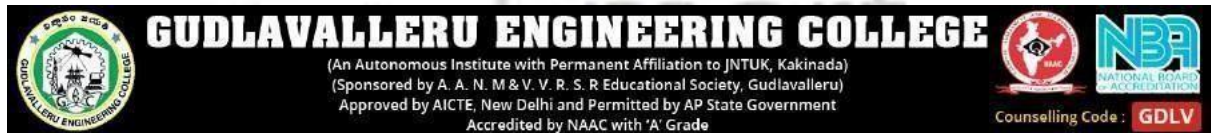


Internship Program Report

By

NERUSU VIJAY KUMAR - 18481A0268



In association with



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Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil & Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical



sessions and Industrial Automation projects.

Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Mr. G. Srinivasa Rao – Internship

coordinator Mr. Ramesh V – Mentor

Mr. Vinay Kumar – System Support

Mr. Harikanth – Software/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May

2021 Daily schedule time shall be 4 PM to 6.30 PM

Mode of Classes: Online through ZOOM Pres

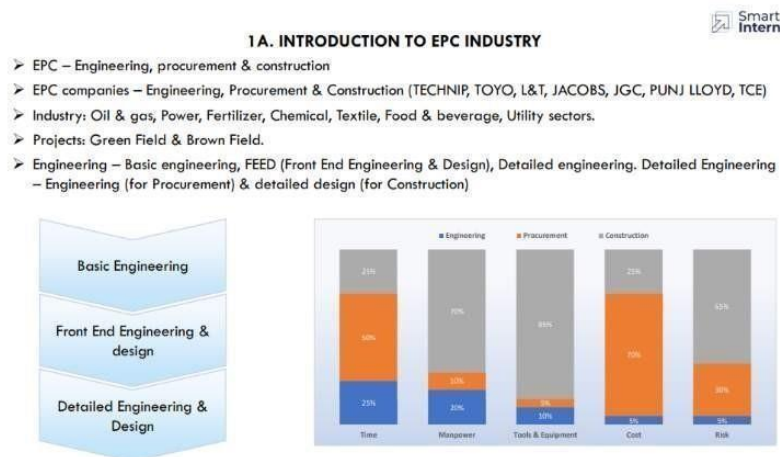
enter: Mr. Ramesh V

Internshipprogram

We have been given the opportunity to learn and interact with industry experienced engineering specialists to learn the Electrical detailed design engineering for various industrial sectors.

3rd May 2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry	Introduction
		Engineering	Types of Engineering
		Procurement	Engineering role in procurement
		Construction	Engineering role during construction



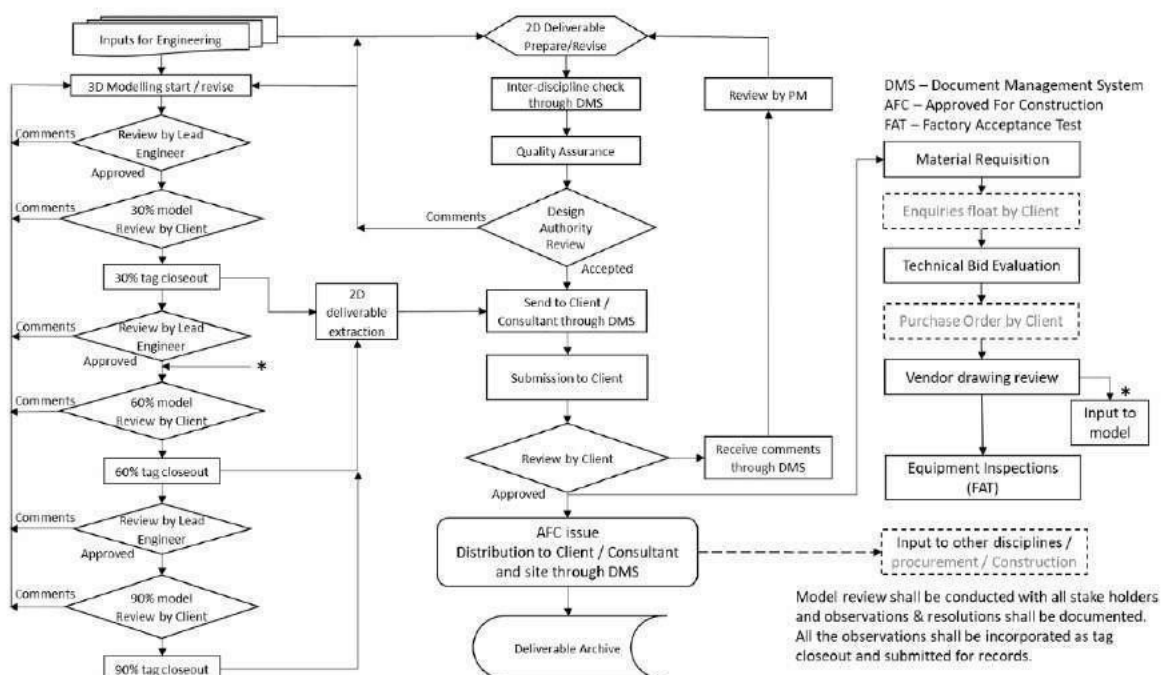
Topic details:

Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4thMay2021:Engineeringdocumentation forEPCprojects

2	Electrical Design Documentation	Engineering Deliverables list	Sequence of deliverables
		Detailed Engineering workflow	Detailed engineering process
		Document transmission	Documents submission and info exchange
		Deliverable types	Different types of deliverables

3. ELECTRICAL DESIGN & DETAILED ENGINEERING - PROCESS



Topic details:

Engineering deliverables list, detailed engineering flow, engineering support flow, engineering support to procurements.

5thMay2021:Engineeringdocumentationforcommandsandformulae

3	Document & Drawingtools	MSWord	Report/Calculations formats
		MSExcel	Basicexcelcommands
		Autocad	Basic line diagrams and layoutcommends

3C. AUTOCAD BASIC COMMANDS

A AUTOCAD BASIC KEYS							
STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINE TYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
{ 0,0; 1000,1000 }		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+D	HORIZONTAL	HOR			
COMMAND WIN	Ctrl+9	VERTICAL	VER			

**Topic details:**

Here we need to learn the basis of the autocad basic keys like standard, modify, draw, format, papersize etc..

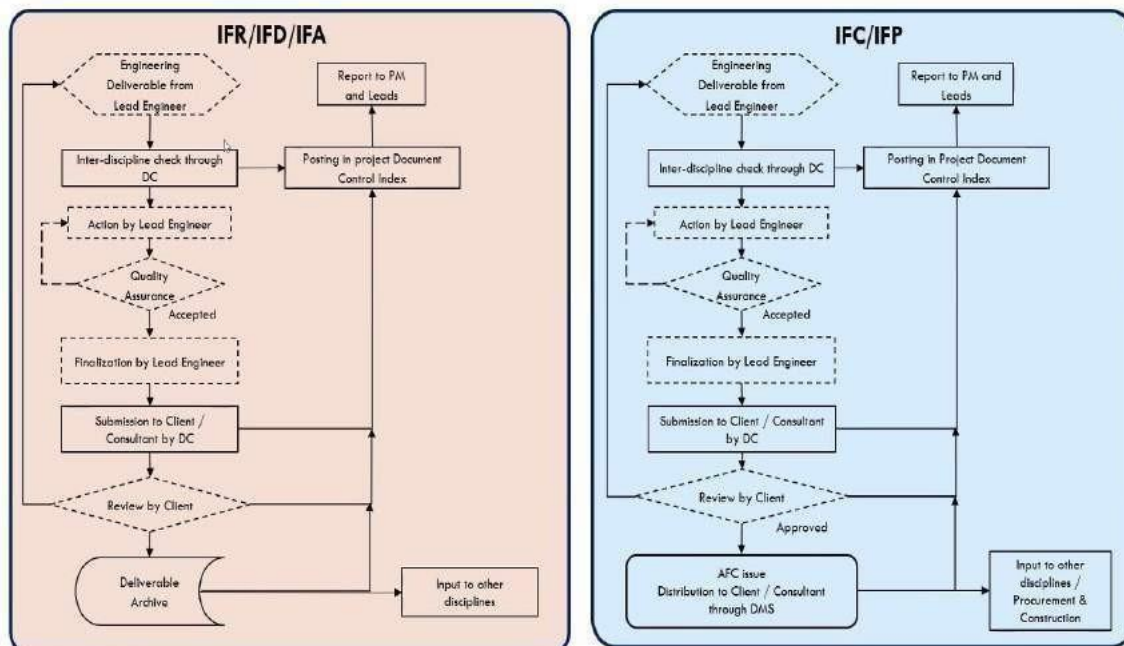
7thMay2021:EngineeringdocumentationforElectricalsystemdesign

4	Electrical system design for a small project	Overall plant description
		Sequence of approach
		Approach to detailed design

Topic details:



1C. DETAILED ENGINEERING



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

11thMay2021:ClassificationofTransformersandGenerators

6	Classificationof Transformers andGenerators	Different types ofTransformers	DifferenttypesofGenerators
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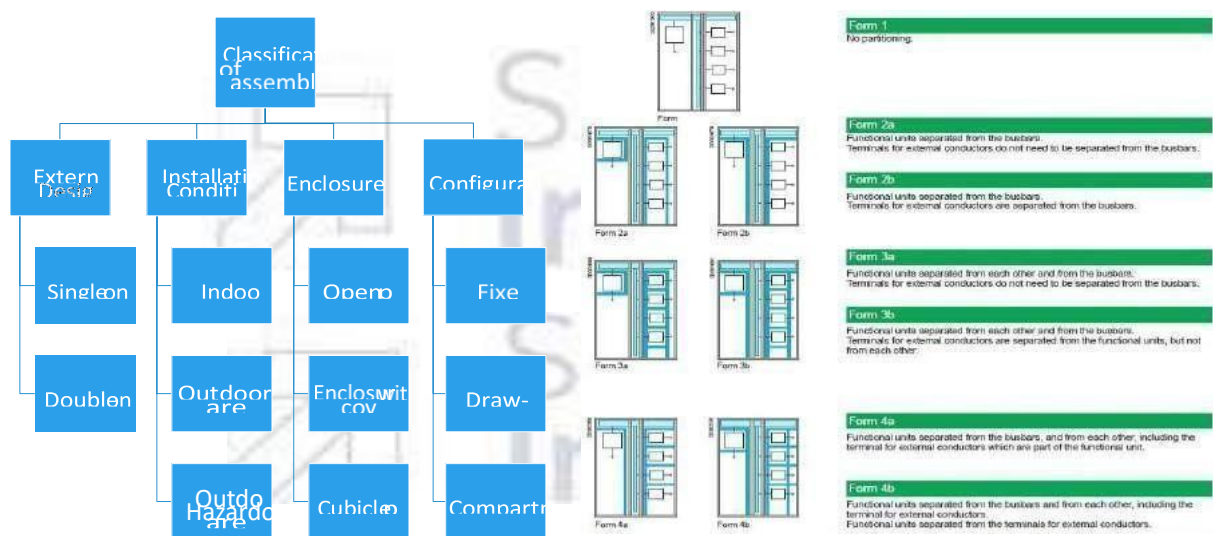


Topicdetails:

ClassificationofTransformersandGenerators

12th May 2021: Classification of Switchgear construction and power factor improvement

7	Classification of Switchgear construction and power factor improvement	Different types of Switchgear assemblies	Power factor improvement

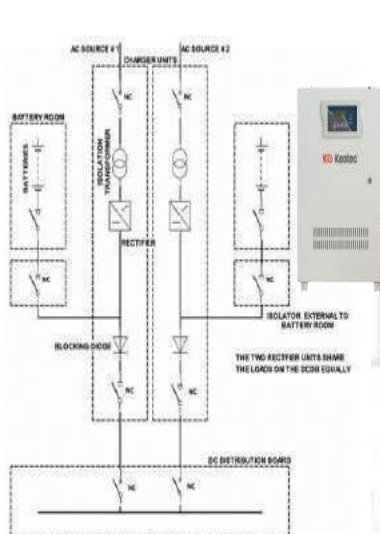


Topic details:

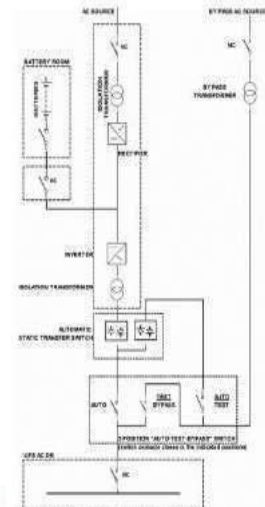
Classification of Switchgear construction and Power Factor Improvement

17thMay2021:DetailingaboutUPSsystemandBusducts.

8	Detailing aboutUPS system andBusducts	Uninterruptiblepowersupplys system	Busdutsofthesystem
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110Vor220VDC
UPSSystem



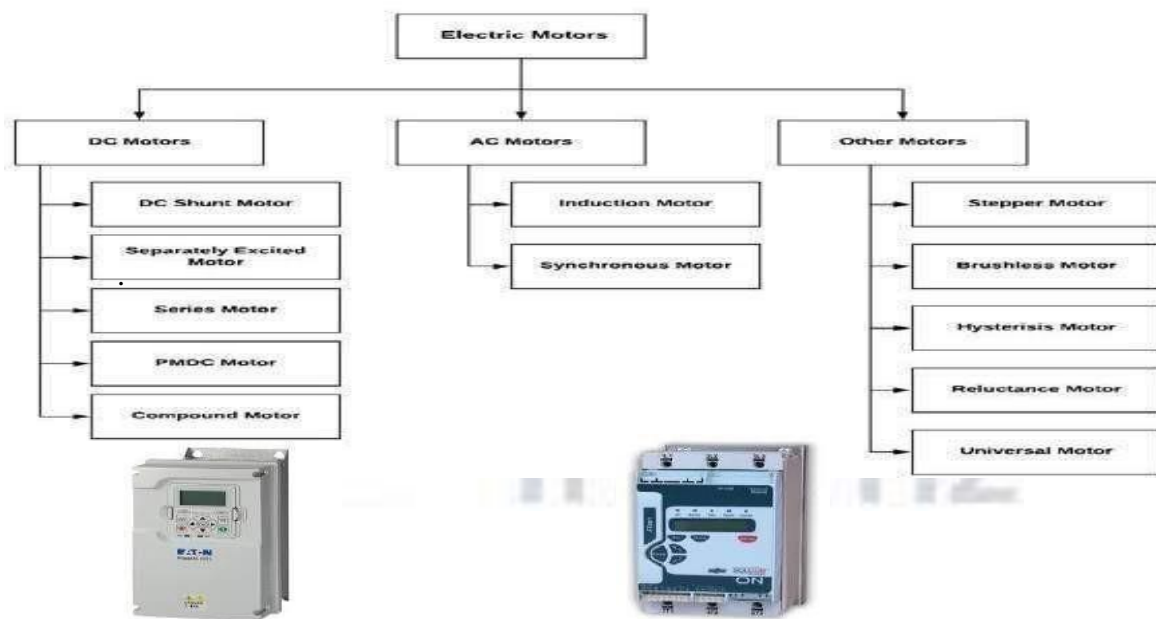
110Vor230V
ACUPSSystem

Topic details:PowerdistributionofUPSsystemandBusducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost vs. need.

18thMay2021:DetailingaboutMotorStarters andSizingofmotors.

9	Detailing about MotorStarters and Sizing ofmotors	Motor startersanddrives	Sizingandselectionof motors
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Topic details:DetailingaboutMotorStarterandSizingofmotorsand theirselection.

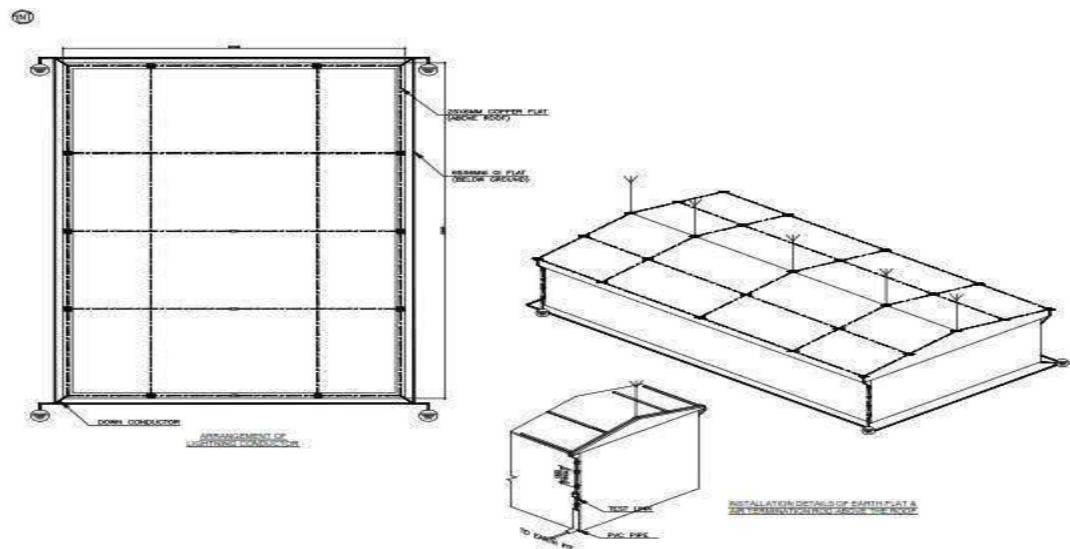
The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter

19thMay2021:DiscribingaboutEarthingsystemandLightingProtection.

10	DiscribingaboutEarthingsystem and LightingProtection.	PlantEarthingsystem	LightingProtectionmaterials
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Topic details: Discribing about Earthings system and Lighting Protection.

Lightning protection required for high rise structures and important buildings against lightning currents during thunderstorms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20thMay2021:Lightingorilluminationssystemsandcalculations.

11	Lightingor Illumination systems and Calculations	Lightingorilluminationssystems	Lightingcalculations
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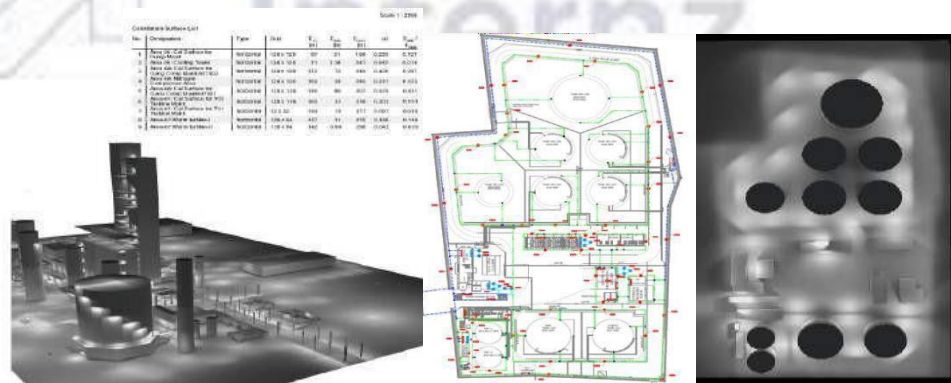
Topicdetails: LightingorilluminationssystemsandCalculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLSPVC wires laid in cable trunks or conduits.

Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fitting to be used, required lux levels

Lighting calculations software: Dialux, Chalmrite, Calculux, Relux, Luxicon, CG

Lux Applicable Standards: IS 6665: Code of practice for industrial



lighting, IS 3646: Code

of practice for interior illumination, IEC 60598: Luminaires,

IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and are lighting layouts. BOQ.

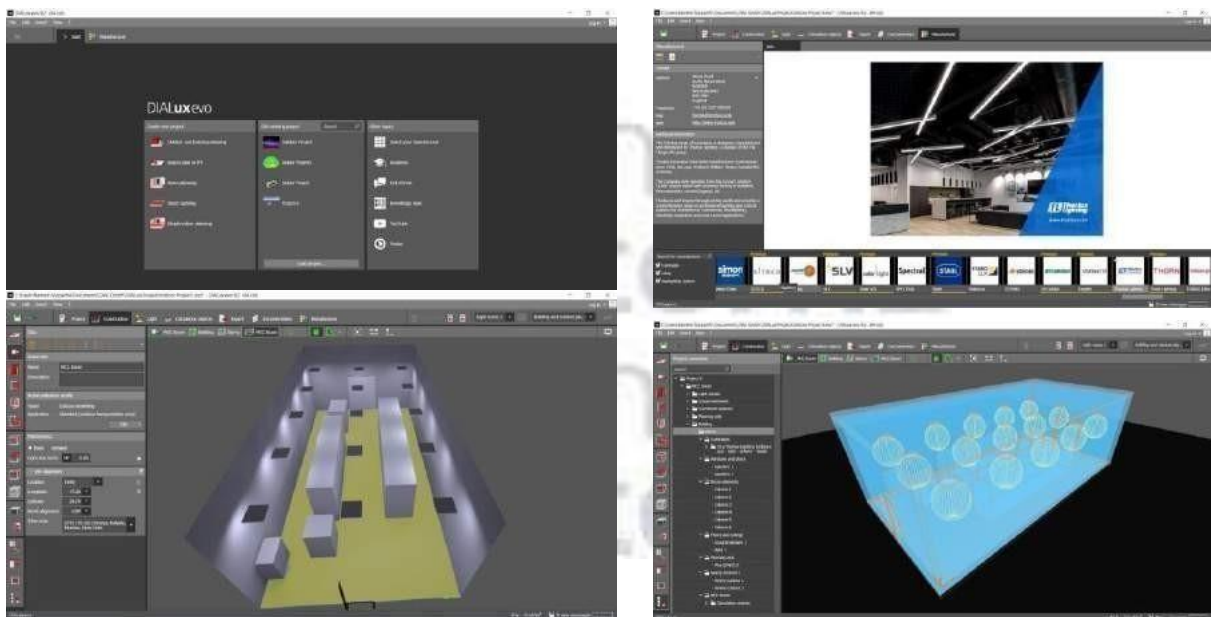
Types of light fittings: Industrial, flameproof type (EXd), increased safety type (Exe).

21thMay2021:LightingorilluminationssystemsusingDIALUXsoftware.

12	LightingorIllu minationusing DIALUX software	Lightingorilluminationssystems	Operation of dialuxsoftwa re
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Topicdetails:LightingorIlluminationCalculations using DIALUXsoftware.

HereweareusingthisDialuxevo5.9.2softwarewindowstoconstructthe
powerplantandwecanperformtheoperationfromthis software.



24thMay2021:Cablingandtheircalculationsandtypes.

13	Cablingandtheir types and claculations	Cablingcalculations	Types of cablingmaterial ls
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Topicdetails:Cablingandtheirtypesandclaculations.



Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

25thMay2021:CablingcalculationsandCableglandselection.

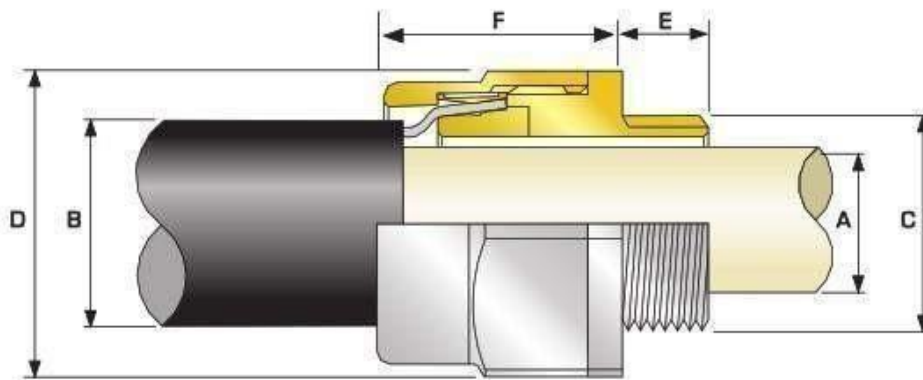
14	Cablingcalculationsandcableglandselection	Cablingcalculations	Cableglandselection
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Topic details: Cablesizingcalculationandcableglandselection.

Inputsrequired: LoadList, Design basis, Electricalequipmentlayout,cableschedule,vendorcataloguesforcabletray.

Cable tray sizing shall be performed for each branch of cable tray routing upto the load point. Results shall be checked with specified limits mentioned indesignbasis.

Cablegland:



Cable Gland Selection Table

Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28thMay2021:LoadcalculationsandTransformersizingcalculations

15	Load calculations and TR calculations	Load calculations	TR calculations
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Topic details:

List of electrical load calculations.

ELECTRICAL LOAD CALCULATIONS LV MCC

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	ELCB Rating	Absorbed Load	Motor / Load Rating	Load Factor [A] / [B]	Efficiency at Load Factor [C]	Power Factor at Load Factor [C]	kW = [A] / [D]		Consumed Load		kVAR = kW x tan φ		Remarks
												Continuous	Intermittent	Stand-by				
			A				[A] kW	[B] kW	[C] decimal	[D] decimal	cos φ	kW	kVAR	kW	kVAR	kW	kVAR	
1	PU2315	Silica filter feed pump					14.34	15.00	0.96	0.85	0.73	16.87	15.79					
2	PU 2314-A	Absorbent/Neutral oil pump (W)					4.16	4.70	0.89	0.85	0.73	4.9	4.6					
3	PU 2314-B	Absorbent/Neutral oil pump (S)					3.58	3.70	0.97	0.85	0.73					4.2	3.9	
4	PU2305	Feed Pump (Separator)					14.47	15.00	0.96	0.85	0.73	17.0	15.9					
5	MX2305	MIXER (W)					14.58	15.00	0.97	0.85	0.73	17.2	16.1					
6	MX 2308	MIXER (S)					14.58	15.00	0.97	0.85	0.73					17.2	16.1	
7	SW2313	Blower					6.27	7.50	0.84	0.85	0.73	7.4	6.9					
8	Rotary valve	TK 2313B (I)					0.61	0.75	0.81	0.85	0.73			0.7	0.7			
9	SC2314	Screw conveyor (I)					1.41	1.50	0.94	0.85	0.73			1.66	1.55			
10	AG 2324A	Citric acid tank agitator (W)					1.05	1.10	0.95	0.85	0.73	1.24	1.16					
11	AG 2324B	Citric acid tank agitator (S)					1.05	1.10	0.95	0.85	0.73					1.2	1.2	
12	AG 2305	Citric oil reaction vessel agitator					3.84	4.70	0.82	0.85	0.73	4.52	4.23					
13	AG 2309	Lye oil reaction vessel agitator					1.39	1.50	0.93	0.85	0.73	1.64	1.53					
14	AG 2310	Lye oil reaction vessel agitator					1.39	1.50	0.93	0.85	0.73	1.64	1.53					
15	AG 2314	Soap Adsorbent Tank Agitator					2.44	3.00	0.81	0.85	0.73	2.87	2.69					

T/F calculation:

Calculation for Transformer Capacity									
1.0 Example of calculation for Transformer Capacity									
1.1 Calculation for consumed load									
Consumed loads used for this example are as follows:									
a. Continuous load	kW	kVar	kVA						
b. Intermittent load / Diversity Factor	247.5	189.4	311.64	--	(i)				
c. Stand-by load required as consumed load	9.37	7.8	13.45	--	(ii)				
	74.35	56.5	95.57	--	(iii)				
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =									
Future expansion load (20% capacity)									
Total Load =									
257.4									
197.4									
324.39									
51.5									
39.5									
64.88									
326.9									
382.22									
1.2 Calculation for 3.3kV / 0.433 kV transformer capacity									
Max. Consumed load = 324.4kVA									
Spare capacity = 64.9kVA									
Required capacity = 389.3kVA									
Transformer rated capacity = 120 kVA									
1.3 Voltage regulation check									
During starting or reacceleration of max. capacity motor (3400 kW), while all the other loads running, the voltage regulation is as follows:									
$P_1 = 315.1 \text{ KVA}$ $(\%Z) = 4$ & Ratio X/R = 3.3									
Hence, %R = 1.126%									
%X = 3.62%									
$P_M = 55 \text{ KW}$ having (K = 6 & C = 1 & Cos $\theta = 0.76$ & Eff. $\eta = 0.88$ & Cos $\theta_s = 0.25$									
$P_s = 193.42106 \text{ KVA}$									
Cos $\theta_s = 0.25$, Corresponding to Angle $\theta_s = 75.522488$ Degrees for which Sin $\theta_s = 0.97$									
$P_4 = 275.74 \text{ KVA}$ & PB in kW is = 275.74 & P_4 in kVar = 197.4 Cos $\theta_4 = 0.85$ 0.956									
Cos $\theta_4 = 0.85$, Corresponding to Angle $\theta_4 = 31.789333$ Degrees, for which Sin $\theta_4 = 0.53$									
$P_{5P} = 190.09555 \text{ KW}$									
$P_{6Q} = 175.15288 \text{ KVAR}$									
$P_6 = 284.28586 \text{ KVA}$									
Cos $\theta_6 = 0.861$, where as Sin $\theta_6 = 0.861$									
Voltage Regulation = 9.7 %									

29thMay2021:DGsetcalculations

16	DG setcalculati
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Topicdetails:

TransformerandDGsetcalculations,types,sizingorselections

DG SIZING CALCULATIONS		
Design Data		
Rated Volatge	415	KV
Power factor (CosØ)	0.76	Avg
Efficiency	0.88	Avg
Total operating load on DG set in kVA at 0.76 power factor	315.1	
Largest motor to start in the sequence - load in KW	55	KW
Running kVA of last motor (CosØ= 0.91)	82	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	493	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	233	KVA
A Continous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	233	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	726	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d'' = (X_d'' + X_d') / 2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d'' \times \frac{(1 - \text{Transient Voltage Dip})}{(\text{Transient Voltage Dip})}$	370	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	726	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	484	KVA
Considering the last value amongst P1, P2 and P3		
Continous operation under load -P1	233	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	370	KVA
Overload capacity P3	484	KVA
Considering the last value amongst P1, P2 and P3	484	KVA
Hence, Existing Generator 484 KVA is adequate to cater the loads as per re-scheduled loads.		
NOTE:VOLTAGE DIP CONSIDERED - 15%		

Conclusion

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback

SmartBridge

They conduct summer internships, workshops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good.

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ASSIGNMENT1

ELECTRICALLOADCALCULATIONSLSVMCC

[illegible]

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	247.5	189.4	311.64	--- (i)
b. Intermittent load / Diversity Factor	8.37	7.8	11.45	--- (ii)
c. Stand-by load required as consumed load	74.36	56.5	93.37	--- (iii)
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	257.4	197.4	324.39	
Future expansion load (20% capacity)	51.5	39.5	64.88	
Total Load =	308.9	236.8	389.27	

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	324.4 kVA
Spare capacity	=	64.9 kVA
Required capacity	=	389.3 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follow

$$P_T = 315.1 \text{ KVA} \quad (\%Z) = 4 \quad \& \text{ Ratio X/R} = 3.3$$

$$\text{Hence , } \%R = 1.176 \%$$

$$\%X = 3.82 \%$$

$$P_M = 55 \text{ KW having (K = 6 \& C = 1 \& Cos } \theta = 0.76 \& \text{ Eff. } \eta = 0.88 \& \text{ Cos } \theta_s = 0.25$$

$$P_S = 493.421 \text{ KVA}$$

$$\text{Cos } \theta_s = 0.25 \text{ ,Corresponding to Angle } \theta_s = 75.5225 \text{ Degrees for which Sin } \theta_s = 0.97$$

$$P_B = 324.4 \text{ KVA} \quad \& \text{ PB in KW is } = 275.74 \quad \& \quad P_B \text{ in Kvar} = 197.4 \quad \therefore \text{Cos } \theta_B = 0.850$$

$$\text{Cos } \theta_B = 0.85 \text{ ,Corresponding to Angle } \theta_s = 31.7883 \text{ Degrees, for which Sin } \theta_s = 0.53$$

$$P_{CP} = 399.095 \text{ KW}$$

$$P_{CQ} = 675.153 \text{ KVAR}$$

$$P_C = 784.288 \text{ KVA}$$

$$\text{Cos } \theta_C = 0.50886 \text{ , where as Sin } \theta_C = 0.861$$

$$\text{Voltage Regulation } \% = 9.7 \%$$

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx. 5.3% , which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

120 kVA transformer selected.

ASSIGNMENT 3

DG SIZING CALCULATIONS		
Design Data		
Rated Volatge	415	KV
Power factor (CosØ)	0.76	Avg
Efficiency	0.88	Avg
Total operating load on DG set in kVA at 0.76 power factor	315.1	
Largest motor to start in the sequence - load in KW	55	KW
Running kVA of last motor (CosØ= 0.91)	82	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	493	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	233	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	233	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	726	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d')/2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{(1 - \text{Transient Voltage Dip})}{(\text{Transient Voltage Dip})}$	370	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	726	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) $= \frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	484	KVA
Considering the last value amongst P1, P2 and P3		
Continous operation under load -P1	233	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	370	KVA
Overload capacity P3	484	KVA
Considering the last value amongst P1, P2 and P3	484	KVA
Hence, Existing Generator 484 KVA is adequate to cater the loads as per re-scheduled loads		
NOTE:VOLTAGE DIP CONSIDERED - 15%		

ASSIGNMENT 4EARTHINGCALCULATION

		10
Maximumline-to-groundfaultinkAfor1sec		14
Earthingmaterial(Earthrod&earthstrip)		GI
Depthofearth flatburrial inmeter		0.5
Averagedepth/lengthofEarthroдинmeters		4
SoilresistivityΩ-meter		17
AmbienttemperatureindegC		50
Plotdimensions(earthgrid)LxBinmeters	65	125
Numberofearthrodsinnos.	6	

Earthelectrodesizing:

Ac-Requiredconductorcrosssectioninsq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

αr-Thermalco-efficientofresistivity,at20Oc	0.0032
pr-Resistivityofgroundconductorat20Oc	20.10
Ta-Ambient Temperatureis°C	50
I _{lg} -RMSfaultcurrent inkA =50KA	14
tc-Shortcircuitcurrent durationsec	1
Thermalcapacityfactor,TCAPJ/(cm3.oC)	3.93
Tm-Maximumallowabletemperatureforcopperconductor,inOc	419
K0-FactoratOc	293
The datatakenfromIEEE80-2000,Clause11.3,Table-1forcladsteelrod:	
	14=Ac* 0.123
Ac-Requiredconductor crossectioninsq.mm	114
Earthroddia inmm	12
Earthroddia(including25%corrosionallowance)inmm	15

Earthflatsizing:

Ac-Requiredconductorcrosssectioninsq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

αr-Thermalco-efficientofresistivity,at20oC	0.0032
pr-Resistivityofgroundconductorat20oC	20.10
Ta-Ambient Temperatureis°C	50
I _{lg} -RMSfaultcurrent inkA =50KA	14
tc-Shortcircuitcurrent durationsec	1

Thermal capacity factor, $TCAPJ/(cm^3 \cdot ^\circ C)$	3.93
T_m -Maximum allowable temperature for copper conductor, in $^\circ C$	419
K_0 -Factor at $^\circ C$	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	

**ASSIGNMENT
LIGHTNING CALCULATION**

	1
Location	Bellari
Building	Concrete, School
Type of Building	Triangle Roofs (c)
Building Length (L)	21
Building breadth (W)	8
Building Height (H)	8

Risk Factor Calculation

1 Collection Area (A_c)

$$A_c = \frac{3.14 \times H^2 + 2(H \times L)}{536.96}$$

2 Probability of Being Struck (P)

$$P = \frac{A_c \times N_g \times 10^{-6}}{0.00080544}$$

3 Overall weighing factor

a) Use of structure (A)	=	1.7
b) Type of construction (B)	=	0.4
c) Contents or consequential effects (C)	=	1.7
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	$A \times B \times C \times D \times E$
	=	0.347

4 Overall Risk Factor

Po	=	$P \times Wo$
Po	=	0.000279327
Pa	=	10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
 Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	$2(L+W)$	
	=	58	Mts.

6 Down Conductors

Perimeter of building	=	58	Mts.
No. of down conductors based on perimeter	=	3	Nos.

Hence 3 nos. of Down conductors have been selected.

Size of Down conductor = 20 X 2.5 mm Galvanized Steel
 (As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

ASSIGNMENT

6CABLESIZING

S.NO.	Description	Equipment No.	Description	Consumed LoadKW	LoadR atingKW	Voltage (V)	No. ofp h	FullLoa dCurre nt(A)	MotorSt artingC urrent(A)	Load P.F.Runn ing	SINΦ Running	Motor P.F.Stari ng	SINΦ Staring	Type	No. ofRu ns	No. ofCor es	Size(mm2)	Current Rating(A)	Derating factork1	Derating factork2	Derating factork3	Derating factork4	Overall Derating factor k	Derated Current (A)	CableL ength(M)	CableRe sistance(O hms/kM)	CableRe actance(O hms/kM)	Voltaged rop(Runni ng) (V)	Voltagedr op(Runni ng)(%)	Voltage drop (Starting) (V)	Voltaged rop(starti ng)(%)	Cable sizere sult	OD ofCab le(m m)	Gland size
3	LVMCC	PJ2316	Shallter Feeding	50.42	55.00	415	3	87.7	526.10	0.8	0.6	0.8	0.5	2	1	4.0	70	230	0.98	0.9	1	1	0.882	202.9	95	0.3430	0.0752	4.61	1.11	27.01	6.51	OK	29	20
4	LVMCC	PJ2314.A	AborbeentHeatit(pump(W)	14.64	15.00	415	3	25.5	152.76	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	95	1.4700	0.0815	5.13	1.24	30.58	7.37	OK	21	20s
5	LVMCC	PJ2314.B	AborbeentHeatit(ol pump(S)	12.60	15.00	415	3	21.9	131.47	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	60	1.4700	0.0815	2.79	0.67	16.62	4.01	OK	21	20s
6	LVMCC	PJ2318	FeedPump(Supentri)	50.92	55.00	415	3	88.6	531.32	0.8	0.6	0.8	0.5	2	1	4.0	70	230	0.98	0.9	1	1	0.882	202.9	85	0.3430	0.0752	4.17	1.00	24.40	5.88	OK	29	20s
7	LVMCC	ME2305	MEER (W)	51.31	55.00	415	3	89.2	535.39	0.8	0.6	0.8	0.5	2	1	4.0	70	230	0.98	0.9	1	1	0.882	202.9	75	0.3430	0.0752	3.70	0.89	21.70	5.23	OK	29	20s
8	LVMCC	ME2306	MEER(S)	51.31	55.00	415	3	89.2	535.39	0.8	0.6	0.8	0.5	2	1	4.0	70	230	0.98	0.9	1	1	0.882	202.9	105	0.3430	0.0752	5.19	1.25	30.38	7.32	OK	29	20s
9	LVMCC	BK2313	Blower	22.03	30.00	415	3	38.3	229.87	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	100	0.9300	0.0816	5.26	1.27	31.25	7.53	OK	22	20s
10	LVMCC	Riser/pv14	TK2313B1	2.14	3.00	415	3	3.7	22.33	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	100	9.4800	0.1007	4.93	1.19	29.53	7.11	OK	16	20s
11	LVMCC	EC2314	Flow waterpump	4.95	5.50	415	3	8.6	51.65	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	3.59	0.86	21.45	5.17	OK	18	20
12	LVMCC	AG2324A	Chloroethene(pump(W)	3.71	4.70	415	3	6.5	38.71	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	110	5.9000	0.0947	5.87	1.41	35.16	8.47	OK	17	20s
13	LVMCC	AG2324B	Chloroethene(pump(S)	3.71	4.70	415	3	6.5	38.71	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	75	5.9000	0.0947	4.00	0.96	23.97	5.78	OK	17	20
14	LVMCC	AG2305	Chloroethene(pump)	13.51	15.00	415	3	23.5	140.97	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	105	1.4700	0.0815	5.23	1.26	31.19	7.52	OK	21	20
15	LVMCC	AG2306	Chloroethene(pump)	4.91	5.50	415	3	8.5	51.23	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	85	3.9400	0.0902	4.03	0.97	24.11	5.81	OK	18	32
16	LVMCC	AG2310	Chloroethene(pump)	4.91	5.50	415	3	8.5	51.23	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	95	3.9400	0.0902	4.50	1.09	26.95	6.49	OK	18	20s
17	LVMCC	AG2314	Chloroethene(T and)gase	8.60	9.20	415	3	15.0	89.74	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	65	2.3400	0.0852	3.24	0.78	19.34	4.66	OK	18	20s
18																																		
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- Basis:
- Overall derating factor $k = k_1 \times k_2 \times k_3 \times k_4$
 - k_1 = Rating factor for variation in air/ground temperature
 - k_2 = Rating factor for depth of laying
 - k_3 = Rating factor for spacing between two circuits
 - k_4 = Rating factor for variation in thermal resistivity of the soil
 - LT Motors: Running Voltage Drop = 3%, Starting Voltage Drop = 15%
 - Cable type:
 - TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed
 - TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC Outer sheathed
 - Effect of Frequency Variation $\pm 5\%$
 - Combined Effect of Voltage & Frequency Variation $\pm 10\%$

ASSIGNMENT 7CABLETRYSIZIN G

LTCABLES									
CABLETRAY:FROM		LT-4		TO	LT-5				
Sr. No.	CableRoute(From-To)	Type&CableSize	Size ofCabl e(mm 2)	No. ofCab le	OverallDia meter ofeach Cable(mm)	Sum of CableOD (mm)	Self Weight ofCable(K g/Mt)	Total WeightofCable(Kg/ Mt)	Remarks
1	PMCC-2 TO NEW COOLING W ATERCIRCULATIONPUMP-MP-3003A	3Cx185Sq.mm,XLPE,FRLSAL Cable	185	1	46	46	3.95	3.95	
2	PMCC-2TOSPACEHEATERFORNEW COOLING W ATER CIRCULATION PUMP- MP-3003A	2C x 4 Sq.mm,XLPE,FRLSCUCable	4	1	14	14	0.37	0.37	
3	PMCC-2 TO NEW COOLING W ATERCIRCULATIONPUMP-MP-3003B	3Cx185Sq.mm,XLPE,FRLSAL Cable	185	1	46	46	3.95	3.95	
4	PMCC-2TOSPACEHEATERFORNEW COOLING W ATER CIRCULATION PUMP- MP-3003A	2C x 4 Sq.mm,XLPE,FRLSCUCable	4	1	14	14	0.37	0.37	
5	PMCC-2 TO NEW COOLING W ATERCIRCULATIONPUMP-MP-3003C	3Cx185Sq.mm,XLPE,FRLSAL Cable	185	1	46	46	3.95	3.95	
6	PMCC-2TOSPACEHEATERFORNEW COOLING W ATER CIRCULATION PUMP- MP-3003A	2C x 4 Sq.mm,XLPE,FRLSCUCable	4	1	14	14	0.37	0.37	
7	PMCC-2TOBLOWDOWNPITPUMP-MP-3111A	3Cx25Sq.mm,XLPE,FRLSAL Cable	25	1	22	22	0.9	0.9	
8	PMCC-2TOBLOWDOWNPITPUMP-MP-3111B	3Cx25Sq.mm,XLPE, FRLSALCable	25	1	22	22	0.9	0.9	
9	PMCC-2TOETPPANEL-MP-3009A	3.5C x 120Sq.mm, XLPE,FRLSALCable	120	1	40	40	2.9	2.9	
10	PMCC-2TO110VACUPS-1	3.5Cx 35 Sq.mm, XLPE, FRLSALCable	35	1	26	26	1.2	1.2	
11	PMCC-2TO110VACUPS-2	3.5Cx 35 Sq.mm, XLPE, FRLSALCable	35	1	26	26	1.2	1.2	
12	PMCC-2TO110VACUPS-3	3.5Cx35Sq.mm,XLPE, FRLSALCable	35	1	26	26	1.2	1.2	
13	PMCC-2TOAUXILIARYPANEL-1	3.5Cx50Sq.mm,XLPE, FRLSALCable	50	1	28	28	1.45	1.45	
14	PMCC-2TOAUXILIARYPANEL-2(A/C)	3.5Cx70Sq.mm,XLPE, FRLSALCable	70	1	33	33	2	2	
15	PMCC-2TOCOOLINGTOWERDOSING SYSTEMPACKAGE	3.5Cx95Sq.mm,XLPE, FRLSALCable	95	1	36	36	2.4	2.4	
16	PMCC-2TOWELDINGRECEPTACLE-1 &2	3.5Cx95Sq.mm,XLPE, FRLSALCable	95	1	36	36	2.4	2.4	
17	MLDB TO LDB(COOLINGTOWERAREA)	4Cx16Sq.mm,XLPE,FRLSAL Cable	16	1	21	21	0.85	0.85	
18	MLDBTOLDB(ETPAREA)	4Cx16Sq.mm,XLPE, FRLSALCable	16	1	21	21	0.85	0.85	
19	MLDBTOLDB(DGAREA)	4Cx16Sq.mm,XLPE,FRLSAL Cable	16	1	21	21	0.85	0.85	
20	MLDBTOLDB(SWITCHYARD)	3.5Cx 25 Sq.mm, XLPE,FRLSALCable	25	1	23	23	1	1	
21	MLDBTOLDB(CONTROLROOM)	4Cx16Sq.mm,XLPE, FRLSALCable	16	1	21	21	0.85	0.85	
Total				21		582	33.91	33.91	
Calculation					Result				
MaximumCableDiameter:	46	mm	SelectedCableTraywidth:		Notadequate				
ConsiderSpareCapacityofCableTray:	30%		SelectedCableTrayDepth:		O.K				
DistancebetweeneachCable:	0	mm	SelectrdCableTrayWeight:		O.K		IncludingSpareCapacity		
CalculatedWidthofCableTray:	757	mm	SelectedCableTraySize:		Notadequate		IncludingSpareCapacity		
CalculatedAreaofCableTray:	34804	Sq.mm	reaseNoofCableTrayorwidthofC						
NoofLayerofCablesinCableTray:	1		RequiredCableTraySize:				mm		
SelectedNoofCableTray:	1	Nos.	RequiredNosofCableTray:				No		
SelectedCableTrayWidth:	600	mm	RequiredCableTray Weight:				Kg/Meter/Tray		
SelectedCableTrayDepth:	100	mm	TypeofCableTray:		Ladder				
SelectedCableTrayWeightCapacity:	90	Kg/Meter							