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SE20UCSE149

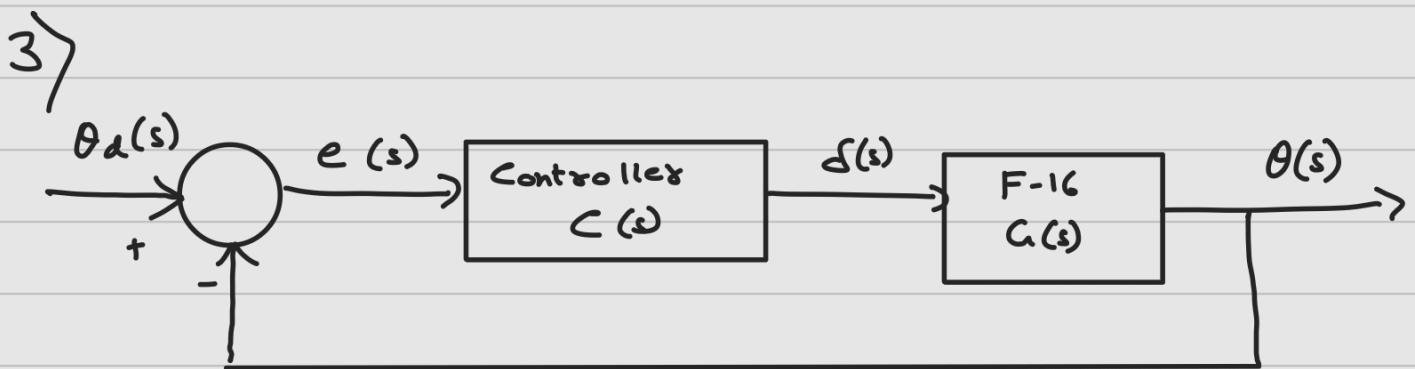
CSE - 3

Control Theory Project.

[Screenshots of code and their
respective outputs are at
last few pages]

1) Unstable System.
(Look at question1.py)

2) (Look at question2.py)



$$Y_{ss} = \lim_{s \rightarrow 0} s \left[\theta_d(s) - \theta(s) \right].$$

[Steady state error is zero]

$$= \lim_{s \rightarrow 0} s \left[\theta_d(s) - \frac{C(s)G(s)\theta_d(s)}{1 + C(s)G(s)} \right]$$

$$= \lim_{s \rightarrow 0} s \theta_d(s) \left(1 + \frac{C(s)G(s) - C(s)G(s)}{1 + C(s)G(s)} \right).$$

$$= \lim_{s \rightarrow 0} s \frac{\theta_d(s)}{1 + C(s)G(s)}$$

Now,

$$\lim_{s \rightarrow 0} s \frac{\theta_d(s)}{1 + C(s)G(s)} = 0$$

$$\Rightarrow \lim_{s \rightarrow 0} \frac{s \times 1/8}{1 + C(s)G(s)} = 0$$

$$\Rightarrow \lim_{s \rightarrow 0} \frac{1}{1 + C(s)G(s)} = 0$$

$$\lim_{s \rightarrow 0} C(s)G(s) \approx \infty$$

$$= \lim_{s \rightarrow 0} \frac{\tilde{C}(s)}{s^N} \times \left(\frac{s+23}{s^2+s-1-19} \right)$$

$$\therefore \lim_{s \rightarrow 0} \frac{\tilde{C}(s)}{s^N} \text{ must be } \infty$$

$$s^N = 0$$

$$\therefore N = 1, 2, 3 \dots$$

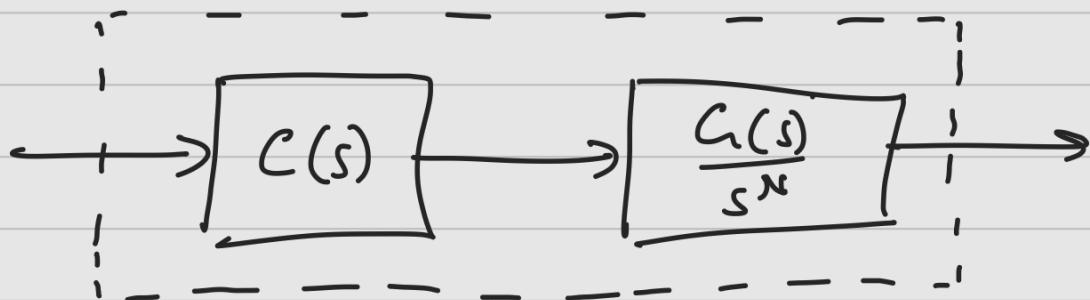
and min of $N = 1$.

$$\therefore \text{Minimum } N = 1$$

$$4) \quad C(s) = \frac{\tilde{C}(s)}{s^N}$$

Let's plug s^N to $C(s)$

\therefore Our block diagram becomes



i) From the question ③, $N=1$.

Assuming $C(s)$ is K as in P-controller,

Characteristic eqn.

$$1 + C(s) \frac{G(s)}{s^N} = 0$$

$$\Rightarrow 1 + \frac{C(s)G(s)}{s} = 0 .$$

$$\Rightarrow 1 + C(s) \times \frac{1}{s} \left(\frac{s+23}{s^2+s-1.19} \right) = 0 .$$

$$\Rightarrow s^3 + s^2 - 1.19s + C(s)s + 23 = 0 .$$

①

Now,
for Max overshoot :

$$\xi = \frac{1}{\sqrt{1 + \left(\frac{\pi}{\log_e(0.2)}\right)^2}} \approx 0.455.$$

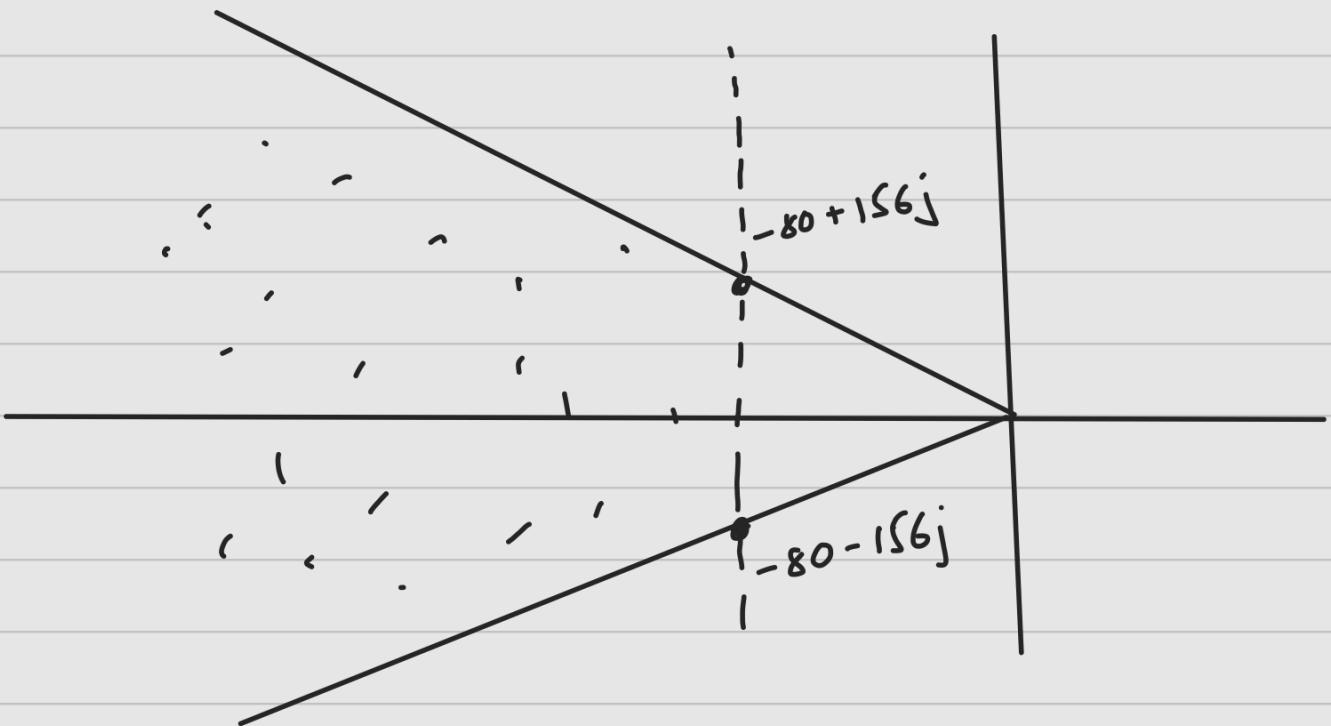
for settling time,

$$\frac{4}{\xi \omega_n} = 0.05.$$

$$\Rightarrow \xi \omega_n = 80.$$

$$\therefore \omega_n = 175.82$$

$$\begin{aligned}\therefore s &= -\bar{\xi} \omega_n \pm \sqrt{1 - (\bar{\xi})^2} \omega_n j \\ &= -80 \pm \sqrt{0.792975} \times 175.82 j \\ &= -80 \pm 156.56 j\end{aligned}$$



$$s_0 = -80 + 156 \cdot 56j.$$

$$\begin{aligned}
 \Rightarrow \angle C(s_0) &= \angle \left(\frac{(s_0 + 23)}{(s_0^2 + s_0 - 1 \cdot 19)} \times \left(\frac{1}{s_0} \right) \right) \\
 &= \angle (s_0 + 23) - \angle (s_0^2 + s_0 - 1 \cdot 19) - \angle s_0 \\
 &= \angle \left(\underbrace{-80 + 156 \cdot 56j + 23}_{\text{circled}} \right) - \left((-80 + 156 \cdot 56)^2 + (-80 + 156 \cdot 56j) - 1 \cdot 19 \right) - \angle s_0 \\
 &= 110^\circ + 126^\circ - 117^\circ \\
 &\approx 119^\circ
 \end{aligned}$$

\therefore we need to change our K to

$$K C_c(s).$$

$$\therefore C(s) \cdot K C_c(s)$$

Now, our characteristic eqn. becomes.

$$1 + KG(s) = 0$$

where $G(j) = G_c(s) \times \frac{(s+23)}{(s^2+s-1.19)} \times \frac{1}{s}$

Accordingly

$$\angle G(s_0) = \angle G_c(s_0) + 119^\circ.$$

$$\therefore \angle G(s_0) \approx 61^\circ$$

Let's consider, $G_c(s) = \frac{s+z}{s+p}$

$p, z \geq 0$. Accordingly,

$$\angle G_c(s_0) = \angle \frac{s_0+z}{s_0+p} = \angle s_0+z - \angle s_0+p.$$

$$\therefore \angle s_0+z - \angle s_0+p = -299^\circ.$$

Assuming $z = 80$, $\angle s_0+z = 90^\circ$

$$90^\circ - \angle s_0+p = CL.$$

$$\Rightarrow 29 = \angle S_0 + P$$

$$\angle (-80 + 156 \cdot 56j + P) = 29$$

$$\Rightarrow \tan^{-1} \left(\frac{156 \cdot 56}{-80 + P} \right) = 29.$$

$$\Rightarrow P = 362 \cdot 441 \approx 362$$

$$\therefore G_C(s) = \frac{s + 80}{s + 362}$$

$$\text{Now, } K = C(s) = \frac{1}{|G(s_0)|}$$

$$= \frac{1}{\left| \left(\frac{s_0 + 80}{s_0 + 362} \right) \times \left(\frac{s_0 + 23}{s_0^2 + s_0 - 1 \cdot 19} \right)^{\frac{1}{8}} \right|}$$

$$= 67028 \cdot 47477$$

$$\therefore C(s) = 67028 \cdot 47 \times \left(\frac{s + 80}{s + 362} \right)$$

$$q5) \quad T(s) = \left[67028 \cdot 47 \times \frac{(s+80)}{(s+362)} \frac{(s+23)}{(s^2+s-1-19)} \frac{1}{s} \right]$$

Open Loop $T_f \uparrow$

Closed Loop tf

$$\begin{aligned} T(s) &= \frac{C(s)G(s)}{1 + C(s)G(s)} \\ &= \frac{\nu \left(\frac{s+80}{s+362} \right) \left(\frac{s+23}{s^2+s-1-19} \right) \frac{1}{s}}{1 + \nu \left(\frac{s+80}{s+362} \right) \left(\frac{s+23}{s^2+s-1-19} \right) \frac{1}{s}} \end{aligned}$$

$$= \frac{\nu (s+80)(s+23)}{(s+362)(s^2+s-1-19)s + \nu (s+80)(s+23)}$$

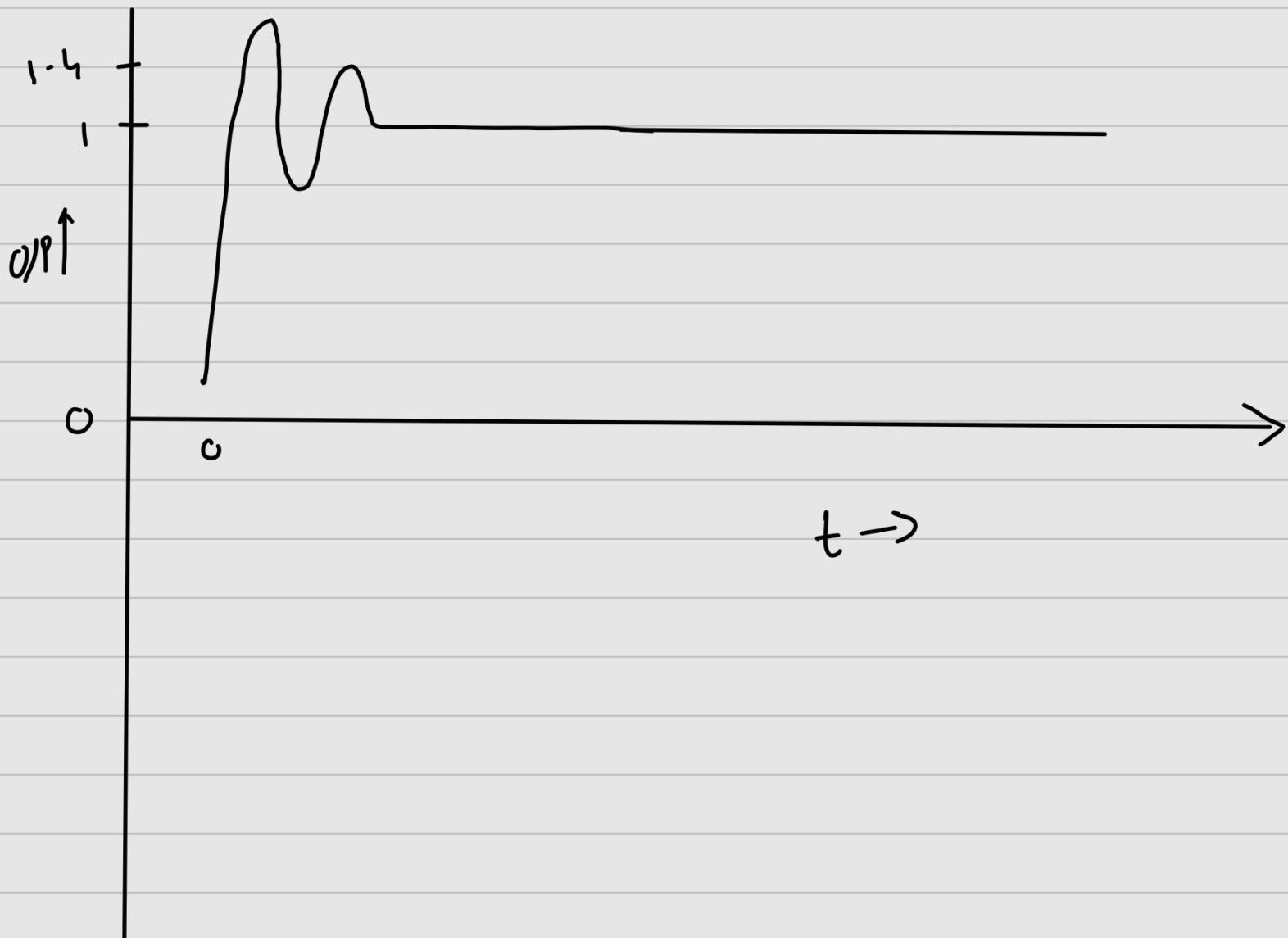
$$= \frac{[s^2 + 103s + 1840] \nu}{(s+362)(s^3+s^2-1-19s) + \nu (s^2+103s+1840)}$$

$$\begin{aligned} &= \frac{(s^2 + 103s + 1840) \nu}{s^4 + s^3 - 1 - 19s^2 + 362s^3 + 362s^2 - 430 \cdot 78s} \\ &\quad - \nu (s^2 + 103s + 1840) \end{aligned}$$

g6) Max overshoot is 20%. Therefore,
O/P shouldn't exceed $1 + \frac{20}{100} = \frac{6}{5} = 1.2$.

But here it exceeds

So, it does not satisfy controller design.



For pole-zero plot, run

question6.py

g7) If we change design requirement
for overshoot to 60%,
then our closed loop system should
satisfy all of the requirements.

$$\xi = \frac{1}{\sqrt{1 + \left(\frac{\pi}{\ln(0.6)}\right)^2}}$$

$$\approx 0.16$$

$$\omega_n = \frac{80}{0.16} \approx 500$$

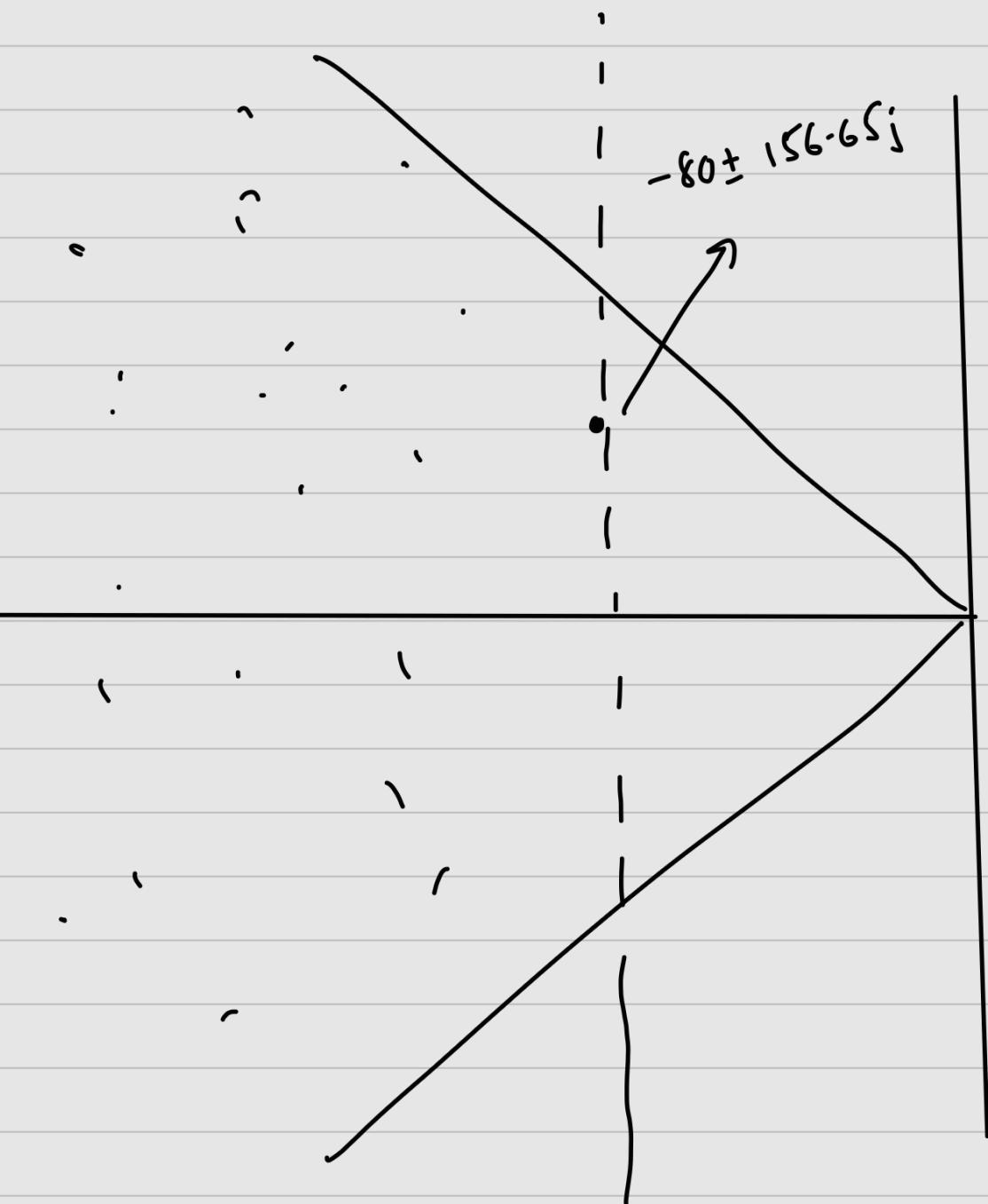
$$s = -\xi \omega_n \pm \sqrt{1 - \xi^2} \omega_n j$$

$$= -80 \pm 493.55 j$$

$$\therefore s_0 = -80 \pm 156.65 j \text{ is under}$$

$$\text{the } -80 \pm 493.55 j$$

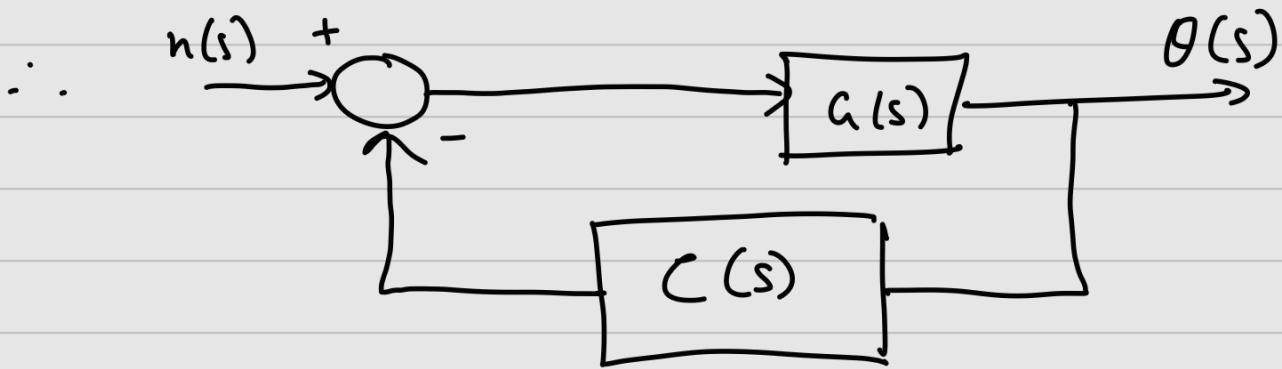
Introducing a pole at s_0
satisfies all design
requirements.



g8)

For finding $n(s)$, we put

$$\theta_d(s) = 0$$



$$\frac{\theta(s)}{n(s)} = \frac{C(s)}{1 + C(s)G(s)}$$

$$n = 67028 \cdot 47$$

$$\frac{\theta(s)}{n(s)} = \frac{(s+23)(s+362)}{s^4 + \overbrace{s^3 - 1 \cdot 19s^2 + 362s^3 + 362s^2 - 430 \cdot 78s}^{n(s^2 + 103s + 1840)} - n(s^2 + 103s + 1840)}$$

$$= \frac{(s^2 + 23s)(s + 362)}{s^4 + 363s^3 + (360 \cdot 81 + n)s^2 - (430 \cdot 78 - 103n)s + 1840n}$$

$$s^4 + 363s^3 + (360 \cdot 81 + n)s^2 - (430 \cdot 78 - 103n)s + 1840n$$

$$= \left(\frac{s^2 + 362s + 23s + 8326}{\dots} \right)$$

It is simulated in

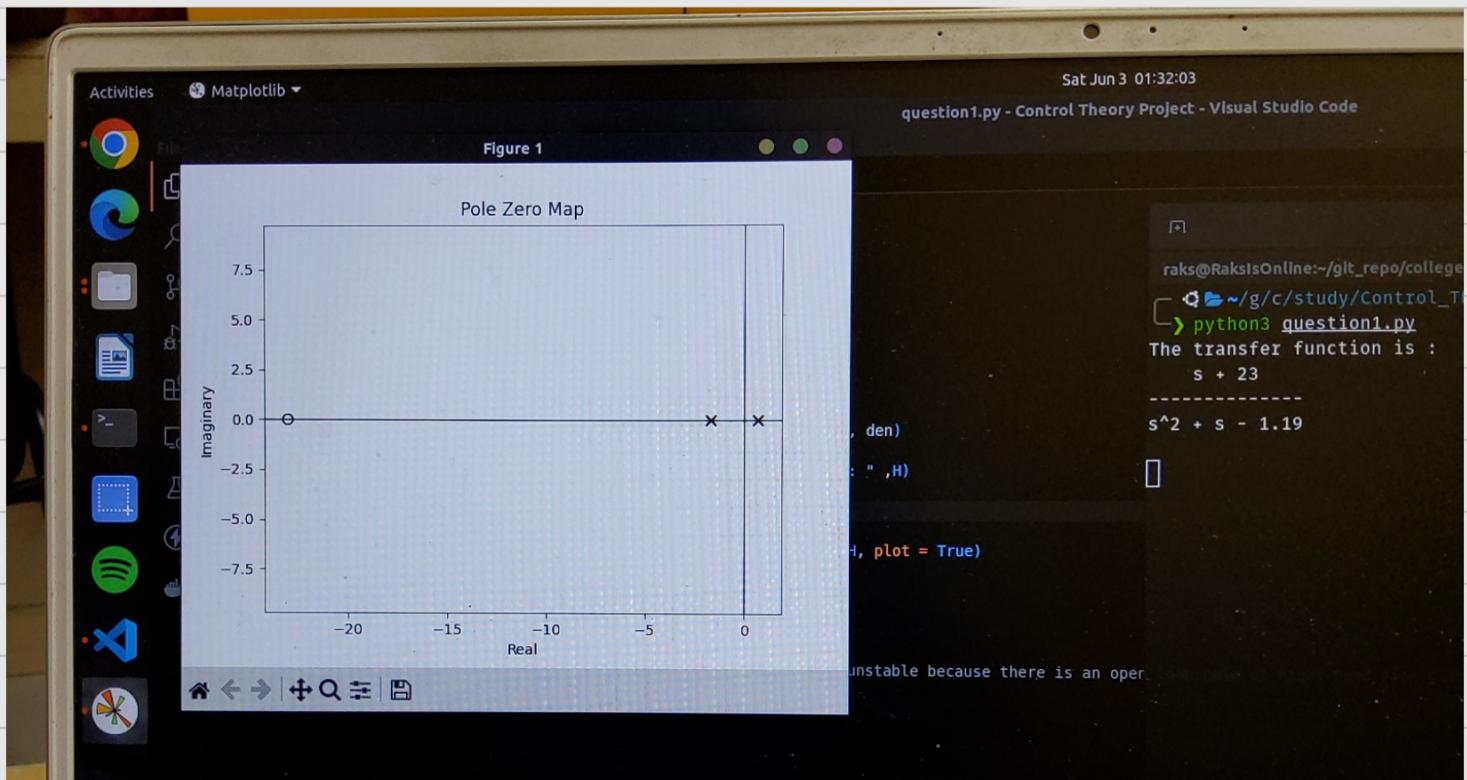
question 8-1.py.

For θ_d input,

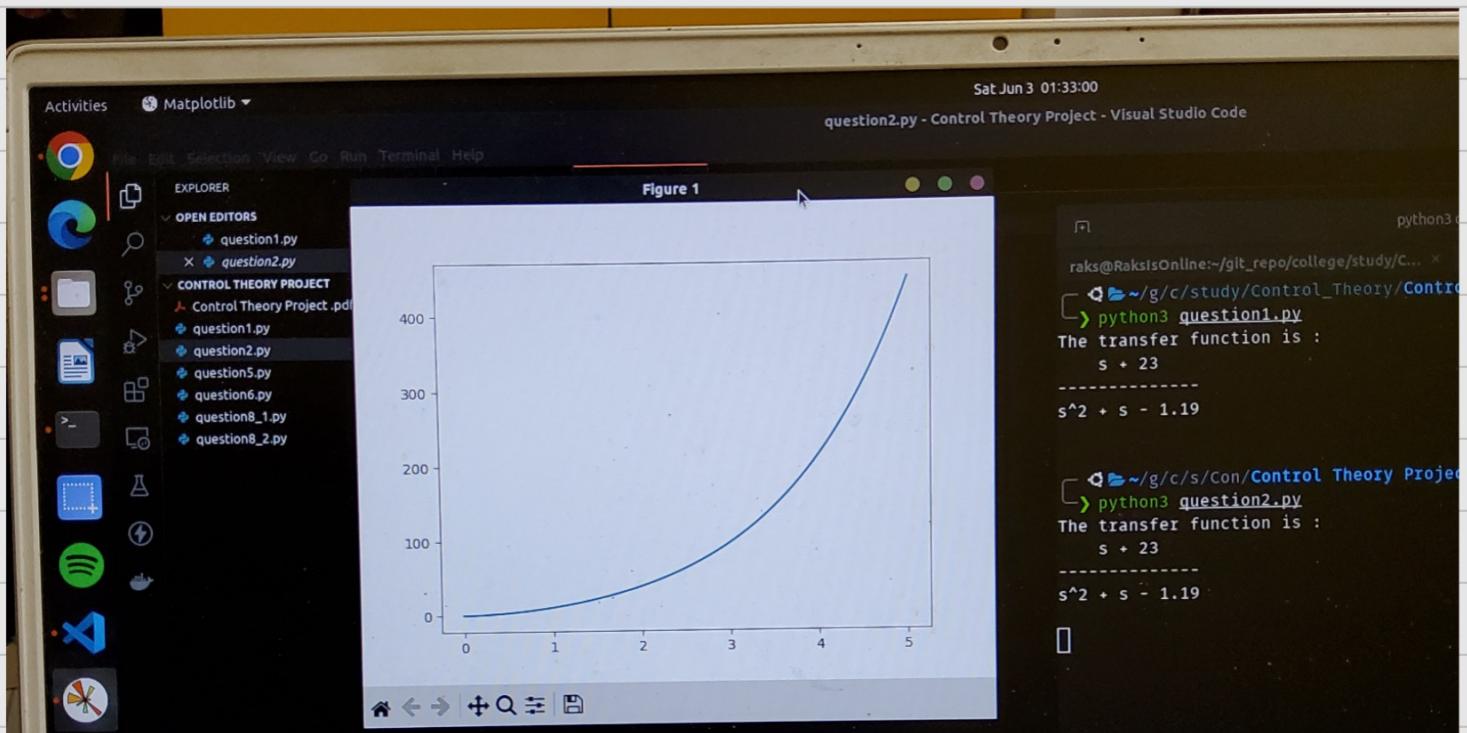
the graph is simulated

in question 8-2.py.

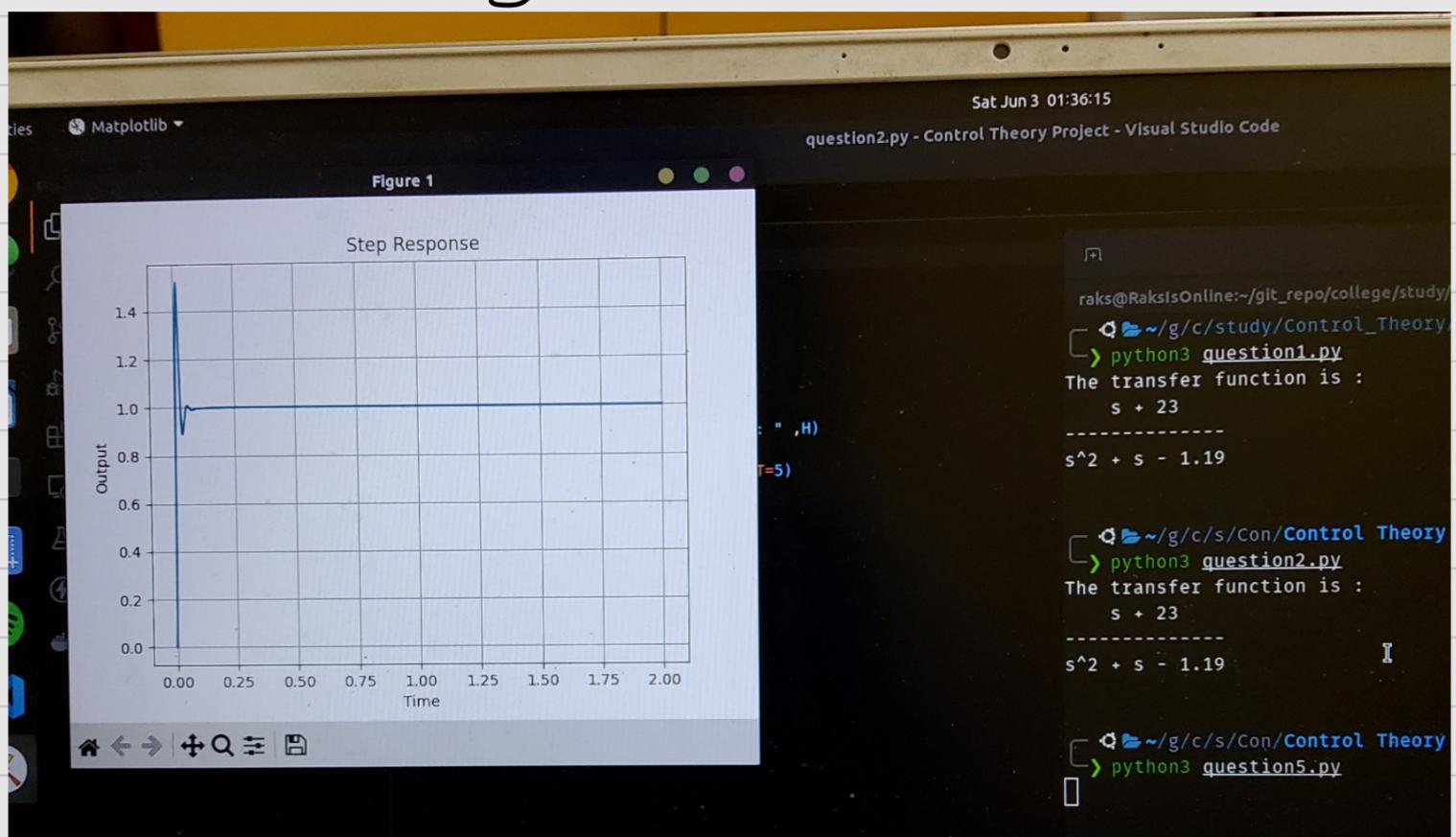
question1.py



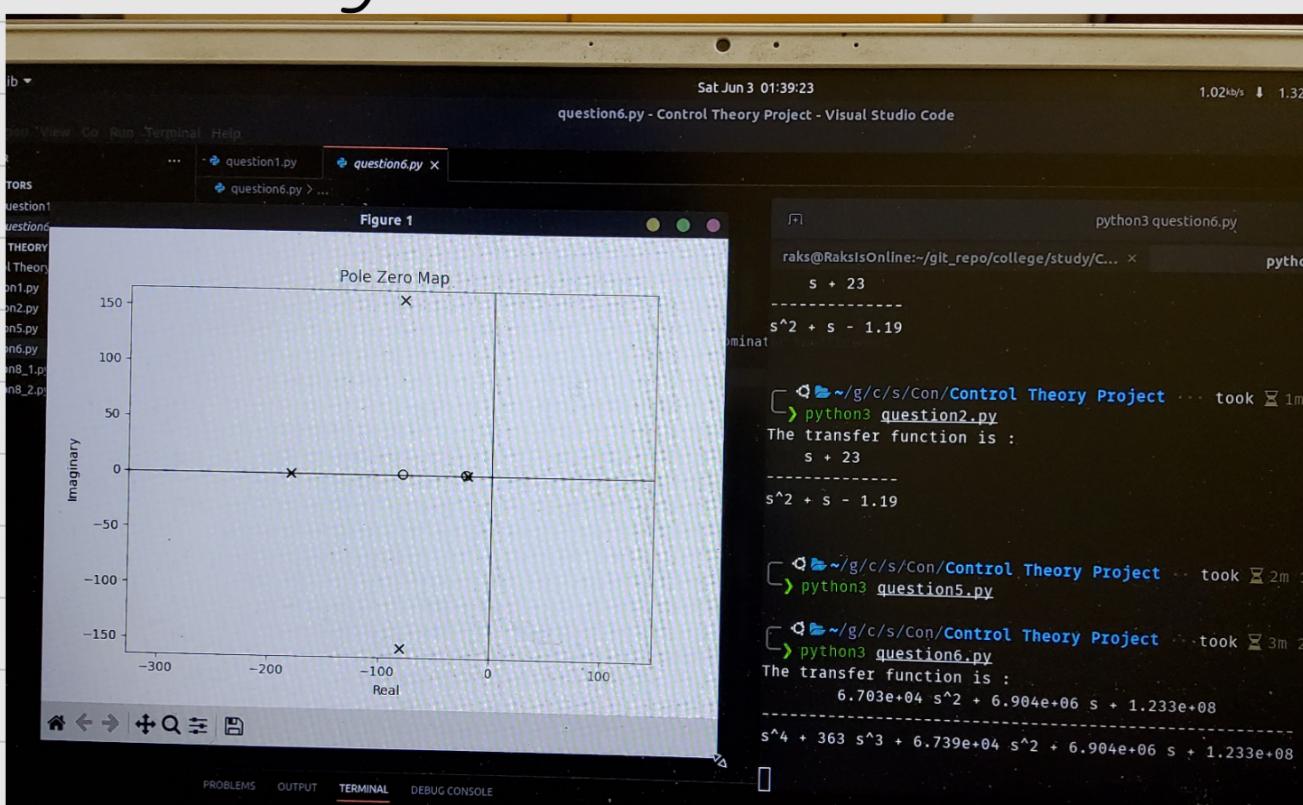
question2.py



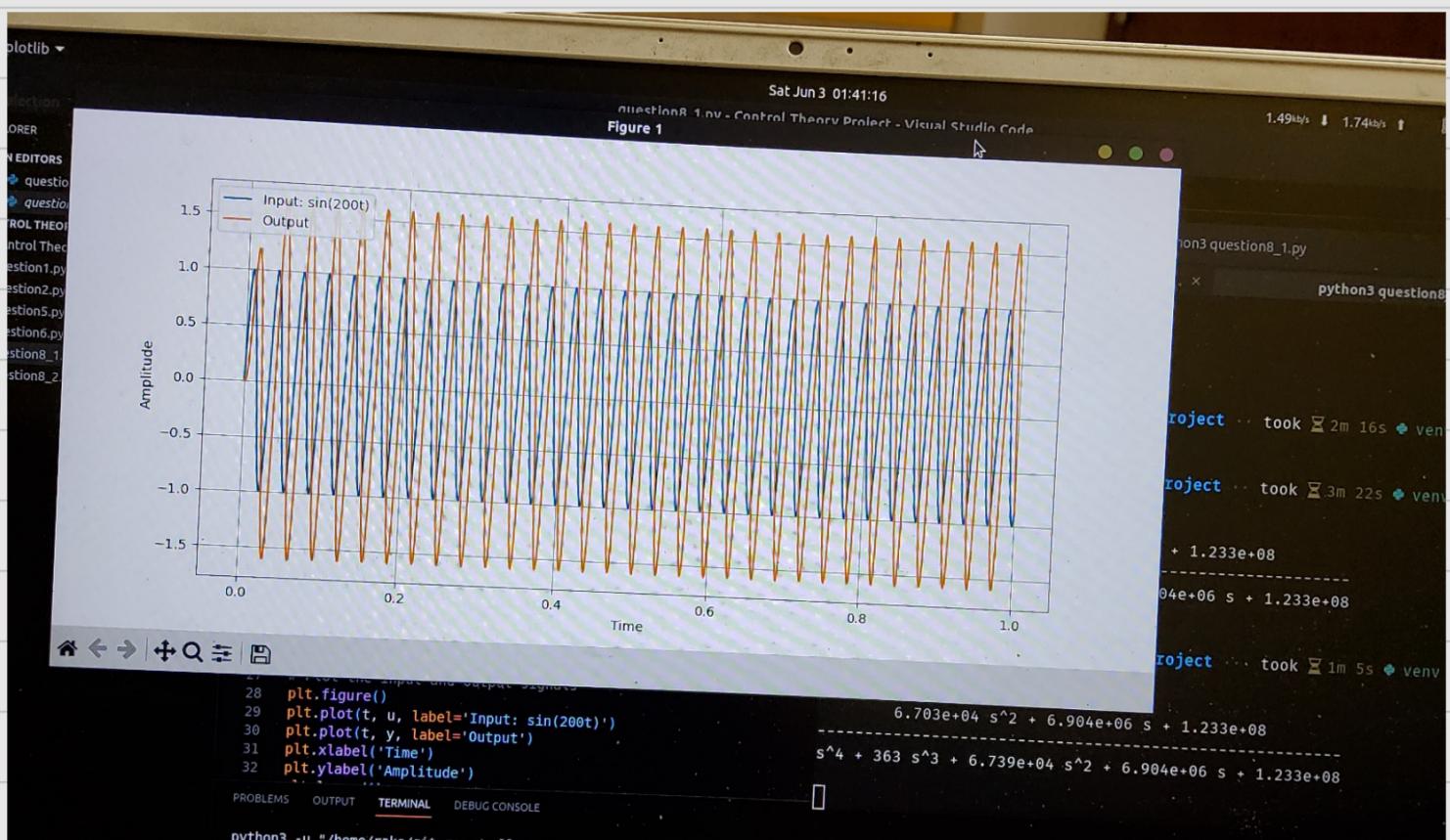
question5.py



question6.py



question 8-1.py



question 8-2.py

