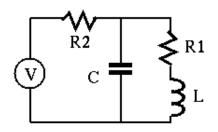


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E84 Home Work 9

1. The load of a voltage soruce of $v(t) = 110\sqrt{2} \cos(2\pi 60 t)$ is shown in the figure, where $R_1 = 100\Omega$, $R_2 = 50\Omega$, $C = 6.63\mu F$, L = 0.53H. Is the load capacitive ($\phi = \tan^{-1}(X/R) < 0$) or inductive ($\phi > 0$)? Find the power factor, the apparent power, the real power and the reactive power.



Solution:

$$Z_C = -\frac{j}{\omega C} = -\frac{j}{2\pi 60 \times 6.63 \times 10^{-6}} = -j400\Omega$$

$$Z_L = j\omega L = j2\pi 60 \times 0.53 = j200\Omega, \quad Z_{RL} = 100 + j200$$

$$Z_{CRL} = \frac{Z_C Z_{RL}}{Z_C + Z_{RL}} = \frac{(100 + j200)(-j400)}{100 + j200 - j400} = \frac{800 - j400}{1 - j2}$$

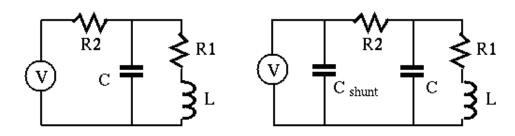
$$Z_{total} = Z_{CRL} + R_2 = \frac{800 - j400}{1 - j2} + 50 = 370 + j240 = 441 \angle 33^{\circ}$$

The load is inductive as $\phi > 0$.

$$\dot{I} = \frac{\dot{V}}{Z_{total}} = \frac{110}{441 \angle 33^{\circ}} = 0.25 \angle - 33^{\circ}$$

power factor is $\lambda = cos(-33^\circ) = 0.839$, the apparent power is $S = 110 \times 0.25 = 27.5W$, the real power is $P = S \cos 33^\circ = 27.5 \times 0.84 = 23W$ the reactive power is $Q = S \sin 33^\circ = 27.5 \times 0.54 = 15W$

2. To improve the power factor of the circuit above to 0.9, a shunt capacitor is added. What should the capacitance *C* be? What should *C* be if the power factor is required to be 1?



Solution:

Adding a shunt capacitor with impedance $1/j\omega C = -jX$ ($X = 1/\omega C$), the overall load impedance is

$$Z_{all} = -jX ||Z_{total} = \frac{-jX(370+j240)}{-jX+(370+j240)} = \frac{240X-j370X}{370-j(X-240)} = |Z| \angle Z = |Z| \angle \phi$$

For the power factor to be 0.9, this impedance need to have a phase

angle $\phi = \cos^{-1} 0.9 = 25.84^{\circ}$, and we need to have:

$$\tan^{-1}\left[\frac{-370X}{240X}\right] - \tan^{-1}\left[\frac{-(X-240)}{370}\right] = -57^{\circ} + \tan^{-1}\left[\frac{X-240}{370}\right] = 25.84^{\circ}$$

$$\tan^{-1}\left[\frac{X-240}{370}\right] = 82.84^{\circ}, \quad \frac{X-240}{370} = \tan 82.84^{\circ} = 7.96, \quad X = 3185.4$$

$$\frac{1}{\omega C} = X = 3185.4, \quad C = \frac{1}{2\pi 60 \times 3185.4} = 0.83 \mu F$$

For the power factor to be 1, we need to have

$$\tan^{-1}\left[\frac{-370X}{240X}\right] - \tan^{-1}\left[\frac{-(X - 240)}{370}\right] = -57^{\circ} + \tan^{-1}\left[\frac{X - 240}{370}\right] = 0^{\circ}$$

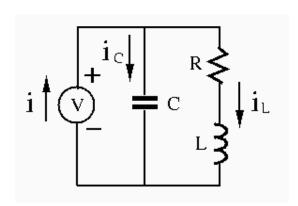
i.e.,

$$\tan^{-1}\left[\frac{X-240}{370}\right] = 57^{\circ}, \quad \frac{X-240}{370} = \tan 57^{\circ} = 1.54, \quad X = 810$$

$$\frac{1}{\omega C} = X = 810, \quad C = \frac{1}{2\pi 60 \times 810} = 3.27 \mu F$$

3. In the circuit shown below, the voltage source $v(t) = 100 \sqrt{2} \sin 314t$ volts, and the effective values of the three currents \underline{i} , i_L and i_C are

the same. The total real energy comsumed by the circuit is 866 W. Find the values of R, L and C. (Hint: represent all currents $\underline{i(t)}$, $\underline{i_C(t)}$, $\underline{i_L(t)}$ and voltage $\underline{v(t)}$ as phasors \dot{I} , $\dot{I_C}$, $\dot{I_L}$, \dot{V} , and draw them as vectors to figure out how they are related.)



Solution: Let $\dot{V} = 100 \angle 0$ be the phasor representation of v(t) so that

$$v(t) = Im[\sqrt{2}\dot{V}e^{j\omega t}] = Im[\sqrt{2}\dot{V}e^{j314t}]$$

where $\omega = 2\pi f = 314$, i.e., f = 50 Hz. We have

$$\dot{I}_C = j\omega C \dot{V} = 100\omega C \angle 90^\circ, ~~\dot{I}_L = \frac{\dot{V}}{R+j\omega L} = \frac{100}{\sqrt{R^2+\omega^2 L^2}} \angle - \phi$$

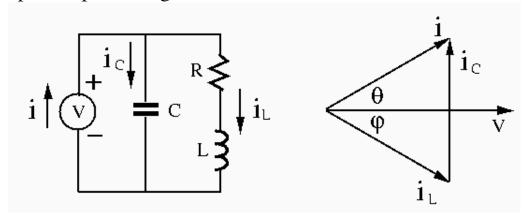
where $\phi = tan^{-1}(\omega L/R)$. Due to KCL, we hav

$$\dot{I} = \dot{I}_C + \dot{I}_L$$

but also as given

$$|\dot{I}| = |\dot{I}_C| = |\dot{I}_L| = I$$

we conclude that these three currents are equal in magnitude and 60° apart in phase angle, as shown below:



where \dot{I}_C is 90° ahead of \dot{V} , \dot{I} is $\theta = 30^\circ$ ahead of \dot{V} , which in turn is $\phi = 30^\circ$ ahead of \dot{I}_L . Therefore,

$$\dot{I} = I \angle \theta = I \angle 30^{\circ}, \quad \dot{I}_L = I \angle \phi = I \angle - 30^{\circ}, \quad \dot{I}_C = I \angle 90^{\circ}$$

As the real power is

$$P = 866 = VI\cos\phi = 100I\cos(-30^\circ) = 86.6I$$

we get

$$I = 10A$$

therefore we also get

$$P = 866 = RI^2 = R100, \quad R = 8.66\Omega$$

and

$$\dot{I} = 10\angle 30^{\circ}, \quad \dot{I}_L = 10\angle - 30^{\circ}, \quad \dot{I}_C = 10\angle 90^{\circ}$$

But from above

$$\dot{I}_C = 100\omega C \angle 90^\circ = 10\angle 90^\circ$$

we get:

$$\omega C = 0.1, \quad C = 0.1/314 = 3.18 \times 10^{-4} \; F$$

Since we also have:

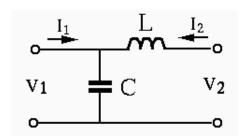
$$\dot{I}_L = \frac{100}{\sqrt{R^2 + \omega^2 L^2}} \angle - \phi = 10 \angle - 30^\circ$$

solving this we get

$$\omega L = 5, \qquad L = 5/\omega = 5/314 = 0.0159 \; H$$

4. Read and understand the notes about two-port networks on <u>this page</u> (before the title ``Principle of reciprocity", which will not be covered), especially the two examples, and then you should be able to do the following three problems.

Find the Z-model and Y-model of the circuit shown in the figures, by assuming one of the two known variables (currents or voltages) is zero at a time. Then verify your results by checking whether $\mathbf{Z}^{-1} = \mathbf{Y}$.



Solution:

For the Z-model, item Assume $I_2 = 0$ (open-circuit), then

$$Z_{11} = V_1/I_1 = 1/j\omega C$$
, $Z_{21} = V_2/I_1 = 1/j\omega C$

• Assume $I_1=0$ (open-circuit), then $Z_{12}=V_1/I_2=1/j\omega C$, $Z_{22}=V_2/I_2=j\omega L+1/j\omega C$

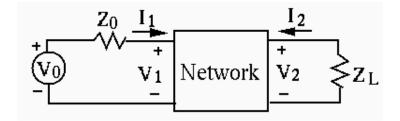
For the Y-model,

- Assume $V_2 = 0$ (short-circuit), then $Y_{11} = I_1/V_1 = j\omega C + 1/j\omega L$, $Y_{21} = I_2/V_1 = 1/j\omega L$
- Assume $V_1 = 0$ (short-circuit), then $Y_{12} = I_1/V_2 = 1/j\omega L$, $Y_{22} = I_2/V_2 = 1/j\omega L$

verify:

$$\mathbf{Z}^{-1} = \left[\begin{array}{cc} 1/j\omega C & 1/j\omega C \\ 1/j\omega C & j\omega L + 1/j\omega C \end{array} \right]^{-1} = \frac{C}{L} \left[\begin{array}{cc} j\omega L + 1/j\omega C & -1/j\omega C \\ -1/j\omega C & 1/j\omega C \end{array} \right] = \left[\begin{array}{cc} j\omega C + 1/j\omega L & -1/j\omega L \\ -1/j\omega L & 1/j\omega L \end{array} \right]$$

5. The parameters of the Y-model of the two-port network are $Y_{11} = -4$, $Y_{12} = 3$, $Y_{21} = 3$, and $Y_{22} = -2$. The voltage source is $V_0 = 5V$, $V_0 = 10$, $V_0 = 10$. Find variables $V_0 = 10$, $V_0 = 10$, $V_0 = 10$. Hint: refer to Method 1 in the example shown in the web notes.



Solution:

• Convert Y-model to Z-model:

$$\mathbf{Z} = \mathbf{Y}^{-1} = \begin{bmatrix} -4 & 3 \\ 3 & -2 \end{bmatrix}^{-1} = \begin{bmatrix} 2 & 3 \\ 3 & 4 \end{bmatrix}$$

$$\begin{cases} V_1 = 2I_1 + 3I_2 \\ V_2 = 3I_1 + 4I_2 \end{cases}$$

Setup additional equations:

$$\begin{cases} V_1 = V_0 - R_0 I_1 \\ V_2 = -Z_L I_2 \end{cases}$$

 \circ Find I_1 and I_2 :

$$\left\{ \begin{array}{l} 2I_1+3I_2=V_0-R_0I_1\\ 3I_1+4I_2=-Z_LI_2 \end{array} \right. \text{ i.e. } \left\{ \begin{array}{l} (2+R_0)I_1+3I_2=V_0\\ 3I_1+(4+Z_L)I_2=0 \end{array} \right.$$

These equations can be solved to get

$$I_1 = \frac{5(4+j)}{3(1+j)}, \qquad I_2 = -\frac{5}{1+j}$$

 \circ Find V_1, V_2 :

$$V_2 = -I_2 Z + L = \frac{j5}{1+j}, \qquad V_1 = -\frac{5(1-j2)}{3(1+j)}$$

6. Repeat the previous problem but this time use Thevenin's theorem to find V_2 across load R_L . (Hint: refer to Method 2 in the example shown in the <u>web notes</u>)

Solution:

$$\begin{cases} V_1 = 2I_1 + 3I_2 \\ V_2 = 3I_1 + 4I_2 \end{cases}$$

$$\begin{cases} V_1 = V_0 - R_0 I_1 \\ V_2 = -Z_L I_2 \end{cases}$$

First, find Z_{Th} when the voltage souce is short circuit:

- Equating $V_1 = V_0 R_0 I_1 = -I_1$ to $V_1 = 2I_1 + 3I_2$, we get $2I_1 + 3I_2 = -I_1$, i.e., $I_1 = -I_2$.
- Substituting $I_1 = -I_2$ into $V_2 = 3I_1 + 4I_2$, we get $V_2 = I_2$, i.e., $Z_{Th} = V_2/I_2 = 1$.

Second, find V_{Th} when the load is open circuit, i.e., $I_2 = 0$:

- Since $I_2 = 0$, the Z-model equations become $V_1 = 2I_1$, $V_2 = 3I_1$.
- We also get $I_1 = (V_0 V_1)/R_0 = 5 V_1 = 5 2I_1$, which can be solved to get $I_1 = 5/3$.

• Then $V_{Th} = V_2 = 3I_1 = 5$.

Finally, we can find voltage across R_L as

$$V_2 = V_{Th} \; \frac{Z_L}{Z_{Th} + Z_L} = \frac{j5}{1+j}$$

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