

13th International Conference on Greenhouse Gas Control Technologies, GHGT-13, 14-18  
November 2016, Lausanne, Switzerland

## Study on dissolution process of liquid CO<sub>2</sub> into water under high pressure condition for CCS

Xiao Ma<sup>a,\*</sup>, Yutaka Abe<sup>a</sup>, Akiko Kaneko<sup>a</sup>, Shuhei Fujimoto<sup>b</sup>, Chikahisa Murakami<sup>b</sup>

<sup>a</sup>University of Tsukuba, 1-1-1 Tennoudai, Tsukuba, Ibaraki 305-8573, Japan

<sup>b</sup>National Maritime Research Institute, 6-38-1 Shinkawa, Mitaka, Tokyo 181-0004, Japan

---

### Abstract

The objective of the present study is set as to clarify the dissolution phenomena of liquid CO<sub>2</sub> in the high pressure corresponding to deep-ocean, and CO<sub>2</sub> concentration profile near the water-liquid CO<sub>2</sub> interface when CO<sub>2</sub> hydrate formation. First of all, visualization unit is constructed which can be observed from all angles. Second, mass transfer coefficient and the solubility of CO<sub>2</sub> with time were calculated via volume change of gas CO<sub>2</sub>, liquid CO<sub>2</sub> and dissolution water by using image processing. As a result, CO<sub>2</sub> mass transfer coefficient decreased with time, and solubility of CO<sub>2</sub> increased with time. Finally, CO<sub>2</sub> solubility calculated by the present study was compared to a previous study, and its indicated good agreement with the previous value of hydrate formation condition which the temperature under 10 °C.

© 2017 The Authors. Published by Elsevier Ltd. This is an open access article under the CC BY-NC-ND license (<http://creativecommons.org/licenses/by-nc-nd/4.0/>).

Peer-review under responsibility of the organizing committee of GHGT-13.

**Keywords:** Dissolution; Visualization observation; Mass transfer; Ocean storage

---

### 1. Introduction

Carbon dioxide capture and storage technologies were now considered one of the powerful tool to mitigate the global warming program. Especially, it is considered that ocean storage technology has 10,000 times ability than the technology to store the CO<sub>2</sub> underground [1]. When CO<sub>2</sub> is stored under the deep ocean, e.g. on the deep sea floor or under the sea bed, it can be thought that CO<sub>2</sub> clathrate hydrate will be formed. It is because deep-ocean satisfy the

---

\* Corresponding author. Tel.: +81-29-853-5268; fax: +81-29-853-5487.

E-mail address: [s1530208@u.tsukuba.ac.jp](mailto:s1530208@u.tsukuba.ac.jp)

formation condition for CO<sub>2</sub> hydrate at low temperature and high pressure [2]. Brewer et al. [3] did field study to visualize the formation of CO<sub>2</sub> hydrate at actual sea condition at Monterey Bay. As the result, CO<sub>2</sub> hydrate was actually observed at the beaker over the liquid CO<sub>2</sub> and pH change by CO<sub>2</sub> hydrate was measured. On the other hand, several experimental studies at lab scale was done and reviewed by Mori [4]. However, some model exists with an assumption which have not been evaluated its validity yet. One of the important property for developing the formation and growth of CO<sub>2</sub> hydrate, the solubility of CO<sub>2</sub> has been measured at previous study [5-8]. Ma et al. [9] observed the formation of CO<sub>2</sub> hydrate at the interface of liquid CO<sub>2</sub> and water, and the velocity of area explanation of CO<sub>2</sub> hydrate was calculated. Moreover, the prediction model to calculate the initial film thickness of CO<sub>2</sub> hydrate immediately following covering the interface was developed using results of above previous studies and a boundary layer thickness of CO<sub>2</sub> concentration. Although the time change of boundary layer thickness at formation of CO<sub>2</sub> hydrate did not measured, and the relation between boundary layer and CO<sub>2</sub> hydrate at hydrate formation process at unsteady condition is now unknown.

In this study, in order to clarify the formation mechanism, visualization apparatus was set up and the dissolution process of CO<sub>2</sub> was first measured at high pressure condition which over 45 bar. Continuously, some physical quantity were measured by image processing.

## 2. Experiment

### 2.1. Experimental apparatus

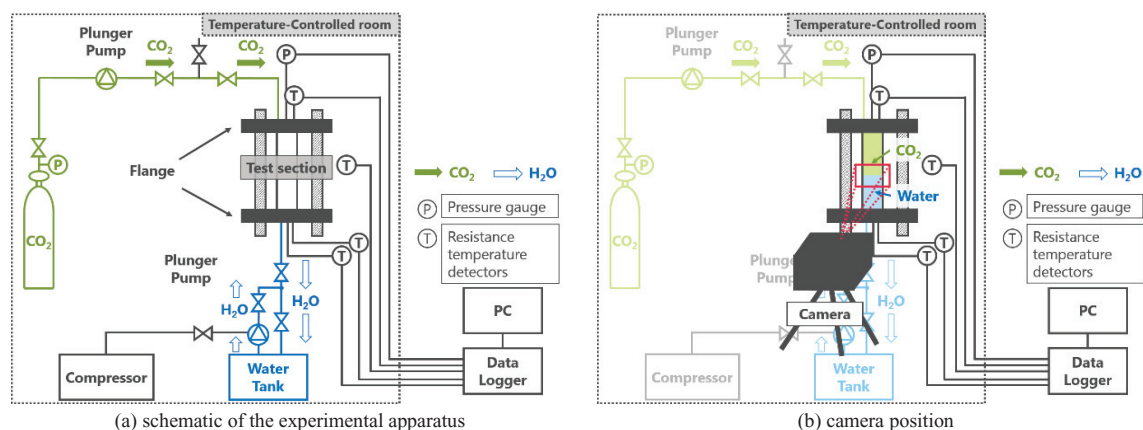


Fig. 1. Schematic of the experimental apparatus

Figure 1 shows a schematic image of an experimental apparatus. Figure 1(a) is a diagram of plumbing at the present study. The unit is composed by plunger pumps, resistance temperature detectors, a CO<sub>2</sub> cylinder, a pressure gage, a water tank, valves, flanges and a test section. In the present study, a test section is made of acrylic and it can be observed from all angles. The acrylic block is secured via flanges set at the top and bottom of the block. The test section is formed by block with circular cylinder at the center, and the inner diameter is 40 mm, height of the block is 150 mm. Resistance temperature detectors measured three points that are room temperature near the test section, a temperature of liquid CO<sub>2</sub> which installed top of the flange, and water temperature installed bottom of the flange. In order to keep and regulate temperature condition, all components were put in a temperature-controlled room. The video camera was also set into the temperature-controlled room and positioned a bit in front of the test section to record a dissolution phenomenon of CO<sub>2</sub> at high pressure condition as Fig. 1(b).

PC which placed outside of the temperature-controlled room record the digital data transfer from pressure gauge and resistance temperature detectors inside the room during the experiment.

## 2.2. Experimental procedure and experimental condition

First, the water was filled into the acrylic block until about the middle. Then, water had been colored by pH indicator (phenol red or methyl red). Second, gas  $\text{CO}_2$  filled the test section and pipeline from a  $\text{CO}_2$  cylinder. At this time, dissolution phenomena of  $\text{CO}_2$  into the water via color change of pH indicator were observed.

After confirming that color of dissolution water with pH detector did not change, pressure at test section was pressurized by plunger pump and liquidized gas  $\text{CO}_2$  till specific volume. Then, experimental condition was set 2 patterns. First, the condition was kept vapor-liquid coexistence that gas  $\text{CO}_2$  and liquid  $\text{CO}_2$  existed over distilled water. In this condition, the pressure at the test section indicate the same value during the experiment. The other condition, experimental pressure has exceeded the coexistence pressure and liquid  $\text{CO}_2$  was filled in the test section. In this section, the pressure reached perfect liquid  $\text{CO}_2$  phase and placed over a distilled water. After that, valves around test section was closed and position changes with time at each interface was photographed by a video camera. At the only liquid  $\text{CO}_2$  condition, liquid  $\text{CO}_2$  was pressed into the test section till the pressure reached to the initial pressure condition when pressure drop by  $\text{CO}_2$  dissolution in water occurred. The experimental temperature condition was set 2.5, 4.5, 13.2, 17.1  $^{\circ}\text{C}$ , pressure condition was set 4, 6, 7 MPa. In the present condition, water density is still larger than  $\text{CO}_2$  density. Each temperature and pressure data were recorded at every 5 seconds. The experiment finished within 18 hours at longest.

## 3. Result and discussion

### 3.1. Visualization result

Figure 2 shows the experimental result of dissolution phenomena of the gas  $\text{CO}_2$  with time at 6  $^{\circ}\text{C}$ , 4 MPa and pH detector was used Methyl red. Figure 2(a) is the initial condition of distilled water with dissolved pH detector was set in the acrylic test section with air. At (b),  $\text{CO}_2$  gas filled the test section and then a color at the interface of gas  $\text{CO}_2$  – distilled water was changed and indicated pH beginning to decrease. At (c) to (f), it can be observed that the red area which indicated low pH region was expanded with time. At the same time, liquefied  $\text{CO}_2$  was observed at the interface between gas  $\text{CO}_2$  and distilled water. It is because the condition in  $\text{CO}_2$  cylinder is in a vapor-liquid coexistence of  $\text{CO}_2$  and a pressure in the test section reached the coexistence condition similar  $\text{CO}_2$  cylinder. After (f), it was observed that the color change rate was decreased at (g) and the color change did not observe at (h). Reaction ranges of pH of Methyl red is 4.4 – 6.5 and it can be thought pH in dissolution water exceed the value 4.4 within 10 seconds at longest.

Figure 3 shows the picture shoot at 160 minutes from Fig. 2 at 6  $^{\circ}\text{C}$  and 4 MPa condition. As the result, area of gas  $\text{CO}_2$  and dissolution water was increasing with time. On the other hand, it was observed region of liquid  $\text{CO}_2$  was decreasing with time. The dissolution rate of each phase was calculated quantitatively at the next section.

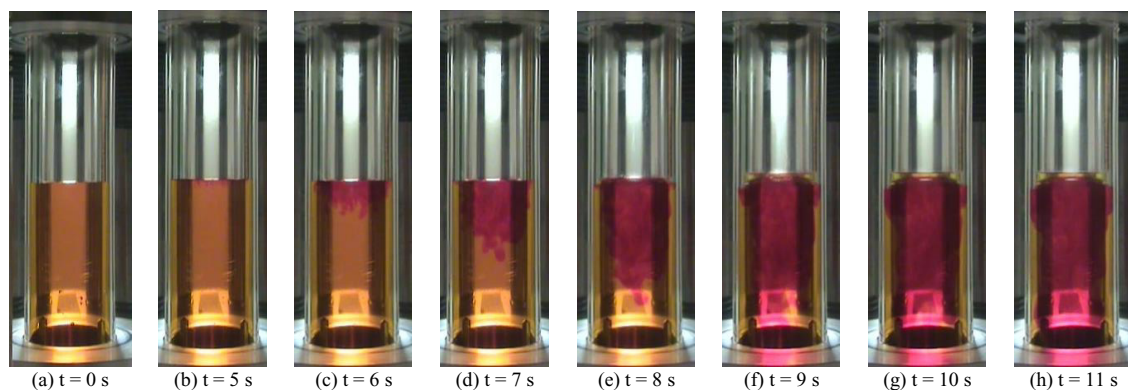


Fig. 2. Visualization of dissolution of gas  $\text{CO}_2$  into distilled water at 6  $^{\circ}\text{C}$ , 4 MPa



Fig. 3. Visualizaition result of the test section

### 3.2. Image processing

In order to evaluate dissolution phenomena quantitatively, a time-space diagram was created. At Fig. 4(a), one pixel at the center of test section as Fig. 3 at  $t=0$  was extracted and lined up the pixel along the time change for right. As the result, created time-space diagram was shown in Fig. 4(a). From the top, the diagram shows the time change of volume of gas  $\text{CO}_2$ , position of gas  $\text{CO}_2$  and liquid interface, volume of liquid  $\text{CO}_2$ , position of liquid  $\text{CO}_2$  and water interface, water volume. Then to tracing each interface, digital image was converted BMP file format into an HSV file format and using Hue image. In consequence, the interfaces were traced perfectly as shown in Fig. 4(b). From the top, each line traced the interface between gas and liquid  $\text{CO}_2$ , between liquid  $\text{CO}_2$  and water at center of the test section, between the interface of liquid  $\text{CO}_2$  and water on the inside wall of the section.

Subsequently, volume of liquid  $\text{CO}_2$ , dissolution water, gas  $\text{CO}_2$  at each time was calculated from above obtained position using time-space diagram. Then, because of different interfacial tension between liquid  $\text{CO}_2$  and water, water volume seems convex upward. Therefore, water volume was calculated using follow Eq. (1):

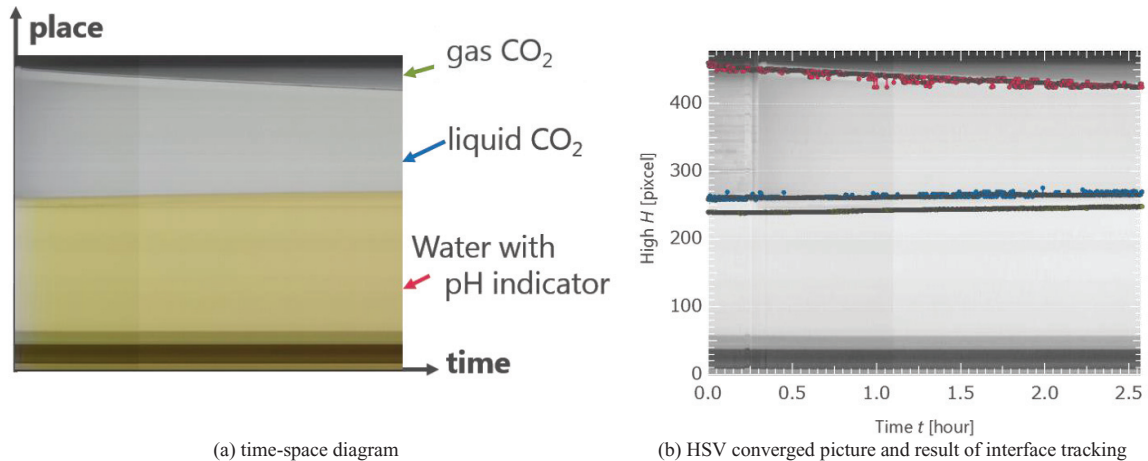
$$V_{\text{water}}(t) = \frac{1}{2} \frac{4}{3} \pi \left( \frac{D}{2} \right)^2 L + \pi \left( \frac{D}{2} \right)^2 (H - L) \quad (1)$$

Where,  $D$  is a diameter of the inter cylinder of acrylic block ( $= 40 \text{ mm}$ ),  $L$  is a height of interface of liquid  $\text{CO}_2$  and dissolution water from the bottom of the acrylic at inside wall,  $H$  is same height of the above interface from bottom at the center which top of convex upward. Volume of liquid  $\text{CO}_2$  was calculated as follows. Eq. (2-1) is used when the experimental condition without gas  $\text{CO}_2$  which include only liquid  $\text{CO}_2$  and water, and Eq.(2-2) is used with gas  $\text{CO}_2$  condition.

$$V_{\text{CO}_2}(t) = V_{\text{test}} - V_{\text{water}}(t) \quad (\text{without gas CO}_2 \text{ region}) \quad (2-1)$$

$$V_{\text{CO}_2}(t) = \pi \left( \frac{D}{2} \right)^2 (h(t) - H(t)) - V_{\text{water}}(t) \quad (\text{with gas CO}_2 \text{ region}) \quad (2-2)$$

Where,  $V_{\text{test}}$  is the volume of test section that circular cylinder inside an acrylic block ( $= \text{about } 188,496 \text{ mm}^3$ ),  $h$  is the height of the interface between liquid  $\text{CO}_2$  and gas  $\text{CO}_2$  from the bottom. Next, a time change of mass and volume were calculated. Each value of dissolution water and liquid  $\text{CO}_2$  was calculated using follow equations Eq. (3) and (4). Mass of dissolution water was calculated as the summation of initial distilled water filled in the test section and dissolved liquid  $\text{CO}_2$  at each time. On the other hand, mass of liquid  $\text{CO}_2$  at a time  $t$  is calculated as a difference between initial mass and dissolved mass as above.



(a) time-space diagram

(b) HSV converged picture and result of interface tracking

Fig. 4. Time-space diagram and the tracing result of each interface

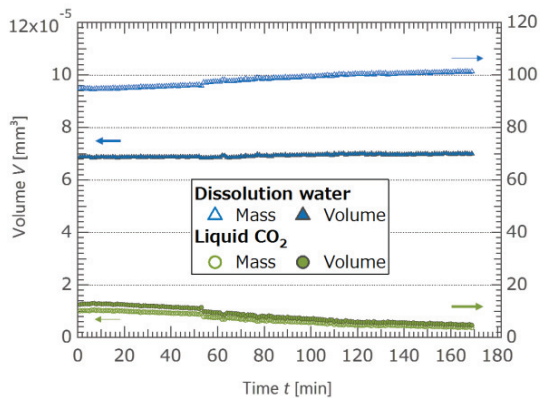
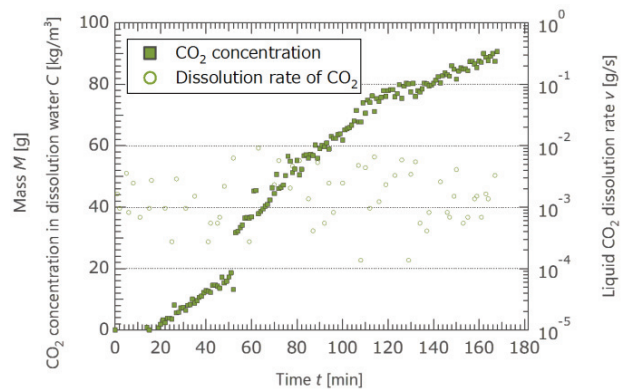
$$M_{\text{water}}(t) = M_{\text{water}}^{\text{initial}} + \rho_{\text{CO}_2} \cdot \Delta V_{\text{CO}_2}(t) \quad (3)$$

$$M_{\text{CO}_2}(t) = M_{\text{CO}_2}^{\text{initial}} - \rho_{\text{CO}_2} \cdot \Delta V_{\text{CO}_2}(t) \quad (4)$$

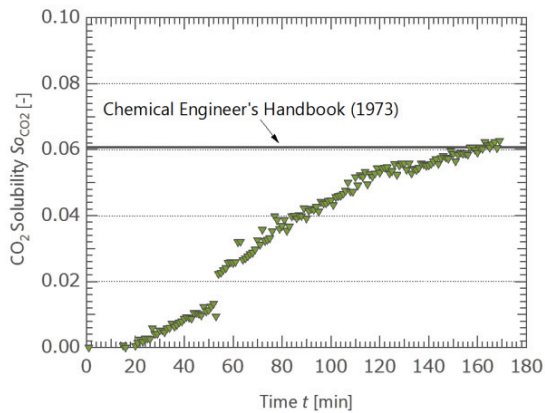
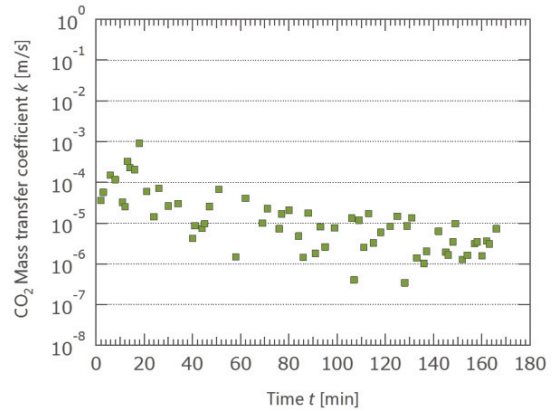
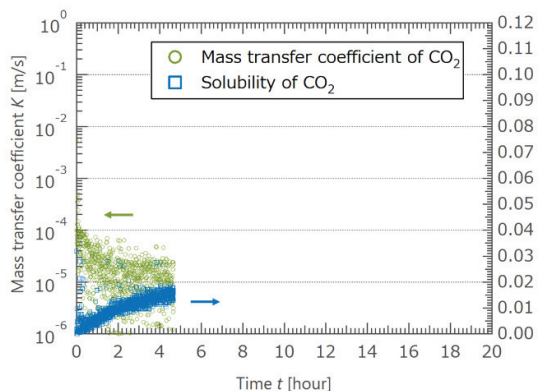
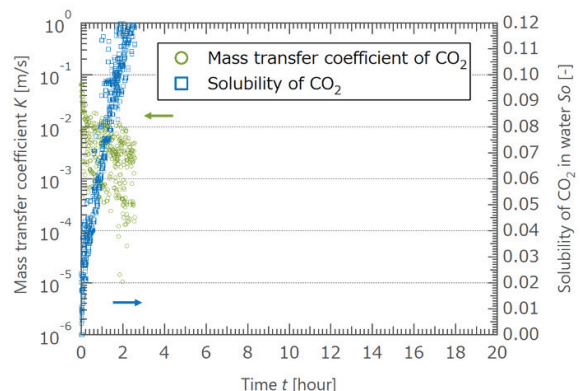
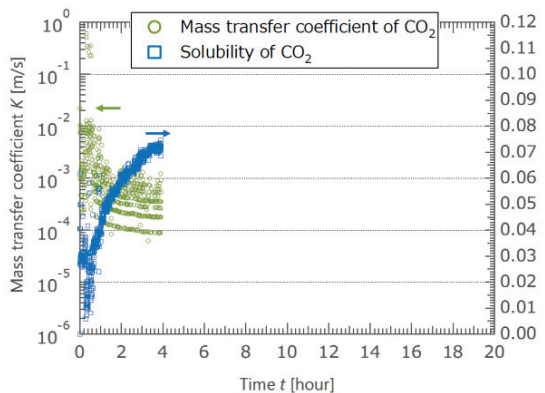
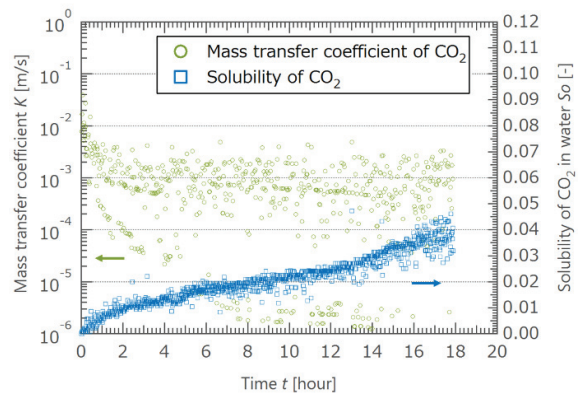
Where,  $V_{\text{CO}_2}$  is dissolved volume of liquid CO<sub>2</sub> from an initial time using time-space diagram,  $\rho_{\text{CO}_2}$  is a density of liquid CO<sub>2</sub> at an experimental condition. Obtained each time change of volume and mass is shown in Fig. 5. The vertical axis of left is volume of dissolution water and liquid CO<sub>2</sub>, and the right axis is the dissolution rate of liquid CO<sub>2</sub>. The time change of mass of both dissolution water and CO<sub>2</sub> was corresponding to the volume change at each time. Then, the concentration of CO<sub>2</sub> in bulk water was calculated with dissolved CO<sub>2</sub> mass divided by volume of dissolution water at each time using Eq. (5). Continuously, dissolution rate of liquid CO<sub>2</sub> was calculated by Eq. (6).

$$C_{\text{CO}_2}^{\text{bulk}} = \frac{\Delta M_{\text{CO}_2}(t)}{V_{\text{water}}(t)} \quad (5)$$

$$v_{\text{CO}_2} = \frac{dM_{\text{CO}_2}}{dt} \quad (6)$$

Fig. 5. Mass change of the liquid CO<sub>2</sub> and the dissolution waterFig. 6. CO<sub>2</sub> concentration change and dissolution rate of CO<sub>2</sub>



Fig. 7. CO<sub>2</sub> solubility changeFig. 8. CO<sub>2</sub> Mass transfer coefficient(a) 13.2 °C, 6 MPa, without CO<sub>2</sub> gas(b) 13.2 °C, 4 MPa, with CO<sub>2</sub> gas(c) 4.5 °C, 6 MPa, with CO<sub>2</sub> gas(d) 2.5 °C, 7 MPa, without CO<sub>2</sub> gas, with HydrateFig. 9. Mass transfer coefficient and solubility of CO<sub>2</sub> in water with time at each experimental condition

These values with time was shown in Fig. 6. The vertical axis of left is CO<sub>2</sub> concentration, and the axis of right is dissolution rate of liquid CO<sub>2</sub>. As the result, it can be confirmed that the concentration increased with time and reached to the saturated condition. On the other hand, the dissolution rate of CO<sub>2</sub> approximately kept the order between 10<sup>-4</sup> to 10<sup>-2</sup> g/s from the initial condition of 6 °C and 4 MPa.

Using calculated above some physical values, CO<sub>2</sub> solubility in water and CO<sub>2</sub> mass transfer coefficient at liquid CO<sub>2</sub> and water interface is now calculated. Each equation was described as follows Eq. (7), (8).

$$So_{CO_2} = \frac{\Delta M_{CO_2}}{M_{water}} \quad (7)$$

$$k_{CO_2} = \frac{1}{A} \frac{dM_{CO_2}}{dt} \frac{1}{\rho_{CO_2} \cdot So_{CO_2}(t) - C_{CO_2}^{bulk}} \quad (8)$$

Where,  $A$  is an area of the test section (= about 1257 mm<sup>2</sup>). Figure 7 and 8 shows above time change of CO<sub>2</sub> solubility and mass transfer coefficient. As a result of calculation a solubility and mass transfer coefficient of CO<sub>2</sub>, solubility increased with time and mass transfer coefficient decreased with time. It can be thought that CO<sub>2</sub> dissolved well into a water at the initial condition because there are no CO<sub>2</sub> in water. After the interface of liquid CO<sub>2</sub> and water was created, mass transfer coefficient decreased with CO<sub>2</sub> concentration increased. Calculated solubility of CO<sub>2</sub> was increased and reached the value similar to the value of Chemical Engineer's Handbook at same condition. Therefore, it was confirmed that the experimental result indicated the validity of the present experimental system and experimental result.

As is the case with above Eq. (1) to (8), solubility and mass transfer coefficient of CO<sub>2</sub> with time was calculated at some experimental conditions. These value changes with time was described in Fig.9 then the vertical axis of all figure is set the solubility of CO<sub>2</sub>, and the right axis of all figure is set mass transfer coefficient of CO<sub>2</sub>. At Fig. 9(a) and (d), the experimental condition did not include gas CO<sub>2</sub> and CO<sub>2</sub> hydrate film was confirmed at condition of Fig. 9(d). On the other hand, Fig. 9(b) and (c) included gas CO<sub>2</sub> in addition to liquid CO<sub>2</sub> and water. As the result, mass transfer coefficient was obtained in the order of 10<sup>-4</sup> to 10<sup>-6</sup> m/s. Compared to previous study measured mass transfer coefficient of CO<sub>2</sub> by Aya et al. [8], calculated value of the present study is 10 or 10<sup>2</sup> times larger than their value. On the other hand, calculated solubility at the experiment finished was plotted with previous study in Fig. 10. As a result, values at Fig. 7 agreed with previous study at no-hydrate existence temperature (over 10 °C) condition. Similarly, Fig. 9(c) and 9(d) agreed with previous study at hydration temperature (under 10 °C) with the observation of CO<sub>2</sub> hydrate film. At Fig. 9(a) and (b), CO<sub>2</sub> solubility of the present study is different from measured value at previous studies [5-8]. At these conditions, hydrate will not be formed. The value of Fig. 9(a) is much smaller than numerical dashed line. It can be thought the experiment needed more experimental time on the condition and dissolution water has not been reached the saturation condition.

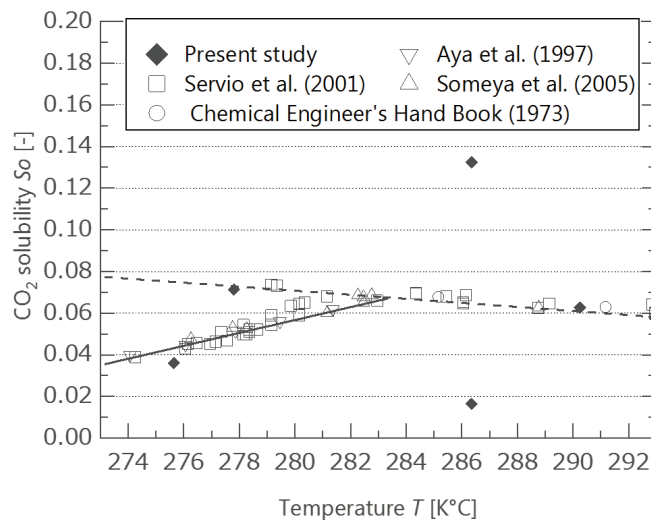


Fig. 10. Calculated saturated concentration of CO<sub>2</sub> in water. The dash line means the solubility at without CO<sub>2</sub> hydrate condition, and the solid line means the solubility with CO<sub>2</sub> hydrate condition by least square approximation.

#### 4. Conclusions

1. Visualization unit for high pressure was produced and dissolution phenomena of CO<sub>2</sub> were observed at two phase condition (liquid CO<sub>2</sub> and water) and three phase condition (gas CO<sub>2</sub>, liquid CO<sub>2</sub> and water). When gas CO<sub>2</sub> filled in the test section, water with pH detector changed immediately within at longest 10 seconds.
2. After the concentration of CO<sub>2</sub> in water exceeded the reaction range of pH detector, pressure was increased and CO<sub>2</sub> was liquidized at the test section. In both conditions of with gas CO<sub>2</sub> and without gas CO<sub>2</sub>, water region increased with time. At with gas CO<sub>2</sub> condition, volume change of liquid CO<sub>2</sub> was observed and it decreased with time.
3. By image processing for photographing pictures, the interface of liquid CO<sub>2</sub> and gas CO<sub>2</sub>, the interface of liquid CO<sub>2</sub> and dissolution water was traced perfectly. Using the position of interfaces, each physical quantity change with time, e.g. the volume of each phase, mass of liquid CO<sub>2</sub>, CO<sub>2</sub> concentration in the water, dissolution rate, solubility of CO<sub>2</sub>, and mass transfer coefficient, was calculated.
4. Compared to previous studies, final CO<sub>2</sub> solubility when the experiment has finished was calculated from the present study. These values agreed with the value of the previous experimental study especially at hydration temperature condition. In addition, mass transfer coefficient indicates the order between  $10^{-6} \sim 10^{-4} \text{ m}^2/\text{s}$ .

#### References

- [1] Bergman PE, Piemer PE, Wokaun A. Geological sequestration of CO<sub>2</sub>. Astatus report. Greenhouse Gas Control Technologies 2000;p.167-173.
- [2] Sloan ED, Koh CA. Clathrate Hydrates of Natural Gases. 3rd ed. Boca Raton: CRC Press, 2007.
- [3] Brewer PG, Edward TP, Gernot F, Aya I, Yamane K. Experiments on the ocean sequestration of fossil fuel CO<sub>2</sub>: pH measurements and hydrate formation. Marine Chemistry 2000;72.p.52-93.
- [4] Mori YH. Clathrate hydrate formation at the interface between liquid CO<sub>2</sub> and water phases – A review of rival models characterizing “Hydrate films”. Energy Convers. Mgmt 1998;39: 15.p.1537-1557.
- [5] Perry RH, Chilton CH. Chemical engineer’s Handbook, New York: McGraw-Hill Book Company, 1973.
- [6] Servio P, Englezos P. Effect of temperature and pressure on the solubility of carbon dioxide in water in the presence of gas hydrate. Fluid Phase Equilibria 2001;190.p.127-134.
- [7] Someya S, Bando S, Chen B, Song Y, Nishio M. Measurement of CO<sub>2</sub> solubility in pure water and the pressure effect on it in the presence of clathrate hydrate, International Journal of Heat and Mass Transfer 2005;48.p.2503-2507.
- [8] Aya I, Yamane K, Nariai H, Solubility of CO<sub>2</sub> and Density of CO<sub>2</sub> Hydrate at 30MPa. Energy 1997;22:2/3.p.263-271.
- [9] Ma X, Abe Y, Kaneko A, Yamane K. Mass Transport Properties on Time Series Variation of CO<sub>2</sub> Hydrate Film. Energy Procedia 2014;63.p.5925-5932.