Ideal F-v motor, Heavy Spring, Rounded Latch @ Constant Force 30 Jan 2020

Parameters:

Motor: F_{max} , d, v_{max}

Spring: $m_{\rm spr}$

Latch: F_l , m_l , v_{l0} , R

Projectile: m

Timing: t_l (time of latch releasing), t_{to} (time of projectile taking off)

Non-dimensionalized variables: see pg. 7, supplemental.

Prior to latch release $(t \le t_l)$

Latch moves in y direction, projectile in x direction (like supplemental).

Position of the rounded latch, w/r/t time (assume y(0) = 0) for a constant force:

$$y(t) = v_0 t + \frac{1}{2} \frac{F_{\text{max}}}{m_l} t^2$$

Position of projectile while in contact with latch:

$$x(t) = R \left(1 - \sqrt{1 - \left(\frac{y(t)}{R}\right)^2} \right)$$

Velocity of projectile, in terms of y(t):

$$v(t) = \frac{y(t)y'(t)}{R\sqrt{1 - \left(\frac{y(t)}{R}\right)^2}}$$

Acceleration:

$$a(t) = \frac{1}{R\sqrt{1 - \left(\frac{y(t)}{R}\right)^2}} \left(y'(t)^2 + y(t)y''(t) + \frac{y(t)^2y'(t)^2}{R^2 - y(t)^2}\right)$$

Game-plan: By leaving these equations in terms of y(t), we can declare y(t) as a separate function in Matlab. This hopefully will also allow changing y(t) easily, if needed (e.g. for testing/debugging).

Sanity checking: Plugging in $y(t) = v_0$ in each of these equations yielded identical results to equations 27-29 in supplemental text.

Non-dimensionalizing: Yields exact same equations (with tildas)

Solving for time of latch release t_l

Using the energy argument of section 6 of supplemental,

$$\frac{1}{2}(1-\tilde{x})^2 + \frac{1}{2}\left(\tilde{m} + \frac{\tilde{m}_{spr}}{3}\right)\tilde{v}^2 - \int_0^{\tilde{x}} f_{latch}(x') dx' = constant.$$

$$\to \left(\tilde{m} + \frac{\tilde{m}_{spr}}{3}\right)\tilde{a}(\tilde{t}_l) = 1 - \tilde{x}(\tilde{t}_l)$$

We can substitude the equations for x(t) and a(t) above into this expression, and solve for t_l .

Solving for velocity at takeoff v_{to} :

Based on conservation of energy: $\tilde{U}(\tilde{t_l}) + \tilde{KE}(\tilde{t_l}) = \tilde{KE}(\tilde{v_{to}})$, we get equation 39 in supplemental:

$$\tilde{v_{\text{to}}} = \sqrt{\tilde{v_l}^2 + \frac{1}{\tilde{m} + \frac{\tilde{m}_{\text{spr}}}{3}} (1 - \tilde{x_l})^2}$$

where \tilde{v}_l and \tilde{x}_l are the equations for $\tilde{v}(\tilde{t})$ and $\tilde{x}(\tilde{t})$ above, evaluated at \tilde{t}_l .

After latch release $t_l < t < t_{to}$:

Equations 61-67 in supplemental.

After takeoff $t > t_{to}$:

$$x(t) = v_{\text{to}}t$$

$$v(t) = v_{\rm to}$$

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Before, all derivations assumed an ideal k value for the spring; i.e. $k_{ideal} = F_{max}/d$. Now, we will madoify these derivations for a non-ideal spring stiffness.

New Parameters:

E, young's modulus (stiffness of material)

A, cross-sectional area of spring

L, rest length of the spring

$$k = \frac{EA}{L}$$

Dimensionless values:

$$\tilde{k} = \frac{k}{k_{ideal}} = \frac{kd}{F_{max}}$$

where

Solving for time of latch release t_l

Modifying the potential energy to include \tilde{k} ,

$$\frac{1}{2}\tilde{k}(1-\tilde{x})^2 + \frac{1}{2}\left(\tilde{m} + \frac{\tilde{m}_{\rm spr}}{3}\right)\tilde{v}^2 - \int_0^{\tilde{x}} f_{\rm latch}(x')\,\mathrm{d}x' = constant.$$

$$\to \left(\tilde{m} + \frac{\tilde{m}_{\rm spr}}{3}\right)\tilde{a}(\tilde{t}_l) = \tilde{k}\left(\tilde{x}_{max} - \tilde{x}(\tilde{t}_l)\right)$$

$$\tilde{x}_{max} = \frac{x_{max}}{d} = \frac{F_{max}/k}{d} = \frac{1}{\tilde{k}}.$$

Solving for velocity at takeoff v_{to} :

$$\tilde{v_{\text{to}}} = \sqrt{\tilde{v_l}^2 + \frac{\tilde{k}}{\tilde{m} + \frac{\tilde{m}_{\text{spr}}}{3}} (\tilde{x}_{max} - \tilde{x_l})^2}$$

After latch release $t_l < t < t_{to}$:

In equation 61, switch in maximum position \tilde{x}_{max} and add spring constant \tilde{k} to give

$$\tilde{x}(\tilde{t}) = \tilde{x}_{max} - \tilde{v}_{to} \sqrt{\frac{\tilde{m} + \frac{\tilde{m}_{spr}}{3}}{\tilde{k}}} \cos\left(\sqrt{\frac{\tilde{k}}{\tilde{m} + \frac{\tilde{m}_{spr}}{3}}} \tilde{t} + \tilde{\phi}\right)$$

In equations 62-67 in supplemental, replace $\tilde{m} + \frac{\tilde{m}_{spr}}{3}$ terms with $(\tilde{m} + \frac{\tilde{m}_{spr}}{3})/\tilde{k}$.