

Minority Carrier Distributions and terminal currents

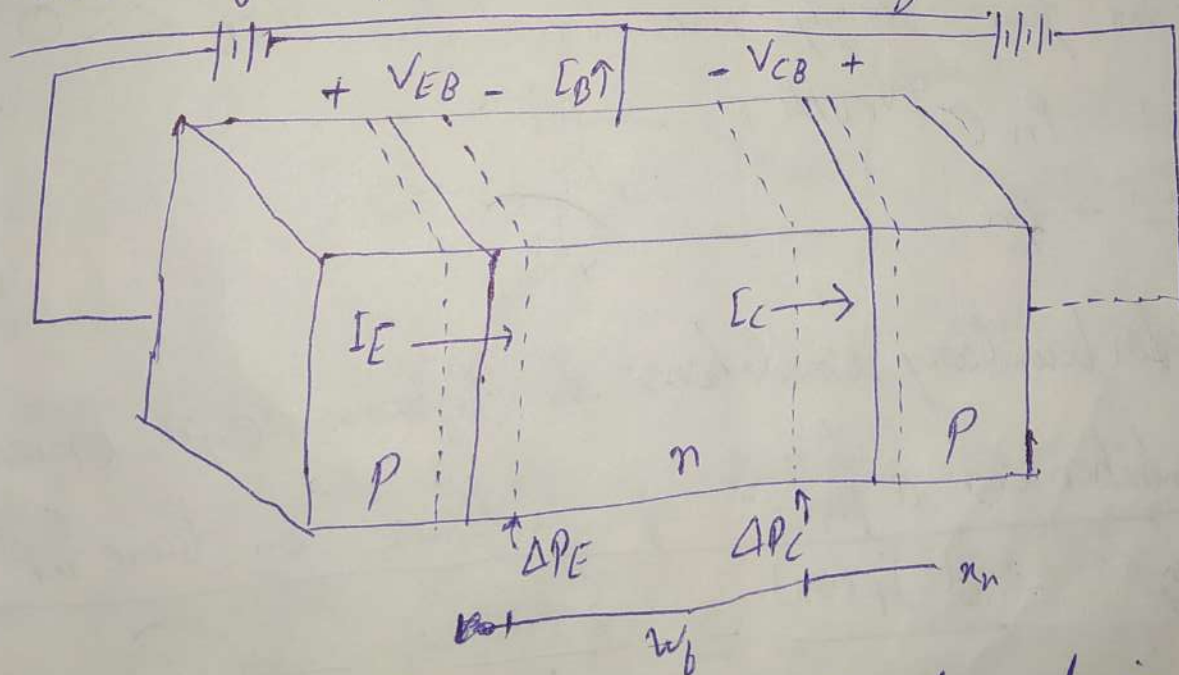
model 3

Holes are injected in base at forward biased emitter, these holes diffuse to collector junction. For the analysis first step is to solve for the excess hole distribution in base, second step is to evaluate I_E & I_C from the gradient of hole distribution on each side of base. Then I_B can be calculated from current summation or from a charge control analysis of recombination in base.

Assumptions required for simplifying the calculation.

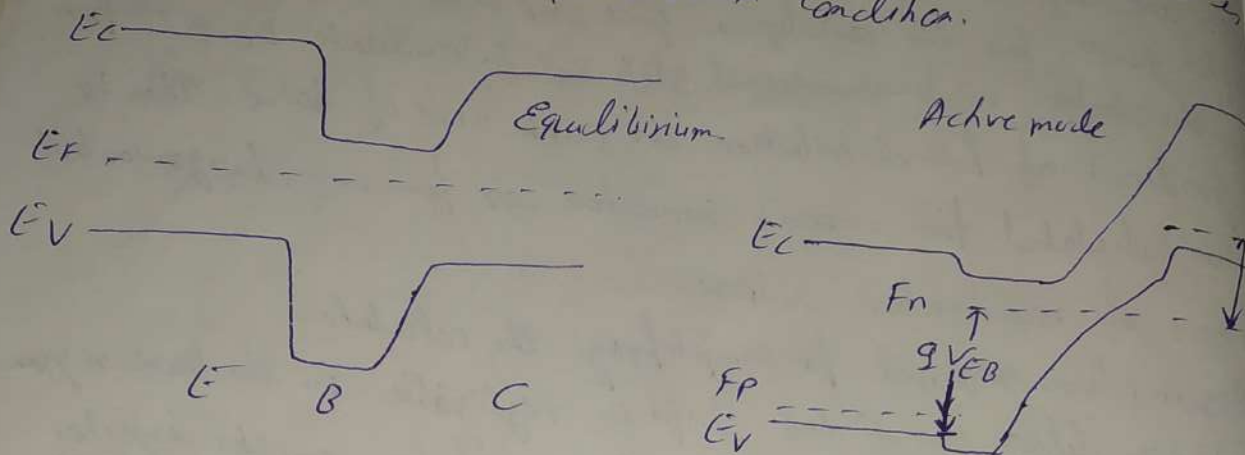
- (i) Holes diffuse from E to C drift is negligible in the base region.
- (ii) Emitter current is made up entirely of holes, emitter injection efficiency $\gamma = 1$.
- (iii) Collector saturation current is negligible.
- (iv) Active part of base and two junctions are of uniform cross sectional area A , current flow in base is essentially one dimensional from E to C.
- (v) All currents and volt are steady state.

Solution of Diffusion eqⁿ in Base region:-



(a) Simplified PNP transistor geometry used in calculations.

- In an active mode (E - B junction forward biased and B - C junction reverse biased) Fermi level split up into quasi-Fermi levels. Whereas it is observed to be flat in equilibrium condition.



- Excess hole concentration at the edge of emitter depletion region ΔP_E & on collector side ΔP_C is given by.

$$\Delta P_E = P_n (e^{qV_{EB}/kT} - 1) \quad \text{--- (I)}$$

$$\Delta P_C = P_n (e^{qV_{CB}/kT} - 1) \quad \text{--- (II)}$$

if emitter junction is strongly forward biased then $V_{EB} \gg kT/q$
 collector junction strongly reverse biased then $V_{CB} \ll 0$

$$\Delta P_E \approx P_n e^{qV_{EB}/kT} \quad \text{--- (III)}$$

$$\Delta P_C \approx -P_n \quad \text{--- (IV)}$$

Using proper boundary condition in diffusion eqn excess hole concentration as a function of distance in base $S_p(x_n)$ is given by

$$\frac{d^2 S_p(x_n)}{dx_n^2} = \frac{S_p(x_n)}{L_p^2} \quad \text{--- (V)}$$

reverse biased)
whereas it is

mod - 4
ED ④

The solⁿ of eq (V) is given by

$$S_p(x_n) = C_1 e^{x_n/L_p} + C_2 e^{-x_n/L_p} \quad \text{--- (VI)}$$

$L_p \rightarrow$ diffusion length of holes in base region.

For any proper designed transistor $w_b \ll L_p$.

Appropriate boundary conditions are

$$S_p(x_n=0) = C_1 + C_2 = \Delta P_E \quad \text{--- (VII)}$$

$$S_p(x_n=w_b) = C_1 e^{w_b/L_p} + C_2 e^{-w_b/L_p} = \Delta P_C \quad \text{--- (VIII)}$$

After solving

$$C_1 = \frac{\Delta P_C - \Delta P_E e^{-w_b/L_p}}{e^{w_b/L_p} - e^{-w_b/L_p}} \quad \text{--- (IX)}$$

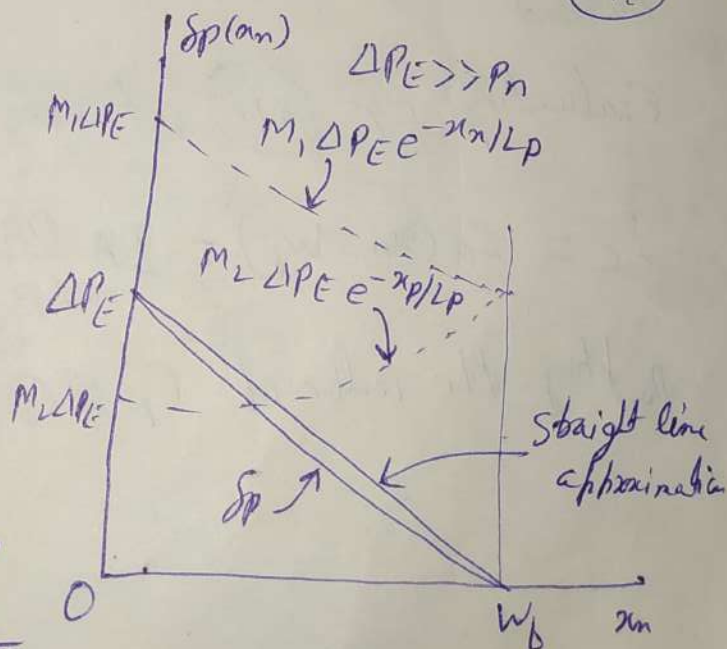
$$C_2 = \frac{\Delta P_E e^{w_b/L_p} - \Delta P_C}{e^{w_b/L_p} - e^{-w_b/L_p}} \quad \text{--- (X)}$$

Applying (IX) & (X) in (VI) we have, excess hole distribution simplifies to

$$S_p(x_n) = \Delta P_E \frac{e^{w_b/L_p} e^{-x_n/L_p} - e^{-w_b/L_p} e^{x_n/L_p}}{e^{w_b/L_p} - e^{-w_b/L_p}} \quad \text{(for } \Delta P_C \approx 0 \text{)} \quad \text{--- (XI)}$$

All the terms in (XI) can be indicated in fig ②, a slight deviation from linearity is observed due to small value i_B introduced by recombination in base region.

$$\begin{aligned} M_1 &= \frac{e^{w_b/L_p}}{e^{w_b/L_p} - e^{-w_b/L_p}} \\ M_2 &= \frac{e^{-w_b/L_p}}{e^{w_b/L_p} - e^{-w_b/L_p}} \end{aligned}$$



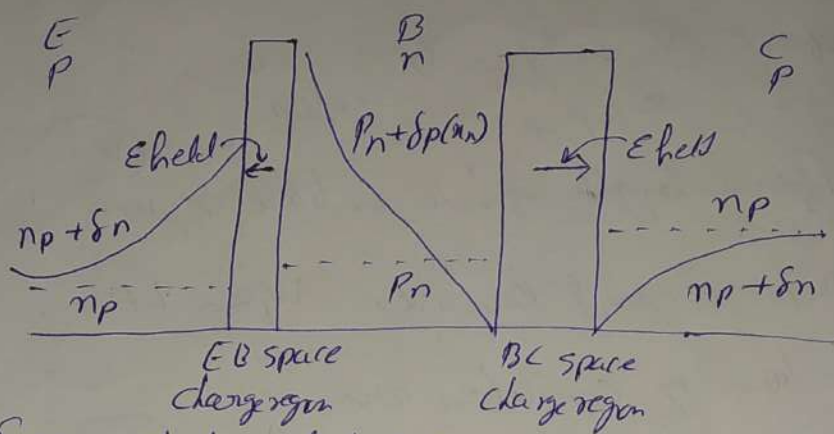


Fig 1 - Electron distributions in emitter & collector.
Evaluation of Terminal currents

Through the relation of hole current & distance we have, (definition)

$$I_p(x_n) = -qAD_p \frac{d p_n(x_n)}{dx_n} \quad \text{--- (XII)}$$

At $x_n = 0$, gives hole component of emitter current

$$I_{Ep} = I_p(x_n = 0) = qAD_p/L_p (C_2 - C_1) \quad \text{--- (XIII)}$$

Now consider I_c to be entirely made up of hole current neglecting e^- crossing from C to B in collector reverse saturation current.

Evaluating eqn (XII) at $x_n = w_b$

$$I_c = I_p(x_n = w_b) = qA \frac{D_p}{L_p} (C_2 e^{-w_b/L_p} - C_1 e^{w_b/L_p}) \quad \text{--- (XIV)}$$

putting the value of C_1 & C_2 from (IX) & (X) to (XIV) we get

$$I_{EP} = qA \frac{D_P}{L_P} \left[\frac{\Delta P_E (e^{w_b/L_P} + e^{-w_b/L_P}) - 2\Delta P_C}{e^{w_b/L_P} - e^{-w_b/L_P}} \right]$$

$$I_{EP} = qA \frac{D_P}{L_P} \left[\Delta P_E \coth \frac{w_b}{L_P} - \Delta P_C \operatorname{csch} \frac{w_b}{L_P} \right] \quad \text{--- (XV)}$$

$$I_C = qA \frac{D_P}{L_P} \left[\Delta P_E \operatorname{csch} \frac{w_b}{L_P} - \Delta P_C \coth \frac{w_b}{L_P} \right] \quad \text{--- (XVI)}$$

Now $I_B = I_E - I_C$

$$= qA \frac{D_P}{L_P} \left[(\Delta P_E + \Delta P_C) \left(\coth \frac{w_b}{L_P} - \operatorname{csch} \frac{w_b}{L_P} \right) \right]$$

$$I_B = qA \frac{D_P}{L_P} \left[(\Delta P_E + \Delta P_C) \tanh \frac{w_b}{2L_P} \right] \quad \text{--- (XVII)}$$

Applying appropriate approximation in eq (XVII), it can also be written as

$$I_B = \frac{qA w_b \Delta P_E}{2T_p} \quad \text{--- (XVIII)}$$

Current transfer Ratio: —

In practice transister $\gamma \neq 1$ as some of e^- will diffuse to Emitter for PNP

Hence γ become $\gamma = \left[1 + \frac{L_P^n n_n \mu_n^p}{L_n^p p_p \mu_p^n} \tanh \frac{w_b}{L_P} \right]^{-1} \approx \left[1 + \frac{w_b n_n \mu_n^p}{L_n^p p_p \mu_p^n} \right]^{-1}$ --- (XIX)

$$\beta = \frac{I_C}{I_{EP}} = \frac{\operatorname{csch} w_b/L_P}{\coth w_b/L_P} = \operatorname{sech} \frac{w_b}{L_P} \quad \text{--- (XX)}$$