

Xe129 - Rb87 Spin Exchange Optical Pumping dynamics

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1 Bloch equations

The Bloch equation for the Xe spin are

$$\frac{d\mathbf{K}}{dt} = -\gamma_{Xe} [(\mathbf{B}_0 + \mathbf{B}_d \cos(\omega_{rf}t)) + b_{KS}\mathbf{S}] \times \mathbf{K} + \Gamma_{se}(\mathbf{S} - \mathbf{K}) - \Gamma_2 \hat{x}(\hat{x} \cdot \mathbf{K}) - \Gamma_2 \hat{y}(\hat{y} \cdot \mathbf{K}) - \Gamma_1 \hat{z}(\hat{z} \cdot \mathbf{K}) \quad (1)$$

Let us assume that $b_{KS}\mathbf{S}$ is part of the DC field $\mathbf{B}_0 = B_0\hat{z}$, that $\Gamma_{se}(\mathbf{S} - \mathbf{K}) = \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix}$ and that the drive is

$$\mathbf{B}_d \cos(\omega_{rf}t) = B_d \cos(\omega_{rf}t)\hat{x}$$

Thus, we end up with the next Bloch equation

$$\frac{d\mathbf{K}}{dt} = -\gamma_{Xe} [(B_0\hat{z} + B_d \cos(\omega_{rf}t)\hat{x})] \times \mathbf{K} + R_{se}\hat{z} - \Gamma_2 \hat{x}(\hat{x} \cdot \mathbf{K}) - \Gamma_2 \hat{y}(\hat{y} \cdot \mathbf{K}) - \Gamma_1 \hat{z}(\hat{z} \cdot \mathbf{K}) \quad (2)$$

$$= -\gamma_{Xe} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ B_d \cos(\omega_{rf}t) & 0 & B_0 \\ K_x & K_y & K_z \end{vmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} - \begin{pmatrix} \Gamma_2 & 0 & 0 \\ 0 & \Gamma_2 & 0 \\ 0 & 0 & \Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} \quad (3)$$

$$= -\gamma_{Xe} \begin{pmatrix} -B_0 K_y & B_0 K_x - B_d \cos(\omega_{rf}t) K_z \\ B_d \cos(\omega_{rf}t) K_y & B_d \cos(\omega_{rf}t) K_x \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} - \begin{pmatrix} \Gamma_2 & 0 & 0 \\ 0 & \Gamma_2 & 0 \\ 0 & 0 & \Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} \quad (4)$$

$$= \begin{pmatrix} -\Gamma_2 & \gamma_{Xe} B_0 & 0 \\ -\gamma_{Xe} B_0 & -\Gamma_2 & \gamma_{Xe} B_d \cos(\omega_{rf}t) \\ 0 & -\gamma_{Xe} B_d \cos(\omega_{rf}t) & -\Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (5)$$

$$= \begin{pmatrix} -\Gamma_2 & \omega_0 & 0 \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf}t) \\ 0 & -\Omega_d \cos(\omega_{rf}t) & -\Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (6)$$

Finally, the Xe NMR dynamics can be described by the next Bloch equations

$$\begin{pmatrix} \dot{K}_x \\ \dot{K}_y \\ \dot{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & \omega_0 & 0 \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf}t) \\ 0 & -\Omega_d \cos(\omega_{rf}t) & -\Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (7)$$

Now, let us move to the rotating frame (frame of Xe) using the next transformation

$$\begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} \quad (8)$$

$$\begin{pmatrix} K_x \\ K_y \\ K_z \end{pmatrix} = \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \quad (9)$$

Also, the derivative with respect to time of the transformation is

$$\begin{pmatrix} \dot{\tilde{K}}_x \\ \dot{\tilde{K}}_y \\ \dot{\tilde{K}}_z \end{pmatrix} = \frac{d}{dt} \left[\begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \right] \quad (10)$$

$$= \frac{d}{dt} \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \quad (11)$$

$$= \omega_0 \begin{pmatrix} -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ -\cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \quad (12)$$

The Bloch equations transform as follows

$$\omega_0 \begin{pmatrix} -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ -\cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \quad (13)$$

$$\begin{pmatrix} -\Gamma_2 & \omega_0 & 0 \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_r f t) \\ 0 & -\Omega_d \cos(\omega_r f t) & -\Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (14)$$

$$\omega_0 \begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ -\cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \quad (15)$$

$$\begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\Gamma_2 & \omega_0 & 0 \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_r f t) \\ 0 & -\Omega_d \cos(\omega_r f t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (16)$$

Let us compute it separately term by term

$$\omega_0 \begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ -\cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \omega_0 \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \quad (17)$$

$$= \omega_0 \begin{pmatrix} \tilde{K}_y \\ -\tilde{K}_x \\ 0 \end{pmatrix} \quad (18)$$

Also,

$$\begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\Gamma_2 & \omega_0 & 0 \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \\ 0 & -\Omega_d \cos(\omega_{rf} t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \cos(\omega_0 t) & \sin(\omega_0 t) & 0 \\ -\sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} = \quad (19)$$

$$\begin{pmatrix} \cos(\omega_0 t) & -\sin(\omega_0 t) & 0 \\ \sin(\omega_0 t) & \cos(\omega_0 t) & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\Gamma_2 \cos(\omega_0 t) - \omega_0 \sin(\omega_0 t) & -\Gamma_2 \sin(\omega_0 t) + \omega_0 \cos(\omega_0 t) & 0 \\ -\omega_0 \cos(\omega_0 t) + \Gamma_2 \sin(\omega_0 t) & -\omega_0 \sin(\omega_0 t) - \Gamma_2 \cos(\omega_0 t) & \Omega_d \cos(\omega_{rf} t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) & -\Gamma_1 \end{pmatrix} = \quad (20)$$

$$\begin{pmatrix} -\Gamma_2 & \omega_0 & -\Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) & -\Gamma_1 \end{pmatrix} \quad (21)$$

combining the terms together we get

$$\omega_0 \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \quad (22)$$

$$\begin{pmatrix} -\Gamma_2 & \omega_0 & -\Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (23)$$

$$\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \quad (24)$$

$$\begin{pmatrix} -\Gamma_2 & \omega_0 & -\Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) \\ -\omega_0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 & -\omega_0 & 0 \\ \omega_0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} \quad (25)$$

$$+ \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (26)$$

so finally

$$\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & 0 & -\Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) \\ 0 & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_0 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_0 t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (27)$$

$$(28)$$

Notice that in the case where we transfer to a different rotating frame of reference which rotates at some frequency ω_1 , then the Bloch equations would be a bit different after the transformation

$$\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & \omega_0 - \omega_1 & -\Omega_d \cos(\omega_{rf} t) \sin(\omega_1 t) \\ -(\omega_0 - \omega_1) & -\Gamma_2 & \Omega_d \cos(\omega_{rf} t) \cos(\omega_1 t) \\ \Omega_d \cos(\omega_{rf} t) \sin(\omega_1 t) & -\Omega_d \cos(\omega_{rf} t) \cos(\omega_1 t) & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (29)$$

$$(30)$$

Using trigonometric identities we can simplify the drive terms in the Bloch matrix

$$\Omega_d \cos(\omega_{rf}t) \sin(\omega_1 t) = \frac{\Omega_d}{2} (\sin((\omega_{rf} + \omega_1)t) + \sin((\omega_{rf} - \omega_1)t)) \quad (31)$$

$$\Omega_d \cos(\omega_{rf}t) \cos(\omega_1 t) = \frac{\Omega_d}{2} (\cos((\omega_{rf} - \omega_1)t) + \cos((\omega_{rf} + \omega_1)t)) \quad (32)$$

$$(33)$$

assuming that $\omega_{rf} - \omega_1 \ll 1$, then we can use the RWA which states that fast oscillations average out to zero

$$\Omega_d \cos(\omega_{rf}t) \sin(\omega_1 t) = \frac{\Omega_d}{2} \sin(2\omega_{rf}t) = 0 \quad (34)$$

$$\Omega_d \cos(\omega_{rf}t) \cos(\omega_1 t) = \frac{\Omega_d}{2} (1 + \cos(2\omega_{rf}t)) = \frac{\Omega_d}{2} \quad (35)$$

$$(36)$$

Then, the Bloch equations with the RWA are

$$\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & \omega_0 - \omega_{rf} & 0 \\ -(\omega_0 - \omega_{rf}) & -\Gamma_2 & \frac{\Omega_d}{2} \\ 0 & -\frac{\Omega_d}{2} & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (37)$$

Next, we add to our model The effective magnetic field the Xe particles fill which produced by the alkali atoms, $b_{KS}\mathbf{S} = b_{KS}S_z\hat{z}$ and also some world rotation $\omega_{\mathbf{r}} = \omega_r\hat{z}$.

The modified equations are

$$\boxed{\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & M_{12} & 0 \\ M_{21} & -\Gamma_2 & \frac{\Omega_d}{2} \\ 0 & -\frac{\Omega_d}{2} & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix}} \quad (38)$$

where $M_{21} = -M_{12}$ and

$$M_{12} = \omega_0 + \gamma_{Xe}b_{KS}S_z + \omega_r - \omega_{rf} \quad (39)$$

$$= \gamma_{Xe}B_0 + \gamma_{Xe}b_{KS}S_z + \omega_r - \omega_{rf} \quad (40)$$

$$(41)$$

Next, let us find the steady state solution of the Bloch equations in the rotating frame with drive in \hat{x} with the RWA

$$\begin{pmatrix} \Gamma_2 & -M_{12} & 0 \\ M_{12} & \Gamma_2 & -\frac{\Omega_d}{2} \\ 0 & \frac{\Omega_d}{2} & \Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (42)$$

$$\begin{pmatrix} \Gamma_2\tilde{K}_x - M_{12}\tilde{K}_y \\ M_{12}\tilde{K}_x + \Gamma_2\tilde{K}_y - \frac{\Omega_d}{2}\tilde{K}_z \\ \frac{\Omega_d}{2}\tilde{K}_y + \Gamma_1\tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (43)$$

$$\tilde{K}_x = \frac{M_{12}}{\Gamma_2}\tilde{K}_y \quad (44)$$

$$(45)$$

$$\begin{pmatrix} \frac{M_{12}^2 + \Gamma_2^2}{\Gamma_2} \tilde{K}_y - \frac{\Omega_d}{2} \tilde{K}_z \\ \frac{\Omega_d}{2} \tilde{K}_y + \Gamma_1 \tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ R_{se} \end{pmatrix} \quad (46)$$

$$\begin{pmatrix} \left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2 \tilde{K}_y - \frac{\Omega_d}{2} \tilde{K}_z \\ \frac{\Omega_d}{2} \tilde{K}_y + \Gamma_1 \tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ R_{se} \end{pmatrix} \quad (47)$$

$$\left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2 \tilde{K}_y = \frac{\Omega_d}{2} \tilde{K}_z \quad (48)$$

$$\tilde{K}_y = \frac{\frac{\Omega_d}{2}}{\left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2} \tilde{K}_z \quad (49)$$

$$(50)$$

$$\frac{\Omega_d}{2} \tilde{K}_y + \Gamma_1 \tilde{K}_z = R_{se} \quad (51)$$

$$\frac{\Omega_d}{2} \frac{\frac{\Omega_d}{2}}{\left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2} \tilde{K}_z + \Gamma_1 \tilde{K}_z = R_{se} \quad (52)$$

$$\frac{\frac{\Omega_d^2}{4} + \left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2 \Gamma_1}{\left(1 + (M_{12}/\Gamma_2)^2\right) \Gamma_2} \tilde{K}_z = R_{se} \quad (53)$$

$$\frac{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)}{\left(1 + (M_{12}/\Gamma_2)^2\right) / \Gamma_1} \tilde{K}_z = R_{se} \quad (54)$$

$$\tilde{K}_z = \frac{R_{se}}{\Gamma_1} \frac{\left(1 + (M_{12}/\Gamma_2)^2\right)}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} \quad (55)$$

$$\tilde{K}_y = \frac{\Omega_d}{2\Gamma_2} \frac{R_{se}}{\Gamma_1} \frac{1}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} \quad (56)$$

$$\tilde{K}_x = \frac{M_{12}}{\Gamma_2} \frac{\Omega_d}{2\Gamma_2} \frac{R_{se}}{\Gamma_1} \frac{1}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} \quad (57)$$

Finally, the solution to the Bloch equation (eq.(38)) is

$$\boxed{\begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \frac{\frac{R_{se}}{\Gamma_1}}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} \begin{pmatrix} \frac{M_{12}}{\Gamma_2} \frac{\Omega_d}{2\Gamma_2} \\ \frac{\Omega_d}{2\Gamma_2} \\ \left(1 + (M_{12}/\Gamma_2)^2\right) \end{pmatrix}} \quad (58)$$

In the case where $M_{12} = 0$ we get

$$\begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \frac{\frac{R_{se}}{\Gamma_1}}{1 + \frac{\Omega_d^2}{4\Gamma_2\Gamma_1}} \begin{pmatrix} 0 \\ \frac{\Omega_d}{2\Gamma_2} \\ 1 \end{pmatrix} \quad (59)$$

Recall that we measure the transverse spin polarization. Let us compute the optimal drive amplitude for maximal \tilde{K}_y polarization

$$\frac{d\tilde{K}_y}{d\Omega_d} = \frac{R_{se}}{2\Gamma_2\Gamma_1} \frac{1}{1 + \frac{\Omega_d^2}{4\Gamma_2\Gamma_1}} - \frac{R_{se}}{2\Gamma_2\Gamma_1} \frac{\Omega_d^2}{\Gamma_2\Gamma_1} \frac{1}{\left(1 + \frac{\Omega_d^2}{4\Gamma_2\Gamma_1}\right)^2} = 0 \quad (60)$$

we get the next optimal drive amplitude

$$\Omega_d^{\text{optimal}} = \sqrt{\frac{4\Gamma_2\Gamma_1}{3}}$$

for the optimal drive, the \hat{z} polarization would be

$$\tilde{K}_z = \frac{3R_{se}}{4\Gamma_1}$$

We can make the same calculation in the case where $M_{12} \neq 0$

$$\frac{d\tilde{K}_y}{d\Omega_d} = \frac{R_{se}}{2\Gamma_2\Gamma_1} \frac{1}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} - \frac{R_{se}}{2\Gamma_2\Gamma_1} \frac{\Omega_d^2}{\Gamma_2\Gamma_1} \frac{1}{\left(\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)\right)^2} = 0 \quad (61)$$

in that case the optimal drive amplitude is

$$\Omega_d^{\text{optimal}} = \sqrt{\frac{4\Gamma_2\Gamma_1}{3}} \sqrt{1 + (M_{12}/\Gamma_2)^2} \quad (62)$$

Just for sports we can also solve the case of drive in \hat{y} , the Bloch equations in that case are

$$\boxed{\frac{d}{dt} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & M_{12} & -\frac{\Omega_d}{2} \\ M_{21} & -\Gamma_2 & 0 \\ \frac{\Omega_d}{2} & 0 & -\Gamma_1 \end{pmatrix} \begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix}} \quad (63)$$

then the steady state solution would be

$$\begin{pmatrix} \Gamma_2\tilde{K}_x - M_{12}\tilde{K}_y + \frac{\Omega_d}{2}\tilde{K}_z \\ M_{12}\tilde{K}_x + \Gamma_2\tilde{K}_y \\ -\frac{\Omega_d}{2}\tilde{K}_x + \Gamma_1\tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (64)$$

$$\tilde{K}_y = -\frac{M_{12}}{\Gamma_2}\tilde{K}_x$$

$$\begin{pmatrix} \frac{\Gamma_2^2 + M_{12}^2}{\Gamma_2}\tilde{K}_x + \frac{\Omega_d}{2}\tilde{K}_z \\ -\frac{\Omega_d}{2}\tilde{K}_x + \Gamma_1\tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ R_{se} \end{pmatrix} \quad (65)$$

$$\begin{pmatrix} \left(1 + (M_{12}/\Gamma_2)^2\right)\Gamma_2\tilde{K}_x + \frac{\Omega_d}{2}\tilde{K}_z \\ -\frac{\Omega_d}{2}\tilde{K}_x + \Gamma_1\tilde{K}_z \end{pmatrix} = \begin{pmatrix} 0 \\ R_{se} \end{pmatrix} \quad (66)$$

$$\tilde{K}_x = -\frac{\Omega_d}{2} \frac{1}{\left(1 + (M_{12}/\Gamma_2)^2\right)\Gamma_2} \tilde{K}_z$$

$$\tilde{K}_z = \frac{R_{se}}{\Gamma_1} \frac{\left(1 + (M_{12}/\Gamma_2)^2\right)}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)}$$

so finally,

$$\begin{pmatrix} \tilde{K}_x \\ \tilde{K}_y \\ \tilde{K}_z \end{pmatrix} = \frac{\frac{R_{se}}{\Gamma_1}}{\frac{\Omega_d^2}{4\Gamma_2\Gamma_1} + \left(1 + (M_{12}/\Gamma_2)^2\right)} \begin{pmatrix} -\frac{\Omega_d}{2\Gamma_2} \\ \frac{M_{12}}{\Gamma_2} \frac{\Omega_d}{2\Gamma_2} \\ \left(1 + (M_{12}/\Gamma_2)^2\right) \end{pmatrix} \quad (67)$$

2 NMR Gyroscope (NMRG)

Using the Xenon NMR model (the Bloch equations) we can implement a gyroscope which measures rotation along the primary axis of the system (in the case above: \hat{z}). Following Walker's notation in [WL16], we break the spin dynamics into two components, parallel and perpendicular to the primary axis \hat{z}

$$\mathbf{K} = K_z \hat{z} + \mathbf{K}_\perp$$

describing \mathbf{K}_\perp using a phasor notation

$$K_+ = K_x + iK_y = K_\perp e^{-i\phi}$$

where

$$K_\perp = \sqrt{K_x^2 + K_y^2} \quad , \quad \phi = \arctan\left(\frac{K_y}{K_x}\right)$$

Now, if we solve for ϕ in the rotating frame of the drive, from eq.(67) we get

$$\phi = \arctan\left(\frac{\tilde{K}_y}{\tilde{K}_x}\right) = \arctan\left(-\frac{M_{12}}{\Gamma_2}\right) \quad (68)$$

for small phase, where $M_{12} \ll 1$ the phase can be approximated with its zeroth order Taylor expansion

$$\phi = -\frac{M_{12}}{\Gamma_2}$$

unfolding M_{12} we get

$$\phi = -\frac{\gamma_{Xe}B_0}{\Gamma_2} - \frac{\gamma_{Xe}b_{KS}S_z}{\Gamma_2} - \frac{\omega_r}{\Gamma_2} + \frac{\omega_{rf}}{\Gamma_2}$$

In a real life NMR system we would also have some magnetic noise in the primary axis $\gamma_{Xe}B_{noise}$, so the phase would be

$$\phi = -\frac{\gamma_{Xe}B_0}{\Gamma_2} - \frac{\gamma_{Xe}B_{noise}}{\Gamma_2} - \frac{\gamma_{Xe}b_{KS}S_z}{\Gamma_2} - \frac{\omega_r}{\Gamma_2} + \frac{\omega_{rf}}{\Gamma_2}$$

all these parameters could in general be time dependent. Notice that in the phase equation we have two unknown parameters: fluctuations of the magnetic field B_{noise} and the world rotation ω_r . In order to extract the world rotation from the phase measurements we need to introduce another specie.

2.1 Dual species open-loop NMRG scheme

Having a system with two species, Xe129 and Xe131, we can compute the world rotation as follows

$$\phi_{129} = -\frac{\gamma_{Xe}^{129}B_0}{\Gamma_2^{129}} - \frac{\gamma_{Xe}^{129}B_{noise}}{\Gamma_2^{129}} - \frac{\gamma_{Xe}^{129}b_{KS}S_z}{\Gamma_2^{129}} - \frac{\omega_r}{\Gamma_2^{129}} + \frac{\omega_{rf}^{129}}{\Gamma_2^{129}} \quad (69)$$

$$\phi_{131} = -\frac{\gamma_{Xe}^{131}B_0}{\Gamma_2^{131}} - \frac{\gamma_{Xe}^{131}B_{noise}}{\Gamma_2^{131}} - \frac{\gamma_{Xe}^{131}b_{KS}S_z}{\Gamma_2^{131}} - \frac{\omega_r}{\Gamma_2^{131}} + \frac{\omega_{rf}^{131}}{\Gamma_2^{131}} \quad (70)$$

Then, subtracting the two equations we get

$$\frac{1}{\gamma_{Xe}^{129}} (\phi_{129} \Gamma_2^{129} - \omega_{rf}^{129}) - \frac{1}{\gamma_{Xe}^{131}} (\phi_{131} \Gamma_2^{131} - \omega_{rf}^{131}) = \omega_r \left(\frac{1}{\gamma_{Xe}^{131}} - \frac{1}{\gamma_{Xe}^{129}} \right) \quad (71)$$

and finally the world rotation in an open-loop setting is given by

$$\omega_r = \left[\frac{\gamma_{Xe}^{129} \gamma_{Xe}^{131}}{\gamma_{Xe}^{129} - \gamma_{Xe}^{131}} \right] \left[\frac{1}{\gamma_{Xe}^{129}} (\phi_{129} \Gamma_2^{129} - \omega_{rf}^{129}) - \frac{1}{\gamma_{Xe}^{131}} (\phi_{131} \Gamma_2^{131} - \omega_{rf}^{131}) \right] \quad (72)$$

A scheme of such dual species open-loop system is illustrated in Fig.(1).

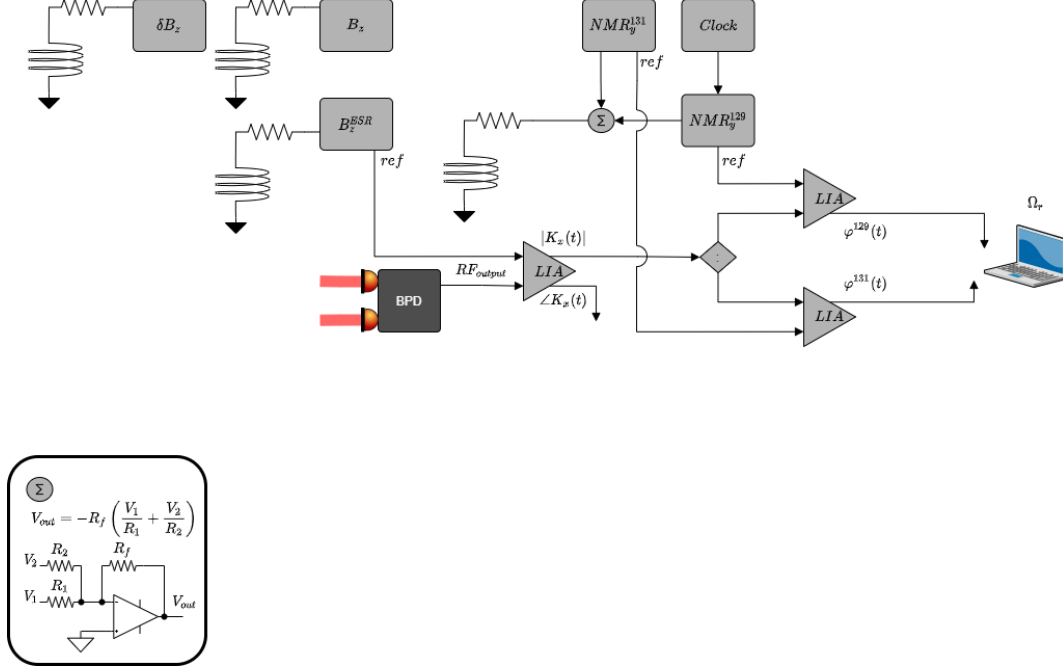


Figure 1: Dual species NMRG open-loop scheme. The Alkali signal is measured in a Balanced Photo detector (BPD) which is then inserted into a Lock-in amplifier (LIA) with a parametric modulation (B_t^{ESSR}) reference. The amplitude extracted from the LIA channel is the Xenon dynamic which is then been splitted and inserted into two more LIAs with two NMR drive references (NMR_y^{129} NMR_y^{131}) one for each Xenon. The two phases extracted from the LIAs are the two Xenon phase differences from their drive signals. These phase signals can be used to compute the world rotation in \hat{z} following eq.(72). B_z and $B_{\delta z}$ are the DC and modulation of the longitudinal magnetic field.

2.2 Dual species closed-loop NMRG scheme

In a Closed-Loop scheme we keep the phase of the spins with respect to the drive constant. To be partially-consistent with Walker in [WL16], we define the constant phase difference as β . Then, $\phi - \beta$ would be the actual accumulated phase of the drive. But, different from Walker we will solve the dynamics in the rotating frame. This means that in our case ϕ stands for the phase accumulated between the drive and the spins in the rotating frame of reference of the spins, so in resonance it is meant to be small, $\phi \approx 0$. Walker solve the dynamics in the lab frame of reference so there, $\phi \approx \frac{\pi}{2}$ for optimal drive (explained in [sine driven damped harmonic oscillator](#)). Also, where Walker uses Ω_z we substitute $M_{12} = \Omega_z - \Omega_d$.

Finally, Walker define a constant phase difference (in the lab frame) $\phi - \beta \approx \frac{\pi}{2}$ so he multiply the drive with $\sin(\phi - \beta) \approx 1$. In our case (in the rotating frame) $\phi - \beta \approx 0$ so we need to multiply the drive with $\cos(\phi - \beta) \approx 1$.

Therefore, the previous solution to ϕ does not hold anymore so we need to solve the Closed-Loop NMRG dynamics in a formal way from the top. Then, in the rotating frame (from eq.(63, we drop the tilde sign for convenience))

$$\frac{dK_+}{dt} = \frac{dK_x}{dt} + i \frac{dK_y}{dt} \quad (73)$$

$$\frac{d}{dt} (K_\perp e^{-i\phi}) = -\Gamma_2 K_x + M_{12} K_y - \frac{\Omega_d}{2} \cos(\phi - \beta) K_z + i M_{21} K_x - i \Gamma_2 K_y \quad (74)$$

$$e^{-i\phi} \frac{dK_\perp}{dt} + K_\perp \frac{d}{dt} e^{-i\phi} = -(\Gamma_2 + i M_{12}) K_x - i(\Gamma_2 + i M_{12}) K_y - \frac{\Omega_d}{2} \cos(\phi - \beta) K_z \quad (75)$$

$$\left(\frac{dK_\perp}{dt} - i K_\perp \frac{d\phi}{dt} \right) e^{-i\phi} = -(\Gamma_2 + i M_{12}) (K_x + i K_y) - \frac{\Omega_d}{2} \cos(\phi - \beta) K_z \quad (76)$$

$$\left(\frac{dK_\perp}{dt} - i K_\perp \frac{d\phi}{dt} \right) e^{-i\phi} = -(\Gamma_2 + i M_{12}) K_\perp e^{-i\phi} - \frac{\Omega_d}{2} \cos(\phi - \beta) K_z \quad (77)$$

$$\frac{dK_\perp}{dt} - i K_\perp \frac{d\phi}{dt} = -(\Gamma_2 + i M_{12}) K_\perp - \frac{\Omega_d}{2} \cos(\phi - \beta) K_z e^{i\phi} \quad (78)$$

$$(79)$$

Now we break the equation into real and imaginary parts such that

$$K_\perp \frac{d\phi}{dt} = M_{12} K_\perp + \frac{\Omega_d}{2} K_z \cos(\phi - \beta) \sin(\phi) \quad (80)$$

$$\frac{dK_\perp}{dt} = -\Gamma_2 K_\perp - \frac{\Omega_d}{2} K_z \cos(\phi - \beta) \cos(\phi) \quad (81)$$

arranging the terms, we get

$$\frac{d\phi}{dt} = M_{12} + \frac{\Omega_d}{2} \frac{K_z}{K_\perp} \cos(\phi - \beta) \sin(\phi) \quad (82)$$

$$\frac{dK_\perp}{dt} = -\Gamma_2 K_\perp - \frac{\Omega_d}{2} K_z \cos(\phi - \beta) \cos(\phi) \quad (83)$$

recall

$$\cos(\phi - \beta) \sin(\phi) = \frac{1}{2} \sin(2\phi - \beta) - \frac{1}{2} \sin(-\beta) = \frac{1}{2} \sin(\beta) \quad (84)$$

$$\cos(\phi - \beta) \cos(\phi) = \frac{1}{2} \cos(-\beta) - \frac{1}{2} \cos(2\phi - \beta) = \frac{1}{2} \cos(\beta) \quad (85)$$

where twice the phase oscillations, 2ϕ , quickly average to zero over time so we end up with

$$\frac{d\phi}{dt} = M_{12} + \frac{\Omega_d}{4} \frac{K_z}{K_\perp} \sin(\beta) \quad (86)$$

$$\frac{dK_\perp}{dt} = -\Gamma_2 K_\perp - \frac{\Omega_d}{4} K_z \cos(\beta) \quad (87)$$

Therefore, solving for steady state transverse polarization

$$\boxed{K_\perp = -\frac{\Omega_d}{4\Gamma_2} K_z \cos(\beta)} \quad (88)$$

such that

$$\boxed{\frac{d\phi}{dt} = M_{12} - \Gamma_2 \tan(\beta)} \quad (89)$$

while, the longitudinal steady state polarization is given by

$$0 = \frac{dK_z}{dt} = -\frac{\Omega_d}{2} \cos(\phi - \beta) K_x - \Gamma_1 K_z + R_{se} \quad (90)$$

$$0 = -\frac{\Omega_d}{2} \cos(\phi - \beta) \sqrt{K_\perp^2 - K_y^2} - \Gamma_1 K_z + R_{se} \quad (91)$$

$$0 = -\frac{\Omega_d}{2} \cos(\phi - \beta) \sqrt{\frac{\Omega_d^2}{16\Gamma_2^2} K_z^2 \cos^2(\beta) - K_y^2} - \Gamma_1 K_z + R_{se} \quad (92)$$

$$0 = -\frac{\Omega_d^2 \cos(\beta) \cos(\phi - \beta)}{8\Gamma_2} \sqrt{1 - \left(\frac{4\Gamma_1}{\Omega_d \cos(\beta)}\right)^2 \left(\frac{K_y}{K_z}\right)^2} K_z - \Gamma_1 K_z + R_{se} \quad (93)$$

$$0 = -\frac{\Omega_d^2 \cos(\beta)}{16\Gamma_2} \sqrt{1 - \left(\frac{4\Gamma_1}{\Omega_d \cos(\beta)}\right)^2 \left(\frac{K_y}{K_z}\right)^2} K_z - \Gamma_1 K_z + R_{se} \quad (94)$$

$$K_z = \frac{R_{se}}{\Gamma_1 + \frac{\Omega_d^2 \cos^2(\beta)}{16\Gamma_2} \sqrt{1 - \left(\frac{4\Gamma_1}{\Omega_d \cos(\beta)}\right)^2 \left(\frac{K_y}{K_z}\right)^2}} \quad (95)$$

recall that we define the drive to be in the \hat{y} direction so we maximize the K_x polarization and minimize K_y so in the case of optimal drive (eq.(62)) and small β we get that

$$K_z \approx \frac{R_{se}}{\Gamma_1 + \frac{\Omega_d^2 \cos^2(\beta)}{16\Gamma_2}} \quad (96)$$

notice that we got the same results as in [WL16] up to few modification caused because we solve the dynamics in rotating frame of reference. The Bloch equations in the lab frame of reference would have drive amplitude Ω_d instead of $\frac{\Omega_d}{2}$ and $\phi \rightarrow \phi - \frac{\pi}{2}$. These changes will results in a lab frame of reference solution

$$\boxed{\begin{aligned} K_\perp &= \frac{\Omega_d}{2\Gamma_2} K_z \cos(\beta) \\ K_z &= \frac{R_{se}}{\Gamma_1 + \frac{\Omega_d^2 \cos^2(\beta)}{4\Gamma_2}} \\ \frac{d\phi}{dt} &= \omega_0 - \Gamma_2 \tan(\beta) \end{aligned}} \quad (97)$$

same as in [WL16]. we can now see that when the gyro is in a steady state the averaged spin is tipped from the \hat{z} axis with an angle

$$\Theta = \arctan\left(\frac{K_\perp}{K_z}\right) = \frac{\Omega_d \cos(\beta)}{2\Gamma_2} \quad (98)$$

2.3 Closing the Loop

Now recall that β is the phase leg of the drive with respect to the gyro so we can write it as follows $\theta = \phi - \beta$, where now θ is the phase of the drive and ϕ is the gyro phase, both in the lab frame of reference (see Fig.2). For small enough phase difference between the two, we can write the phase precession in eq.(97) as follows

$$\frac{d\phi}{dt} = \omega_0 - \Gamma_2(\beta) \quad (99)$$

$$= \omega_0 + \Gamma_2(\theta - \phi) \quad (100)$$

In a closed-loop NMRG configuration we use negative feedback to lock the phase leg β to a constant value $\beta = \beta_0$. Though, in the most general case the phase leg would be

$$\beta(t) = \beta_0 + \epsilon(t) \quad (101)$$

We can compute the small deviation feedback relation for the drive using eqs.(100)(101)

$$\frac{d\theta}{dt} = \frac{d\phi}{dt} - \frac{d\beta}{dt} \quad (102)$$

$$\frac{d\theta}{dt} = \frac{d\phi}{dt} - \frac{d\epsilon(t)}{dt} \quad (103)$$

$$\frac{d\theta}{dt} = \Omega_z - \Gamma_2(\beta_0 + \epsilon(t)) - \frac{d\epsilon(t)}{dt} \quad (104)$$

$$\frac{d\theta}{dt} = \omega_0 - \frac{\epsilon(t)}{T_2} - \frac{d\epsilon(t)}{dt} \quad (105)$$

where $\omega_0 = \Omega_z - \Gamma_2\beta_0$ is the clock-derived frequency.

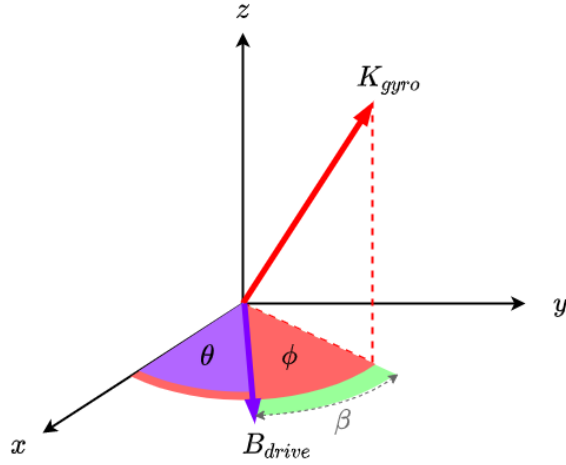


Figure 2: NMRG phase dynamics in the lab frame of reference illustration. ϕ and θ are the gyro and drive phases respectively, while β is the phase leg of the drive from the gyro.

There are few ways to use feedback in a dual-species NMRG configuration. One way is to lock the bias magnetic field to match a clock-derived NMR Xenon drive signal. We do that by keeping the gyro phase (ϕ) locked to the NMR drive phase (θ) by measuring the phase difference between the two (β) and using negative feedback to change the bias magnetic field (B_0) in a way that locks the phase difference to a constant value (β_0) using a PID controller following the next relation

$$B_0^{(t+1)} = B_0^{(t)} - K_p \underbrace{\left[\epsilon(t) + \frac{1}{T_i} \int_{t_i}^t \epsilon(t') dt' + T_d \frac{d\epsilon(t)}{dt} \right]}_{\delta B_0^{(t)}} \quad (106)$$

where T_i and T_d are the integration and derivative times respectively. We can extract $\epsilon(t)$ from the measurement of β following eq.(101). Another way is to use the same technique to lock the NMR drive frequency.

2.4 PID

PID generator with python

$$\beta_t = \phi_t - \theta_t = \phi_t - \phi_{t-1} = \Delta\phi$$

3 Alkali Dynamics - ESR

The Block equation for the Alkali (Rb87) spin are given by

$$\frac{d\mathbf{S}}{dt} = \gamma_A [(B_0 + B_1 \cos(\omega_1 t)) \hat{z} + b_{SK} \mathbf{K}] \times \mathbf{S} + \Gamma_{se} (\mathbf{K} - \mathbf{S}) - \Gamma_2 \hat{x} (\hat{x} \cdot \mathbf{S}) - \Gamma_2 \hat{y} (\hat{y} \cdot \mathbf{S}) - \Gamma_1 \hat{z} (\hat{z} \cdot \mathbf{S}) \quad (107)$$

In a matrix form

$$\begin{pmatrix} \dot{S}_x \\ \dot{S}_y \\ \dot{S}_z \end{pmatrix} = \begin{pmatrix} -\Gamma_2 & -\omega_0 - \Omega_1 \cos(\omega_1 t) - \gamma_A b_{SK} K_z & \gamma_A b_{SK} K_y \\ \omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z & -\Gamma_2 & -\gamma_A b_{SK} K_x \\ -\gamma_A b_{SK} K_y & \gamma_A b_{SK} K_x & -\Gamma_1 \end{pmatrix} \cdot \begin{pmatrix} S_x \\ S_y \\ S_z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ R_{se} \end{pmatrix} \quad (108)$$

thus,

$$\dot{S}_+ = -\Gamma_2 S_x - (\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z) S_y + \gamma_A b_{SK} K_y S_z \quad (109)$$

$$+ i(\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z) S_x - i\Gamma_2 S_y - i\gamma_A b_{SK} K_x S_z \quad (110)$$

$$\dot{S}_+ = [-\Gamma_2 + i(\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z)] S_+ - i\gamma_A b_{SK} (K_x + iK_y) S_z \quad (111)$$

$$\dot{S}_+ = [-\Gamma_2 + i(\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z)] S_+ - i\gamma_A b_{SK} K_+ S_z \quad (112)$$

$$(113)$$

moving to the oscillating frame of reference $S_+ = A_+ e^{i\mu_1}$, where $\mu_1 = \frac{\Omega_1}{\omega_1} \sin(\omega_1 t)$ we get

$$\dot{A}_+ e^{i\mu_1} + i\dot{\mu}_1 e^{i\mu_1} A_+ = [-\Gamma_2 + i(\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z)] A_+ e^{i\mu_1} - i\gamma_A b_{SK} K_+ S_z \quad (114)$$

$$\dot{A}_+ + i\Omega_1 \cos(\omega_1 t) A_+ = [-\Gamma_2 + i(\omega_0 + \Omega_1 \cos(\omega_1 t) + \gamma_A b_{SK} K_z)] A_+ - i\gamma_A b_{SK} K_+ S_z e^{-i\mu_1} \quad (115)$$

$$\dot{A}_+ = [-\Gamma_2 + i(\omega_0 + \gamma_A b_{SK} K_z)] A_+ - i\gamma_A b_{SK} K_+ S_z e^{-i\mu_1} \quad (116)$$

we use the Jacobi-Anger expansion $e^{iz \sin(\theta)} = \sum_{n=-\infty}^{\infty} J_n(z) e^{in\theta}$, using the Bessel function relation $J_{-n}(z) = (-1)^n J_n(z)$

$$e^{\pm iz \sin(\theta)} = J_0(z) \pm 2i \sum_{n=0}^{\infty} J_{2n+1}(z) \sin((2n+1)\theta) + 2 \sum_{n=1}^{\infty} J_{2n}(z) \cos(2n\theta) \quad (117)$$

so finally

$$e^{-i\mu_1} = J_0\left(\frac{\Omega_1}{\omega_1}\right) + 2iJ_1\left(\frac{\Omega_1}{\omega_1}\right) \sin(\omega_1 t) + 2J_2\left(\frac{\Omega_1}{\omega_1}\right) \cos(2\omega_1 t) + \dots \quad (118)$$

Substituting this expansion back into eq.(116)

$$\dot{A}_+ = [-\Gamma_2 + i(\omega_0 + \gamma_A b_{SK} K_z)] A_+ \quad (119)$$

$$- i\gamma_A b_{SK} K_+ S_z \left[J_0\left(\frac{\Omega_1}{\omega_1}\right) + 2iJ_1\left(\frac{\Omega_1}{\omega_1}\right) \sin(\omega_1 t) + 2J_2\left(\frac{\Omega_1}{\omega_1}\right) \cos(2\omega_1 t) + \dots \right] \quad (120)$$

Next we would like to transform to the Fourier space so it would be easier to do so with the Jacobi-Anger expansion exponential notation, then $\mathcal{F}[e^{-in\omega_1 t}] = \sqrt{2\pi} \delta(\omega - n\omega_1)$ and

$$i\omega A_+(\omega) = [-\Gamma_2 + i(\omega_0 + \gamma_A b_{SK} K_z)] A_+(\omega) - i\gamma_A b_{SK} K_+ S_z \sum_{n=-\infty}^{\infty} J_n\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \delta(\omega + n\omega_1) \quad (121)$$

$$(122)$$

finally

$$A_+(\omega) = \frac{-i\gamma_A b_{SK} K_+ S_z}{\Gamma_2 + i(\omega - \omega_0 - \gamma_A b_{SK} K_z)} \sum_{n=-\infty}^{\infty} J_n\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \delta(\omega + n\omega_1) \quad (123)$$

Next we swallow the $\gamma_A b_{SK} K_z$ term into ω_0 , and placing the $\frac{1}{\omega - \omega_0}$ inside the sum

$$A_+(\omega) = -i\gamma_A b_{SK} K_+ S_z \sum_{n=-\infty}^{\infty} J_n\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \frac{\delta(\omega + n\omega_1)}{\Gamma_2 + i(\omega - \omega_0)} \quad (124)$$

$$= -i\gamma_A b_{SK} K_+ S_z \sum_{n=-\infty}^{\infty} J_n\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \frac{\delta(\omega + n\omega_1)}{\Gamma_2 + i(n\omega_1 - \omega_0)} \quad (125)$$

$$= -\frac{i\gamma_A b_{SK} K_+ S_z}{\Gamma_2} \sum_{n=-\infty}^{\infty} J_n\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \frac{\delta(\omega + n\omega_1)}{1 + i\frac{(n\omega_1 - \omega_0)}{\Gamma_2}} \quad (126)$$

Now, if $\omega_1 - \omega_0 \ll \Gamma_2 \ll \omega_0$, we are left only with the J_{-1} term in the sum

$$A_+(\omega) = -\frac{i\gamma_A b_{SK} K_+ S_z}{\Gamma_2} J_{-1}\left(\frac{\Omega_1}{\omega_1}\right) \sqrt{2\pi} \delta(\omega - \omega_1) \quad (127)$$

back to the time domain

$$A_+ = -\frac{i\gamma_A b_{SK} K_+ S_z}{\Gamma_2} J_{-1}\left(\frac{\Omega_1}{\omega_1}\right) e^{i\omega_1 t} \quad (128)$$

going back to the lab frame of reference while keeping only the $n < 3$ Bessel terms in the expansion
=

$$A_+ = -\frac{i\gamma_A b_{SK} J_{-1} K_+ S_z}{\Gamma_2} e^{i\omega_1 t} \quad (129)$$

$$S_+ = -\frac{i\gamma_A b_{SK} J_{-1} K_+ S_z}{\Gamma_2} e^{i\omega_1 t} e^{i\mu_1} \quad (130)$$

$$S_+ = -\frac{i\gamma_A b_{SK} J_{-1} K_+ S_z}{\Gamma_2} e^{i\omega_1 t} [J_0 + 2iJ_1 \sin(\omega_1 t) + 2J_2 \cos(2\omega_1 t)] \quad (131)$$

recall that we only care about the S_x part of the transverse signal

$$S_x + iS_y = -\frac{i\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} (K_x + iK_y) (\cos(\omega_1 t) + i \sin(\omega_1 t)) [J_0 + 2iJ_1 \sin(\omega_1 t) + 2J_2 \cos(2\omega_1 t)] \quad (132)$$

so

$$S_x = -\frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left[(i)^4 2K_y J_1 \sin(\omega_1 t) \sin(\omega_1 t) \right] \quad (133)$$

$$+ (i)^2 K_y \cos(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \quad (134)$$

$$+ (i)^2 K_x \sin(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \quad (135)$$

$$+ (i)^2 2K_x \cos(\omega_1 t) J_1 \sin(\omega_1 t) \quad (136)$$

$$S_x = -\frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left[K_y J_1 (1 - \cos(2\omega_1 t)) \right] \quad (137)$$

$$- K_y (J_0 \cos(\omega_1 t) + J_2 \cos(-\omega_1 t) + J_2 \cos(3\omega_1 t)) \quad (138)$$

$$- K_x (J_0 \sin(\omega_1 t) + J_2 \sin(3\omega_1 t) + J_2 \sin(-\omega_1 t)) \quad (139)$$

$$- K_x J_1 (\sin(2\omega_1 t)) \quad (140)$$

Next, assuming Lock-in detection of S_x with a reference signal $\cos(\omega_1 t + \alpha)$, then every term which is factored with a sine / cosine function (after using trigonometric product→sum identities) will be averaged out to zero, such that we are left with the next relation

$$\langle S_x \cos(\omega_1 t + \alpha) \rangle = \frac{\gamma_A b_{SK} J_{-1} S_z}{2\Gamma_2} [K_y \cos(\alpha) (J_0 + J_2) + K_x \sin(\alpha) (-J_0 + J_2)] \quad (141)$$

which is the same Lock-in relation put out in [WL16]. We can get a less course Lock-in relation by returning back to eq.(126) and keeping another term in the approximation, such that we take

$$\frac{1}{1 + i \frac{(n\omega_1 - \omega_0)}{\Gamma_2}} \approx 1 - i \frac{(n\omega_1 - \omega_0)}{\Gamma_2} \quad (142)$$

then, assigning eq.(141) with $S_x^{(0)}$, let us calculate the additional term to $S_x = S_x^{(0)} + S_x^{(1)}$ using eq.(132)

$$S_x^{(1)} + iS_y^{(1)} = -\frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left(\frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) (K_x + iK_y) (\cos(\omega_1 t) + i \sin(\omega_1 t)) [J_0 + 2iJ_1 \sin(\omega_1 t) + 2J_2 \cos(2\omega_1 t)] \quad (143)$$

we need only $S_x^{(1)}$

$$S_x^{(1)} = -\frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left(\frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) \left[(i)^2 K_y \cos(\omega_1 t) 2J_1 \sin(\omega_1 t) \right. \quad (144)$$

$$+ (i)^2 K_y \sin(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \quad (145)$$

$$+ (i)^2 K_x \sin(\omega_1 t) 2J_1 \sin(\omega_1 t) \quad (146)$$

$$\left. + K_x \cos(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \right] \quad (147)$$

$$S_x^{(1)} = \frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left(\frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) \left[2J_1 K_y \cos(\omega_1 t) \sin(\omega_1 t) \right. \quad (148)$$

$$+ K_y \sin(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \quad (149)$$

$$+ 2J_1 K_x \sin(\omega_1 t) \sin(\omega_1 t) \quad (150)$$

$$\left. - K_x \cos(\omega_1 t) (J_0 + 2J_2 \cos(2\omega_1 t)) \right] \quad (151)$$

$$S_x^{(1)} = \frac{\gamma_A b_{SK} J_{-1} S_z}{\Gamma_2} \left(\frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) \left[J_1 K_y \sin(2\omega_1 t) \right. \quad (152)$$

$$+ K_y (J_0 \sin(\omega_1 t) + J_2 \sin(3\omega_1 t) + J_2 \sin(-\omega_1 t)) \quad (153)$$

$$+ J_1 K_x (1 - \cos(2\omega_1 t)) \quad (154)$$

$$\left. - K_x (J_0 \cos(\omega_1 t) + J_2 \cos(-\omega_1 t) + J_2 \cos(3\omega_1 t)) \right] \quad (155)$$

Computing the addition to the Lock-in measurement

$$\langle S_x^{(1)} \cos(\omega_1 t + \alpha) \rangle = \frac{\gamma_A b_{SK} J_{-1} S_z}{2\Gamma_2} \left(\frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) [K_y \sin(\alpha) (-J_0 + J_2) - K_x \cos(\alpha) (J_0 + J_2)] \quad (156)$$

finally, putting all together

$$\langle (S_x^{(0)} + S_x^{(1)}) \cos(\omega_1 t + \alpha) \rangle = \frac{\gamma_A b_{SK} J_{-1} S_z}{2\Gamma_2} \left[\left(K_x + K_y \frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) \sin(\alpha) (-J_0 + J_2) \right. \quad (157)$$

$$\left. + \left(K_y - K_x \frac{(\omega_1 - \omega_0)}{\Gamma_2} \right) \cos(\alpha) (J_0 + J_2) \right] \quad (158)$$

In an on resonance working point $\omega_1 = \omega_0$, and the measured signal would be

$$\langle (S_x^{(0)} + S_x^{(1)}) \cos(\omega_1 t + \alpha) \rangle = \frac{\gamma_A b_{SK} J_0 J_{-1} S_z}{\Gamma_2} K_y \cos(\alpha) \quad (159)$$

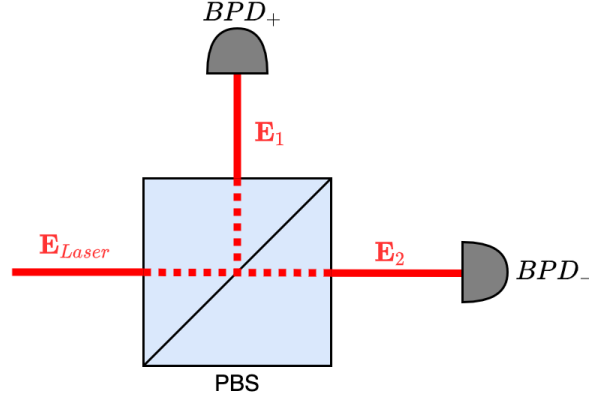


Figure 3: Faraday Rotation measurement optical setup using a PBS with a BPD.

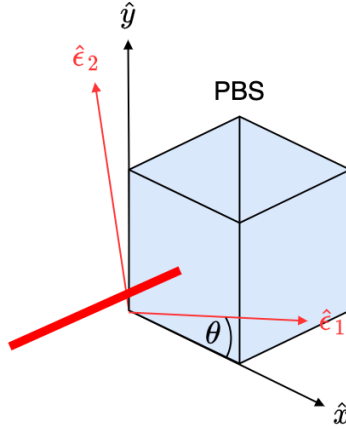


Figure 4: Laser to PBS frame of reference transformation.

4 Balanced Photo Diode Measurement

In this section we will describe a Faraday Rotation measurement technique using a Balanced Photo Diode (BPD) with a Polarized Beam Splitter (PBS). The optical setup is illustrated in Fig.3.

We start by stating the frames of reference that we are going to use in the following computation. The PBS frame is described by (\hat{x}, \hat{y}) , while the laser polarization frame described by (\hat{e}_1, \hat{e}_2) with the following transformation

$$\begin{cases} \hat{e}_1 &= \cos \theta \hat{x} + \sin \theta \hat{y} \\ \hat{e}_2 &= -\sin \theta \hat{x} + \cos \theta \hat{y} \end{cases} \quad (160)$$

the transformation is illustrated in Fig.4.

The Laser's electromagnetic field is given by

$$\mathbf{E}_{\text{Laser}}(z, t) = E_0 (\alpha \hat{e}_1 + e^{i\delta} \beta \hat{e}_2) e^{i(kz - \omega t)} \quad (161)$$

where $\{E_0, \alpha, \beta, \delta\} \in \mathbb{R}$. Next we use the transformation in (160) to describe the laser polarization in the frame of reference of the PBS. Therefore eq.(163) become

$$\mathbf{E}_{\text{Laser}}(z, t) = E_0 [\alpha \cos \theta \hat{x} + \alpha \sin \theta \hat{y} - \beta e^{i\delta} \sin \theta \hat{x} + \beta e^{i\delta} \cos \theta \hat{y}] e^{i(kz - \omega t)} \quad (162)$$

$$= E_0 [(\alpha \cos \theta - \beta e^{i\delta} \sin \theta) \hat{x} + (\alpha \sin \theta + \beta e^{i\delta} \cos \theta) \hat{y}] e^{i(kz - \omega t)} \quad (163)$$

Next we define the PBS transmission matrix as follows

$$\mathbf{T} = \begin{bmatrix} \frac{1}{2} - \epsilon & 0 \\ 0 & \frac{1}{2} + \epsilon \end{bmatrix} \quad (164)$$

where we have a 50 – 50 transmission-reflection up to a small $\epsilon \ll 1$. Therefore, the electromagnetic field after the PBS is given by

$$\begin{cases} \mathbf{E}_1 = (\mathbf{T}\mathbf{E}_{\text{Laser}} \cdot \hat{x}) \hat{x} = E_0 [\alpha \cos \theta - e^{i\delta} \beta \sin \theta] \left(\frac{1}{2} - \epsilon\right) \hat{x} \\ \mathbf{E}_2 = (\mathbf{T}\mathbf{E}_{\text{Laser}} \cdot \hat{y}) \hat{y} = E_0 [\alpha \sin \theta + e^{i\delta} \beta \cos \theta] \left(\frac{1}{2} + \epsilon\right) \hat{y} \end{cases} \quad (165)$$

Now let us calculate the laser intensity measured in the RF channel of the BPD, which is given by $I_{RF} = I_1 - I_2$, thus

$$I_{RF} = I_1 - I_2 \quad (166)$$

$$\propto \mathbf{E}_1 \cdot \mathbf{E}_1 - \mathbf{E}_2 \cdot \mathbf{E}_2 \quad (167)$$

$$= E_0^2 [\alpha^2 \cos^2 \theta + \beta^2 \sin^2 \theta - 2\alpha\beta \cos \theta \sin \theta \cos \delta] \left(\frac{1}{2} - \epsilon\right)^2 \quad (168)$$

$$- E_0^2 [\alpha^2 \sin^2 \theta + \beta^2 \cos^2 \theta + 2\alpha\beta \cos \theta \sin \theta \cos \delta] \left(\frac{1}{2} + \epsilon\right)^2 \quad (169)$$

$$= E_0^2 \left[(\alpha^2 - \beta^2) (\cos^2 \theta - \sin^2 \theta) \left(\frac{1}{4} + \epsilon^2\right) - (\alpha^2 + \beta^2) \epsilon - 4\alpha\beta \cos \theta \sin \theta \cos \delta \left(\frac{1}{4} + \epsilon^2\right) \right] \quad (170)$$

$$= E_0^2 \left[[(\alpha^2 - \beta^2) (\cos^2 \theta - \sin^2 \theta) - 4\alpha\beta \cos \theta \sin \theta \cos \delta] \left(\frac{1}{4} + \epsilon^2\right) - (\alpha^2 + \beta^2) \epsilon \right] \quad (171)$$

$$= E_0^2 \left[[(\alpha^2 - \beta^2) (\cos(2\theta)) - 2\alpha\beta \sin(2\theta) \cos \delta] \left(\frac{1}{4} + \epsilon^2\right) - (\alpha^2 + \beta^2) \epsilon \right] \quad (172)$$

$$\stackrel{\epsilon \ll 1}{\approx} E_0^2 \left[[(\alpha^2 - \beta^2) (\cos(2\theta)) - 2\alpha\beta \sin(2\theta) \cos \delta] \frac{1}{4} - (\alpha^2 + \beta^2) \epsilon \right] \quad (173)$$

$$= \boxed{\frac{E_0^2}{4} [(\alpha^2 - \beta^2) (\cos(2\theta)) - 2\alpha\beta \sin(2\theta) \cos \delta - 4(\alpha^2 + \beta^2) \epsilon]} \quad (174)$$

Now let us analyze eq.(174). The left term corresponds to the laser polarization in the laser frame of reference. If $\alpha^2 = \beta^2$ the laser polarization prime axis would be at 45° (in the laser frame of reference) and this term would be zero. The middle term is the *real* RF signal, δ would be the amount of laser circular polarization. For $\delta = 0$ we get laser light with linear polarization and then the RF signal corresponds to twice the polarization angle of incidence. The right term corresponds to the quality of the PBS, where for a perfect PBS we get 50-50 transmission-reflection with $\epsilon = 0$ and this term would be also zero.

Finally, for a perfect PBS, and perfectly linear laser polarization at 45° (in the laser frame of reference), the RF signal would be

$$\boxed{I_{RF} = -\frac{E_0^2}{2} \sin(2\theta)} \quad (175)$$

References

- [WL16] Thad G Walker and Michael S Larsen. Spin-exchange-pumped nmr gyros. *Advances in atomic, molecular, and optical physics*, 65:373–401, 2016.