Seawater Intrusion

Groundwater Engineering | CE60205

Lecture:21

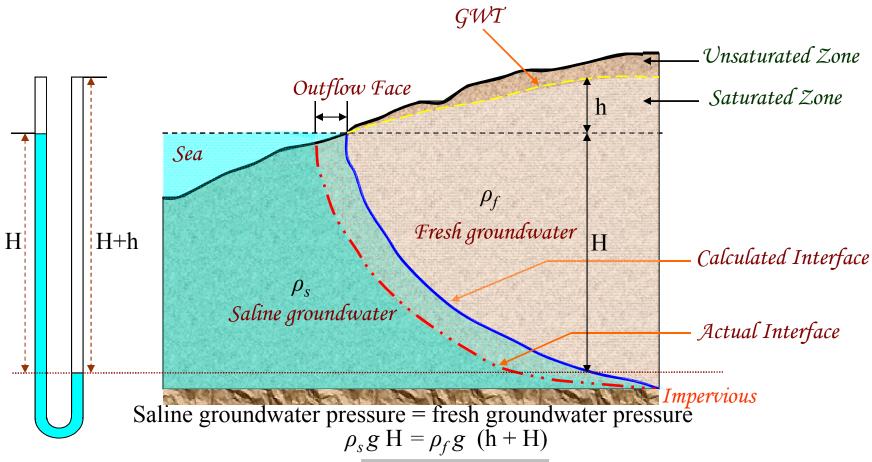
Learning Objective(s)

To explain saltwater intrusion in the context of flow and transport models.

Descriptive modeling of saltwater intrusion

- Simple approximation based solution.
- Sharp interface simulation.
- Density dependent flow simulation

Bodon Ghyben-Herzberg Principle



$$\rho_s = 1025 \text{ kg/m}^3$$
 $\rho_f = 1000 \text{ kg/m}^3$

$$h = \frac{\rho_s - \rho_f}{\rho_f} - H$$

Darcy's law for a homogeneous isotropic aquifer

$$q_x = -k \frac{\partial \phi}{\partial x} \qquad q_y = -k \frac{\partial \phi}{\partial y}$$

Discharge vector

$$Q_x = hq_x = -kh \frac{\partial \phi}{\partial x}$$
 $Q_y = hq_y = -kh \frac{\partial \phi}{\partial y}$

• Thickness of the aguifer may be represented as a linear function

$$h = \alpha \phi + \beta$$

Case where $\alpha \neq 0$

$$Q_x = -\frac{\partial}{\partial x} \left[\frac{1}{2\alpha} k(\alpha \phi + \beta)^2 \right] \qquad Q_y = -\frac{\partial}{\partial y} \left[\frac{1}{2\alpha} k(\alpha \phi + \beta)^2 \right]$$

Case where $\alpha = 0$

$$Q_x = -\frac{\partial}{\partial x} [\beta k \phi] \qquad Q_y = -\frac{\partial}{\partial y} [\beta k \phi]$$

By defining the potential Φ as

Case where $\alpha \neq 0$

$$\Phi = \frac{1}{2}k\alpha(\phi + \beta/\alpha)^2 + C$$

where C stands for a constant

Case where $\alpha = 0$

$$\Phi = k\beta\phi + C$$

• Discharge Vector

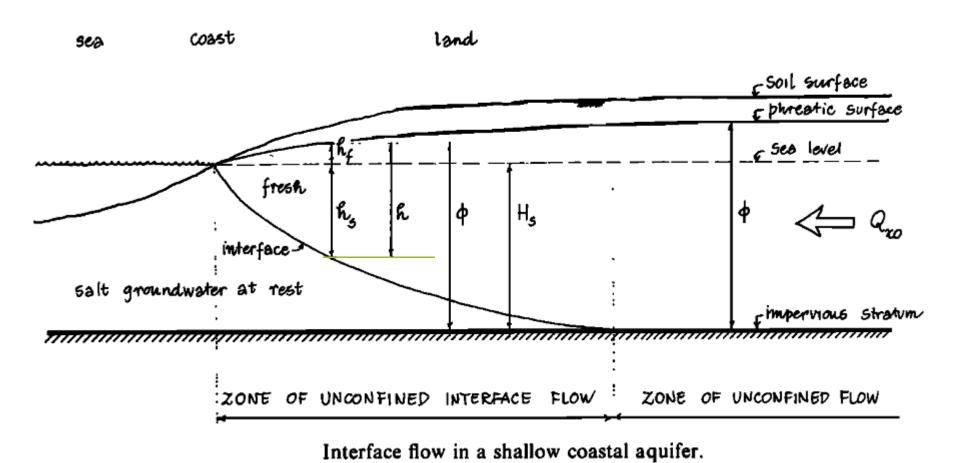
$$Q_x = -\partial \Phi/\partial x$$
 $Q_y = -\partial \Phi/\partial y$

$$\frac{\partial Q_x}{\partial x} + \frac{\partial Q_y}{\partial y} = I$$

where I represents some constant influx into the aquifer from either above or below.

$$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} = -I$$

Sharp Interface Approximation



• The total height of the flow region

$$h = h_f + h_s$$

• Ghyben-Herzberg formula

$$h_{s} = h_{f} [\rho_{f} / (\rho_{s} - \rho_{f})]$$

Head

$$\phi = h_f + H_S$$

Total height

$$h = h_f [\rho_f / (\rho_S - \rho_f)] = h_S (\rho_S / \rho_f)$$

Potential Φ

$$\Phi = \frac{1}{2}K[\rho_s/(\rho_s - \rho_f)](\phi - H_s)^2 + C_{ui}$$

• Dupuit-Forchheimer assumption

$$\phi = h$$

$$\phi = h$$
 $\alpha = 1$ $\beta = 0$

$$\Phi = \frac{1}{2}k\phi^2 + C_u$$

zone 1

$$\Phi = \frac{1}{2}k \frac{l_s}{l_s - l_t} [\phi - H_s]^2 + C_{ut}$$

zone 2

$$\Phi = \frac{1}{2}k\phi^2 + C_u$$

• The location of the tip of the tongue is defined by the condition

$$h_s = H_s$$

$$\phi = h_f + H_s = \frac{l_s - l_f}{l_f} h_s + H_s$$

$$= \frac{l_s - l_f}{l_f} H_s + H_s = \frac{l_s}{l_f} H_s$$

• Along the tip of the tongue

$$\Phi = \frac{1}{2} \frac{l_s}{l_s - l_f} k \left[\frac{l_s}{l_f} - 1 \right]^2 H_s^2 + C_{ui}$$

$$= \frac{1}{2} \frac{l_s}{l_f} \frac{l_s - l_f}{l_f} k H_s^2 + C_{ui}$$

and

$$\Phi = \frac{1}{2}k\frac{l_s^2}{l_f^2}H_s^2 + C_u$$

$$C_{ul} - C_u = \frac{1}{2}kH_s^2 \frac{l_s}{l_t}$$

Choosing $C_{ut} = 0$

$$C_{ut} = 0 C_u = -\frac{1}{2}kH_s^2 \frac{l_s}{l_t}$$

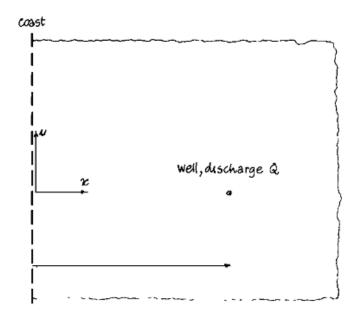
Zone 1

$$\Phi = \frac{1}{2}k\frac{l_s}{l_s-l_f}(\phi-H_s)^2$$

Zone 2

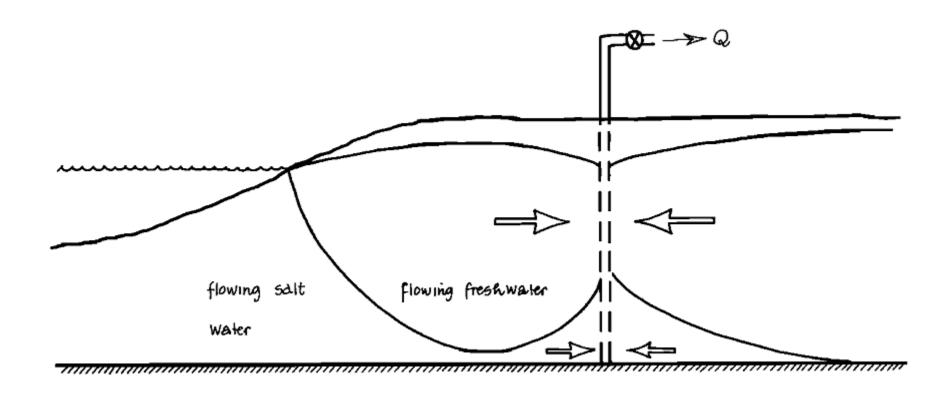
$$\Phi = \frac{1}{2}k\phi^2 - \frac{1}{2}kH_{8}^2 \frac{l_8}{l_f}$$

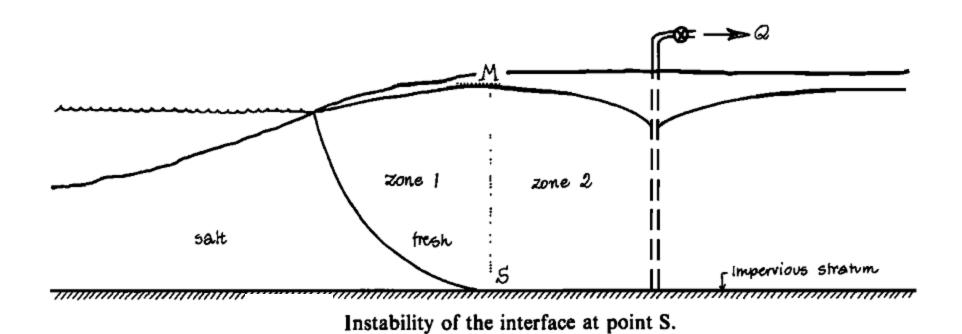
$$\Phi = Q_{x0}x$$



$$\Phi = 0$$
 $x = 0$ $-\infty < y < +\infty$

$$\Phi = \frac{1}{2}kH_{\theta}^{2} \frac{l_{s}}{l_{f}} \frac{l_{s} - l_{f}}{l_{f}} \qquad \Phi = Q_{x0}x + \frac{Q}{2\pi} \ln \left[\frac{(x - x_{w})^{2} + y^{2}}{(x + x_{w})^{2} + y^{2}} \right]^{1/2}$$





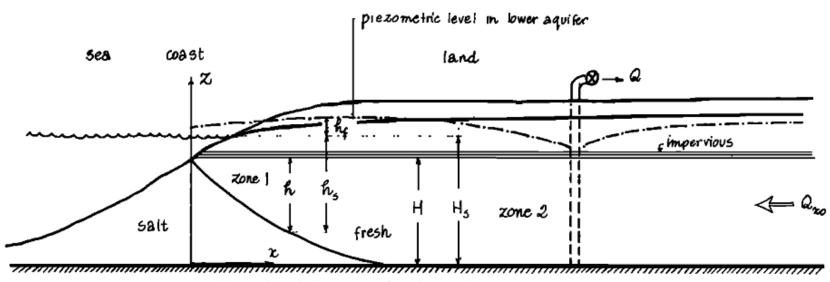
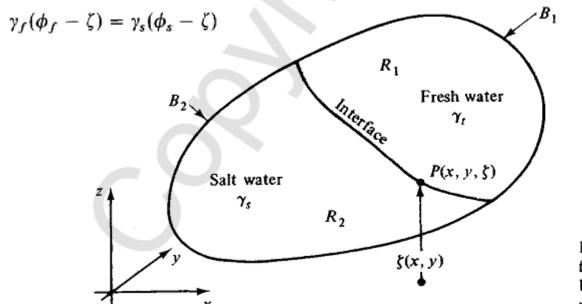


Fig. 10. Mixed confined-confined interface flow.

Determine ϕ_f in R_1 and ϕ_s in R_2 such that

$$\nabla \cdot (K_f \cdot \nabla \phi_f) = S_0 \frac{\partial \phi_f}{\partial t} \quad \text{in } R_1; \qquad \nabla \cdot (K_s \cdot \nabla \phi_s) = S_0 \frac{\partial \phi_s}{\partial t} \quad \text{in } R_2$$



$$F(x, y, z, t) = 0$$

$$F \equiv z - \zeta(x, y, t) = 0$$

Figure 9-3 An abrupt interface between regions occupied by fresh water and by salt water.

$$\zeta(x, y, t) = \phi_s \frac{\gamma_s}{\gamma_s - \gamma_f} - \phi_f \frac{\gamma_f}{\gamma_s - \gamma_f}$$

$$= \phi_s (1 + \delta) - \phi_f \delta; \qquad \delta = \gamma_f / (\gamma_s - \gamma_f)$$

$$F \equiv z - \phi_s(1+\delta) + \phi_f \delta = 0$$

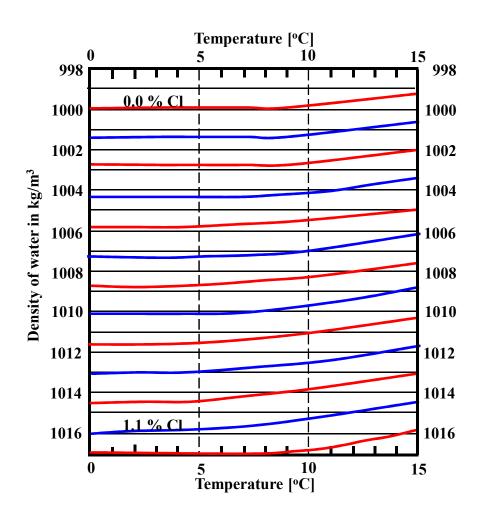
$$dF/dt \equiv \partial F/\partial t + \mathbf{V}_f \cdot \nabla F = 0; \qquad \partial F/\partial t + \mathbf{V}_s \cdot \nabla F = 0$$

$$n\mathbf{V}_f = -\mathbf{K}_f \cdot \nabla \phi_f$$
; $n\mathbf{V}_s = -\mathbf{K}_s \cdot \nabla \phi_s$

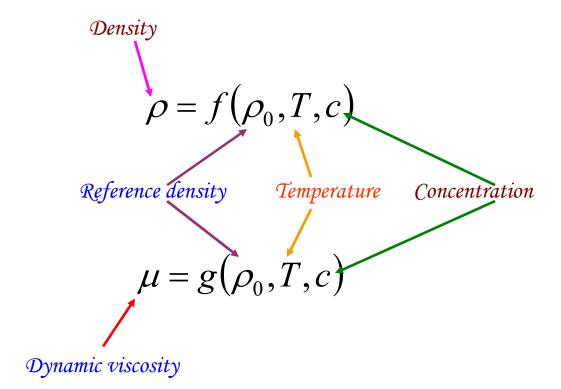
$$n\delta\frac{\partial\phi_f}{\partial t} - n(1+\delta)\frac{\partial\phi_s}{\partial t} - \mathbf{K}_f \cdot \left[\nabla z - (1+\delta)\nabla\phi_s + \delta\nabla\phi_f\right] \cdot \nabla\phi_f = 0$$

$$n\delta\frac{\partial\phi_f}{\partial t} - n(1+\delta)\frac{\partial\phi_s}{\partial t} - K_s \cdot \left[\nabla z - (1+\delta)\nabla\phi_s + \delta\nabla\phi_f\right] \cdot \nabla\phi_s = 0$$

Density of water as a function of the chlorinity and temperature



Equation of state



Diffused Interface Approach (FEMWATER)

• Flow equation:

$$\frac{\rho}{\rho_0} F \frac{\partial \hbar}{\partial t} + \frac{\theta}{\rho_0} \frac{\partial \rho}{\partial C} \frac{\partial C}{\partial t} = \nabla \cdot \left[\mathbf{K} \cdot \left(\nabla \hbar + \frac{\rho}{\rho_0} \nabla z \right) \right] + \frac{\rho^*}{\rho_0} q$$

• Transport equation:

$$\begin{split} \theta \frac{\partial \mathcal{C}}{\partial t} + \rho_b \frac{\partial \bar{\mathcal{C}}}{\partial t} + \mathbf{V} \cdot \nabla \mathcal{C} - \nabla \cdot (\theta \mathbf{D} \, \nabla \mathcal{C}) \\ = \left(\alpha' \frac{\partial \hbar}{\partial t} + \lambda \right) (\theta \mathcal{C} + \rho_b \bar{\mathcal{C}}) - (\theta K_w \mathcal{C} + \rho_b K_s \bar{\mathcal{C}}) + q \mathcal{C}_{in} - \frac{\rho^*}{\rho_0} q + \left(F \frac{\partial \hbar}{\partial t} + \frac{\rho}{\rho_0} \mathbf{V} \cdot \nabla \left(\frac{\rho}{\rho_0} \right) - \frac{\partial \theta}{\partial t} \right) \mathcal{C} \end{split}$$

Thank you