} \right)$$
 (6.28)

This corresponds to a half-hyperbola whose foci are the hydrophones, and whose semi-major (or transverse) axis is given by  $c \tau_{ij} / 2$  (Fig. 6.7), where c is the speed of sound in water.



**Fig. 6.7** The locus of whale positions for a given value of the TDOA  $\tau_{ij}$  between hydrophones i and j

Obtaining the 2D position of the whale therefore requires two TDOAs (i.e. 3 hydrophones, which implicitly offers a third TDOA): a 2D *multilateration* system solves a system of two non-linear equations such as (6.28) to find the position of a whale in real time.

In practice, though, the half-hyperbola defined by the third TDOA may not have the same intersection as the first two ones, since TDOA estimates may not be very precise. It is then useful to increase the number of hydrophones. The location problem must then be restated as an optimization problem and solved by a least squares approach or with a Kalman filter (Huang *et al.* 2008). To keep things simple, we do not address this problem here.

## 6.2 MATLAB proof of concept: ASP\_audio\_effects.m

In this Section, we analyze sperm whale clicks received by several hydrophones (6.2.1), and use them to find the position of the cetacean. We start by processing the clicks with the (non-linear) Teager-Kaiser operator (6.2.2), so as to increase their signal-to-noise ratio. We then test cross-correlation estimation algorithms (6.2.3) to compute the time difference of

arrival (TDOA) between pairs of hydrophones, and compare them to an efficient adaptive estimation algorithm based on least means squares minimization (6.2.4). We conclude by a simple multilateration algorithm, which uses two TDOAs to estimate the position of the sperm whale (6.2.5).

## 6.2.1 Sperm whale sounds

Throughout Section 6.2, we will work on hydrophone signals collected at the Atlantic Undersea Test and Evaluation Center (AUTEC), Andros Island, Bahamas, and made available by the Naval Undersea War-fare Center (NUWC). These signals were provided to the 2nd International Workshop on Detection and Localization of Marine Mammals using Passive Acoustics, held in Monaco November 16–18, 2005 (Adam *et al.* 2006) and can be obtained from their website (Adam 2005). The Andros Island area has over five hundred square nautical miles of ocean that are simultaneously monitored via 68 broad-band hydrophones. The distance between most hydrophones is 5 nautical miles (about 7.5 km).

We will work with the sounds received by hydrophones I, G, and H (which we will rename as #1, #2, and #3 here), for about 30 seconds, recorded with a digital audio recorder at Fs=48 kHz.

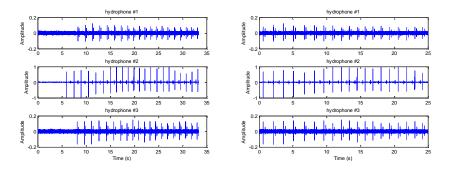
Plotting the signals received by all three hydrophones (Fig. 6.8) shows variable attenuations and delays between clicks, as well as variable noise levels. Each direct path click is followed by an echo due to surface reflection. Obviously, clicks arrive at hydrophone #2 much earlier than at the other hydrophones. The amplitude of the signal on hydrophone #2 is also higher, and the noise level is lower. Moreover, the echo in signal #2 is much more delayed than in signals #1 and #3. All this suggests that the sperm whale is in the vicinity of hydrophone #2.

```
[hydrophone1,Fs]=wavread('hydrophone1.wav');
[hydrophone2,Fs]=wavread('hydrophone2.wav');
[hydrophone3,Fs]=wavread('hydrophone3.wav');

time=(0:length(hydrophone1)-1)/Fs;
ax(1)=subplot(3,1,1); plot(time,hydrophone1)
hold on;
ax(2)=subplot(3,1,2); plot(time,hydrophone2)
ax(3)=subplot(3,1,3); plot(time,hydrophone3)
linkaxes(ax,'x');
```

Since the delay between clicks is larger than the interclick interval, we will first apply a fixed time-shift between signals, so as to approximately align corresponding clicks. We shift the first signal by 7.72 ms to the left,

the second signal by 5.4 s to the left, third signal by 7.58 s to the left, and keep 25 s of each signal. We will later account for these artificial shifts.



**Fig. 6.8** Left: Clicks received by hydrophones #1, #2, and #3. Echoes are clearly visible between clicks (notice that the echo received at hydrophone #2 is more delayed than for the other hydrophones); Right: Same signals, time-shifted so as to approximately align corresponding clicks.

Zooming on a single click (Fig. 6.9) shows that whale clicks are not as simple as Dirac samples, which makes the visual estimation of TDOAs not very precise, and their automatic estimation not trivial.

Let us compute the PSD of the background noise in hydrophone #3 and compute its standard deviation, for later use. It appears (Fig. 6.10) that the noise is pink<sup>7</sup>, with 40 dB more power around f=0Hz than around f=24000 Hz.

```
real_noise=hydrophone3(1.26e4:1.46e4);
real_noise_std=std(real_noise)
pwelch(real_noise,[],[],[],Fs);
```

<sup>&</sup>lt;sup>7</sup> Strictly speaking, a *pink noise* is defined as a signal b(t) whose power spectral density  $S_{bb}(f)$  is proportional to the reciprocal of the frequency 1/f. We use the term *pink* very loosely here, to indicate that the PSD of the noise decreases with frequency.

real\_noise\_std = 0.0073

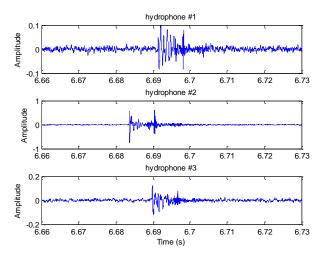


Fig. 6.9 Zoom on a single click

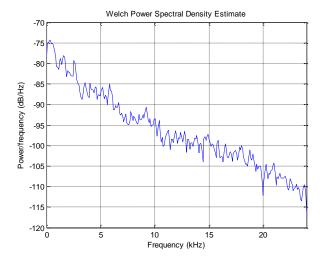


Fig. 6.10 Power spectral density of the background pink noise measured by hydrophone #3.

Notice that the data used here does not reveal LF interferences, which may however occur in measurements and make the estimation of TDOA still more complex.

## 6.2.2 Teager-Kaiser filtering

In order to better understand the Teager-Kaiser non-linear filter, we first apply it to synthetic signals, composed of clicks (assimilated to Dirac impulses), background noise (white and pink noise), and an interference component (modelled as a sinusoid). We then show that, even though the effect of a general non-linear filter on a sum of signals is not the sum of its outputs to isolated input signals, the effect of the TK operator on synthetic clicks with background noise and sinusoidal interference can still somehow be analyzed in terms of its effect on isolated components.

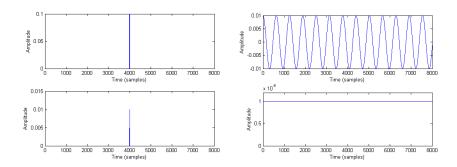
We finally apply the TK operator on real sperm whale sounds, and compare it to a simple linear high-pass filter.

## Dirac pulse input

We start with the response of the TK operator to a Dirac impulse  $0.1\delta$ (n-4000), with the same order of magnitude as that of the clicks we found in the previous Section. The output is the input impulse, squared (Fig. 6.11, left).

## Sinusoidal input

Sinusoidal interference signals of the form  $A \cos(n\phi_0)$  produce a constant output  $A^2 \sin^2(\phi_0)$ . To check this, we generate 8000 samples of a chirp  $\cos(n\phi_0(n))$  with  $\phi_0(n) = \phi_{\max} n/8000$  and  $\phi_{\max} = 0.1$  (which corresponds to frequencies from 0 to  $F_s \phi_{\max}/2\pi = 763$  Hz). The result is plotted on Fig. 6.12 (left).

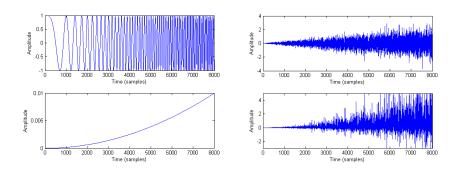


**Fig. 6.11** Response of the TK filter to a Dirac pulse  $0.1 \delta$ (n-4000) (Left) and to a cosine  $0.01\cos(0.01n)$  (Right)

## **MATLAB function involved:**

• y = teager\_kaiser(x) applies the Teager-Kaiser energy operator to input signal x.

```
Fs=48000;
phi_max=0.1;
test=chirp(0:1/Fs:7999/Fs,0,7999/Fs,Fs*phi_max/2/pi);
test_response=teager_kaiser(test);
subplot(2,1,1); plot(test);
subplot(2,1,2); plot(test_response);
```



**Fig. 6.12** Response of the TK filter to a chirp (Left) and to to white noise with linearly increasing standard deviation (Right)

The value of the output is close to zero when  $\phi_0$  is small, which will be the case for a typical LF interference component in sperm whale click measurements (Fig. 6.11, right).

```
interference = 0.01*cos (0.01*(0:7999)); % A<sup>2</sup>sin<sup>2</sup>(0.01)~1e-8
interference_response=teager_kaiser(interference);
subplot(2,1,1); plot(interference);
subplot(2,1,2); plot(interference_response);
```

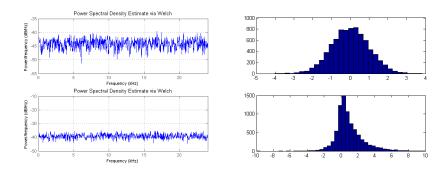
## White noise input

TK filtering of Gaussian white noise  $N(0,\sigma)$  produces noise with mean of the order of  $\sigma^2$  and standard deviation proportional to  $\sigma^2$ . We check this on white noise with linearly increasing standard deviation (see Fig. 6.12, right).

```
test = (1/8000:1/8000:1).*randn(1, 8000);
test_response = teager_kaiser(test);
subplot(2,1,1); plot(test);
subplot(2,1,2); plot(test_response);
```

The output noise is still white, but it is not Gaussian (Fig. 6.13).

```
noise = randn(1, 8000);
noise_response = teager_kaiser(noise);
subplot(2,1,1); pwelch(noise,[],[],[],Fs);
subplot(2,1,2); pwelch(noise_response,[],[],[],Fs);
subplot(2,1,1); hist(noise,30);
subplot(2,1,2); hist(noise_response,60);
```

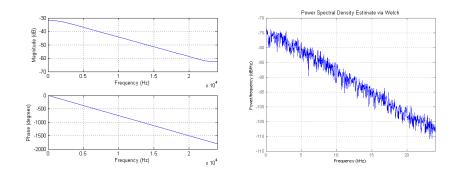


**Fig. 6.13** Left: PSD of white noise input and its filtering thought the TK filter; Right: Histograms of the corresponding samples

## Pink noise input

Let us now test the TK filter on pink noise similar to the one we found on real hydrophone signals in 0. We first create a filter with linear frequency response from -30 dB at f=0 to -65dB at  $f=F_s/2$ . Applying this filter to white noise N(0,1) produces a realistic pink noise component (Fig. 6.14).

```
w=0:0.1:1;
   a_dB=-35*w-30;
   a=10.^(a_dB/20);
   [B,A] = fir2(20,w,a);
   freqz(B,A,512,48000);
  pink_noise=filter(B,A,noise);
  pwelch(pink_noise,[],[],[],Fs);
  pink_noise_std=std(pink_noise)
```



**Fig. 6.14** Left: Frequency response of a noise shaping filter; Right: PSD of the resulting pink noise

TK filtering of pink noise produces pink noise, whose standard deviation is still proportional to the square of that of the original noise (although with a smaller proportionality factor than for white input noise; Fig. 6.15 Left).

```
test=100*(1/8000:1/8000:1).*pink_noise;
test_response = teager_kaiser(test);
subplot(2,1,1);
plot(test);
subplot(2,1,2);
plot(test_response);
```

The output noise is whiter; the PSD of the input noise has been decreased by about 50 dB in low frequencies and by about 30 dB in high frequencies (Fig. 6.15 Right).

```
pink_noise_response = teager_kaiser(pink_noise);

subplot(2,1,1);
pwelch(pink_noise,[],[],[],Fs);
subplot(2,1,2);
pwelch(pink_noise_response,[],[],[],Fs);

Power Spectral Density Estimate via Welch

Time (samples)

Power Spectral Density Estimate via Welch

Power Spectral Density Estimate via Welch

Power Spectral Density Estimate via Welch

Power Spectral Density Estimate via Welch
```

**Fig. 6.15** Left: TK filtering of pink noise with linearly increasing standard deviation; Right: PSDs of input pink noise (with constant variance) and of its filtering through the TK filter.

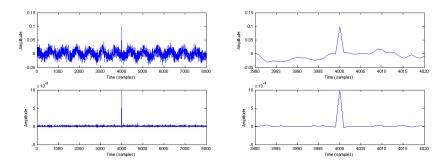
## **Complex input**

We now apply the TK operator to the complete synthetic signal, obtained by summing all three components: click, interference, and pink noise (Fig. 6.16, left). Thanks to the TK operator, the impulse is highlighted in the signal. The LF signal is removed, and the pink noise is very much attenuated relatively to the impulse. The SNR is therefore highly increased.

```
input=click+interference+pink_noise;
output_tk=teager_kaiser(input);
subplot(2,1,1);
plot(input);
subplot(2,1,2);
plot(output_tk);
```

Notice that the TK operator did not smear the impulsive part of the input waveform (Fig. 6.16, right).

```
set(gca,'xlim',[3980 4020]);
```



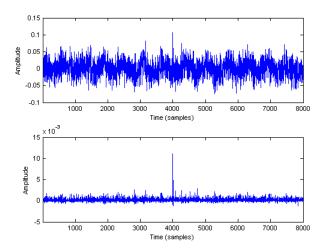
**Fig. 6.16** Top left: Synthetic hydrophone signal composed of the sum of a Dirac pulse, sinusoidal interference, and background noise; Bottom left: Same signal, filtered by the TK operator; Right: Same signal as on the left, zoom around the Dirac pulse

Notice also that the effect of the TK filter on the SNR depends on the original value of the SNR. As a matter of fact, TK squares the amplitude A of the impulse and the standard deviation  $\sigma$  of the noise. Let us characterize the "visibility" of the pulse by the ratio  $A/3\sigma$ , since noise samples take most of their values in  $[-3\sigma, 3\sigma]$ . If this ratio is significantly higher than 1 (in the previous plot it was 0.1/0.033=3), the visibility of the pulse in the TK filtered signal,  $A^2/9\sigma^2$ , is higher than in the original signal. If  $A/3\sigma$  approaches 1 but is still higher, the impulse may not be visible in the original signal, but more easily detected in the output signal. To check this, we multiply the standard deviation of the noise by two (Fig. 6.17).

#### input=click+2\*pink\_noise+interference; output\_tk=teager\_kaiser(input);

Summarizing, the TK operator has a high-pass filtering effect on background pink noise (and it squares its standard deviation), a notch effect on possible low-frequency interference (while a DC component appears), and almost no effect on Dirac pulses (apart from squaring their amplitude): it acts as a signal-dependent filter and amplifier<sup>8</sup>.

<sup>&</sup>lt;sup>8</sup> In practice, it also produces cross terms when several components are summed at the input. We did not examine them here, as they are not essential for the kind of signal we deal with.



**Fig. 6.17** Top: a Dirac pulse hidden in background noise; Bottom: same signal, after TK filtering

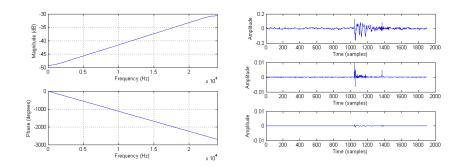
## Hydrophone signal

Finally we apply the TK operator to a real click taken from a hydrophone signal, as examined in Section 1, and compare its effect to that of a linear filter.

We first create a linear-phase high-pass symmetric FIR filter whose frequency response has approximately the same effect on the pink background noise as the TK filter: a frequency-linear attenuation, from -50 dB close to f=0 to -30 dB close to  $f=F_s/2$  (Fig. 6.18, Left). The length of its impulse response is 31 (its order is 30). It therefore has a delay of 15 samples.

```
clf;
w=0:0.1:1;
a_dB=20*w-50;
a=10.^(a_dB/20);
N=30;
[B,A] = fir2(N,w,a);
freqz(B,A,512,Fs);
```

Obviously the TK operator does a very good job at highlighting the click. While the linear filter has a similar effect on background noise, it also decreases the power of the click, thereby decreasing the overall SNR (Fig. 6.18, Right).



**Fig. 6.18** Left: Frequency response of a linear filter having the same effect on background noise as the TK filter; Right: a real click (top), filtered by the TK operator (middle) and by the linear filter (bottom).

```
input=wavread('hydrophone3.wav',[464750 466650]);
output_tk=teager_kaiser(input);
% Taking the filter dealy into account
output_lin=[filter(B,A,input(16:end)) ; zeros(15,1)];
subplot(3,1,1); plot(input);
subplot(3,1,2); plot(output_tk);
subplot(3,1,3); plot(output_lin);
```

## 6.2.3 TDOA estimation using generalized cross-correlation

We will now show how generalized cross correlation (GCC) can be used for estimating TDOAs. We start again by applying it to simple synthetic signals, and end with real hydrophone signals.

## Synthetic input

We first create a simple synthetic signal, as in Section 6.2.2, but with more severe interference and noise, and a second signal, with other noise samples, a phase-shifted interference signal, and an attenuated click, delayed by 60 samples (Fig. 6.19, Left).

```
click = [zeros(1,499) 0.1 zeros(1,500)];
interference = 0.03*cos (0.01*(0:999));
noise = 2*randn(1, 1000);
w=0:0.1:1;
a_dB=-35*w-30;
a=10.^(a_dB/20);
[B,A] = fir2(20,w,a);
pink_noise=filter(B,A,noise);
signal_1=click+interference+pink_noise;
```

```
click_2=circshift(click'*0.5,60)';
interference_2 = 0.02*cos (pi/4+0.01*(0:999));
noise_2 = randn(1, 1000); % new noise samples
pink_noise_2=filter(B,A,noise_2);
signal_2=click_2+interference_2+pink_noise_2;
subplot(2,1,1); plot(signal_1);
subplot(2,1,2); plot(signal_2);
```

**Fig. 6.19** Left: two synthetic hydrophone signals, with a delay of 60 samples between their respective Dirac pulses; Right: same signal, filtered by the TK operator.

Estimating the time difference of arrival (TDOA) between the filtered signals with the standard cross-correlation does not provide the expected value (-60 samples), as the total cross-correlation function is dominated by the correlation between the sinusoidal interference components. Notice that the (biased) cross-correlation is obtained via FFT-IFFT (Fig. 6.20), after making sure that the number of FFT samples is high enough for linear convolution to be identical to circular convolution (as obtained by multiplying FFTs).

```
% Computing the standard biased cross-correlation via FFT-IFFT
M = min(length(signal_1),length(signal_2));
NFFT = 2*M-1; % so that linear convolution = circular convolution
x1 = signal_1 - mean(signal_1);
x2 = signal_2 - mean(signal_2);
X1 = fft(x1,NFFT);
X2 = fft(x2,NFFT);
S_x1x2 = x1.*conj(x2);
phi_x1x2 = ifft(S_x1x2);
% re-arranging the IFFT
standard_xcorr = [phi_x1x2(NFFT-M+2:NFFT) phi_x1x2(1:M)];
[val,ind]=max(standard_xcorr);
TDOA_standard_xcorr = 41
```

arg(S<sub>X1x2</sub>) (rad)

```
subplot(2,1,1);
plot((0:1/M:(M-1)/M), 20*log10(abs(S_x1x2(1:M))));
subplot(2,1,2);
plot((0:1/M:(M-1)/M), unwrap(angle(S_x1x2(1:M))));
```

Fig. 6.20 Left: Cross PSD between the signals in (Fig. 6.19, Right); Right: Corresponding cross correlation function

-200 0 200 Time lag (sample)

```
plot((-M+1:M-1),standard_xcorr); grid;
```

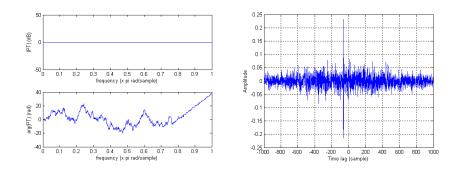
Notice that the linear phase component in the HF part of (Fig. 6.20, left), where the pink noise is weak, reveals a delay. But since the amplitude of the noise and of the LF interference strongly dominate that of the HF part of the cross PSD, this delay cannot be observed in the cross correlation function.

Using the phase transform version of the generalized cross-correlation removes the LF interference and gives the same importance to all frequency bands in the phase spectrum. It produces a more prominent maximum, which leads to a correct estimate of the TDOA (Fig. 6.21).

```
phi_x1x2 = ifft(S_x1x2 ./ max(abs(S_x1x2),eps));
% re-arranging the IFFT
phase_transform = [phi_x1x2(NFFT-M+2:NFFT) phi_x1x2(1:M)];
[val,ind]=max(phase_transform);
TDOA_phase_transform = ind-M

subplot(2,1,1);
plot((0:1/M:(M-1)/M), 20*log10(abs(PT(1:M))));
subplot(2,1,2);
plot((0:1/M:(M-1)/M), unwrap(angle(PT(1:M))));
plot((-M+1:M-1),phase_transform); grid;

TDOA_phase_transform = -60
```



**Fig. 6.21** Left: Discrete Fourier transform of the phase transform between the signals in (Fig. 6.19, Left); Right: Corresponding phase transform

Applying the TK operator obviously increases the SNR (Fig. 6.19, Right).

```
signal_1_tk=teager_kaiser(signal_1);
signal_2_tk=teager_kaiser(signal_2);
subplot(2,1,1);
plot(signal_1_tk);
subplot(2,1,2);
plot(signal_2_tk);
```

As a result of the suppression of the sinusoidal component, GCC produces an accurate result (Fig. 6.22, Left).

## **MATLAB function involved:**

• gcc(z1, z2, flag) computes the generalized cross correlation (GCC) between signals z1 and z2, from FFT/IFFT, as specified in (Knapp & Carter 1976). [flag] makes it possible to choose the type of cross-correlation: standard cross correlation if flag='cc'; phase transform if flag='phat'.

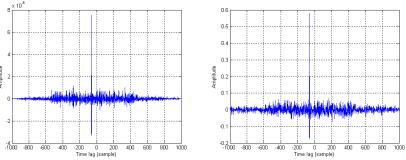
```
standard_xcorr_tk = gcc(signal_1_tk, signal_2_tk, 'cc');
[val,ind]=max(standard_xcorr_tk);
TDOA_standard_xcorr_tk = ind-M % in samples
plot((-M+1:M-1),standard_xcorr_tk); grid;

TDOA_standard_xcorr_tk = -60
```

Using the phase transform on TK-filtered data still produces an even more prominent maximum (Fig. 6.22, Right).

```
phase_transform_tk = gcc(teager_kaiser(signal_1),
    teager_kaiser(signal_2), 'phat');
    [val,ind]=max(phase_transform_tk);
    TDOA_phase_transform_tk = ind-M
    plot((-M+1:M-1),phase_transform_tk); grid;

TDOA_phase_transform_tk = -60
```



**Fig. 6.22** Left: Cross correlation computed on TK-filtered signals; Right: Corresponding phase transform

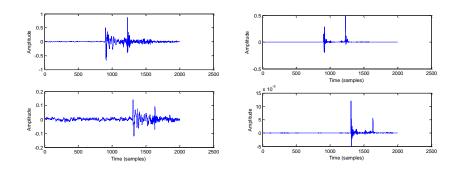
## Hydrophone signals

We now apply GCC to real hydrophone signals. Clicks are separated by about 400 samples (Fig. 6.23, Left).

Again, applying the TK operator has a positive effect on the SNR (Fig. 6.23, Right).

```
signal_1_tk=teager_kaiser(signal_1);
signal_2_tk=teager_kaiser(signal_2);
subplot(2,1,1); plot(signal_1_tk);
subplot(2,1,2); plot(signal_2_tk);
```

Applying the Phase Transform to these signals delivers a correct estimate of the TDOA: -404 samples (negative, since the click hits hydrophone #1 before hydrophone #2).



**Fig. 6.23** Left: Two clicks, showing a delay of about 400 samples. Right: same, after TK filtering.

```
phase_transform_tk = gcc(signal_1_tk, signal_2_tk, 'phat');
  [val,ind]=max(phase_transform_tk);

M = min(length(signal_1),length(signal_2));
  TDOA_phase_transform_tk = ind-M
TDOA_phase_transform_tk = -404
```

## 6.2.4 TDOA estimation using least-mean squares

In this section we will apply the Least Mean Squares (LMS) adaptive approach to TDOA estimation, again first on synthetic signals (with imposed TDOA), and then on real hydrophone signals.

## Synthetic input

We start with the same synthetic signals as in Fig. 6.19, apply TK preprocessing, and run the Benesty's adaptive filtering algorithm for TDOA estimation within [-600,600] (samples) and step mu=0.01 (for full scale signals in [-1,+1]).

```
load synthetic_signals signal_1 signal_2
signal_1_tk=teager_kaiser(signal_1);
signal_2_tk=teager_kaiser(signal_2);

% Normalizing max signal amplitudes to +1
x1=signal_1_tk/max(signal_1_tk);
x2=signal_2_tk/max(signal_2_tk);

% LMS initialization
M = 600; % max value of the estimated TDOA
x1c = zeros(M,1);
x2c = zeros(M,1);
u = zeros(2*M,1);
```

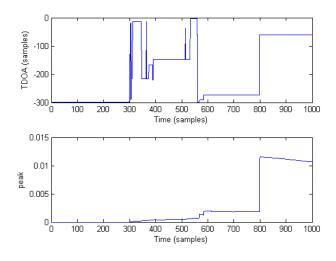
```
u(M/2) = 1;
N = length(x1);
e = zeros(1,N);
tdoa = zeros(1,N);
peak = zeros(1,N);
mu = 0.01; % LMS step

% LMS loop
for n=1:N

    x1c = [x1(n);x1c(1:length(x1c)-1)];
    x2c = [x2(n);x2c(1:length(x2c)-1)];
    x = [x1c;x2c];
    e(n) = u'*x;
    u = u-mu*e(n)*x;
    u(M/2) = 1; %forcing g2 to an impulse response at M/2
    u = u/norm(u); %forcing ||u|| to 1

    [peak(n),ind] = min(u(M+1:end));
    peak(n)=-peak(n); % (positive) impulse in g1
    TDOA(n) = ind-M/2;
end

% Estimated TDOA(n), with values of the maximum peak in g1
subplot(2,1,1);
plot(TDOA);
xlabel('Time (samples)'); ylabel('TDOA (samples)');
subplot(2,1,2);
plot(peak);
xlabel('Time (samples)'); ylabel('peak');
```



**Fig. 6.24** Top: TDOA estimated by the LMS approach on the signals in Fig. 6.19, on an adaptive, sample-by-sample basis; Bottom: Value of the peak found in **h1** (the higher the peak, the more reliable the TDOA estimate)

It appears that the TDOA estimate is wrong at the beginning of the frame, as the adaptive filter must have started processing a click to start converging (Fig. 6.24). The value of the peak in **h1** (the impulse response between the source and the first signal) is very low for these wrong TDOA values. The best TDOA estimate is the one that produced the most prominent peak in **h1**. This estimate is correct: -60 samples. After a click has been processed, the peak in **h1** starts decreasing again, but the value of TDOA remains correct.

```
[val,ind]=max(peak);
Best_estimate_TDOA=TDOA(ind)
```

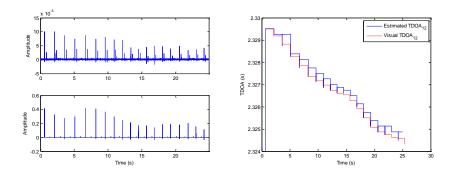
Best\_estimate\_TDOA = -60

## Hydrophone signals

Applying the same algorithm to hydrophone signals #1 and #2 is straightforward.

The estimated TDOAs change by a few tens of milliseconds in our 25-seconds recording (Fig. 6.25)<sup>9</sup>. This shows that the sperm whale moved during the recording. Plotting our TODAs with the ones obtained by visual inspection of the signals proves that the LMS algorithm provided accurate results (the error is less than a millisecond).

<sup>&</sup>lt;sup>9</sup> Again, the first TDOA estimates are not significant.

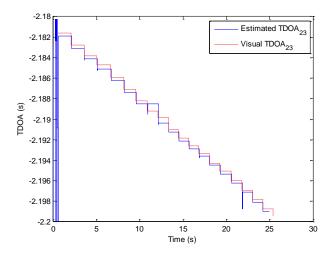


**Fig. 6.25** Left: Hydrophone signals #1 and #2, after TK-filtering. Right; TDOA estimated from these signals, as a function of time, compared to the estimate obtained by visual inspection of the signals

## **MATLAB function involved:**

• [tdoa, peak] = TDOA\_LMS(x1, x2, max\_tdoa, mu) is an implementation of (Benesty 2000) for source localization. It returns the time difference of arrival, in samples, between signals x1 and x2, as a function of time, together with the value of the peak found in the estimate of the main propagation path for signal x1. This value can be used as a confidence value for the TDOA. max\_tdoa is the maximum TDOA value returned and mu is the step weight.

We repeat the operation for hydrophone signals #2 and #3 (Fig. 6.26).



**Fig. 6.26** TDOA estimated from hydrophone signals #2 and #3, as a function of time, compared to the estimate obtained by visual inspection of the signals

## 6.2.5 Multilateration

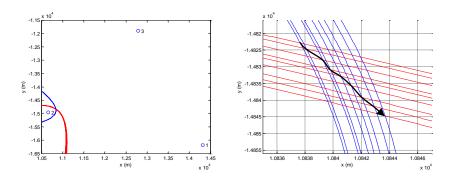
In this final Section, we use the TDOAs estimated in the previous Section from real hydrophones signals, for tracking a sperm whale on a 2D map. We develop a rudimentary multilateration system, on the basis of 2 TDOAs only.

The position of the hydrophones, taking some common point as a reference, is given in Table 6.1.

 Table 6.1 Hydrophone relative locations and depth

Hydrophone	X	Y	Z
#1	14318,86m	-16189,18m	-1553,58m
#2	10658,04m	-14953,63m	-1530,55m
#3	12788,99m	-11897,12m	-1556,14m

We first show the position of the hydrophones on the map (Fig. 6.27), and then plot the hyperbolas corresponding to each pair of TDOA, assuming the speed of sound in water is 1510 m/s. Notice we drop the first TDOA estimates, which the LMS algorithm used for converging, and only use 10 estimates for our plot.



**Fig. 6.27** Multilateration hyperbolas on the 2D hydrophone map. Left: general view; Right: zoom on the intersection area and observed movement

Since the maximum speed of a whale is close to 30 km/h (i.e. 8 m/s), it obviously could not move much around hydrophone #2 in the 25 s of data we have used for this proof-of-concept (Fig. 6.27, left).

Zooming around hydrophone #2 (Fig. 6.27, right) reveals its trajectory: it moved from (10837.5,-14822) to (10844,-14847), i.e. by about 26 m in 25 seconds, i.e. at a speed of about 1 m/s.

*distance = 25.8312* 

## 6.3 Going further

Readers interested in methods for estimating the position of a source from multiple TDOA estimations should report to (Huang *et al.* 2008).

MATLAB code for localization, including more elaborate multilateration algorithms, is available from the Beam Reach Marine Science and Sustainability School (Beam Reach 2007).

ISHMAEL (Integrated System for Holistic Multi-channel Acoustic Exploration and Localization) is free software for acoustic analysis, including localization, made freely available by Prof. Dave Mellinger at Oregon State University(Mellinger 2008). The same group also provides Moby-Sound, a public a database for research in automatic recognition of marine animal calls (Mellinger 2007).

MATLAB-based UWB positioning software can also be found in Senad Canovic's Master thesis, from Norwegian University of Science and Technology (Canovic 2007).

## 6.4 Conclusion

In this Chapter, we have provided signal processing solutions for cleaning impulsive signals mixed in noise and low-frequency interferences, and for automatically estimating TDOAs based on either generalized cross-correlation or adaptive filtering.

Although we have examined these techniques in the specific context of whale spotting, they can easily be generalized to many positioning problems, such as the localization of speakers in a room, that of GSM mobile phones, of Global Positioning System (GPS) receivers, or to that of aircrafts or vehicles using either sonar or radar.

Last but not least, this Chapter also highlights one of the many "natural" abilities of human beings: that of using both ears to locate sound sources.

## 6.5 References

Adam O (2005) Website of the 2nd International Workshop on Detection and Localization of Marine Mammals using Passive Acoustics [online] Available: http://www.circe-asso.org/workshop/ [26/4/2008]

Adam O, Motsch JF, Desharnais F, DiMarzio N, Gillespie D, Gisiner RC (2006) Overview of the 2005 workshop on detection and localization of marine mammals using passive acoustics, Applied Acoustics 67:1061–1070

- Beam Reach (2007) Acoustic Localization [online] Available:
  - http://beamreach.org/soft/AcousticLocation/AcousticLocation-041001/[23/6/2008]
- Benesty J (2000) Adaptive eigenvalue decomposition algorithm for passive acoustic source localization. J. Acoust. Soc. Am. 107 (1): 384–391
- Canovic S (2007) Application of UWB Technology for Positioning, a Feasibility Sudy. Master thesis, Norwegian University of Science and Technology [online] Available:
  - http://www.diva-portal.org/ntnu/undergraduate/abstract.xsql?dbid=2091 [23/06/08]
- Huang Y, Benesty J, Chen J (2007) Time delay estimation and source localization. In Springer Handbook of Speech Processing, Benesty J, Sondhi MM, Huang Y (eds), Springer:Berin, 51:1043–1063
- Drouot V (2003) Ecology of sperm whale (Physeter macrocephalus) in the Mediterranean Sea. Ph.D. Thesis, Univ. of Whales, Bangor, UK
- Fang J, Atlas LE (1995) Quadratic detectors for energy estimation. IEEE Transactions on Signal Processing 43–11: 2582–2594
- Huang Y, Benesty J, Chen J (2008) Time delay estimation and source localization. In: Springer Handbook of Speech Processing, Benesty J, Sondhi MM, Huang Y (Eds.), Springer: Berlin. 1043–1063.
- Kaiser JF (1990) On a simple algorithm to calculate the "Energy" of a signal. In: Proc. IEEE ICASSP, 381–384, Albuquerque, NM, USA
- Kandia V, Stylianou Y (2005) Detection of creak clicks of sperm whales in low SNR conditions. In CD Proc. IEEE Oceans, Brest, France
- Kandia V, Stylianou Y (2006) Detection of sperm whale clicks based on the Teager–Kaiser energy operator, Applied Acoustics 67:1144–1163
- Kandia V, Stylianou Y (2006) Accurate TDOA (Time Difference of Arrival) using the Teager Kaiser Energy Operator. In CD Proceedings of the 20th Annual Conference of the European Cetacean Society, Gdynia, Poland
- Knapp CH and Carter GC (1976) The generalized correlation method for estimation of time delay. In: IEEE Transactions on Acoustic, Speech and Signal Processing 24, 320–327
- ICES (International Council for the Exploration of the Sea Advisory Committee on Ecosystems, ICES CM 2005/ACE:01) (2005) Report of the Ad-hoc Group on the Impact of Sonar on Cetaceans and Fish (AGISC).
- Madsen PT (2002) Sperm whale sound production in the acoustic realm of the biggest nose on record, In Madsen P.T., PhD. Dissertation, Sperm whale sound production., Dep. of Zoophysiology, University of Aarhus, Denmark
- Mellinger D (2007) MobySound [online] Available:
  - http://hmsc.oregonstate.edu/projects/MobySound/ [23/6/2008]
- Mellinger D (2008) Ishmael Integrated System for Holistic Multi-channel Acoustic Exploration and Localization [online] Available: http://www.pmel.noaa.gov/vents/acoustics/whales/ishmael [23/6/2008]
- Morrissey RP, Ward J, DiMarzio N, Jarvis S, Moretti DJ (2006) Passive acoustic detection and localization of sperm whales (Physeter macrocephalus) in the tongue of the ocean. Applied Acoustics 67:1091–1105

- Møhl B, Wahlberg M, Madsen PT, Heerfordt A, Lund A (2000) Sperm whale clicks: Directionality and source level revisited, J. Acoust. Soc. Am. 107 (1): 638–648.
- Sicuranza G (1992) Quadratic filters for signal processing. In: Proceedings of the IEEE, 80(8):1263–1285
- Widrow B, Stearns SD (1985) Adaptive Signal Processing. Prentice-Hall,Inc., Upper Saddle River, NJ
- Zimmer WMX, Madsen PT, Teloni V, Johnson MP, Tyack PL (2005) Off-axis effects on the multi-pulse structure of sperm whale usual clicks with implications for the sound production. J. Acoust. Soc. Am. 118: 3337–3345