

HiperLife Tutorial: Cavity flow (Steady Navier-Stokes)

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1 Problem Definition

A number of important phenomena in fluid mechanics are described by the Navier-Stokes equations. They are a statement of the dynamical effect of the externally applied forces and the internal forces of a fluid that we shall assume Newtonian. The internal forces are due to the pressure and the viscosity of the fluid. Then, the time-dependent flow of a viscous incompressible fluid is governed by the following form of the momentum equation and the mass-conservation equation, called the Navier-Stokes equations:[1]

$$\begin{aligned} -\nabla \cdot \mathbf{v} &= 0, \\ \rho \left(\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} \right) + \nabla p - \mu \nabla \cdot \left[(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T) \right] &= \rho \mathbf{b}. \end{aligned} \quad (1)$$

Here, ρ is the fluid density and \mathbf{b} the volume force per unit mass of fluid, and μ is dynamic viscosity of the fluid ($Pa \cdot s$). Here we are going to solve the exact same cavity flow problem but for Navier-Stokes formulation. Figure 1 shows a schematic representation of the problem. It models a plane flow of an isothermal fluid in a square lid-driven cavity. The upper side of the cavity moves in its own plane at unit speed, while the other sides are fixed.

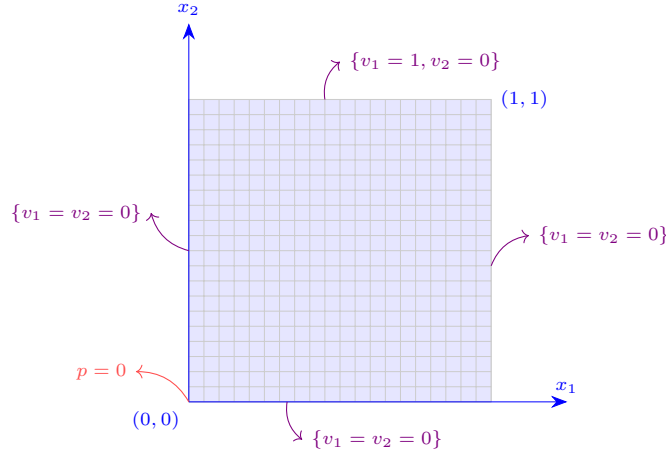


Figure 1: Geometry, boundary conditions and computational domain used for the analysis.

2 Governing Equation

Introducing the Reynolds number as

$$Re = \frac{\rho V L}{\mu} = \frac{V L}{\nu}. \quad (2)$$

where ν denotes the kinematic viscosity of the fluid (m^2/s) and L and V are characteristic of the length and velocity scales of the flow, and dividing both sides of Eq. (1) by V^2/L , allows us to rewrite it in a dimensionless form:

$$-\nabla \cdot \mathbf{v} = 0, \quad \frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} + \nabla P - \frac{1}{Re} \nabla \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] = \mathbf{f}. \quad (3)$$

where the $x = x/L$ and $\mathbf{v} = \mathbf{v}/V$ and $P = p/\rho V^2$ and $f = \mathbf{b}(L/V^2)$ and $t = t(V/L)$. The boundary conditions for the flow problem are given by

$$\mathbf{v} = \bar{\mathbf{v}} \quad \text{on } \Gamma_D, \quad \mathbf{t} \equiv \hat{\mathbf{n}} \cdot \boldsymbol{\sigma} = \hat{\mathbf{t}} \quad \text{on } \Gamma_N. \quad (4)$$

where $\hat{\mathbf{n}}$ is the unit normal to the boundary and $\hat{\mathbf{t}}$ is the traction. The Cauchy stress tensor $\boldsymbol{\sigma}$ can be define as

$$\boldsymbol{\sigma} = 2\mu \mathbf{D} - P \mathbf{I} \quad (5)$$

where $\mathbf{D} = \frac{1}{2}[(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)]$ and \mathbf{I} is the unit tensor.

3 Weak Form

The starting point for the development of the finite element models of Eq. (3) is their weak forms. Here we consider steady flow ($\frac{d\mathbf{v}}{dt} = 0$) two-dimensional case. The variation formulation of our model problem can be introduced as find $(\mathbf{v}, p) \in W$ such that

$$\mathcal{F}(\mathbf{v}, P; \mathbf{u}, q) = 0 \quad \forall (\mathbf{u}, q) \in \hat{W}. \quad (6)$$

where $W = V \times P$ is a mixed function space, and

$$\mathcal{F}(\mathbf{v}, p; \mathbf{u}, q) = \int_{\Omega} \mathbf{u}(\mathbf{v} \cdot \nabla) \mathbf{v} + \mathbf{u} \nabla P - \frac{1}{Re} \mathbf{u} \nabla \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] - q \nabla \cdot \mathbf{v} - \mathbf{u} \mathbf{f} \, d\Omega. \quad (7)$$

and

$$\hat{W} = \{\mathbf{u} \in H^1(\Omega) : \mathbf{u} = 0 \text{ on } \Gamma\}, \quad W = \{\mathbf{u} \in H^1(\Omega) : \mathbf{u} = 0 \text{ on } (x=0, x=1, y=0), u_2 = 1 \text{ on } y=1\}. \quad (8)$$

where (\mathbf{u}, q) is a test functions, which will be equated, in the our FE model to the interpolation function used for (\mathbf{v}, P) . Applying integration by part, and using the definition of stress, we can rewrite the weak form as following

$$\begin{aligned} \mathcal{F}(\mathbf{v}, p; \mathbf{u}, q) &= \int_{\Omega^e} \mathbf{u}(\mathbf{v} \cdot \nabla) \mathbf{v} + \mathbf{u} \nabla P - \frac{1}{Re} \mathbf{u} \nabla \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] - \mathbf{u} \mathbf{f} \, dV - \int_{\Omega^e} q \nabla \cdot \mathbf{v} \, dV \\ &= \int_{\Omega^e} \left\{ \mathbf{u}(\mathbf{v} \cdot \nabla) \mathbf{v} \right\} + \left\{ \nabla \cdot [\mathbf{u} P] - P \nabla \mathbf{u} \right\} + \left\{ \frac{1}{Re} \nabla \mathbf{u} \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] - \nabla \cdot (2\mu \mathbf{D}) \right\} - \mathbf{u} \mathbf{f} \, dV \\ &\quad - \int_{\Omega^e} q \nabla \cdot \mathbf{v} \, dV \\ &= \int_{\Omega^e} \mathbf{u}(\mathbf{v} \cdot \nabla) \mathbf{v} \, dV + \int_{\Gamma^e} \mathbf{u} P \mathbf{I} \cdot \mathbf{n} \, dS - \int_{\Omega^e} P \nabla \mathbf{u} \, dV - \int_{\Gamma^e} (2\mu \mathbf{D}) \cdot \mathbf{n} \, dS + \int_{\Omega^e} \frac{1}{Re} \nabla \mathbf{u} \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] \, dV \\ &\quad - \int_{\Omega^e} \mathbf{u} \mathbf{f} \, dV - \int_{\Omega^e} q \nabla \cdot \mathbf{v} \, dV \\ &= - \int_{\Gamma^e} \mathbf{u} \hat{\mathbf{t}} \, dS + \int_{\Omega^e} \mathbf{u}(\mathbf{v} \cdot \nabla) \mathbf{v} + \frac{1}{Re} \nabla \mathbf{u} \cdot [(\nabla \mathbf{v}) + (\nabla \mathbf{v}^T)] - P \nabla \mathbf{u} - \mathbf{u} \mathbf{f} \, dV - \int_{\Omega^e} q \nabla \cdot \mathbf{v} \, dV. \end{aligned} \quad (9)$$

Since \mathcal{F} is a nonlinear function of \mathbf{v} , the variational statement gives rise to a system of nonlinear algebraic equations. we now need to linearize it, we may use Newton's method to solve the system of nonlinear algebraic

equations. Newton's method for the system $\mathcal{F}(V_1, \dots, V_j)$ can be formulated by the first terms of a Taylor series approximation for the value of the variational as

$$\sum_{j=1}^N \frac{\partial}{\partial V_j} \mathcal{F}(V_1^k, \dots, V_N^k) \delta V_j = -\mathcal{F}(V_1^k, \dots, V_N^k), \quad i = 1, \dots, N, \quad (10)$$

$$V_j^{k+1} = V_j^k + \delta V_j, \quad j = 1, \dots, N,$$

where k is an iteration index. An initial guess \mathbf{v}^0 must be provided to start the algorithm. We need to compute the $\partial \mathcal{F} / \partial V_j$ and the right-hand side vector $-\mathcal{F}$. Our present problem has \mathcal{F} given by above.

$$\frac{\partial F}{\partial V_j} = \int_{\Omega} \mathbf{u} \left(\frac{\partial \mathbf{v}}{\partial V_j} \cdot \nabla \right) \mathbf{v} + \mathbf{u} \left(\mathbf{v} \cdot \nabla \right) \left[\frac{\partial \mathbf{v}}{\partial V_j} \right] + \frac{1}{Re} \nabla \mathbf{u} \left[\nabla \left[\frac{\partial \mathbf{v}}{\partial V_j} \right] + (\nabla \left[\frac{\partial \mathbf{v}}{\partial V_j} \right])^T \right] - q \nabla \cdot \left(\frac{\partial \mathbf{v}}{\partial V_j} \right) d\Omega. \quad (11)$$

by adding the pressure term, Hessian is given by

$$\mathcal{J}(\mathbf{v}, p; \mathbf{u}, q) = \int_{\Omega} \mathbf{u} \left(\frac{\partial \mathbf{v}}{\partial V_j} \cdot \nabla \right) \mathbf{v} + \mathbf{u} \left(\mathbf{v} \cdot \nabla \right) \left[\frac{\partial \mathbf{v}}{\partial V_j} \right] + \frac{1}{Re} \nabla \mathbf{u} \left[\nabla \left[\frac{\partial \mathbf{v}}{\partial V_j} \right] + (\nabla \left[\frac{\partial \mathbf{v}}{\partial V_j} \right])^T \right] - q \nabla \cdot \left(\frac{\partial \mathbf{v}}{\partial V_j} \right) - \frac{\partial P}{\partial P_j} \nabla \mathbf{u} d\Omega. \quad (12)$$

4 Finite Element Model

Since we are developing the Ritz-Galerkin finite element models, the choice of the weight functions is restricted to the spaces of approximation functions used for the pressure and velocity fields. Suppose that the dependent variables (v_i, P) are approximated by expansions of the form

$$v_i(\mathbf{x}, t) = \sum_{m=1}^M \psi_m(\mathbf{x}) \mathbf{v}_i^m(t) = \mathbf{\Psi}^T \mathbf{V}_i, \quad (13)$$

$$p(\mathbf{x}, t) = \sum_{n=1}^N \phi_n(\mathbf{x}) P^n(t) = \mathbf{\Phi}^T \mathbf{P}.$$

where $\mathbf{\Psi}$ and $\mathbf{\Phi}$ are vectors of interpolation (or shape) functions, $\mathbf{V}^{k+1} = \{v_1, v_2\}^T$ and \mathbf{P} are vectors of nodal values of velocity components and pressure, respectively. Substitution of these equation into Eq. (15) results in the following finite element equation.

$$\mathcal{J} = \left[\int_{\Omega^e} \mathbf{\Psi} (\mathbf{\Psi} \cdot \nabla) \mathbf{v}^k d\Omega \right] \mathbf{V} + \left[\int_{\Omega^e} \mathbf{\Psi} (\mathbf{v}^k \cdot \nabla) \mathbf{\Psi} d\Omega \right] \mathbf{V} + \left[\int_{\Omega^e} \frac{1}{Re} \nabla \mathbf{\Psi} [(\nabla \mathbf{\Psi}) + (\nabla \mathbf{\Psi})^T] d\Omega \right] \mathbf{V} - \left[\int_{\Omega^e} \mathbf{\Phi} \nabla \cdot \mathbf{\Psi} dV \right] \mathbf{V} - \left[\int_{\Omega^e} \mathbf{\Phi} \nabla \mathbf{\Psi} dV \right] \mathbf{P}. \quad (14)$$

and

$$\mathcal{F} = \int_{\Omega^e} \mathbf{\Psi} \mathbf{v}^k \cdot \nabla \mathbf{v}^k + \frac{1}{Re} \nabla \mathbf{\Psi} [(\nabla \mathbf{v}^k) + (\nabla \mathbf{v}^k)^T] - P^k \nabla \mathbf{\Psi} dV - \int_{\Omega^e} q \nabla \cdot \mathbf{v}^k dV. \quad (15)$$

The above equations can be written in a matrix form as

$$\begin{aligned} -\mathbf{Q}^T \mathbf{v} &= \mathbf{0}, \\ \mathbf{K} \mathbf{v} - \mathbf{Q} \mathbf{P} &= \mathbf{F}. \end{aligned} \quad (16)$$

By combining continuity and momentum equations into one, Eq. (8) has the following explicit matrix form:

$$\begin{bmatrix} \mathbf{C}_{11} & \mathbf{C}_{12} & 0 \\ \mathbf{C}_{21} & \mathbf{C}_{22} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \\ \mathbf{P} \end{Bmatrix} + \begin{bmatrix} 2\mathbf{K}_{11} + \mathbf{K}_{22} & \mathbf{K}_{12} & -\mathbf{Q}_1 \\ \mathbf{K}_{21} & \mathbf{K}_{11} + 2\mathbf{K}_{22} & -\mathbf{Q}_2 \\ -\mathbf{Q}_1^T & -\mathbf{Q}_2^T & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \\ \mathbf{P} \end{Bmatrix} = \begin{Bmatrix} \mathbf{F}_1 \\ \mathbf{F}_2 \\ \mathbf{F}_3 \end{Bmatrix}. \quad (17)$$

47 The coefficient matrices shown in Eq. (9) are defined by

$$\begin{aligned}
\mathbf{K}_{ij} &= \int_{\Omega^e} \nu \frac{\partial \Psi}{\partial x_i} \frac{\partial \Psi^T}{\partial x_j} dV, \quad \mathbf{Q}_i = \int_{\Omega^e} \frac{\partial \Psi}{\partial x_i} \Phi^T dV, \\
\mathbf{C}_{11} &= \int_{\Omega^e} \Psi \Psi^T \frac{\partial v_1}{\partial x} + \Psi v_1 \frac{\partial \Psi^T}{\partial x} + \Psi v_2 \frac{\partial \Psi^T}{\partial y} dV, \quad \mathbf{C}_{12} = \int_{\Omega^e} \Psi \Psi^T \frac{\partial v_1}{\partial y} dV, \\
\mathbf{C}_{21} &= \int_{\Omega^e} \Psi \Psi^T \frac{\partial v_2}{\partial x} dV, \quad \mathbf{C}_{22} = \int_{\Omega^e} \Psi \Psi^T \frac{\partial v_2}{\partial y} + \Psi v_1 \frac{\partial \Psi^T}{\partial x} + \Psi v_2 \frac{\partial \Psi^T}{\partial y} dV.
\end{aligned} \tag{18}$$

48 and

$$\begin{aligned}
\mathbf{F}_1 &= \int_{\Omega^e} \Psi v_1 \frac{\partial v_1}{\partial x} + \Psi v_2 \frac{\partial v_1}{\partial y} + \nu \left(2 \frac{\partial \Psi}{\partial x} \frac{\partial v_1}{\partial x} + \frac{\partial \Psi}{\partial y} \left[\frac{\partial v_1}{\partial y} + \frac{\partial v_2}{\partial x} \right] \right) - P \frac{\partial \Psi}{\partial x} dV, \\
\mathbf{F}_2 &= \int_{\Omega^e} \Psi v_1 \frac{\partial v_2}{\partial x} + \Psi v_2 \frac{\partial v_2}{\partial y} + \nu \left(2 \frac{\partial \Psi}{\partial y} \frac{\partial v_2}{\partial y} + \frac{\partial \Psi}{\partial x} \left[\frac{\partial v_1}{\partial y} + \frac{\partial v_2}{\partial x} \right] \right) - P \frac{\partial \Psi}{\partial y} dV, \\
\mathbf{F}_3 &= \int_{\Omega^e} \Phi \left(\frac{\partial v_1}{\partial x} + \frac{\partial v_2}{\partial y} \right) dV.
\end{aligned} \tag{19}$$

49 5 Choice of Elements

50 There are lots of elements available for using in mixed finint elements model, but here for sake of simplicity
51 we choose $Q2Q1$ elements. The quadratic quadrilateral elements shown in Figure 2 are known to give reliable
solutions for velocity and pressure fields.

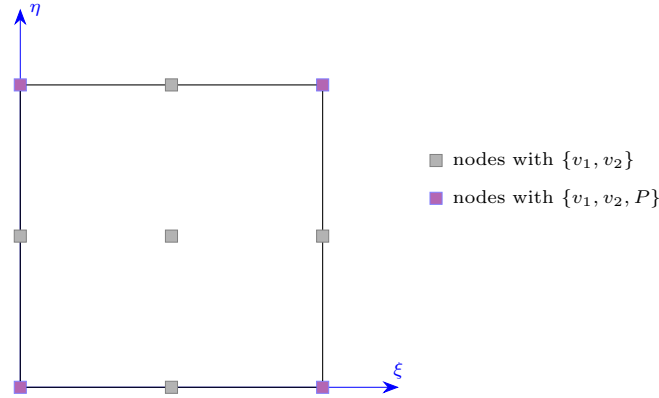


Figure 2: Quadratic quadrilateral element used for the mixed finite element model.

53 6 Implementation

54 In this section, we present the implementation of our solution in the Hiperlife. The program is divided into
55 three separate files, main part which we create our problem by the Hiperlife headers, auxiliary header where we
56 introduce parameters and declare our functions, and at last auxiliary file, where we define some functions which
57 provide required matrices like the Hessian and Jacobian.

58 6.1 CavityFlowNavier.cpp

```

1  /*
2  * Incompressible Navier stokes flow: Cavity flow problem
3  */
4  // cpp headers
5  #include <iostream>

```

```

6  #include <fstream>
7  #include <cmath>
8
9  // hiperlife headers
10 #include "hl-Core.h"
11 #include "hl-Parser.h"
12 #include "hl-Tensor.h"
13 #include "hl-TypeDefs.h"
14 #include "hl-DOFsHandler.h"
15 #include "hl-HiPerProblem.h"
16 #include "hl-FillStructure.h"
17 #include "hl-ParamStructure.h"
18 #include "hl-DistributedMesh.h"
19 #include "hl-StructMeshGenerator.h"
20 #include "hl-GlobalBasisFunctions.h"
21 #include "hl-LinearSolver_Direct_MUMPS.h"
22 #include "hl-NonlinearSolver_NewtonRaphson.h"
23 #include "hl-LinearSolver_Iterative_AztecOO.h"
24 #include <hl-ConsistencyCheck.h>
25
26 // Header to auxiliary functions
27 #include "AuxCavityFlowNavier.h"
28
29 // =====//
30 ///      MAIN FUNCTION      ///
31 // =====//
32
33 int main(int argc, char** argv)
34 {
35     using namespace std;
36     using namespace hiperlife;
37     using namespace hiperlife::Tensor;
38
39     // =====//
40     ///      *****      INITIALIZATION      *****//
41     // =====//
42
43     // Initialize MPI
44     hiperlife::Init(argc, argv);
45
46     // =====//
47     ///      *****      DATA INPUT      *****//
48     // =====//
49
50     // Put parameters in the user structure
51     SmartPtr<ParamStructure> paramStr = CreateParamStructure<CavityNParams>();
52
53     // Data
54     double Re = 100.0;
55     paramStr->setRealParameter(CavityNParams::nu, 1.0/Re);
56     paramStr->setRealParameter(CavityNParams::f1, 0.0);
57     paramStr->setRealParameter(CavityNParams::f2, 0.0);
58
59     double nu = paramStr->getRealParameter(CavityNParams::nu);
60     double f1 = paramStr->getRealParameter(CavityNParams::f1);
61     double f2 = paramStr->getRealParameter(CavityNParams::f2);
62
63
64     // analysis parameter
65     ElemType elemType = ElemType::Square; // Triang or Square
66     int n = 10; // number of elements in x and y direction
67     // =====//
68     ///      *****      MESH CREATION      *****//
69     // =====//
70     // Create a structural mesh
71     SmartPtr<StructMeshGenerator> StrMesh = Create<StructMeshGenerator>();
72
73     StrMesh->setNDim(3);

```

```

74 StrMesh->setBasisFuncType (BasisFuncType::Lagrangian);
75 StrMesh->setBasisFuncOrder (1);
76 StrMesh->setElemType (elemType);
77 StrMesh->genSquare (n, 1.0);
78
79 //-----Distributed Mesh-----//
80 // For Pressure
81 SmartPtr<DistributedMesh> disMeshPress = Create<DistributedMesh>();
82
83 disMeshPress->setMesh (StrMesh);
84 disMeshPress->setBalanceMesh (true);
85 disMeshPress->setElementLocatorEngine (ElementLocatorEngine::BoundingVolumeHierarchy);
86 disMeshPress->Update();
87
88 // For Velocity
89 SmartPtr<DistributedMesh> disMeshVeloc = Create<DistributedMesh>();
90
91 disMeshVeloc->setMeshRelation (MeshRelation::pRefin, disMeshPress);
92 disMeshVeloc->setPRefinement (1);
93 disMeshVeloc->setBalanceMesh (true);
94 disMeshVeloc->setElementLocatorEngine (ElementLocatorEngine::BoundingVolumeHierarchy);
95 disMeshVeloc->Update();
96
97 cout << "—check-meshv/p- files-to-see-the-mesh-for-velocity-and-pressure—" << endl;
98 disMeshVeloc->printFileLegacyVtk ("meshv");
99 disMeshPress->printFileLegacyVtk ("meshp");
100
101 //-----//
102 /// ***** DOFsHANDLER CREATION ***** ///
103 //-----//
104
105 // DOFHandler
106 // For Velocity
107 SmartPtr<DOFHandler> dhandV = Create<DOFHandler>(disMeshVeloc);
108 dhandV->setNameTag ("dhandV");
109 dhandV->setNumDOFs (2);
110 dhandV->setDOFs ({ "vx", "vy" });
111 dhandV->Update();
112
113 // For Pressure
114 SmartPtr<DOFHandler> dhandP = Create<DOFHandler>(disMeshPress);
115 dhandP->setNameTag ("dhandP");
116 dhandP->setNumDOFs (1);
117 dhandP->setDOFs ({ "p" });
118 dhandP->Update();
119 cout << "—DOFHandler-for-Velocity-and-Pressure-successfully-created—" << endl;
120
121
122 //-----Boundary conditions-----//
123 //-----//
124 // Set boundary conditions for the velocity
125 // velocities are zero everywhere except at Ymax vx=1
126 for (int i = 0; i < disMeshVeloc->loc_nPts(); i++)
127 {
128     if (disMeshVeloc->isNodeInMAxis (MAxis::Xmin, i, IndexType::Local))
129     {
130         dhandV->nodeDOFs->setValue ("vx", i, IndexType::Local, 0.0);
131         dhandV->nodeDOFs->setValue ("vy", i, IndexType::Local, 0.0);
132         dhandV->setConstraint ("vx", i, IndexType::Local, 0.0);
133         dhandV->setConstraint ("vy", i, IndexType::Local, 0.0);
134     }
135     if (disMeshVeloc->isNodeInMAxis (MAxis::Xmax, i, IndexType::Local))
136     {
137         dhandV->nodeDOFs->setValue ("vx", i, IndexType::Local, 0.0);
138         dhandV->nodeDOFs->setValue ("vy", i, IndexType::Local, 0.0);
139         dhandV->setConstraint ("vx", i, IndexType::Local, 0.0);
140         dhandV->setConstraint ("vy", i, IndexType::Local, 0.0);
141     }

```

```

142         if (disMeshVeloc->isNodeInMAxis(MAxis::Ymin, i, IndexType::Local))
143         {
144             dhandV->nodeDOFs->set Value("vx", i, IndexType::Local, 0.0);
145             dhandV->nodeDOFs->set Value("vy", i, IndexType::Local, 0.0);
146             dhandV->set Constraint("vx", i, IndexType::Local, 0.0);
147             dhandV->set Constraint("vy", i, IndexType::Local, 0.0);
148         }
149         if (disMeshVeloc->isNodeInMAxis(MAxis::Ymax, i, IndexType::Local))
150         {
151             dhandV->nodeDOFs->set Value("vx", i, IndexType::Local, 1.0);
152             dhandV->nodeDOFs->set Value("vy", i, IndexType::Local, 0.0);
153             dhandV->set Constraint("vx", i, IndexType::Local, 0.0);
154             dhandV->set Constraint("vy", i, IndexType::Local, 0.0);
155         }
156     }
157
158     // Set boundary conditions for the pressure
159     // Set initial value for the pressure at (0,0) p=0
160     // if (disMeshPress->myRank() == 0)
161     dhandP->set BoundaryCondition(0,0, IndexType::Local, 0.0);
162
163     // Save into nodeDOFS0
164     dhandP->nodeDOFs0->set Value(dhandP->nodeDOFs);
165     dhandV->nodeDOFs0->set Value(dhandV->nodeDOFs);
166
167     // Update
168     dhandV->UpdateGhosts();
169     dhandP->UpdateGhosts();
170
171     // initial condition
172     cout << "—check-pressure/velocityBC0-file-to-see-the-applied-BCs—" << endl;
173     dhandP->printFileLegacyVtk("pressureBC0");
174     dhandV->printFileLegacyVtk("velocityBC0");
175
176     // -----//
177     /// ***** HIPERPROBLEM CREATION *****//
178     // -----//
179
180     SmartPtr<HiPerProblem> hiperProbl = Create<HiPerProblem>();
181     hiperProbl->set ParameterStructure(paramStr);
182     hiperProbl->set DOFsHandlers({dhandV, dhandP});
183     hiperProbl->set Integration("IntegCavity", {"dhandV", "dhandP"});
184
185     if (elemType==ElemType::Square)
186     hiperProbl->set CubatureGauss("IntegCavity", 9);
187     else if (elemType==ElemType::Triang)
188     hiperProbl->set CubatureGauss("IntegCavity", 3);
189
190     hiperProbl->set ElementFillings("IntegCavity", LS);
191     if (true)
192     {
193         hiperProbl->set ConsistencyDOFs("dhandV", {"vx", "vy"});
194         hiperProbl->set ElementFillings("IntegCavity", ConsistencyCheck<LS>);
195         hiperProbl->set ConsistencyCheckType(ConsistencyCheckType::Hessian);
196     }
197     hiperProbl->Update();
198     // -----//
199     // -----//
200     /// ***** SOLVER CREATION *****//
201     // -----//
202     // Create linear solver direct
203     SmartPtr<MUMPSDirectLinearSolver> linSolver = Create<MUMPSDirectLinearSolver>();
204     linSolver->set HiPerProblem(hiperProbl);
205     linSolver->set Verbosity(MUMPSDirectLinearSolver::Verbosity::Low);
206     linSolver->set DefaultParameters();
207     linSolver->Update();
208
209     // Create non-linear solver

```

```

210     SmartPtr<NewtonRaphsonNonlinearSolver>nonlSlvr=Create<NewtonRaphsonNonlinearSolver>();
211     nonlSlvr->setLinearSolver ( linSolver );
212     nonlSlvr->setMaxNumIterations (25);
213     nonlSlvr->setResTolerance (1.E-8);
214     nonlSlvr->setSolTolerance (1.E-8);
215     nonlSlvr->setLineSearch (true);
216     nonlSlvr->setPrintIntermInfo (true);
217     nonlSlvr->setConvRelTolerance (true);
218     nonlSlvr->Update ();
219
220     // =====//
221     /// ***** SOLVE *****//
222     // =====//
223
224     // Initial guess
225     dhandV->nodeDOFs->set Value (dhandV->nodeDOFs0);
226     dhandP->nodeDOFs->set Value (dhandP->nodeDOFs0);
227     hiperProbl->UpdateGhosts ();
228
229     // Solve
230     bool converged = nonlSlvr->solve ();
231
232     // Check convergence
233     if (converged)
234     {
235         // Save solution
236         dhandV->nodeDOFs0->set Value (dhandV->nodeDOFs);
237         dhandP->nodeDOFs0->set Value (dhandP->nodeDOFs);
238
239         // Write results and update solution
240         dhandV->printFileLegacyVtk ("CavityNavier_v", true);
241         dhandP->printFileLegacyVtk ("CavityNavier_p", true);
242     } else
243     {
244         throw runtime_error ("Error: -NonLinear- solver -did- not- converge.");
245     }
246
247     // mpi finilizing
248     hiperlife :: Finalize ();
249     return 0;
250 }

```

6.2 AuxCavityFlowNavier.h

```

1  #ifndef AUXCavityN_H
2  #define AUXCavityN_H
3
4  // C headers
5  #include <iostream>
6
7  // hiperlife headers
8  #include "hl_Core.h"
9  #include "hl_Parser.h"
10 #include "hl_TypeDefs.h"
11 #include "hl_DOFsHandler.h"
12 #include "hl_HiPerProblem.h"
13 #include "hl_FillStructure.h"
14 #include "hl_ParamStructure.h"
15 #include "hl_DistributedMesh.h"
16 #include "hl_StructMeshGenerator.h"
17 #include "hl_GlobalBasisFunctions.h"
18 #include "hl_NonlinearSolver_NewtonRaphson.h"
19 #include "hl_LinearSolver_Iterative_AztecOO.h"
20
21 struct CavityNParams
22 {

```



```

23     enum RealParameters
24     {
25         nu,
26         f1,
27         f2,
28     };
29     HLPARAMETERLIST DefaultValues
30     {
31         {"nu," , 0.01},
32         {"f1," , 0.0},
33         {"f2," , 0.0},
34     };
35 };
36
37 void LS(hiperlife::FillStructure& fillStr);
38
39 #endif

```

6.3 AuxCavityFlowNavier.cpp

```

1  // Header to cpp
2  #include <fstream>
3  #include <iostream>
4  #include <string>
5
6  // Header to auxiliary functions
7  #include "AuxCavityFlowNavier.h"
8
9  // Hiperlife headers
10 #include "hl-Core.h"
11 #include "hl_ParamStructure.h"
12 #include "hl_Parser.h"
13 #include "hl_TypeDefs.h"
14 #include "hl_GlobalBasisFunctions.h"
15 #include "hl_StructMeshGenerator.h"
16 #include "hl_DistributedMesh.h"
17 #include "hl_FillStructure.h"
18 #include "hl_DOFsHandler.h"
19 #include "hl_HiPerProblem.h"
20 #include "hl_LinearSolver_Iterative_AztecOO.h"
21 #include "hl_NonlinearSolver_NewtonRaphson.h"
22
23 using namespace std;
24 using namespace hiperlife;
25 using namespace hiperlife::Tensor;
26
27
28 // Cavity flow
29
30 void LS(hiperlife::FillStructure& fillStr)
31 {
32     using namespace std;
33     using namespace hiperlife;
34     using hiperlife::Tensor::tensor;
35
36     double nu = fillStr.getRealParameter(CavityNParams::nu);
37     double f1 = fillStr.getRealParameter(CavityNParams::f1);
38     double f2 = fillStr.getRealParameter(CavityNParams::f2);
39     ttl::tensor<double,1> F{f1,f2};
40
41
42     //-----
43     // INPUT DATA -----
44     //-----
45
46     //-----Velocity-related-----

```

```

47 // Dimensions
48 SubFillStructure& subFill = fillStr["dhandV"];
49 int pDim = subFill.pDim;
50 int eNN = subFill.eNN;
51 int numDOFs = subFill.numDOFs;
52
53 // Shape functions and derivatives at Gauss points
54 double jac{};
55 ttl::wrapper<double,2> nborCoords(subFill.nborCoords.data(),eNN,pDim);
56 ttl::wrapper<double,2> nborDOFs(subFill.nborDOFs.data(),eNN,numDOFs);
57 ttl::tensor<double,1,false> bf(subFill.nborBFs(),eNN);
58 ttl::tensor<double,2> Dbf_g(eNN,pDim);
59 GlobalBasisFunctions::gradients(Dbf_g, jac, subFill);
60
61 //-----Pressure-related-----//
62 // Dimensions
63 SubFillStructure& subFill_p = fillStr["dhandP"];
64 int nDim_p = subFill_p.nDim;
65 int eNN_p = subFill_p.eNN;
66 int numDOFs_p = subFill_p.numDOFs;
67
68 // Shape functions and derivatives at Gauss points
69 ttl::wrapper<double,2> nborCoords_p(subFill_p.nborCoords.data(),eNN_p,nDim_p);
70 ttl::wrapper<double,1> nborDOFs_p(subFill_p.nborDOFs.data(),eNN_p);
71 ttl::tensor<double,1,false> bf_p(subFill_p.nborBFs(),eNN_p);
72
73 //-----OUTPUT DATA-----//
74 //-----OUTPUT DATA-----//
75 //-----OUTPUT DATA-----//
76 ttl::wrapper<double,2> Bk0(fillStr.Bk(0).data(),eNN,numDOFs);
77 ttl::wrapper<double,1> Bk1(fillStr.Bk(1).data(),eNN_p);
78
79 ttl::wrapper<double,4> Ak00(fillStr.Ak(0,0).data(),eNN,numDOFs,eNN,numDOFs);
80 ttl::wrapper<double,3> Ak01(fillStr.Ak(0,1).data(),eNN,numDOFs,eNN_p);
81 ttl::wrapper<double,3> Ak10(fillStr.Ak(1,0).data(),eNN_p,eNN,numDOFs);
82 ttl::wrapper<double,2> Ak11(fillStr.Ak(1,1).data(),eNN_p,eNN_p);
83
84 //-----EQUATIONS-----//
85 //-----EQUATIONS-----//
86 tensor<double,1> v = bf * nborDOFs;
87 double pre = bf_p * nborDOFs_p;
88
89 tensor<double,2> Dv = product(nborDOFs,Dbf_g,{0,0});
90 double divv = trace(Dv);
91
92 //tensor form
93 // create a 4th order tensor out of Dbf_g
94 tensor<double,4> Dbf4 = outer(Dbf_g,Identity(pDim));
95 Ak00 += jac * nu * product(Dbf4,Dbf4 + Dbf4.transpose({0,2,1,3}},{1,1},{2,2}));
96 Ak00 += jac * outer(outer(bf,Dv),bf).transpose({0,1,3,2});
97 Ak00 += jac * outer(outer(bf,Identity(pDim)),Dbf_g*v).transpose({0,1,3,2});
98
99 Ak01 += -jac * outer(Dbf_g,bf_p);
100 Ak10 += -jac * outer(bf_p,Dbf_g);
101
102 Bk0 += jac * outer(bf,Dv*v);
103 Bk0 += -jac * pre * Dbf_g;
104 Bk0 += jac * nu * Dbf_g * (Dv + Dv.T());
105 Bk1 += -jac * divv * bf_p;
106
107 //indices form
108 //for (int i=0;i < eNN;i++)
109 //{
110 //    for (int j=0;j < eNN;j++)
111 //    {
112 //        Ak00(i,0,j,0)+=jac*nu*(2.0*Dbf_g(i,0)*Dbf_g(j,0)
113 //        //+Dbf_g(i,1)*Dbf_g(j,1));
114 //        Ak00(i,0,j,0)+=jac*(bf(i)*Dv(0,0)*bf(j)

```

```

115         +bf(i)*v(0)*Dbf_g(j,0)+bf(i)*v(1)*Dbf_g(j,1));
116
117         //Ak00(i,0,j,1)+=jac*nu*(Dbf_g(i,1)*Dbf_g(j,0));
118         //Ak00(i,0,j,1)+=jac*(bf(i)*bf(j)*Dv(0,1));
119
120         //Ak00(i,1,j,0)+=jac*nu*(Dbf_g(i,0)*Dbf_g(j,1));
121         //Ak00(i,1,j,0)+=jac*(bf(i)*Dv(1,0)*bf(j));
122
123         //Ak00(i,1,j,1)+=jac*nu*(2.0*Dbf_g(i,1)*Dbf_g(j,1)
124         //+Dbf_g(i,0)*Dbf_g(j,0));
125         //Ak00(i,1,j,1)+=jac*(bf(i)*bf(j)*Dv(1,1)
126         //+bf(i)*v(0)*Dbf_g(j,0)+bf(i)*v(1)*Dbf_g(j,1));
127         //}
128     //for (int j=0;j < eNN_p;j++)
129     //{
130         //Ak01(i,0,j)+=-jac*(Dbf_g(i,0)*bf_p(j));
131         //Ak01(i,1,j)+=-jac*(Dbf_g(i,1)*bf_p(j));
132
133         //Ak10(j,i,0) +=-jac*(bf_p(j)*Dbf_g(i,0));
134         //Ak10(j,i,1) +=-jac*(bf_p(j)*Dbf_g(i,1));
135         //}
136     //Bk0(i,0)+=jac*(bf(i)*v(0)*Dv(0,0) + bf(i)*v(1)*Dv(0,1));
137     //Bk0(i,0)+=jac*nu*(2.0*Dbf_g(i,0)*Dv(0,0)+Dbf_g(i,1)*(Dv(1,0)+Dv(0,1)));
138     //Bk0(i,0)+=-jac*pre*Dbf_g(i,0);
139
140     //Bk0(i,1)+=jac*(bf(i)*v(0)*Dv(1,0)+bf(i)*v(1)*Dv(1,1));
141     //Bk0(i,1)+=jac*nu*(2.0*Dbf_g(i,1)*Dv(1,1)+Dbf_g(i,0)*(Dv(0,1)+Dv(1,0)));
142     //Bk0(i,1)+=-jac*pre*Dbf_g(i,1);
143     //}
144 //for (int i=0;i < eNN_p;i++)
145 //{
146     //Bk1(i)+=-jac*bf_p(i)*divv;
147 //}
148
149 }

```

7 Results

In this section, we present the results of our solution. Figure 3 shows the velocities distribution in the cavity for $v_x = 1$ on top and $Re = 100$.

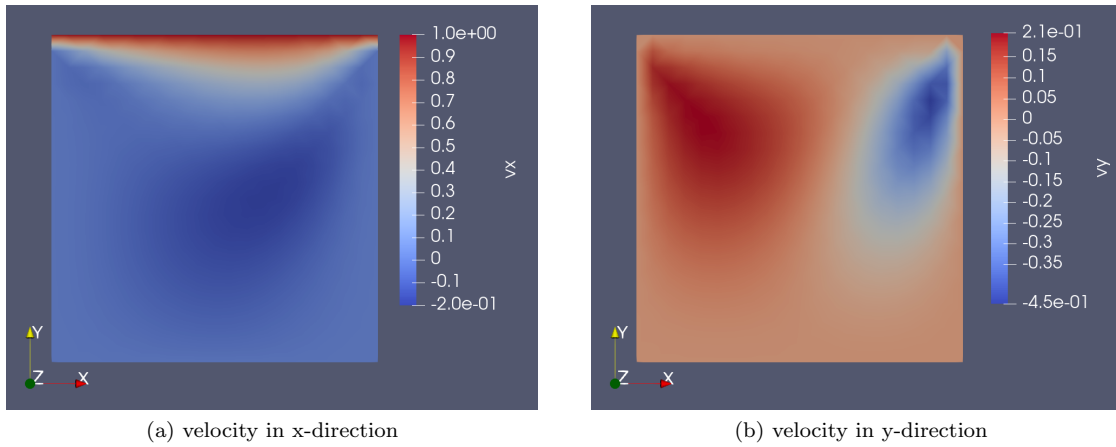


Figure 3: velocity of flow in cavity for $Re = 100$

Pressure contour is presented in Figure 4.

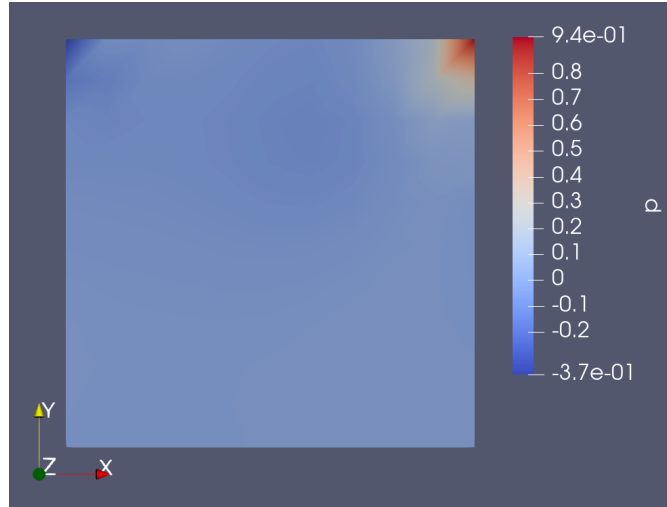


Figure 4: Pressure distribution in the domain for $Re = 100$.

References

- [1] Jean Donea and Antonio Huerta. *Finite element methods for flow problems*. John Wiley & Sons, 2003.