

Q-1 A 2nd order transfer fn $G(s)$ without zeros is to be designed such that the step response has 2 or 3 of the following specifications
 $10\% OS$, 2% setting time = 20 seconds, = T_s
 Peak time $T_p = 3$ seconds.

(a) Design G_1 with all 3 properties.
 (b) Design G_2, G_3, G_4 with 2 of the 3 properties, i.e.

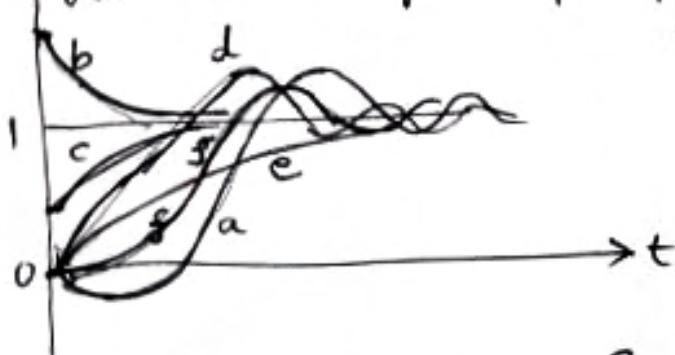
$G_2(s)$ having %OS of T_s as specified

$G_3(s)$ having %OS & T_p as specified.

$G_4(s)$ having $T_p & T_s$ as specified.

($G_1, G_2, G_3 + G_4$ should have no zero of DC-gain = 1).

B-2 (y(t)) Consider plots of step responses 6 of them. (2 of them are marked "f".)



Consider 7 transfer functions: Seven of them.

$$\frac{+s+8}{s^2+2s+8}, \frac{+s+8}{s^2+30s+8}, \frac{3s+2}{2s+2}, \frac{s+2}{2s+2}, \frac{-s+8}{s^2+2s+8}$$

$\frac{8}{s^2+2s+8}, \frac{+s+8}{s-8}$ (i) For each of the 6 plots, associate a transfer fn & give a brief reason.

(ii). For each of 7 transfer fns, find initial value, final value, initial disc rate: (find for all 7 even if not associated to a plot.)

$$\frac{s-8+16}{s^2+2s+8}$$

Q-3: For analyzing the unit-step response of $G(s) = \frac{\omega_n^2}{(s^2 + 2\zeta\omega_n s + \omega_n^2)}$

$$0 < \zeta < 1$$

plot in \mathbb{C} (the s-plane),

the curves corresponding to constant $\% OS$ (say C_1)

and curve corresponding to constant T_s (settling time)

Give direction to C_1 & C_2 : going further from origin say C_2 .

(b). Along C_1 & C_2 , specify how the following change:
increase or decrease or remain same: give brief reason.

$T_p, T_s, T_{\sigma} \downarrow$ rise time (from 10% to 90%).

\uparrow
peak time \uparrow
settling time (20%)

Q-4: Give an RLC circuit ($R > 0, L > 0, C > 0$) such that

(a) underdamped (\Rightarrow Resistance R is very small).

(b) or overdamped (\Rightarrow Resistance R is very large).

(c) What should be input & output here? (introduce current/voltage source appropriately & suggest output variable) Do this for each circuit (a) & (b).

(Answer for (c) could be different for a & b)

Q-5: Consider $G(s) = \frac{1}{s^2 + 2\zeta s + 1}$, $0 < \zeta < 1$, & study the step response.

(a) Under what condition can effect of an additional pole be neglected? Prove this.

(b) Under what condition can effect of additional zeros be neglected? Prove this.

(Note: Effect of zero & additional pole is to be analyzed individually & not together. Effect on step response.)

Note: Read all questions fully first and ask queries within 10 minutes.

No clarifications after that: assume appropriately yourself.

Each question carries 5 marks. Attempt all questions.

1] (a) $G_1 \Rightarrow$ Not possible as all the three conditions won't satisfy at the same time. (2)

(b) 10% OS, $T_s = 20$

$$\exp\left(\frac{-\pi \xi_1}{\sqrt{1-\xi_1^2}}\right) = 0.1$$

$$\xi_1 = 0.5911$$

for 2% tolerance, $T_s = 20 = 4T$

$$\frac{4}{\omega_{n_1} \xi_1} = 20 \Rightarrow \omega_{n_1} = 0.3383$$

(1)

$$G_2 = \frac{\omega_{n_1}^2}{s^2 + 2\xi_1 \omega_{n_1} s + \omega_{n_1}^2}$$

 10% OS, $T_p = 3 \text{ sec}$

$$\xi_2 = 0.5911$$

$$T_p = \frac{\pi}{\omega_{n_2} \sqrt{1-\xi_2^2}} = 3$$

$$\omega_{n_2} = 1.298$$

(1)

$$G_3 = \frac{\omega_{n_2}^2}{s^2 + 2\xi_2 \omega_{n_2} s + \omega_{n_2}^2}$$

$$T_p = 3 \text{ sec}, T_s = 20 \text{ sec}$$

$$\frac{4}{\xi_3 \omega_{n_3}} = 20 \Rightarrow \omega_{n_3} = \frac{1}{5 \xi_3}$$

$$T_p = \frac{\pi}{\omega_{n_3} \sqrt{1 - \xi_3^2}} = 3$$

~~$$\frac{5\pi \xi_3}{\sqrt{1 - \xi_3^2}} = 3$$~~

①

$$\xi_3 = 0.1875$$

$$\omega_{n_3} = 1.0661$$

$$G_g = \frac{\omega_{n_3}^2}{s^2 + 2\xi_3 \omega_{n_3} s + \omega_{n_3}^2}$$

- 2.(a)
- ① $\frac{8}{s^2 + 2s + 8} \rightarrow f \rightarrow$
 - System underdamped
 - Simple 2nd Order system

 - ② $\frac{s+8}{s^2 + 2s + 8} \rightarrow d \rightarrow$
 - system underdamped
 - addition of zero with +ve coeff.
 - rise time decreases

 - ③ $\frac{-s+8}{s^2 + 2s + 8} \rightarrow a \rightarrow$
 - system underdamped
 - addition of zero with -ve coeff.
 - rise time increases initially goes below zero & comes up

 - ④ $\frac{s+8}{s^2 + 30s + 8} \rightarrow e \rightarrow$
 - 2nd order system
 - overdamped system (no peak)

 - ⑤ $\frac{3s+2}{2s+2} \rightarrow b \rightarrow$
 - 1st order system
 - unit step + decaying exponential
 - $u(t) + \frac{1}{2}e^{-t}$

 - ⑥ $\frac{s+2}{2s+2} \rightarrow c \rightarrow$
 - 1st order System
 - unit step - decaying exponential
 - $u(t) - \frac{1}{2}e^{-t}$

 - ⑦ $\frac{s+8}{s-8} \rightarrow NA \rightarrow$
 - 1st order
 - unstable system

$$a) \frac{s+8}{s^2+2s+8}$$

$$b) \frac{s+8}{s^2+9s+8}$$

$$c) \frac{3s+9}{2s+2}$$

$$d) \frac{s+2}{2s+2}$$

$$e) \frac{-s+8}{s^2+2s+8}$$

$$f) \frac{s}{s^2+2s+8}$$

$$g) \frac{s+8}{s-8}$$

Tvt

$$\lim_{s \rightarrow \infty} s f(s),$$

$$= \lim_{s \rightarrow \infty} \frac{1}{s} \cdot s \cdot f(s).$$

a) 0

b) 0

c) $\frac{3}{2}$

d) $\frac{1}{2}$

e) 0

f) ± 0

g) 1

Fvt

$$\lim_{s \rightarrow 0} F(s)$$

a) 1

b) 1

c) 1

d) 1

e) 1

f) 1

g) N/A

FPP.

$$\lim_{s \rightarrow \infty} s f(s)$$

a) 1

b) 1

c) $\frac{3}{2} + \frac{-1}{(2s+2)}$
 $\tilde{L}^{-1} \left(\frac{1}{2s+2} \right) \Big|_{s=0} = -\frac{1}{2^2}$

d) $\frac{1}{2} + \tilde{L}^{-1} \left(\frac{1}{2(s+1)} \right) \Big|_{s=0} = \frac{1}{2}$

e) -1

f) 0

g) 16.

1.

Aufgabe

Q.2 (a)

Sub-parts	Marks
6	2
4	1.5
2	0.5
1	0.5
0	0

(b)

Subparts	Marks
7	3
4	2
2	1
1	0.5
0	0

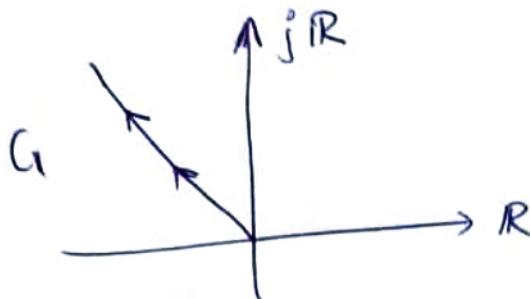
if all subparts are correct

Q3)

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

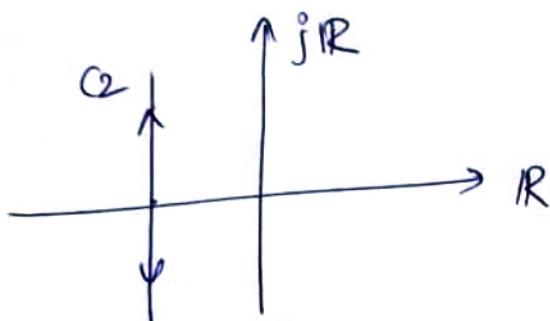
$0 < \zeta < 1$

a) constant % overshoot curve (C_1)



① mark

b) constant T_s curve (C_2)



Real part of root
is constant.

① mark

b) Along $C_2 \Rightarrow T_p$ decreases (since $\omega_d \uparrow$)

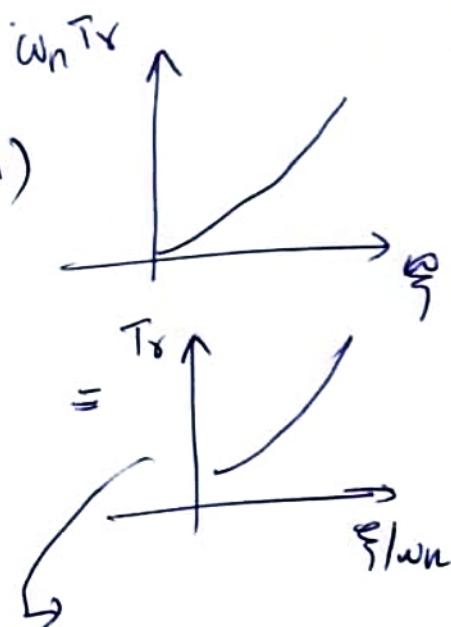
(1.5) % OS increases

mark T_r decreases

Along $C_1 \Rightarrow T_p$ decreases

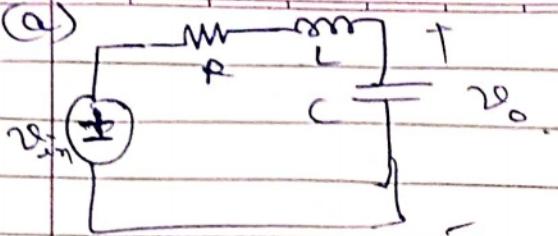
(1.5) T_s decreases

mark T_r decreases



ζ decreases ω_n increases $\Rightarrow T_r$ decreases

Q04 (a)



$$\frac{v_o}{v_{in}} = \frac{Y_{SC}}{Y_{SC} + R + \beta L}$$

$$\frac{v_o}{v_{in}} = \frac{1}{s^2 LC + RCs + 1}$$

$$\frac{v_o}{v_{in}} = \frac{1/LC}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$

$$\omega_m = \frac{1}{\sqrt{LC}}, \quad 2\zeta\omega_m = \frac{R}{L}$$

$$\zeta = \frac{R\sqrt{LC}}{2L} \Rightarrow$$

$$\boxed{\zeta = \frac{R}{2}\sqrt{\frac{C}{L}}}$$

taking $C = 10^{-8} F$, $L = 10^{-6} H$, $R = 10 \Omega$.

$$\zeta = \frac{10}{2} \sqrt{\frac{10^{-8}}{10^{-6}}} = 0.5$$

\hookrightarrow Underdamped.

(b) Same circuit with large R value can be an over damped system.

~~Let take~~ Let take $R = 10 k$.
 $C = 10^{-8} F$, $L = 10^{-6} H$

$$\zeta = \frac{10 \times 10^3}{2} \approx$$

$$\zeta = 500$$

\hookrightarrow hence over damped for large R.

(c) In both the above cases (a) & (b)

input is taken Voltage source of V_i

output is taken voltage across capacitor (V_o)

Marking factor

a) 1 marks \rightarrow Circuit with transfer fn.

1 marks \rightarrow choosing R, L, C s.t. it is
overdamped & R is small.
Underdamped.

b) 1 marks \rightarrow circuit with transfer fn.

1 marks \rightarrow choosing R, L, C , s.t. it is
underdamped if R is large.

c) 1 marks 0.5 mark for part (a) i/p & o/p

0.5 mark for part (b) o/p & i/p

Q5

$$(a) \quad G(s) = \frac{1}{s^2 + 2fs + 1}$$

Transfer function after addition of pole and taking the step response will look like :-

$$C(s) = \frac{a \leftarrow \text{to handle steady state value}}{s(s^2 + 2fs + 1)(s+a)}$$

taking partial fraction of $C(s)$

$$C(s) = \frac{A}{s} + \frac{Bs - C}{s^2 + 2fs + 1} + \frac{D}{(s+a)}$$

here we assumed that the non dominant pole a is located at $-c$ on the real axis

After calculation for A, B, C and D , we get :-

$$A = 1$$

$$B = \frac{2fa - a^2}{a^2 - 2fa + 1}$$

$$C = \frac{4f^2a - 2fa^2 - a}{a^2 - 2fa + 1}$$

$$D = \frac{-1}{a^2 - 2fa + 1}$$

now as the nondominant pole $a \rightarrow \infty$,

$$\lim_{a \rightarrow \infty} D = \lim_{a \rightarrow \infty} \frac{-1}{a^2 - 2fa + 1} = 0$$
$$\therefore D = 0$$

$$\lim_{a \rightarrow \infty} C = \lim_{a \rightarrow \infty} \frac{4f^2a - 2fa^2 - a}{a^2 - 2fa + 1} = -2f$$
$$\therefore C = -2f$$

$$\lim_{a \rightarrow \infty} B = \lim_{a \rightarrow \infty} \frac{2fa - a^2}{a^2 - 2fa + 1} = -1$$
$$\therefore B = -1$$

$$\lim_{a \rightarrow \infty} A = \lim_{a \rightarrow \infty} (1) = 1$$
$$\therefore A = 1$$

Thus we observed the residue (i.e. D) of the nondominant pole and its response becomes zero as the non dominant pole approaches infinity.

(b)

$$G(s) = \frac{1}{s^2 + 2fs + 1}$$

adding a pole to $G(s)$ "such that steady state gain is not disturbed" \Rightarrow

But here two cases may happen zero can lie on left half plane or on right half plane too.

Case 1: \rightarrow on left half plane

$$G(s) = \frac{(s/a + 1)}{s^2 + 2fs + 1}$$

Step response \Rightarrow

$$C(s) = \frac{(s/a + 1)}{s(s^2 + 2fs + 1)}$$

$$C(s) = \frac{1}{s(s^2 + 2fs + 1)} (s/a) + \frac{1}{s(s^2 + 2fs + 1)}$$

if $\alpha \rightarrow \infty$ then

$$C(s) = \frac{1}{s(s^2 + 2fs + 1)} \left(\frac{s}{\alpha} \right) + \frac{1}{s(s^2 + 2fs + 1)}$$

$$\therefore C(s) = \frac{1}{s(s^2 + 2fs + 1)}$$

case 2: when zero added on right half plane

$$C(s) = \frac{(1 - \frac{s}{\alpha})}{s(s^2 + 2fs + 1)}$$

$$C(s) = \frac{1}{s(s^2 + 2fs + 1)} - \left(\frac{s}{\alpha} \right) \left(\frac{1}{s(s^2 + 2fs + 1)} \right)$$

if $\alpha \rightarrow \infty$

$$C(s) = \frac{1}{s(s^2 + 2fs + 1)} - \left(\frac{s}{\alpha} \right) \left(\frac{1}{s(s^2 + 2fs + 1)} \right)$$

$$\therefore C(s) = \frac{1}{s(s^2 + 2fs + 1)}$$

method 2:

For additional zero to be neglected

take zero as :→

$$S = -\frac{1}{\epsilon}$$

$$TF = \frac{\epsilon S + 1}{S^2 + 2fs + 1}$$

now proceed further.