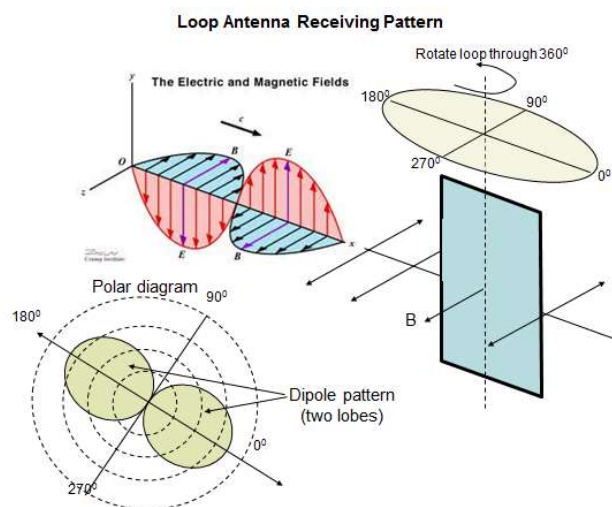


LOOP ANTENNA FOR VERY LOW FREQUENCY

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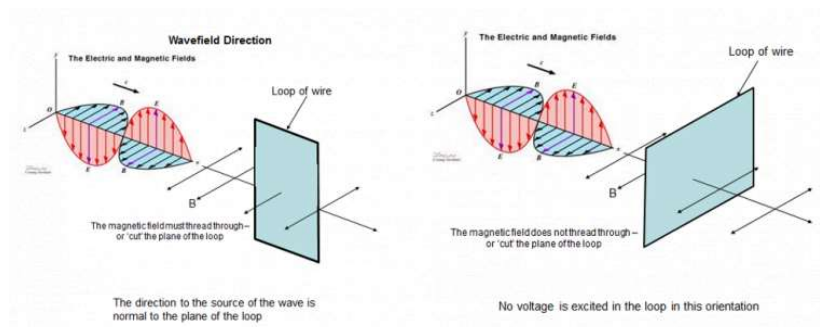


Abstract : in this Post we describe the construction and tuning of a magnetic loop antenna whose purpose is reception in the VLF band, to be coupled with a suitable VLF receiver for monitoring SID events (sudden ionospheric disturbances) caused by solar flares.

Introduction

From the theory of electromagnetism we know that a variable magnetic field produces, in a loop linked to the flux lines, a voltage proportional to the speed of change of the magnetic flux (first order derivative with respect to time). If we consider a vertically polarized electromagnetic wave, the magnetic field will be polarized in a horizontal plane and subject to cyclic variations at the frequency of the electromagnetic wave.

If we place a loop oriented parallel to the direction of propagation, an electrical voltage will therefore be produced, if the loop is instead oriented orthogonal to the direction of the wave there will be no magnetic flux and therefore the voltage will be zero. The drawings below show the two cases: on the left the voltage will be maximum, while on the right the voltage will be zero.



What we have described above is the principle of operation of a magnetic loop antenna, suitable for the detection of low frequency electromagnetic signals (VLF band).

Construction

To build a magnetic loop antenna it is necessary to maximize the signal that is produced. To increase the signal we can both increase the surface of the loop, and this leads to a larger antenna, and increase the number of turns. Larger dimensions means having an antenna that is more difficult to build and more difficult to handle, increasing the number of turns means having greater resistance and greater stray capacitance, with the result of having a smaller Q factor. A compromise must be reached. From the examples found in literature, it is clear that the classic size is around a meter, while the number of turns is about 100.

After choosing the dimensions, the wooden structure is made, as shown in the image below:

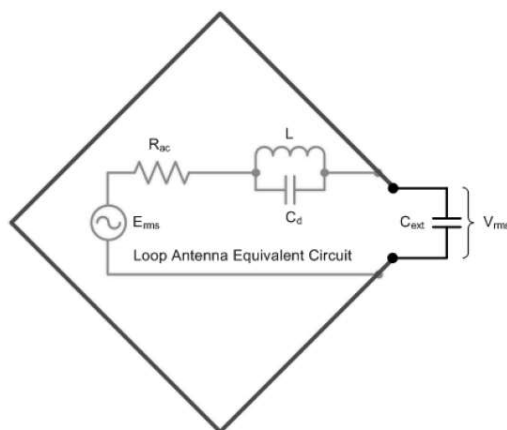


Once the structure is finished, the enameled copper wire is wound in order to create the chosen number of turns. Wrapping the copper wire is not always easy, you need a little patience and do some tests before reaching the final result. The image below shows the antenna almost finished.



The antenna data are summarized in the table below. The square size is **0,7 m**, the copper wire has a diameter of 0,5 mm, the turns are **83**. On the basis of these geometric data it is possible to calculate the inductance that results **27,6 mH**, while the measured value is **27,4 mH**. The measured value of the resistance is **25,7 Ω** .

The antenna is represented by an equivalent circuit with an **LC parallel** having a resistance in series, as seen in the diagram below, where the external capacity used for tuning has also been inserted.



With a signal generator and an oscilloscope it is easy to determine the resonant frequency of the antenna. The generator is connected to the antenna by means of a load resistance, for example 100 K Ω . With the oscilloscope the signal at the terminals of the antenna is measured while the frequency of the signal is varied. At the resonance frequency the impedance of the parallel LC is maximum and therefore the signal is also maximum. In this way we determined that the **fris = 45.6 KHz**, from which we derive the value of the antenna capacitance, which is **445 pF**.

Loop Antenna	
Parameter	Value
Dimensions (Side)	0,7 m
Wire	24 AWG = 0,5 mm
Turns	83
Inductance (L)	27,6 mH calculated 27,4 mH measured
Resistance (DC)	25,7 Ω
Self Resonant Frequency	45,6 KHz
Self Capacitance (C)	445 pF (from Res Freq.)
Tuned Resonant frequency	26,7 KHz
Tuning Capacitance (C)	1292 pf
Tuning Capacitor (C)	847 pf
Q (26,7 KHz)	22,3

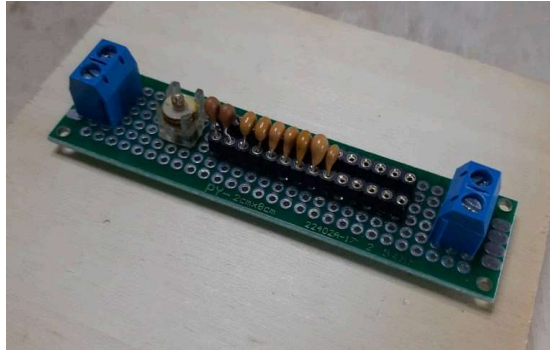
Tuning

From the examination of the VLF signals received in our area we have seen that the **26.7 KHz** signal of the BAFA (NATO) transmitter located in Turkey is well received, at a distance of about 1500 km. This distance should allow you to clearly distinguish situations in which the propagations by ground wave and by ionospheric wave differ, for example due to a solar flare. It is therefore necessary to proceed with the tuning of the antenna so that the new resonance frequency corresponds to the emission frequency of the chosen transmitter. For tuning, an additional capacity must be inserted in parallel with the antenna, the value of which must be appropriately calibrated.

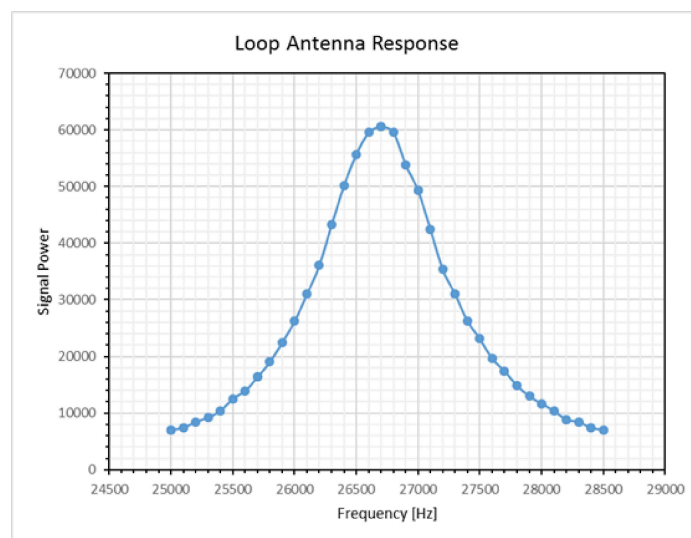
In practice, also the tuning is carried out with a signal generator and an oscilloscope. Set the generator to the desired frequency, 26.7 KHz in our case, connect it to the antenna with a resistance of 100 K Ω and vary the external capacity so as to maximize the signal collected at the terminals of the antenna.

The image below shows our tuner circuit in which the capacitors can be easily added or removed in order

to vary the capacitance. **Note : the tuning must be done with the cable connected to the receiver because the cable adds itself a capacitance.**



After tuning we measured the response curve of the antenna for frequencies near the resonance value, the result is shown below. From this curve we obtain a Q equal to 22.3.



Signal Calculation

Knowing the geometric and electrical data of the antenna we can try to calculate the signal produced by the antenna in order to evaluate the amplification parameters that will be necessary.

From Farady-Lenz law : $V = -d\phi(t)/dt$

V = open circuit voltage rms

$\phi(t)$ = magnetic flux

t = time

For a loop antenna : $V = -n(d\phi(t)/dt)$

n = number of turns

The magnetic flux is : $\phi(t) = B(t) \cdot A_e \cdot \cos(\vartheta)$

A_e = Surface of circular equivalent loop

ϑ = angle between flux lines and the orthogonal of turns plane

$B(t)$ = magnetic induction field

The magnetic field of an **em wave** is : **$B(t) = B \cdot \cos(\omega t)$**

$\omega = 2\pi \cdot f$ where f = frequency

Differentiating we obtain : **$d\phi(t)/dt = -B \cdot A_e \cdot \omega \cdot \sin(\omega t) \rightarrow V = 2\pi \cdot n \cdot A_e \cdot f \cdot B \cdot \cos(\theta)$**

$\theta = 0$ because the antenna is oriented correctly

$f = 26,7 \text{ KHz}$ (chosen frequency)

$n = 83$ (number of turns)

$A_e = 0,56 \text{ m}^2$ (calculated from geometric data and corrected according to formulas)

we obtain : **$V = 7797302 \cdot B$**

We can also calculate the equivalent height of the antenna : **$V = h_e \cdot E$**

h_e = equivalent height

E = electric field = $c \cdot B$

We obtain **$h_e = V/E = V/c \cdot B = 2\pi \cdot n \cdot A_e \cdot f \cdot B \cdot \cos(\theta) / c \cdot B = 2\pi \cdot n \cdot A_e \cdot f \cdot \cos(\theta) / c$**

$h_e = 2\pi \cdot n \cdot A_e \cdot \cos(\theta) / \lambda$

$h_e = 0,026 \text{ m}$

The electric field value of an em wave could be **$E = 1 \text{ mV/m}$**

$V = 0,026 \cdot 1 = 0,026 \text{ mV} = 26 \mu\text{V}$

Multiplying by the Q value of the antenna we get **$V = Q \cdot 26 = 580 \mu\text{V} = 0,58 \text{ mV}$**

You can see how, in order to obtain measurable final values, it is necessary to amplify the signal over 1000 times !

In the next post: **VLF Receiver for SID Monitoring** we will deal with the VLF receiver and ionospheric propagation monitoring.

References

UKRAA site : <https://www.ukraa.com/>

Application of the UKRAA Very Low Frequency Receiver System – Reeve

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