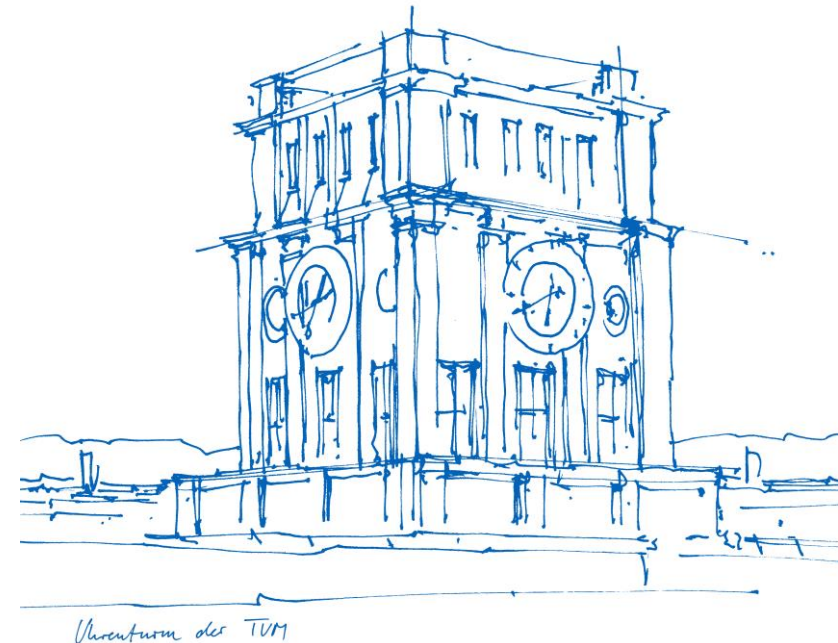


PDE-constrained optimization problems in the field of shallow geothermal energy

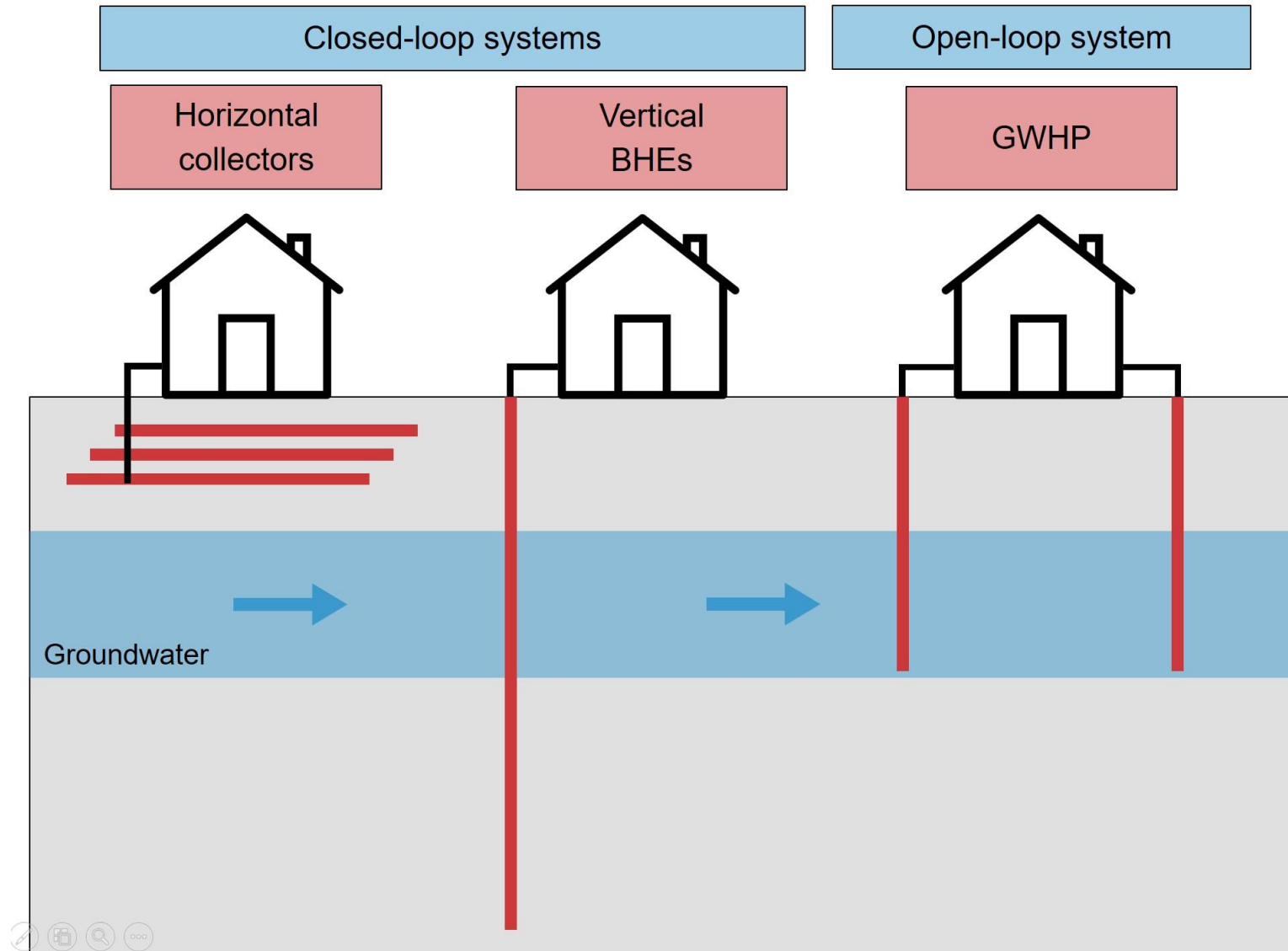
Smajil Halilović¹, Thomas Hamacher¹

¹Chair of Renewable and Sustainable Energy Systems, Technical University of Munich, Germany

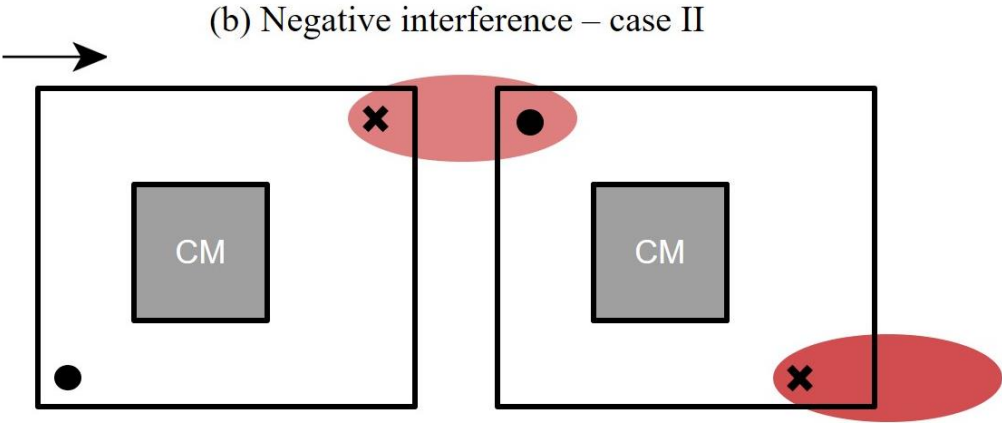
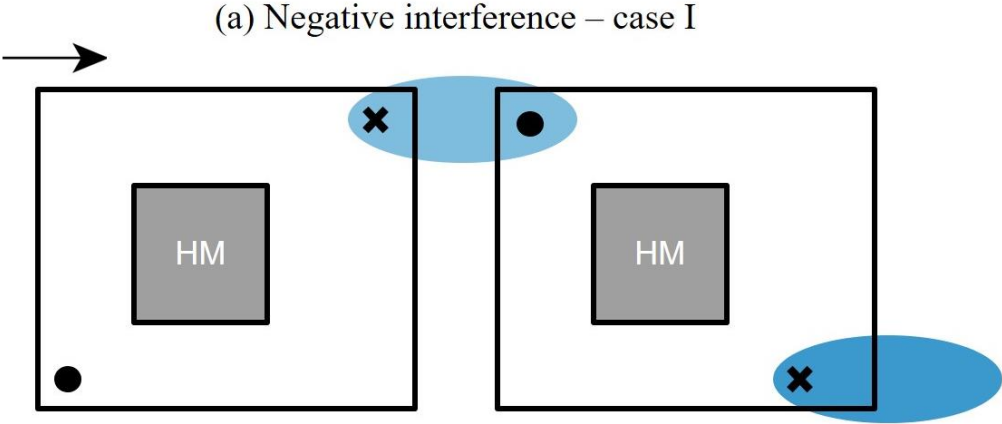
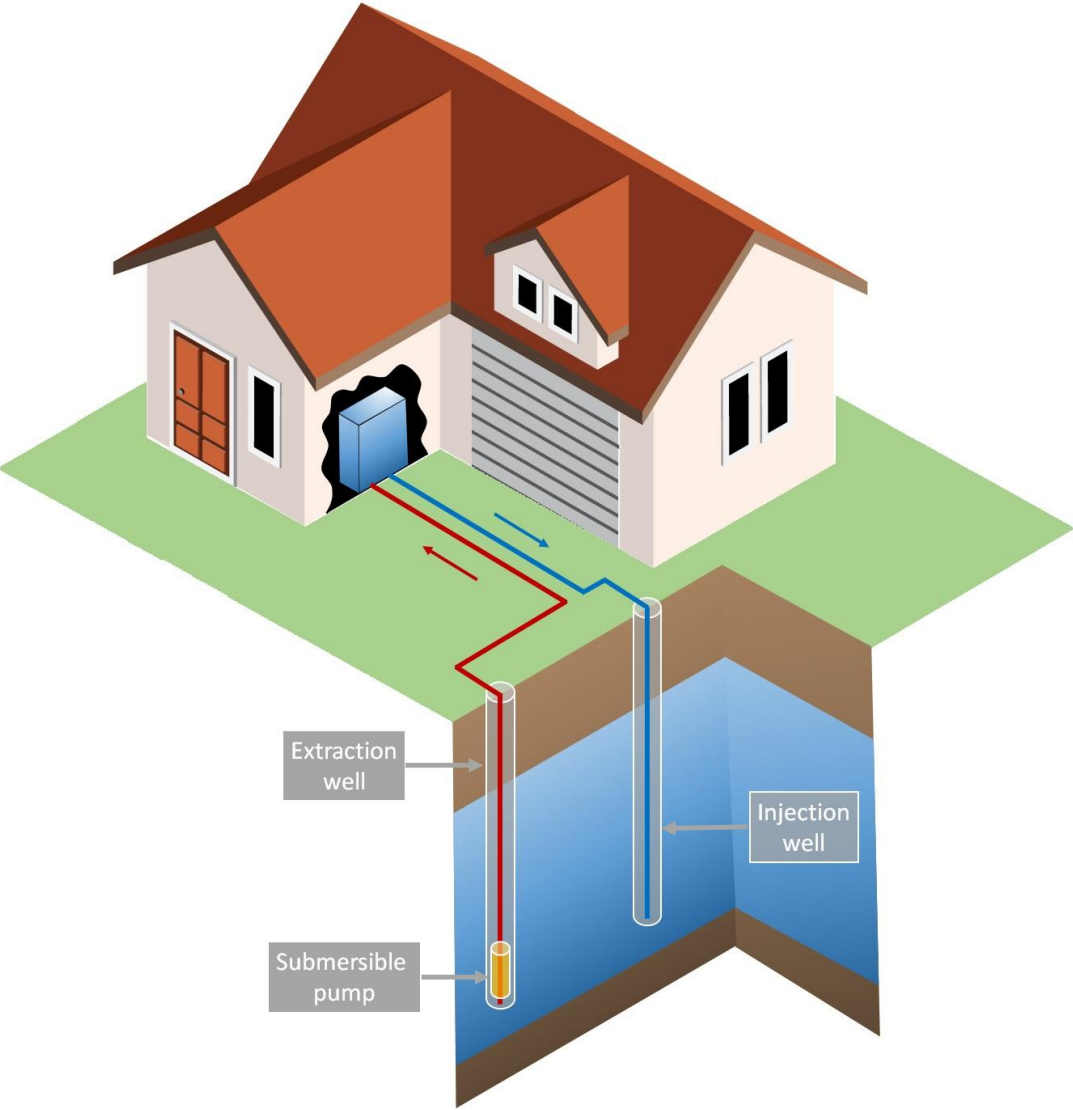
EUCCO 2023, Heidelberg



Shallow geothermal energy (SGE) systems

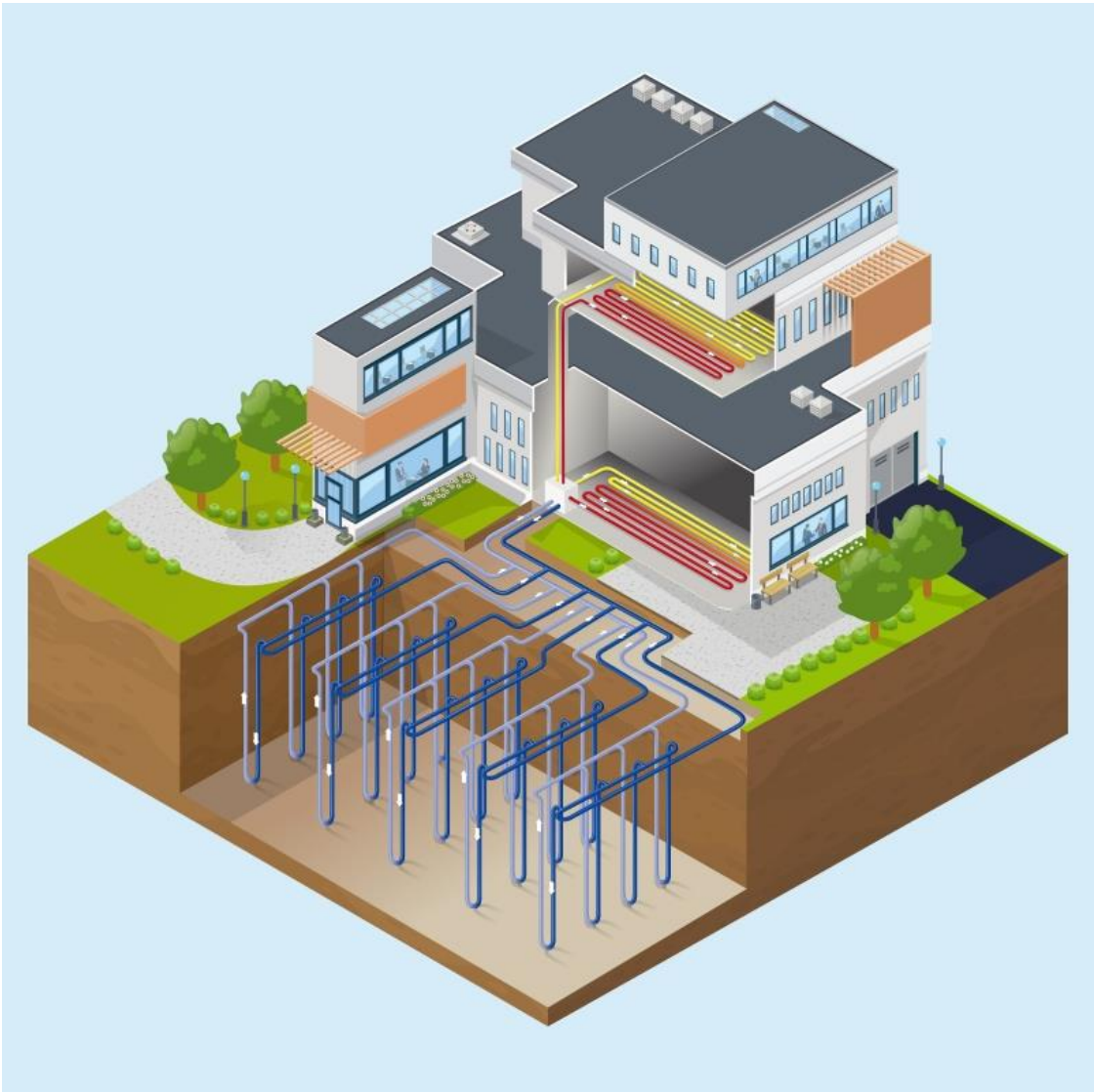


Groundwater heat pumps (GWHPs)

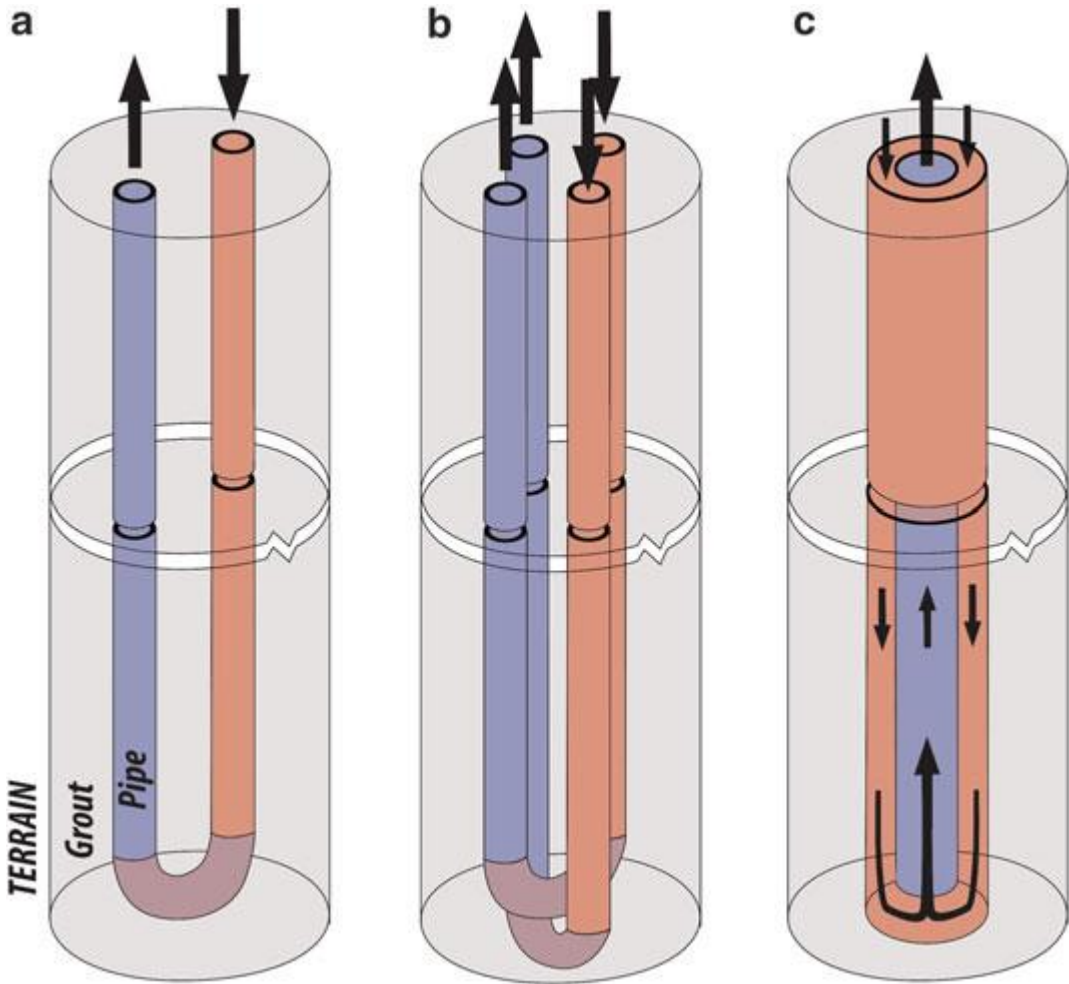


Building	Plot of land	Flow direction
Extraction well	Cold plume	HM Heating mode
Injection well	Warm plume	CM Cooling mode

Ground source heat pumps (GSHPs) with v. BHEs



[1]



Different designs of vertical BHEs [2]

Maximizing the efficiency of SGE systems while meeting regulatory and technical conditions

GWHP optimization [3]

Optimal well placement for multiple GWHPs

Adjoint approach
FEM (Firedrake)

GSHP optimization [4]

Optimal control of individual BHE loads

Collaborators:

- Fabian Böttcher, Stefan C. Kramer, Prof. Matthew D. Piggott, Kai Zosseder, Prof. Thomas Hamacher
- Bodo Lipp, Prof. Michael Ulbrich

[3] Halilovic, S., Böttcher, F., Kramer, S. C., Piggott, M. D., Zosseder, K., & Hamacher, T. (2022). *Well layout optimization for groundwater heat pump systems using the adjoint approach*. Energy Conversion and Management, 268, 116033.
<https://doi.org/10.1016/j.enconman.2022.116033>

2D vertically averaged steady state groundwater flow and heat transport in aquifer

- Flow PDEs:

$$(BS_0 + \varepsilon_e) \frac{\partial h}{\partial t} + \nabla \cdot (B\mathbf{q}) = \bar{Q}$$

$$\mathbf{q} = -\mathbf{K} \cdot \nabla h$$

$$B = h - f^B$$

$$\bar{Q} = \sum_{i=1}^N q_i(t) \delta(\mathbf{x} - \mathbf{x}_i^{\text{inj}}) - q_i(t) \delta(\mathbf{x} - \mathbf{x}_i^{\text{ext}})$$

- Heat transport PDE:

$$BC_m \frac{\partial T}{\partial t} + BC_w \mathbf{q} \cdot \nabla T - \nabla \cdot (B\mathbf{\Lambda} \cdot \nabla T) = \bar{P}_t$$

$$\bar{P}_t = \sum_{i=1}^N q_i(t) C_w [T(\mathbf{x}_i^{\text{inj}}, t) - T] \delta(\mathbf{x} - \mathbf{x}_i^{\text{inj}})$$



- Steady state PDE system:

$$\nabla \cdot (B\mathbf{q}) = \bar{Q}$$

$$\mathbf{q} = -\mathbf{K} \cdot \nabla h$$

$$BC_w \mathbf{q} \cdot \nabla T - \nabla \cdot (B\mathbf{\Lambda} \cdot \nabla T) = \bar{P}_t$$

- Tensor of hydrodynamic thermal dispersion:

$$\mathbf{\Lambda} = \mathbf{\Lambda}_0 + \mathbf{\Lambda}_0^s + \rho c \mathbf{D}_{\text{mech}}$$

$$\mathbf{\Lambda}_0 = \varepsilon s \mathbf{\Lambda} \mathbf{I}$$

$$\mathbf{\Lambda}_0^s = (1 - \varepsilon) \mathbf{\Lambda}^s \mathbf{I}$$

$$\mathbf{D}_{\text{mech}} = \beta_T \|\mathbf{q}\| \mathbf{I} + (\beta_L - \beta_T) \frac{\mathbf{q} \otimes \mathbf{q}}{\|\mathbf{q}\|}$$

Smooth approximation of Dirac functions

Dirac delta functions problematic for gradient based optimization
→ Replace them with smooth 'bump' functions

- Using exponential terms

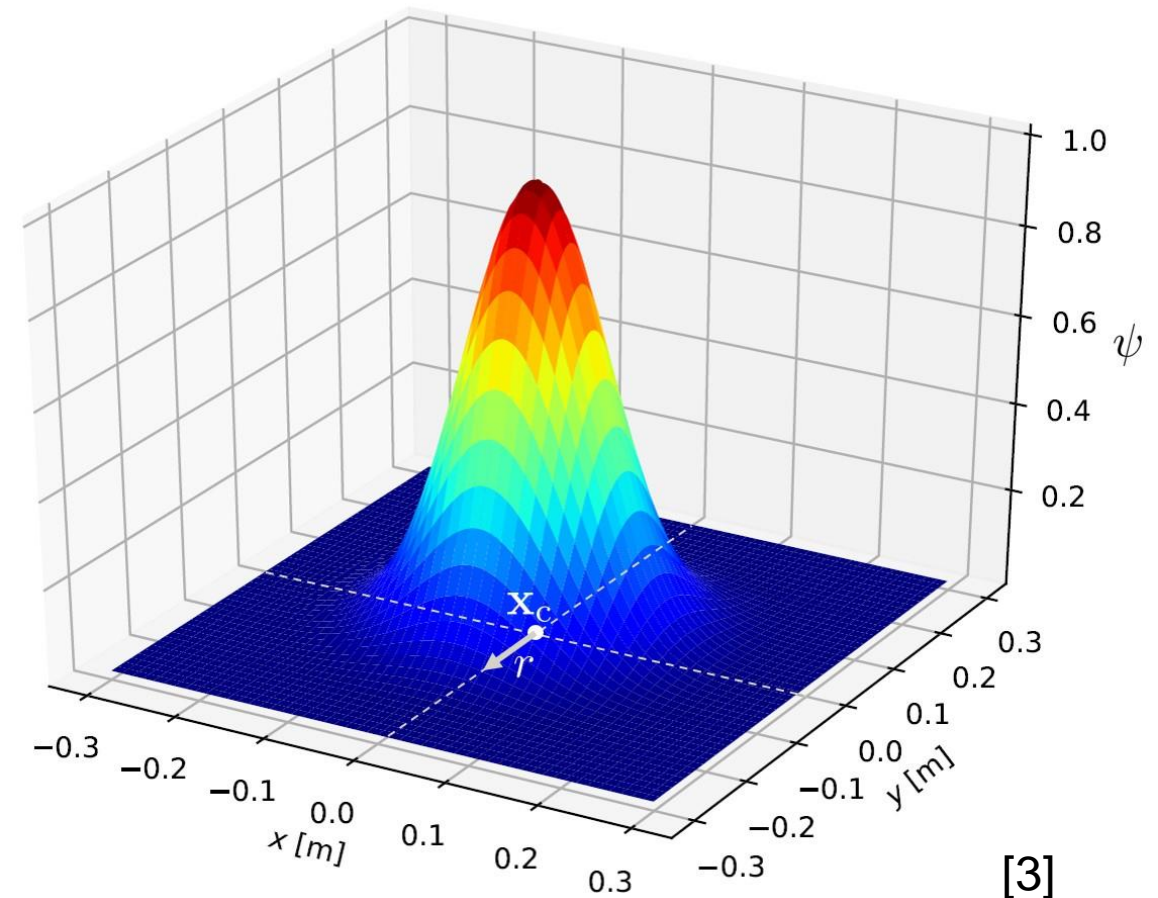
$$\delta(\mathbf{x} - \mathbf{x}_i) = \delta(x - x_i)\delta(y - y_i)$$

$$\delta(\mathbf{x} - \mathbf{x}_i) \rightarrow e^{-\frac{(x-x_i)^2 + (y-y_i)^2}{r^2}} = \psi(x, y, x_i, y_i)$$

- Normalize the values with the volume:

$$V = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \psi(x, y, x_i, y_i) dx dy = r^2 \pi$$

r : Radius of wells



Functional of interest and constraints

- Controls:

$$\mathbf{m} = [x_1^{\text{ext}}, \dots, x_N^{\text{ext}}, y_1^{\text{ext}}, \dots, y_N^{\text{ext}}, x_1^{\text{inj}}, \dots, x_N^{\text{inj}}, y_1^{\text{inj}}, \dots, y_N^{\text{inj}}]^T$$

- Functional of interest:

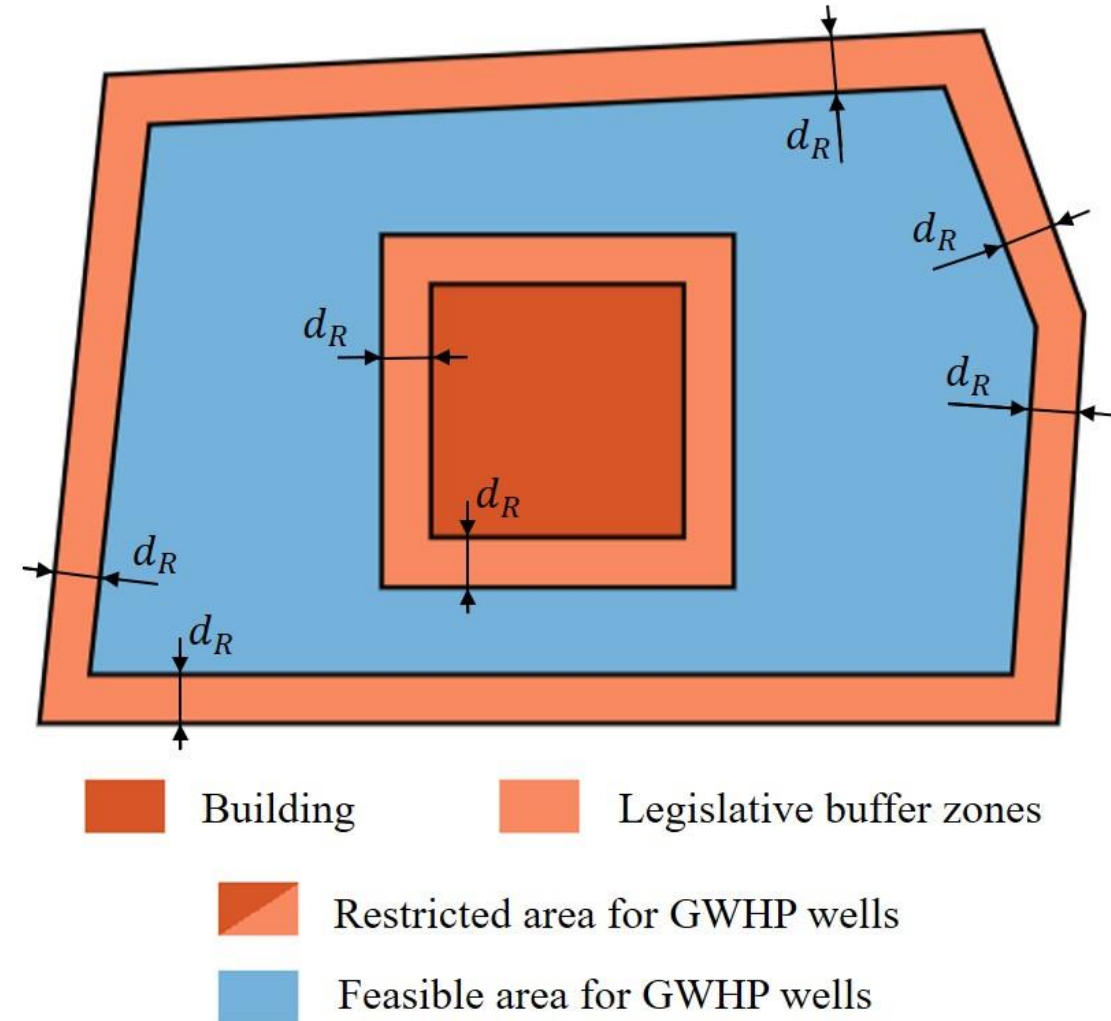
$$J_0(\mathbf{u}, \mathbf{m}) = \sum_{i=1}^N T(\mathbf{x}_i^{\text{ext}}) = \sum_{i=1}^N \int_{\Omega} T(\mathbf{x}) \cdot \delta(\mathbf{x} - \mathbf{x}_i^{\text{ext}}) d\Omega$$

- Constraints:

$$\mathbf{x}_i^{\text{ext}}, \mathbf{x}_i^{\text{inj}} \in D_i, \quad \forall i \in \{1, \dots, N\} \quad \longrightarrow \quad \mathbf{A}\mathbf{m} \leq \mathbf{b}$$

$$d(\mathbf{x}_i^{\text{ext}}, \mathbf{x}_i^{\text{inj}})^2 = (x_i^{\text{ext}} - x_i^{\text{inj}})^2 + (y_i^{\text{ext}} - y_i^{\text{inj}})^2 \geq d_{\min}^2,$$

$$\mathbf{x}_i^{\text{ext}}, \mathbf{x}_i^{\text{inj}} \notin R_i^j, \quad \forall i \in \{1, \dots, N\}, \forall j \in \{1, \dots, r_i\}$$



Soft constraints – penalty approach

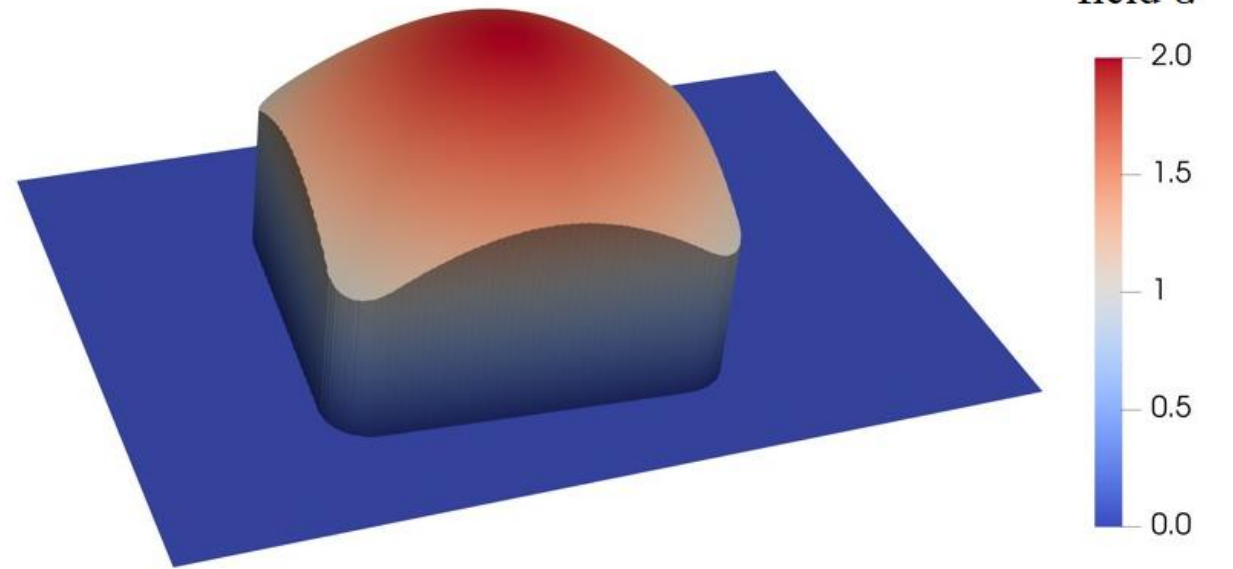
- Penalty function:

$$P_R = \alpha \cdot \sum_{i=1}^N \left(p(\mathbf{x}_i^{\text{ext}}) + p(\mathbf{x}_i^{\text{inj}}) \right)$$

$$p(\mathbf{x}_i) = \int_{\Omega} G(\mathbf{x}) \cdot \delta(\mathbf{x} - \mathbf{x}_i) d\Omega$$

- Penalty field:

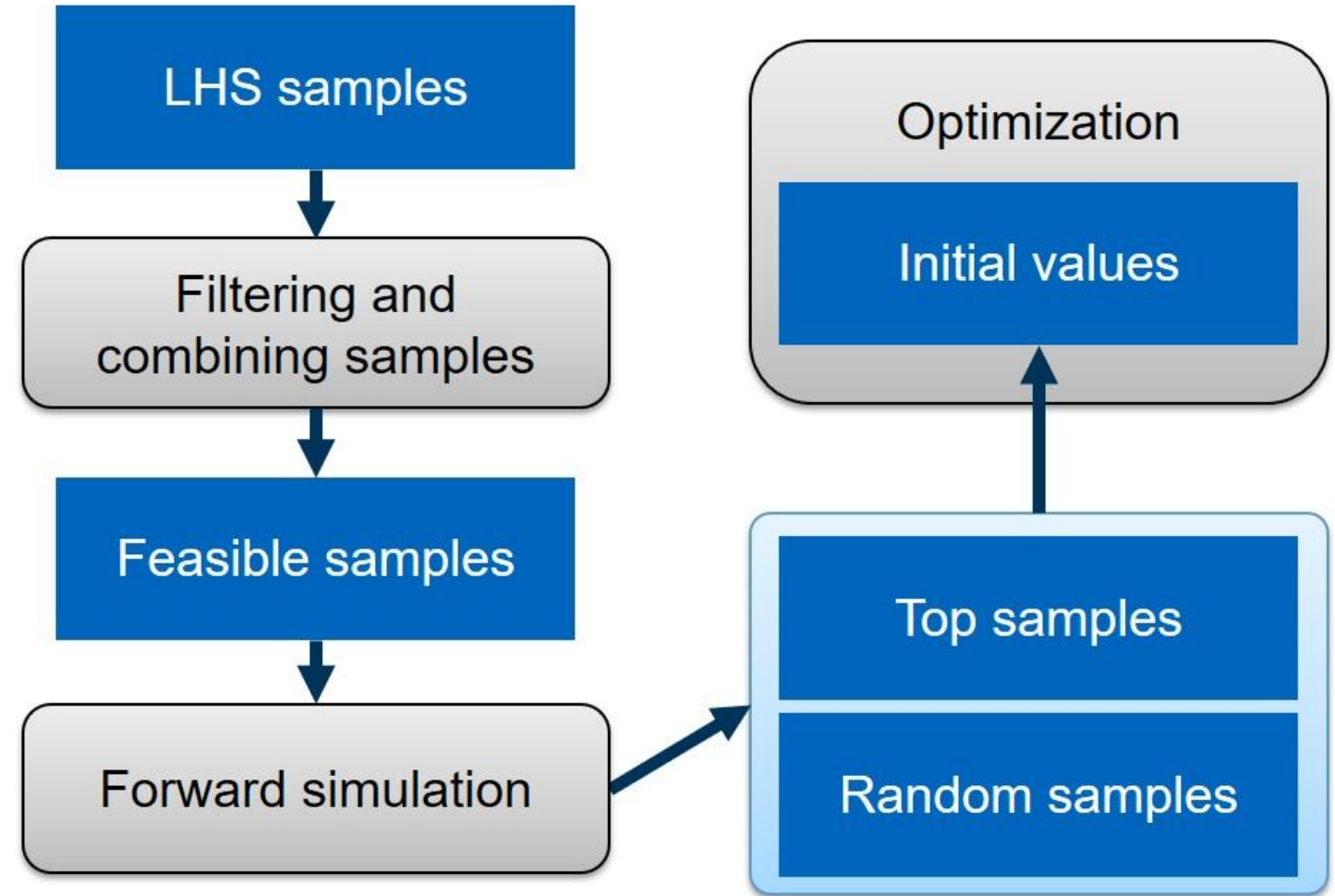
$$G(\mathbf{x}) = \begin{cases} 0 & \text{if } \mathbf{x} \notin R_i^j, \\ 1 + \cos \left[\frac{d(\mathbf{x}, \mathbf{x}_{i,j}^p)}{r_{i,j}^p} \cdot \frac{\pi}{2} \right] & \text{if } \mathbf{x} \in R_i^j, \end{cases} \quad \forall i \in \{1, \dots, N\}, \forall j \in \{1, \dots, r_i\}$$



[3]

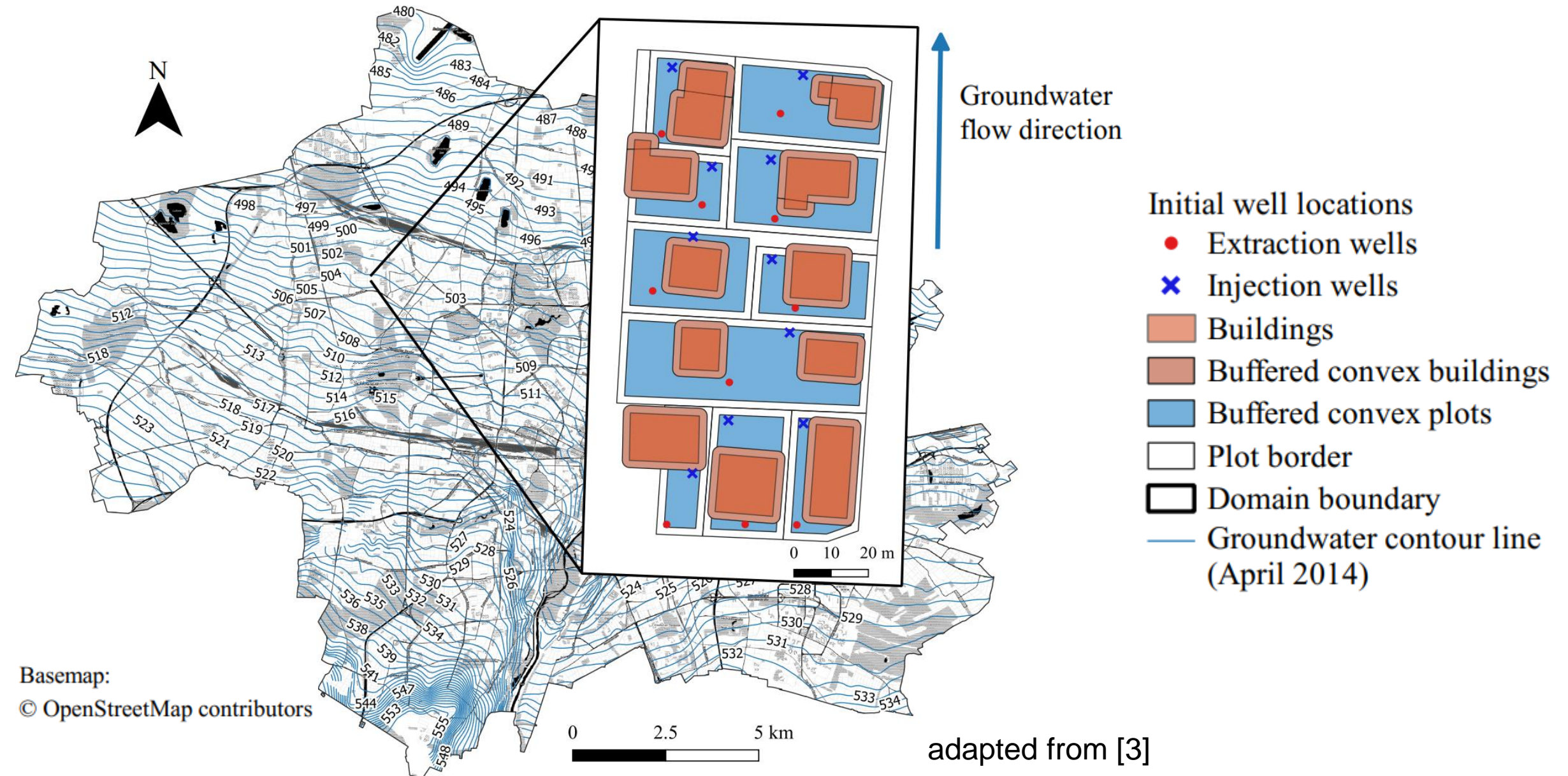
Reduced-space problem:

$$\begin{aligned} \min_{\mathbf{m}} \quad & -\hat{J}_0(\mathbf{m}) + P_R(\mathbf{m}), \\ \text{subject to} \quad & g_1(\mathbf{m}) \leq 0, \\ & g_2(\mathbf{m}) \leq 0, \end{aligned}$$

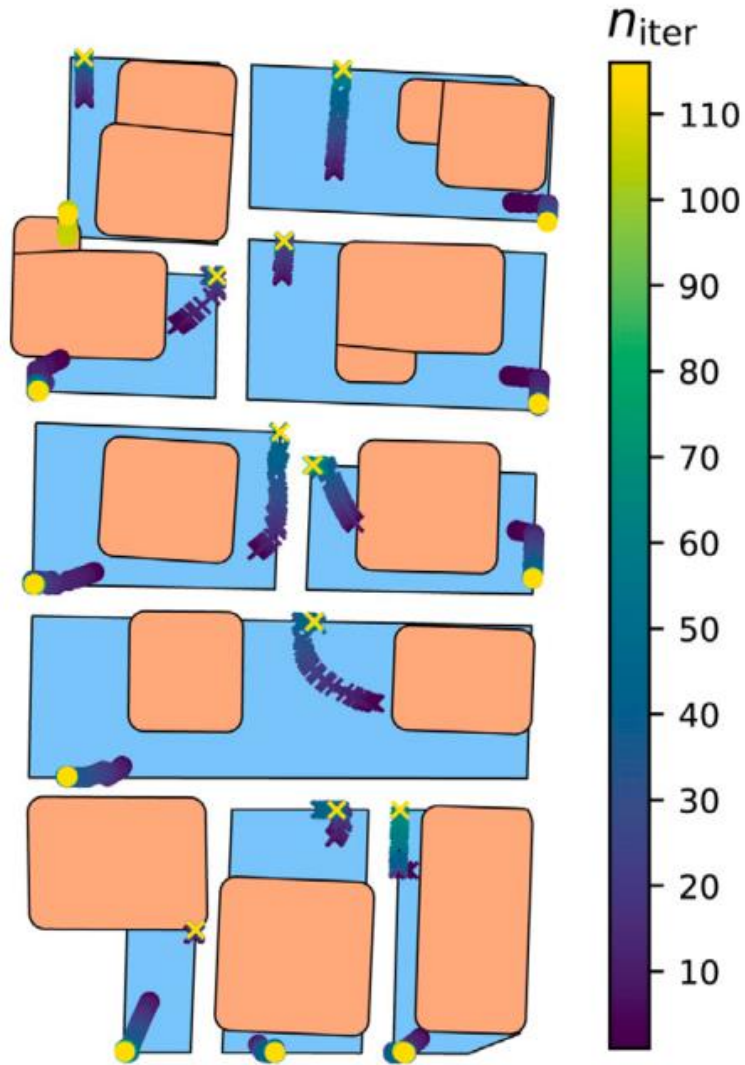


Multi-start initialization strategy [3]

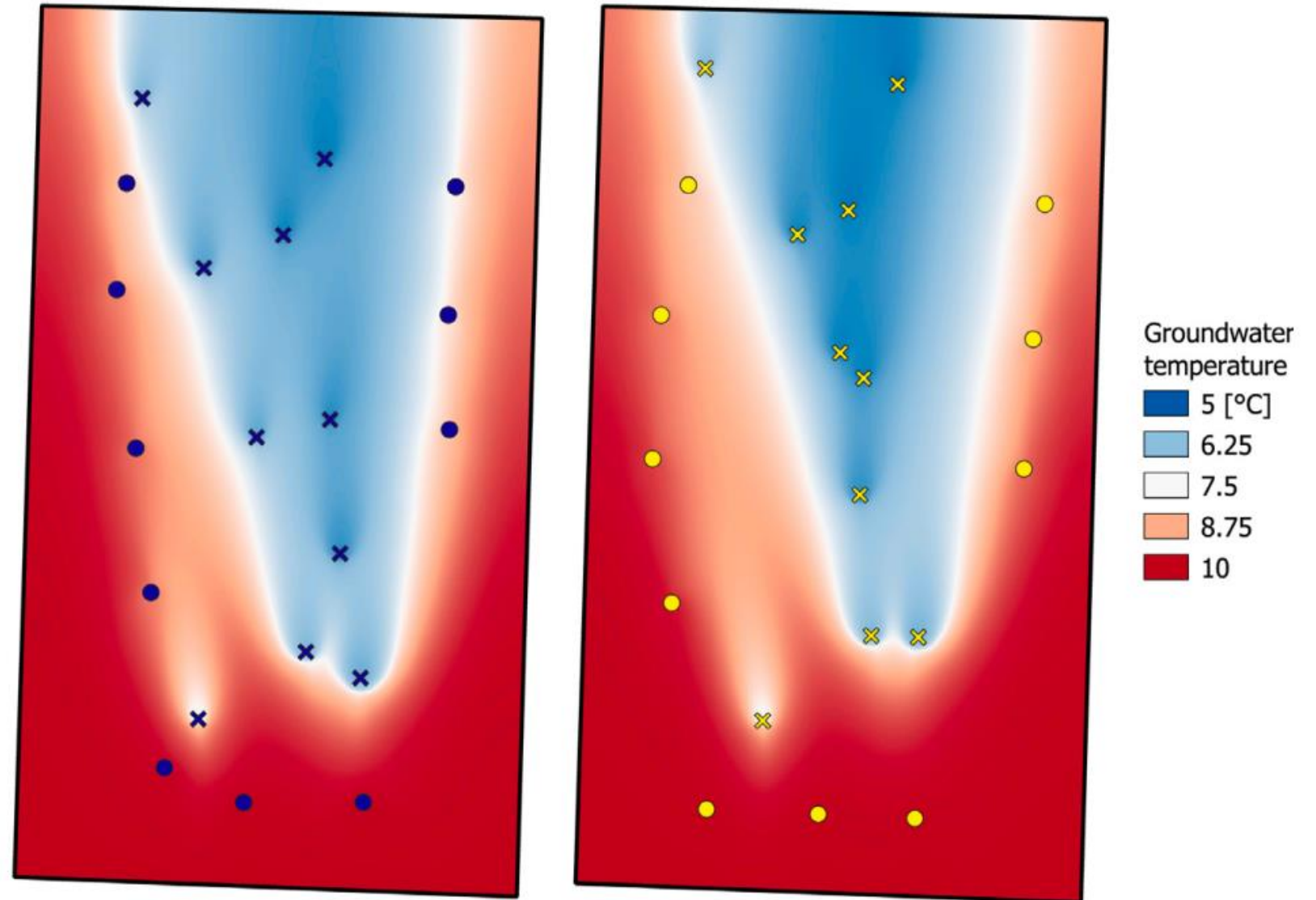
GWHP optimization – Case study



Basemap:
© OpenStreetMap contributors

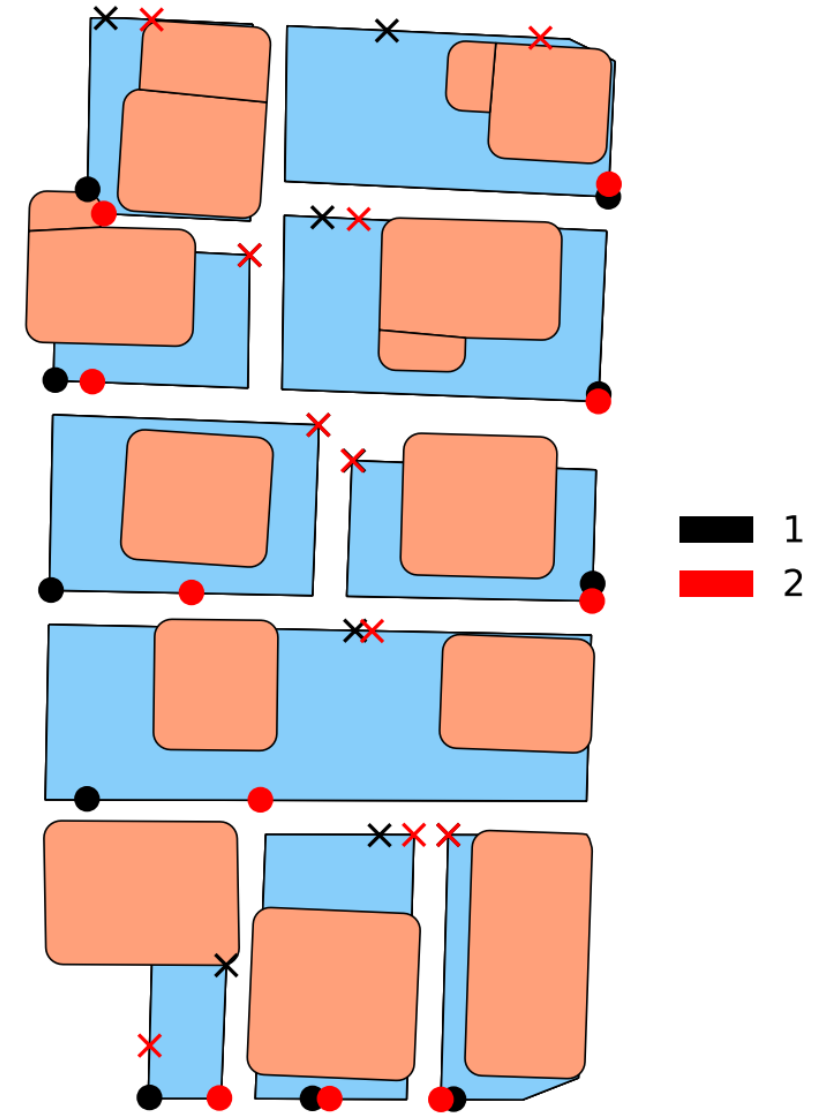
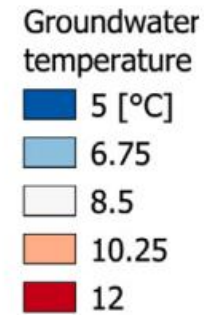
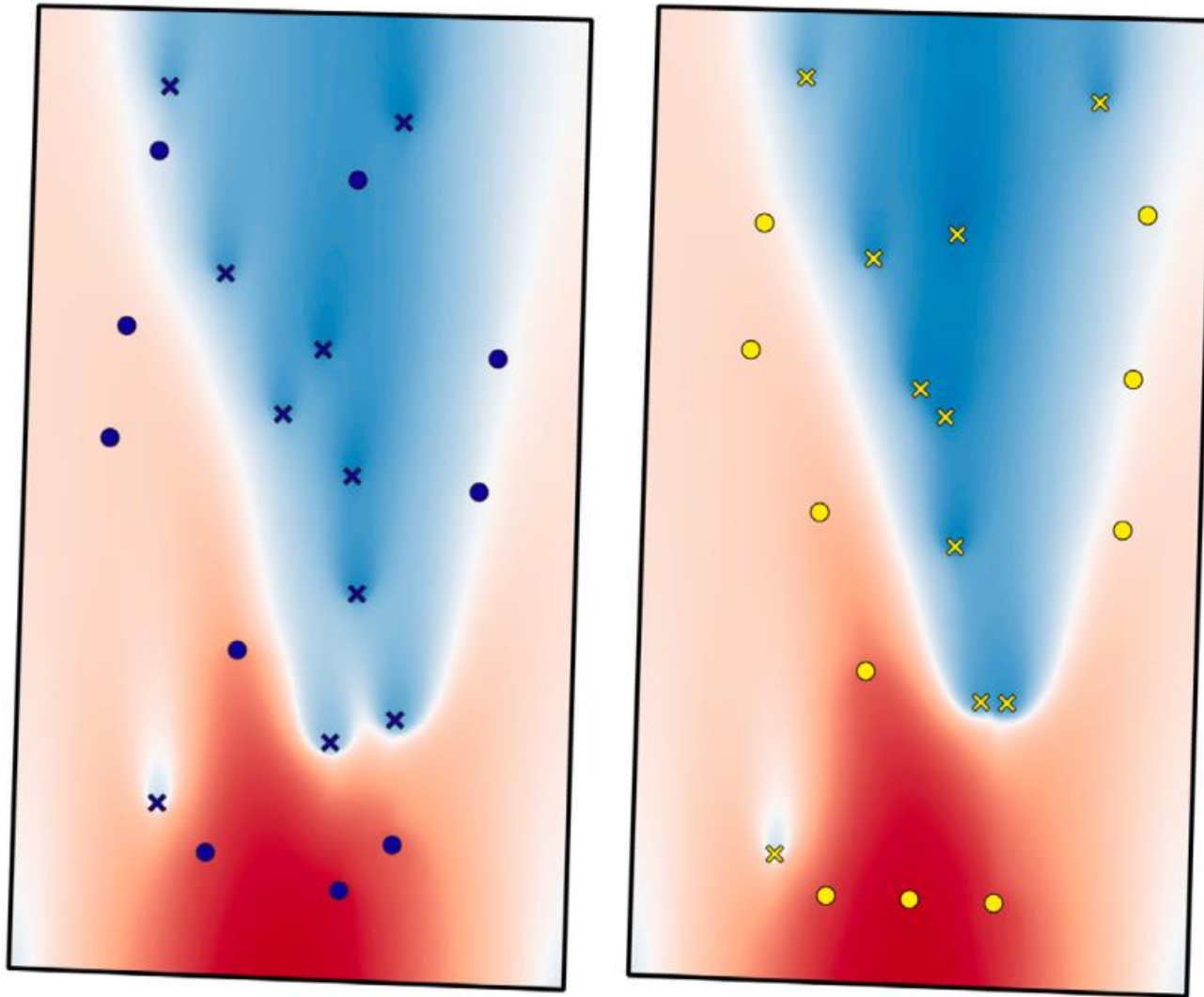


Well positions during optimization [3]



Initial and final GW temperature fields and well layouts [3]

GWHP optimization – Results 2



Initial and final GW temperature fields and well layouts [3]

Optimal well layouts – Scenario 1 & 2 [3]

2D vertically averaged transient heat transport in porous media

Scenario 1

without groundwater flow

$$\begin{aligned} C^s \frac{\partial T}{\partial t} - \nabla \cdot (\mathbf{\Lambda} \nabla T) &= 0 & I \times \Omega \\ \mathbf{n} \cdot (\mathbf{\Lambda} \nabla T) &= -q_i & I \times \Gamma_i \\ \mathbf{n} \cdot (\mathbf{\Lambda} \nabla T) &= 0 & I \times \Gamma_0 \\ T(0) &= T_0 & \{0\} \times \Omega \end{aligned}$$

- T ground temperature
- q_i load at BHE i
- C volumetric heat capacity

Scenario 2

with groundwater flow (confined aquifer):

$$\begin{aligned} C^g \frac{\partial T}{\partial t} + C^f \mathbf{u} \cdot \nabla T - \nabla \cdot (\mathbf{\Lambda} \nabla T) &= 0 & I \times \Omega \\ \mathbf{n} \cdot (\mathbf{\Lambda} \nabla T) &= -q_i & I \times \Gamma_i \\ \mathbf{n} \cdot (\mathbf{\Lambda} \nabla T) &= 0 & I \times \Gamma_0 \\ T(0) &= T_0 & \{0\} \times \Omega \end{aligned}$$

- \mathbf{u} velocity of groundwater
- $\mathbf{\Lambda}$ tensor of hydrodynamic thermodispersion

- Controls:

$$\mathbf{q} = (q_1, \dots, q_{n_b})^T \in Q = L^2(I; \mathbb{R}^{n_b})$$

- Borehole wall temperature as the mean over the respective boundary:

$$T_{b_i} = \frac{\int_{\Gamma_i} T ds}{\int_{\Gamma_i} ds} = \frac{1}{2\pi r_b} \int_{\Gamma_i} T ds \quad \longrightarrow$$

$$\frac{\sum_{i=1}^{n_b} T_{b_i}}{n_b} = \frac{1}{2\pi r_b n_b} \sum_{i=1}^{n_b} \int_{\Gamma_i} T ds \quad \text{Average temperature on all boreholes}$$

- Functional of interest:

$$\frac{1}{t_{end}} \int_I \frac{\sum_{i=1}^{n_b} T_{b_i}}{n_b} dt = \frac{1}{2\pi r_b n_b t_{end}} \int_I \sum_{i=1}^{n_b} \int_{\Gamma_i} T ds dt \quad \longrightarrow \text{Problematic}$$

- Functional of interest:

$$J_1(T, \mathbf{q}) := \frac{1}{t_{end}} \int_I \sum_{i=1}^{n_b} T_{b_i} q_i dt = \frac{1}{2\pi r_b n_b t_{end}} \int_I \sum_{i=1}^{n_b} \int_{\Gamma_i} T ds q_i dt$$

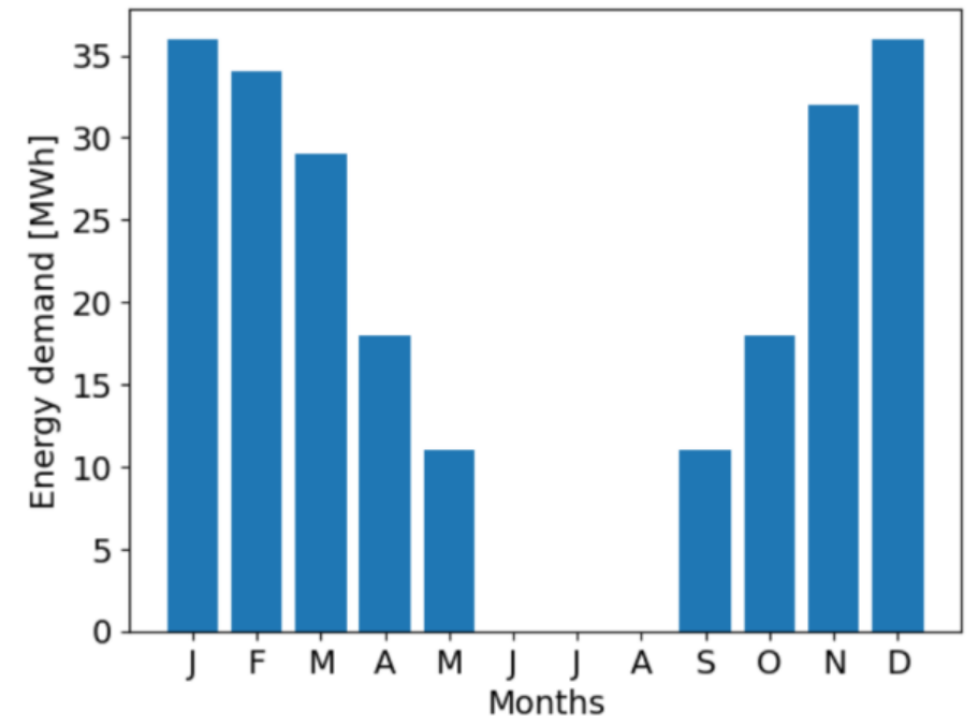
Constraints:

- The energy demand must be satisfied at each time step:

$$\int_{t_k}^{t_{k+1}} \sum_{i=1}^{n_b} 2\pi r_b l_b q_i(t) dt = Q_k$$

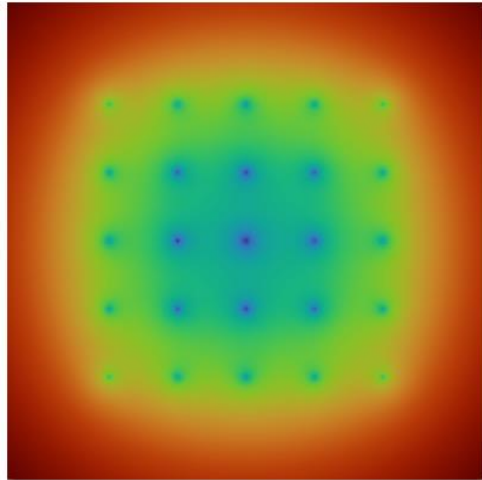
- Only heating is considered:

$$0 \leq q_i \leq q_{up}$$

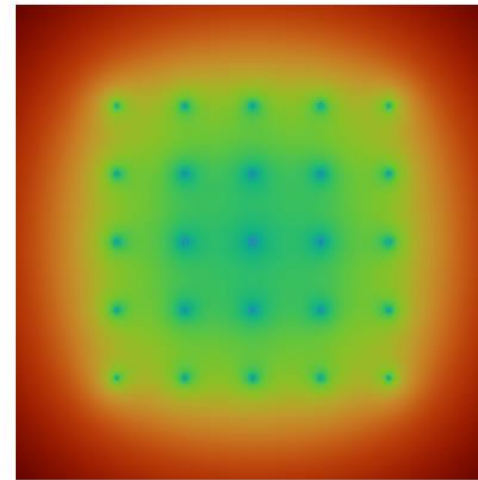


Monthly energy demand [4]

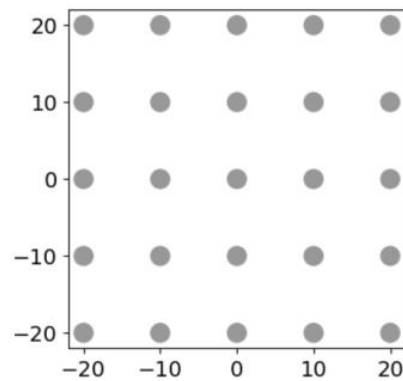
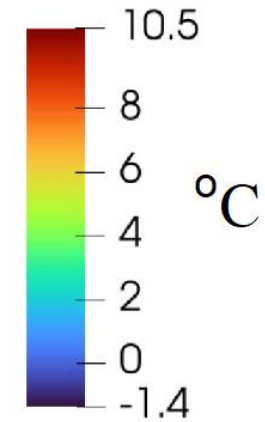
GSHP optimization results (Scenario 1)



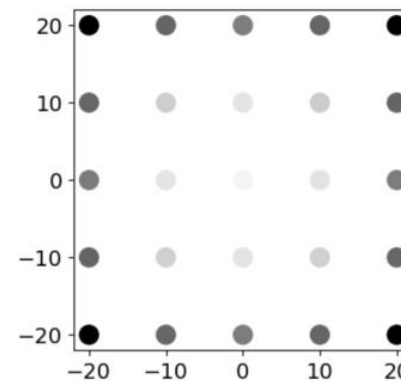
(a) Unopt. temperature after 10a



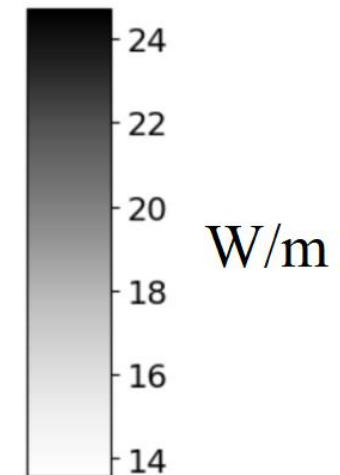
(b) Opt. temperature after 10a



(c) Equal loads in January



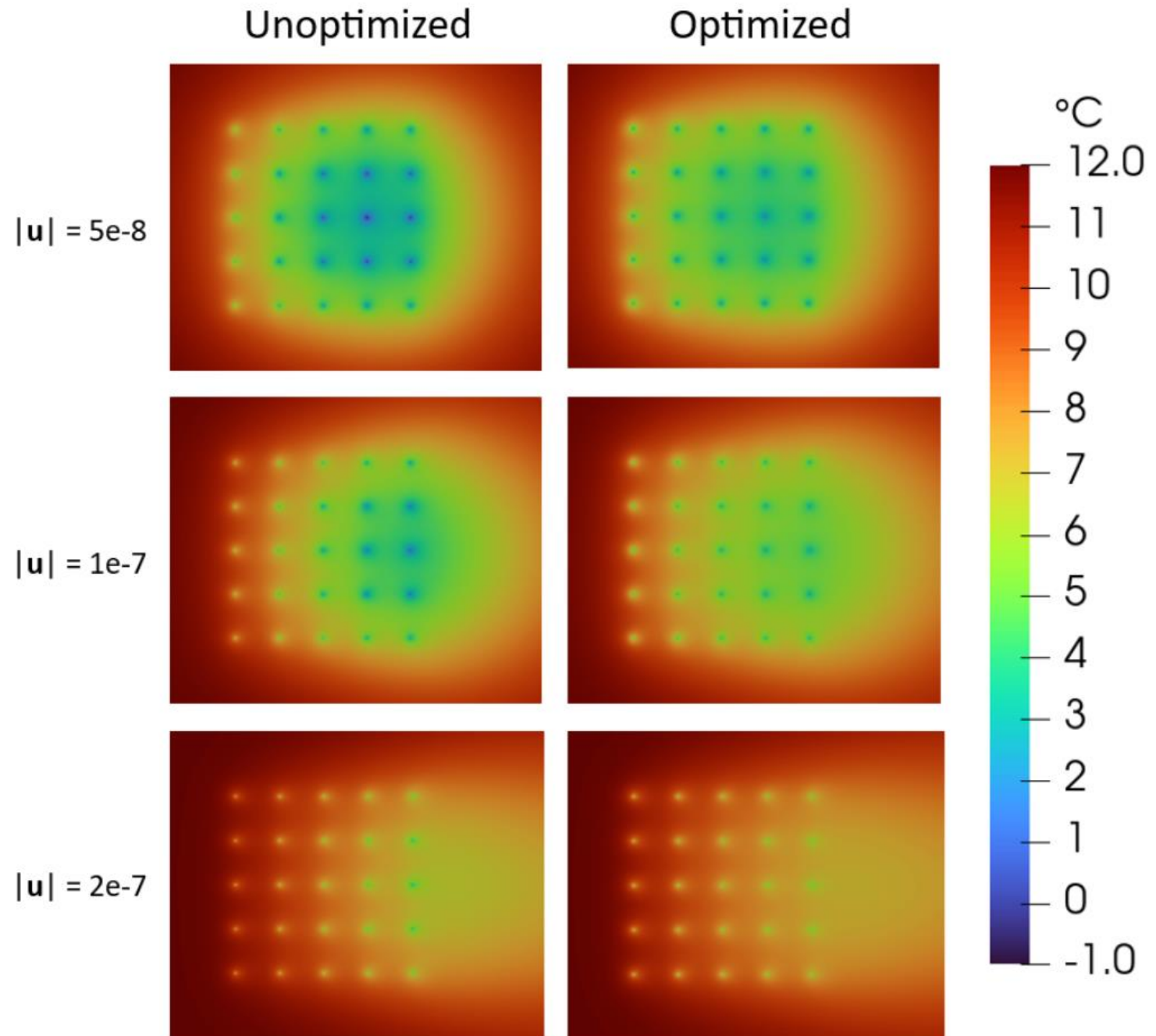
(d) Optimized loads in January



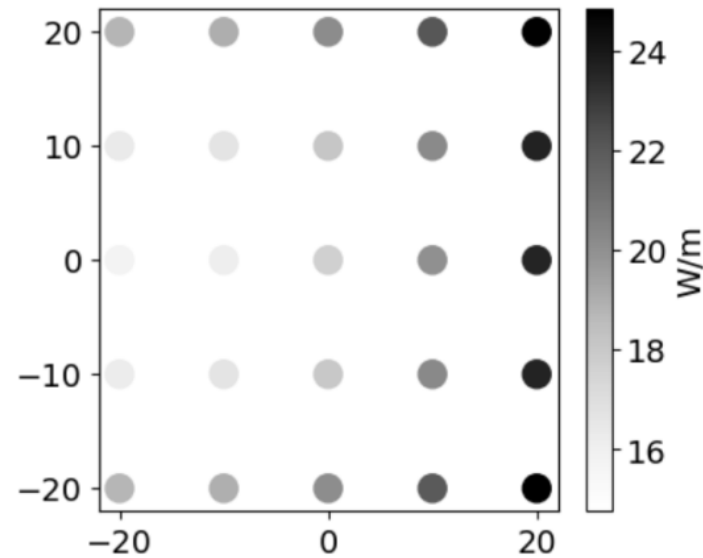
[4]

GSHP optimization results (Scenario 2)

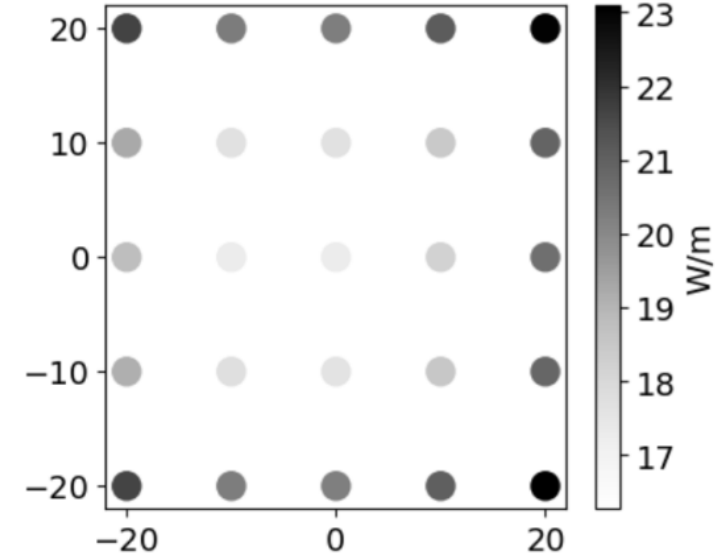
Temperature fields
for different
groundwater velocities [4]



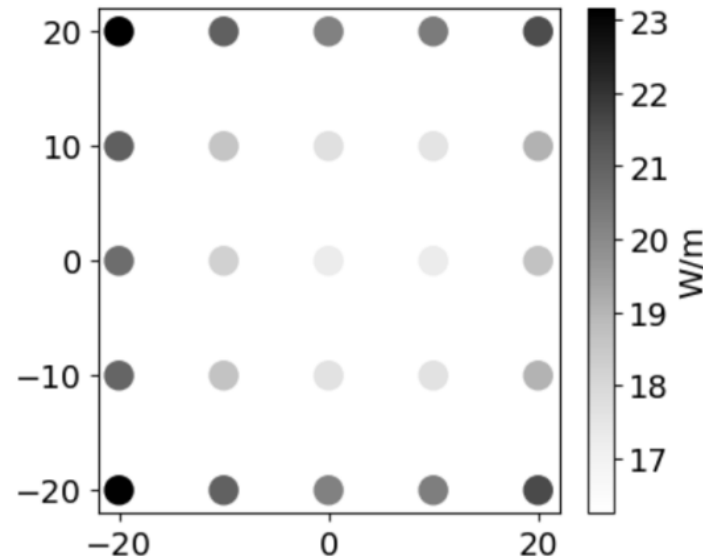
GSHP optimization results (Scenario 2)



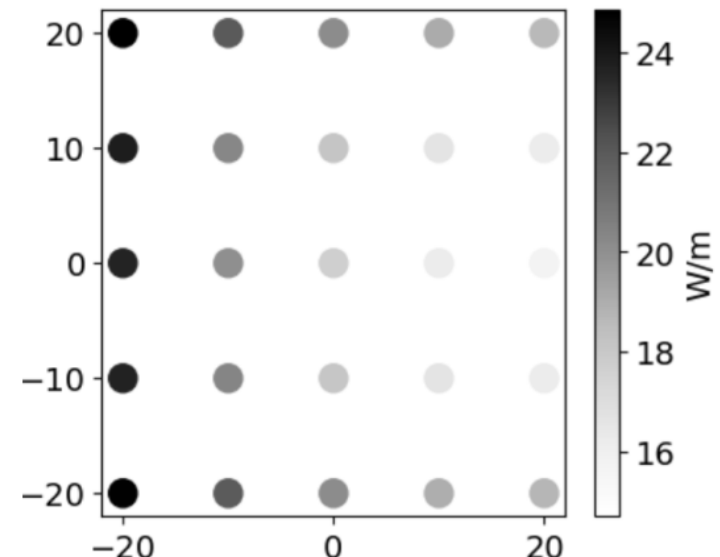
(a) 2nd year



(b) 5th year



(c) 7th year



(d) 10th year

Optimized loads
for $|u| = 10^{-7}$ m/s
in January [4]

Optimization application		
	GWHP	GSHP
Forward model	2D	2D
Time dependency	no	yes
Convexity	no	yes
Type of problem	Design / Distributed control	Boundary control

Comparison of the application examples

Outlook

- 3D models, design + control
- Rigorous mathematical proofs
- Other SGE applications: ATES, BTES

Contact:

smajil.halilovic@tum.de

<https://www.epe.ed.tum.de/en/ens>

- [1] © GRETA - INTERREG ALPINE SPACE FEDER
<https://rapport-activite.brgm.fr/en/complementing-energy-mix-with-properties-resources-subsurface>
- [2] A. García Gil, E. A. Garrido Schneider, M. Mejías Moreno, and J. C. Santamarta Cerezal. Shallow Geothermal Energy. Springer, 2022.
- [3] Halilovic, S., Böttcher, F., Kramer, S. C., Piggott, M. D., Zosseder, K., & Hamacher, T. (2022). *Well layout optimization for groundwater heat pump systems using the adjoint approach*. Energy Conversion and Management, 268, 116033. <https://doi.org/10.1016/j.enconman.2022.116033>
- [4] B. Lipp. Optimization of closed-loop shallow geothermal systems using the adjoint approach. Master's Thesis, 2023.