

1)

2.3 For the circuit shown in Fig. P2.1, select node b as the reference node. (a) Use nodal analysis to find the node voltages. (b) Use the node voltages to determine i_1 , i_2 , i_3 , and i_4 .

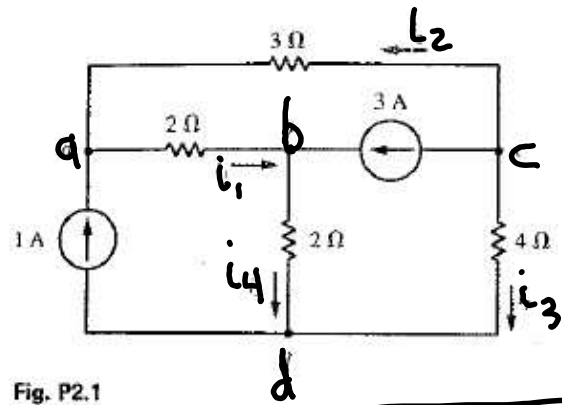


Fig. P2.1

a) KCL at:

$$(a) 1 + i_2 = i_1$$

$$(c) i_2 + 3 + i_3 = 0$$

$$(d) i_4 + i_3 = 1$$

$$(a) 1 + \frac{v_c - v_a}{3} = \frac{v_a}{2}$$

$$6 + 2v_c = 5v_a$$

$$(c) \frac{v_c - v_a}{3} + 3 + \frac{v_c - v_d}{4} = 0$$

$$4v_c - 4v_a + 36 + 3v_c - 3v_d = 0$$

$$7v_c - 4v_a - 3v_d = -36$$

$$(d) -\frac{v_d}{2} + \frac{v_c - v_d}{4} = 1$$

$$-2v_d + v_c - v_d = 4$$

$$v_c - 3v_d = 4$$

Using Ohm's law:

$$i_1 = \frac{v_a - v_b}{2}$$

$$i_3 = \frac{v_c - v_d}{4}$$

$$i_2 = \frac{v_c - v_a}{3}$$

$$i_4 = \frac{v_b - v_d}{2}$$

Remember $v_b = 0$ V.

$$\begin{bmatrix} 5 & 2 & 0 \\ 4 & -7 & 3 \\ 0 & 1 & -3 \end{bmatrix} \begin{bmatrix} v_a \\ v_c \\ v_d \end{bmatrix} = \begin{bmatrix} 6 \\ 36 \\ 4 \end{bmatrix}$$

$$\begin{bmatrix} v_a \\ v_c \\ v_d \end{bmatrix} = \begin{bmatrix} 5 & 2 & 0 \\ 4 & -7 & 3 \\ 0 & 1 & -3 \end{bmatrix}^{-1} \begin{bmatrix} 6 \\ 36 \\ 4 \end{bmatrix} = \begin{bmatrix} -2 \\ -8 \\ -4 \end{bmatrix}$$

$$v_a = -2 \text{ V}, v_c = -8 \text{ V}, v_d = -4 \text{ V}$$

b) Using the equations above:

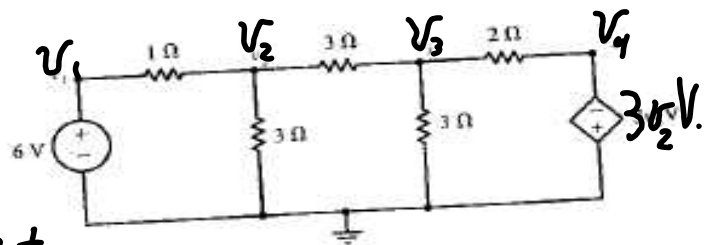
$$i_1 = \frac{v_a - v_b}{2} = \frac{-2 - 0}{2} = -1A$$

$$i_2 = \frac{v_c - v_a}{3} = \frac{-8 - -2}{3} = -\frac{6}{3} = -2A$$

$$i_3 = \frac{v_c - v_d}{4} = \frac{-8 - -4}{4} = -\frac{4}{4} = -1A$$

$$i_4 = \frac{v_b - v_d}{2} = \frac{0 - -4}{2} = \frac{4}{2} = 2A$$

2) 2.7 Find the node voltages for the circuit shown in Fig. P2.7. (See p. 100.)



Using nodal analysis, but skipping the current labels we can write 4 eqns with 4 unknowns.

$$v_1 = 6V \quad (\text{due to source}) \quad (1)$$

$$\text{KVL@ } v_2: \frac{v_2 - v_1}{1\Omega} + \frac{v_2}{3} + \frac{v_2 - v_3}{3\Omega} = 0 \Rightarrow -18 + 5v_2 - v_3 = 0 \Rightarrow 18 = 5v_2 - v_3 \quad (2)$$

$$\text{KVL@ } v_3: \frac{v_3 - v_2}{3} + \frac{v_3}{3} + \frac{v_3 - v_4}{2} = 0 \Rightarrow 7v_3 - 2v_2 - 3v_4 = 0 \quad (3)$$

$$\text{Eqn using dep. source: } v_4 = -3v_2 \quad (4)$$

$$(4) \rightarrow (3) \text{ yields } 7v_3 + 7v_2 = 0 \Rightarrow v_3 + v_2 = 0 \quad (5)$$

$$v_2 = -v_3 \text{ into } (2) \quad 5v_2 + v_2 = 18 \Rightarrow 6v_2 = 18$$

$$v_2 = 3V$$

$$v_3 = -3V$$

$$v_4 = -3v_2 = -9V$$

$$v_1 = 6V$$

3)

3. (20 points) In FoEE, Fig. P1.39: Assume $R_1=4\Omega$ and $R_2=4\Omega$.

- Calculate the current i , using mesh analysis.
- Find the Thevenin equivalent circuit as seen from the two terminals that are connected by the 4Ω "bridge" resistor (the one that "I" is traveling through). Label the left node as "a" and the right node as "b." Be sure to actually draw your Thevenin equivalent circuit.
- Find the Norton equivalent circuit from the same two terminals as in part (b). Again, be sure to draw your Norton equivalent circuit.
- Using your result from (b) or (c), calculate the current i through a 4Ω load resistor.

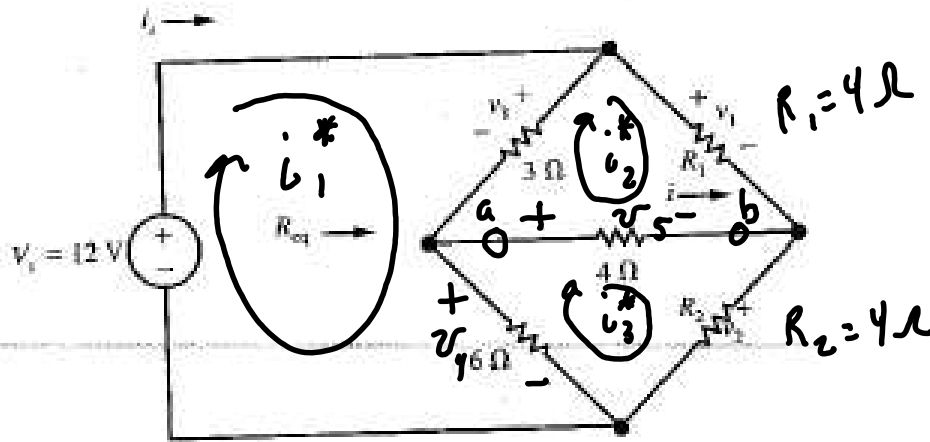


Fig. P1.39

a) Mesh analysis: $12 = v_3 + v_4$
 $v_3 + v_5 = v_1$
 $v_4 = v_5 + v_2$ } our 3 KVL eqns.

$$\begin{aligned} v_1 &= i_1^* 4 \\ v_2 &= i_3^* 4 \\ v_3 &= (i_1^* - i_2^*) 3\Omega \\ v_4 &= (i_1^* - i_3^*) 6 \\ v_5 &= (i_3^* - i_2^*) 4 \end{aligned} \quad \left. \begin{array}{l} \text{Our 5} \\ \text{Ohm's} \\ \text{Law} \\ \text{Egns.} \end{array} \right\}$$

Combining the above eqns we get:

$$12 = (i_1^* - i_2^*) 3 + (i_1^* - i_3^*) 6 \Rightarrow 12 = 9i_1^* - 3i_2^* - 6i_3^*$$

$$\Rightarrow 4 = 3i_1^* - i_2^* - 2i_3^*$$

$$(i_1^* - i_2^*) 3 + (i_3^* - i_2^*) 4 = i_2^* 4 \Rightarrow 3i_1^* - 11i_2^* + 4i_3^* = 0$$

$$(i_1^* - i_3^*) 6 = (i_3^* - i_2^*) 4 + i_3^* 4 \Rightarrow 6i_1^* + 4i_2^* - 14i_3^* = 0$$

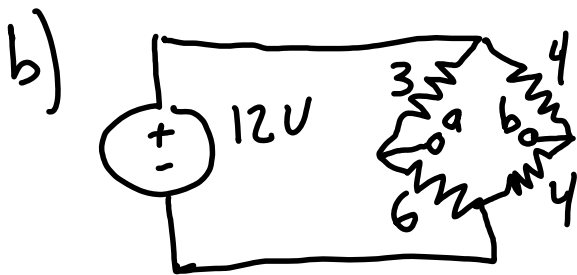
Solving this system of equations gives us:

$$i_1^* = 2.875$$

$$i_2^* = 1.375$$

$$i_3^* = 1.625$$

$$i = i_3^* - i_2^* = .25 \text{ A}$$



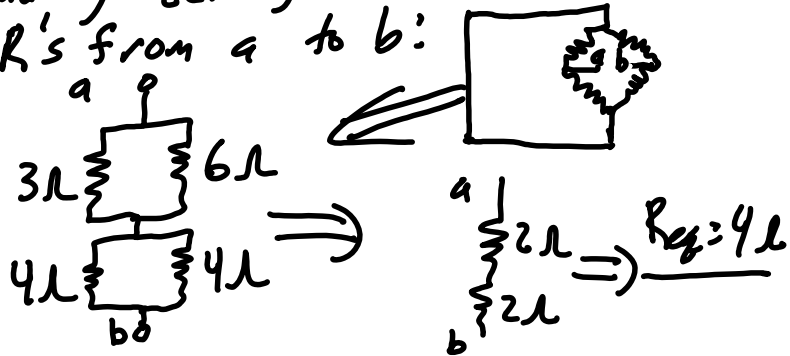
$$V_{oc} = V_a - V_b$$

$$V_a \text{ by voltage division is } \frac{6}{9} \cdot 12 = 8V$$

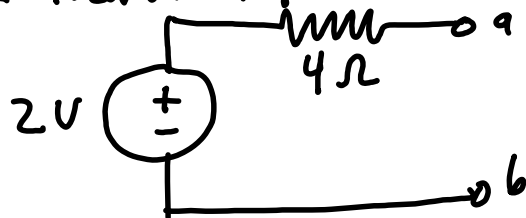
$$V_b \text{ by voltage div is } 6V.$$

$$\therefore V_{oc} = 2V$$

R_{eq} can be found by zeroing our indep. source and combining R's from a to b:

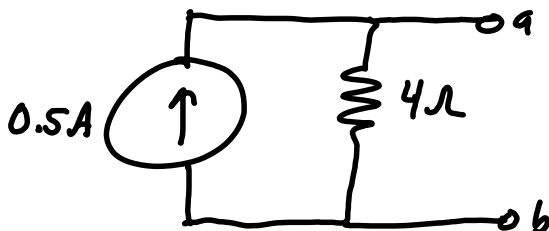


So, the Thevenin Equivalent will be

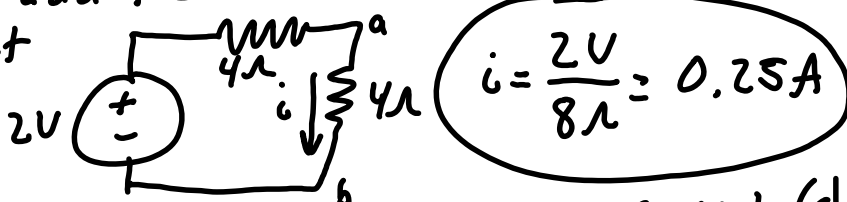


c) We can find $i_{sc} = \frac{V_{oc}}{R_{eq}} = \frac{2}{4} = 0.5A$

So, the Norton Equivalent is



d) Using the Thevenin Eq. from part (b) we can add the load resistance of 4Ω to get



$$i = \frac{2V}{8\Omega} = 0.25A$$

Same answer as in (a).

4)

2.41 For the circuit given in Fig. P2.41, determine the value of R_L , which absorbs the maximum amount of power, and find this power when $v_s = 20$ V.

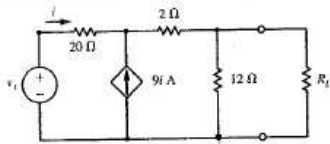
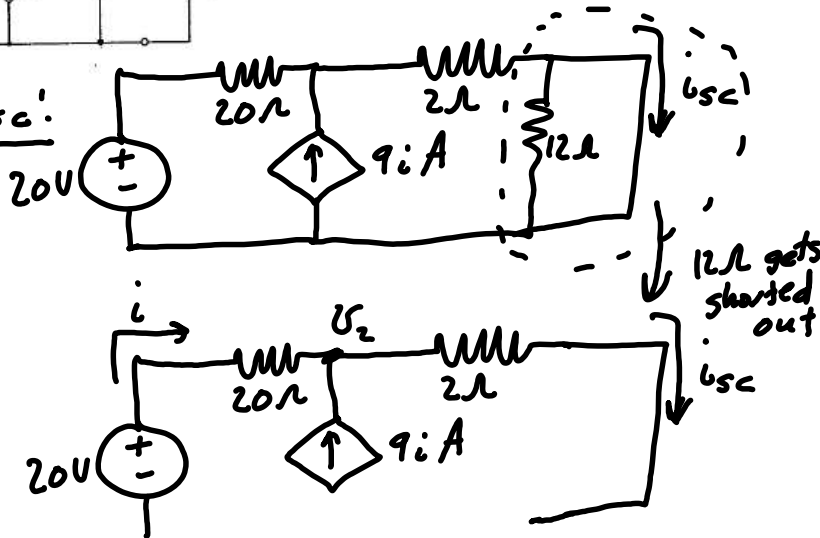


Fig. P2.41

Find R_{eq} to determine R_L for max power.

We can find V_{oc} & i_{sc} :

For i_{sc} :

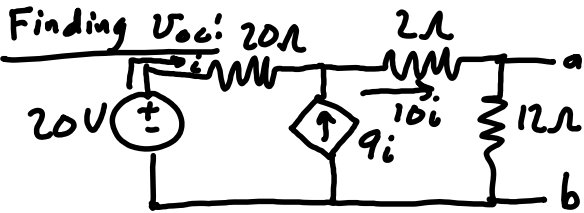


Ohm's Law:

$$\frac{20 - V_2}{20} = i \quad \& \quad 10i = \frac{V_2}{2} \quad \text{by KCL} \quad \text{Combine & solve: } 10\left(\frac{20 - V_2}{20}\right) = \frac{V_2}{2}$$

$$\frac{20 - V_2}{2} = \frac{V_2}{2} \Rightarrow V_2 = 10V$$

$$i_{sc} = \frac{10V}{2\Omega} = 5A$$



KVL around outer loop:

$$20 = 20i + (10i)2 + (10i)12$$

$$i = \frac{1}{8}A$$

$$\text{So } V_{ab} = V_{oc} = (10i)12 = 10\left(\frac{1}{8}\right)(12) = 15V$$

$$\therefore R_{eq} = \frac{15V}{5A} = 3\Omega$$

$$Max \text{ Power} = \frac{V_{oc}^2}{4R_L} = \frac{225}{(4)(3)} = 18.75W$$

5)

2.61 Consider the circuit shown in Fig. P2.61. (a) Find the portion of i and the portion of v that are due to the 2-A current source. (b) Find the portion of i and the portion of v that are due to the 6-V voltage source. (c) Find the portion of i and the portion of v that are due to the 4-V voltage source. (d) Find i and v .

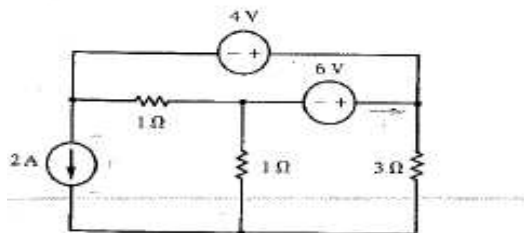
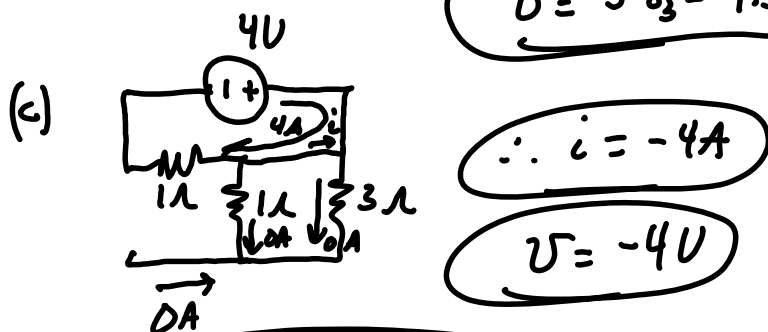
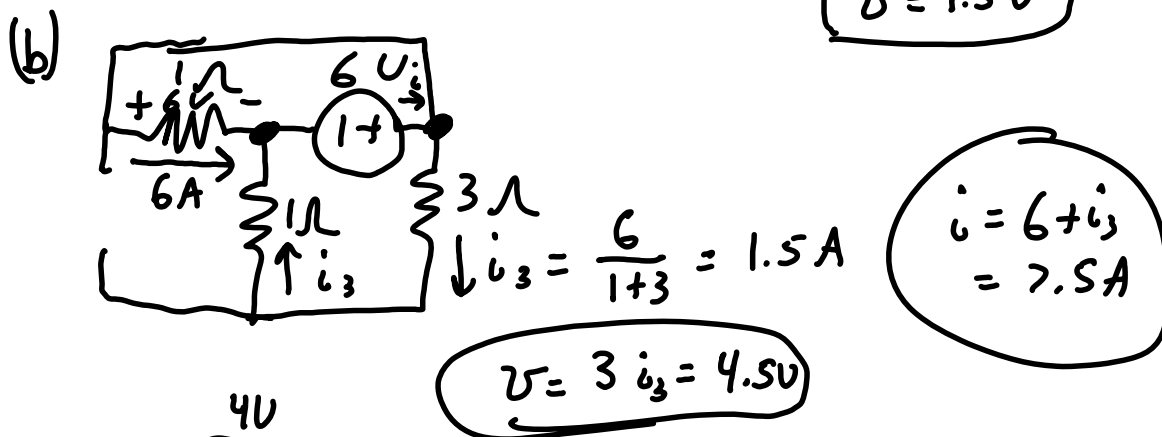
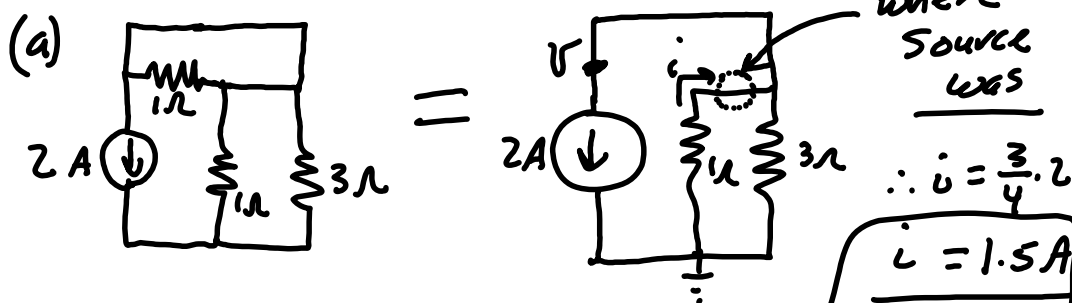


Fig. P2.61

Using Superposition/Linearity:



(d)

$$\sum i \text{ from a, b, c} = 5A$$

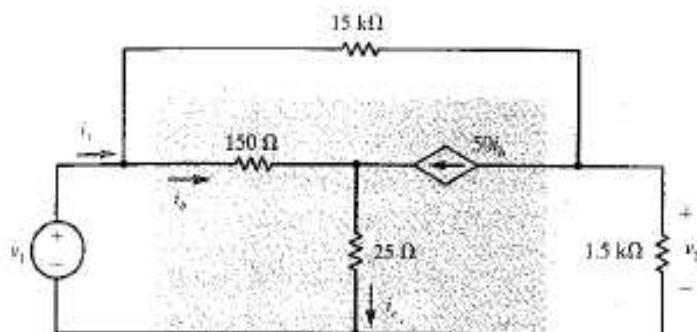
$$v = -1V$$

Optional Problems

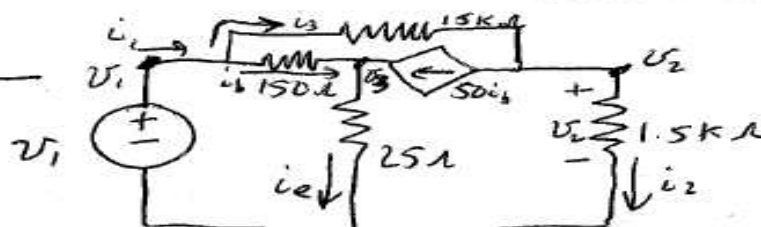
6)

2.14 The circuit shown in Fig. P2.14 is a single BJT amplifier with "feedback." The portion of the circuit in the shaded box is an approximate T-model of a transistor in the common-emitter configuration. (a) Use nodal analysis to find the voltage gain

v_2/v_1 of the amplifier. (b) Use the results of part (a) to determine the input resistance v_1/i_1 of the amplifier.



③ For 2.14



KCL @ v_1 node: $i_1 = i_b + i_3$ ①

" @ v_3 node: $i_b + 50i_b = i_e$ ②

@ v_2 node: $i_3 = 50i_b + i_2$ ③

Make replacements where possible using Ohm's law:

① $i_1 = \frac{v_1 - v_3}{150} + \frac{v_1 - v_2}{15,000}$

② $\frac{v_1 - v_3}{150} + 50\left(\frac{v_1 - v_3}{150}\right) = \frac{v_3}{25}$

③ $\frac{v_1 - v_2}{15,000} = 50\left(\frac{v_1 - v_3}{150}\right) + \frac{v_2}{1500}$

From ②: $51\left(\frac{v_1 - v_3}{150}\right) = \frac{v_3}{25} \Rightarrow 51v_1 - 51v_3 = 6v_3$
 $\Rightarrow v_3 = \frac{51}{57}v_1$

For ③: $v_1 - v_2 = 5000(v_1 - v_3) + 10v_2$

$v_1 - v_2 = 5000\left(\frac{6}{57}v_1\right) + 10v_2$

$v_1 - \frac{30,000}{57}v_1 = 11v_2$

$\frac{v_2}{v_1} = \frac{-29943}{11 \times 57} = -47.76$

⑥ From ① above: $i_1 = \frac{v_1 - \frac{51}{57}v_1}{150} + \frac{v_1 - -47.76v_1}{15,000}$

$\frac{i_1}{v_1} = \frac{\frac{6}{57}}{150} + \frac{48.76}{15,000} = 0.00395$

$50 \frac{v_1}{i_1} = 253.3 \Omega$

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Using mesh currents:

$$v_a = i_1 \cdot 4$$

$$v_b = i_2 \cdot 4$$

$$v_c = (i_2 - i_3) \cdot 3$$

$$v_d = i_3 \cdot 3$$

$$\begin{pmatrix} i_1^* - i_3^* \\ -2 - i_3^* + 6 \end{pmatrix} + 6 = 3 \hat{i}_3^* \implies 4i_3^* = 4$$

