Equation 3 is

$$\dot{ heta}(t) = |P(jw)| A sin(\omega t + \angle P(jw))$$

let c = 22.55 and $\omega = \omega_0$

♠ Result

$$|P(jw)| = \frac{22.55}{\sqrt{1^2 + 1}} = \frac{22.55}{\sqrt{2}} = 15.95$$

2

\phi(\omega) = \angle P(jw)= $-\tan^{-1}\left(\frac{\infty}{\infty} \right)$ \right) $let \omega = \omega_0 > [!tip]Result >$

 $\phi(\omega) = -\tan^{-1}(1) = -45 \deg e$

3 From lab 1 $\alpha = 0.158 \text{ }$ text{ s}\$, then the break frequency is >[!tip] Result >

 $\omega_{0} = \frac{1}{\tau} = \frac{1}{0.158} = 6.33 \frac{1}{s}$

4 Converting to a frequency (Hz)

 $f = \frac{\infty}{2\pi} = 1.007 \text{ Hz}$

Then calculating the period > [!tip] Result >

 $T = \frac{1}{f} = \frac{1}{1.007} = 0.993 \text{ s}$

5 Equation 8 is

 $\phi = -\frac{T_{D}}{T}\times(360^{0})$

 $Using\$\phi = -45^o\$frompart2 and\$T = 0.993 \ s\$frompart4, solvingfor\$T_D\$ > [!tip]Result > 1000 \ substitution for the substitution of the substitu$

 $T_{D} = -\frac{T}{360^{o}} = -\frac{45^{o}(0.993)}{360^{o}} = 0.124 \text{ s}$

6 Equation 9 is

$$v = k\{p\}e + k\{d\} \setminus \{e\}$$

$$v = (k\{p\}+k\{d\})e \to C(D) = \frac{v}{c} = k\{p\} + k\{d\}D$$

Then the transfer function is > [!tip] Result >

 $T\{r\backslash theta\} = \{frac\{CP\}\{1+CP\} = \{frac\{bk\{d\}D + bk\{p\}\}\{D^{2}\} + bk\{d\}D + bk_{p}\}\}\}$

where > [!tip] Supplementary >

```
b = \frac{c}{\frac{22.55}{0.158}}=142.7
 \operatorname{dega}\{n\}^{2} = bk\{p\} \setminus \operatorname{dega}\{n\} = \operatorname{dega}\{b\}
                                                                                                  Let\$b = 142.7\$ and\$k_p = \{4, 50\}\$\$k_p = 4:\$ > [!tip]Result > [*]
 \omega_{n} = 23.9 \frac{rac{rad}{s}}
                                                                                                                                                            k_p = 50 :  > [!tip]Result >
 \omega_{n} = 84.5 \frac{rad}{s}
                           ## 8 From the characteristic equation of a 2nd order system, the poles are the roots of the denominator
-bk\{d\} \pm \sqrt\{ (bk\{d\})^{2} - 4bk\{p\} \} \to (bk\{d\})^{2} - 4bk_{p} = 0
                                                                                                                                                                then the equation for \$k_d\$ is
 k{d} = 2 \setminus \{frac\{k\{p\}\}\{b\}\}\}
                                                                                                                                  Let\$b = 142.7\$\$k_p = 4:\$ > [!tip]Result >
 k_{d} = 2\sqrt{\frac{4}{142.7}} = 0.335
                                                                                                                                                            k_p = 50 :  > [!tip]Result >
 k_{d} = 2\sqrt{frac{50}{142.7}} = 1.184
                                                                                                                                                             ## 9 The transfer function is
T\{r \setminus theta\} = \int frac\{bk\{d\}D + bk\{p\}\}\{D^{2} + bk\{d\}D + bk_{p}\}\}
                                                                                                                                           Then the magnitude is > [!tip] Result >
jbk\{d\} \neq bk\{p\} \mid d\} = \frac{(bk\{p\})^{2} + (k\{d\} \mid b)^{2}}{}
 {\sqrt{ (bk{p})^{2}+(-\omega^{2})^{2}+(bk_{d}\omega)^{2} }}
                                                                                                                                            and the phase shift is > [!tip]Result >
 \angle T\{r \setminus \{jw\} = tn^{-1} \setminus \{frac\{bk\{p\} + jk\{d\} \setminus b\}\} = tn^{-1} \setminus 
 \label{eq:constraint} $$ \operatorname{a^{2}+jbk\{d\} \cap eqa+bk\{p\}} = \operatorname{tn^{-1}\setminus left(\ frac\{k\{d\} \cap eqa\ b\}\{bk\{p\}\}\ right)} $$
 - tn^{-1} \frac{k{d}\omega b}{bk_{p}-\omega^{2}}
                                                                                                                                  ## 10 Letting \sigma = 0 >[!tip] Result >
T\{r \mid theta\}(0) = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jbk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jbk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jbk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}\} = \int frac\{bk\{p\} + jbk\{d\}(0)\}\{-(0)^{2} + jbk\{d\}(0) + bk\{p\}(0) +
 \frac{bk{p}}{bk_{p}} = 1
                                                                Letting\$k_p = 4\$, \$\omega = 23.9\$, \$b = 142.7\$, and\$k_d = 0.335\$Thenthemagnitude is
T_{r\theta}(j\omega) = \frac{142.7 \pm 0.335 \pm 0.39}
\times 142.7 \\times 142.7)^{2} \}{\sqrt{ (142.7 \times 4)^{2} + ((23.9)^{2})^{2} + (0.335)}
 \times 23.9 \times 142.7)^{2}}}
                                                                                                                                                                                  >[!tip]Result>
```

 $T_{r\theta} = \frac{1261.5}{1384.6} = 0.91$

and the phase shift is

\angle $T\{r \mid (j \mid n^{-1} \mid f(\mid f(0.33 \mid 23.9 \mid 142.7) \{142.7 \mid n^{-1} \mid f(\mid f(0.33 \mid 23.9 \mid 142.7) \{142.7 \mid 23.9^{2} \mid f(0.33 \mid 23.9 \mid 23.$

>[!tip]Result>

\angle $T\{r \setminus \{j \setminus \{j \in \{n\}\}\}\} = 63.1^{\circ} - 89.99^{\circ} = -26.89^{\circ} \}$