

Lecture 16 – Sinusoidal sources

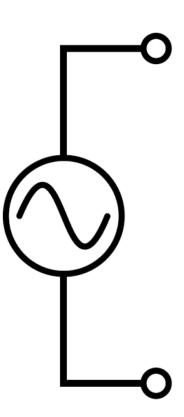
Dr. Aftab M. Hussain,
Associate Professor, PATRIoT Lab, CVEST

Sinusoidal sources

- It is very common to apply sinusoidal sources to circuits because power is produced in sine, rotating things are easier to represent in sine, sound is easier to represent as sine etc.
- Thus, the response of a circuit to sine excitation should be studied and understood
- The sine source is represented as shown

$$V = V_m \sin \omega t$$

- At any given time, the magnitude of the voltage can be calculated
- Because it is a time varying function, application of it to inductors and capacitors can lead to interesting responses

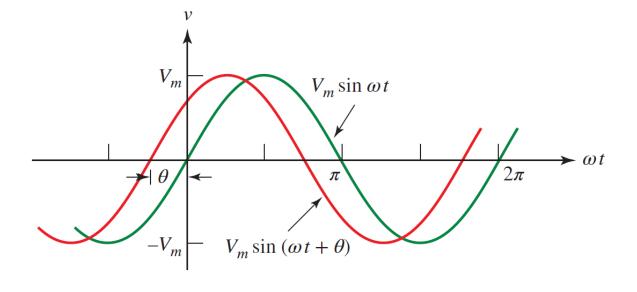


Leading and Lagging

A sine wave can be shifted in time

• The shift is defined by the phase angle, if a sine wave is not zero at t=0, then it is represented by $v(t)=V_m\sin(\omega t+\theta)$

• If θ is positive, the wave is said to be lagging $V_m \sin \omega t$, if θ is negative, the wave is said to be leading



RL circuit

- Let us start with a simple RL circuit
- We focus on the "steady-state", so the assumption is that the circuit has been in this state for a long time

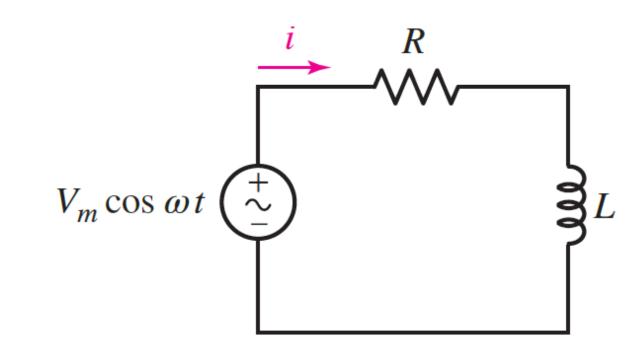
$$L\frac{di}{dt} + Ri = V_m \cos \omega t$$

The general solution to this is of the form:

$$i(t) = A_1 \cos \omega t + A_2 \sin \omega t$$

Substituting in the equation:

$$L\omega(-A_1 \sin \omega t + A_2 \cos \omega t) + R(A_1 \cos \omega t + A_2 \sin \omega t) = V_m \cos \omega t$$



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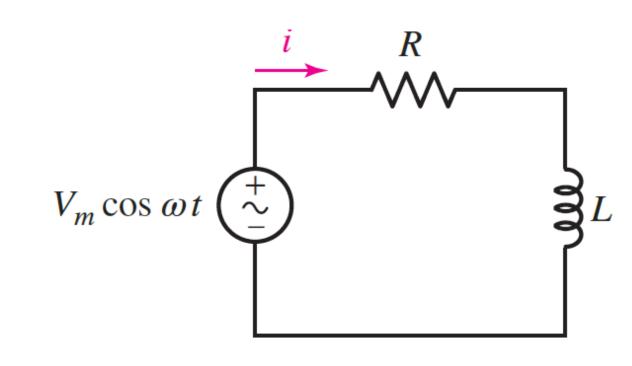
$$(-LA_1\omega + RA_2)\sin \omega t + (LA_2\omega + RA_1 - V_m)\cos \omega t = 0$$

This equation needs to be true for all values of *t*

Thus,

$$-LA_1\omega + RA_2 = 0$$

$$LA_2\omega + RA_1 - V_m = 0$$



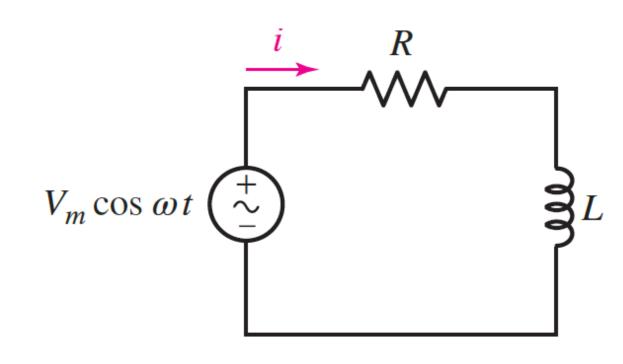
$$-LA_1\omega + RA_2 = 0$$

$$LA_2\omega + RA_1 - V_m = 0$$

$$A_1 = \frac{RV_m}{R^2 + \omega^2 L^2}$$

$$A_2 = \frac{\omega L V_m}{R^2 + \omega^2 L^2}$$

$$i(t) = \frac{RV_m}{R^2 + \omega^2 L^2} \cos \omega t + \frac{\omega LV_m}{R^2 + \omega^2 L^2} \sin \omega t$$



RL circuit

Turns out, you can express the current as a cosine function with a phase

$$i(t) = A\cos(\omega t + \theta)$$

$$A\cos\theta\cos\omega t + A\sin\theta\sin\omega t$$

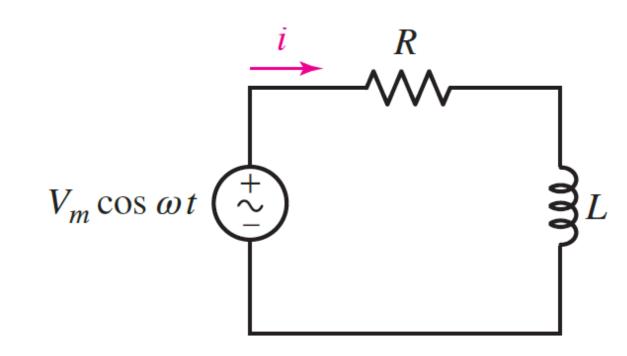
$$= \frac{RV_m}{R^2 + \omega^2 L^2}\cos\omega t + \frac{\omega LV_m}{R^2 + \omega^2 L^2}\sin\omega t$$

$$A\cos\theta = \frac{RV_m}{R^2 + \omega^2 L^2}$$

$$A\sin\theta = \frac{\omega L V_m}{R^2 + \omega^2 L^2}$$

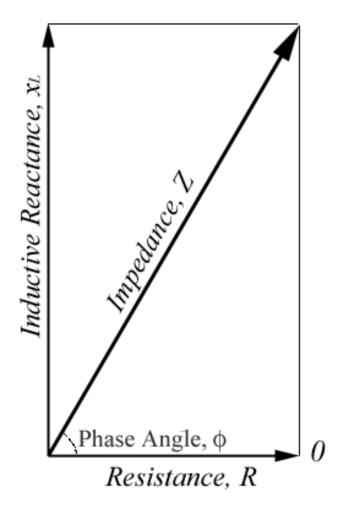
$$A = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}}$$
 and $\tan \theta = \frac{\omega L}{R}$

If
$$Z \equiv R + j\omega L$$
, $|Z| = \sqrt{R^2 + \omega^2 L^2}$



Complex impedance

- The impedance of inductor in the s-domain is sL, and the complex frequency $s=\sigma+j\omega$
- In AC response, the damping coefficient $\sigma=0$, thus, inductor impedance is ωL
- Similarly, capacitor inductance is $1/j\omega \mathcal{C}$
- The series/parallel sum of these impedances provides the complex impedance of the circuit
- Typically represented in the complex plane



RLC impedance

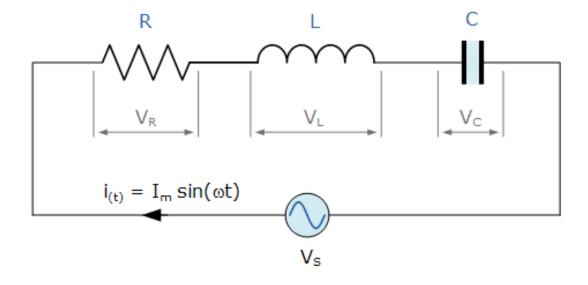
- Say we have a series RLC circuit, what is its complex impedance for a pure AC response?
- For a pure AC response, we can assume $s=j\omega$

$$Z = R + j\omega L + \frac{1}{j\omega C}$$

$$Z = R + j\omega L - \frac{j}{\omega C}$$

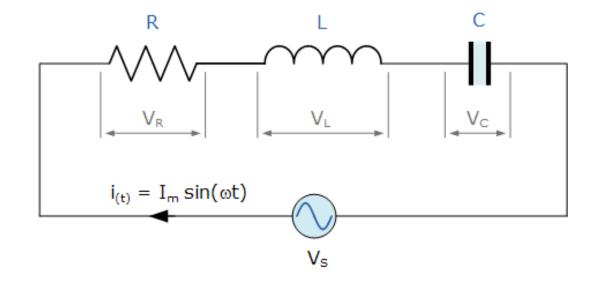
$$Z = R + j\left(\omega L - \frac{1}{\omega C}\right)$$

$$|Z| = \sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}$$



RLC impedance

- What is the minimum value of Z wrt ω ?
- When $\omega = \omega_0 = 1/\sqrt{LC}$, we get |Z| = R. This is called resonance and ω_0 is called resonant frequency
- Thus, just like the s-domain analysis, impedances can be approximated as $j\omega L$ and $1/j\omega C$ for <u>pure sinusoidal</u> responses
- In case of other stimuli, a combination of pure AC and pure DC response can also be studied (superposition theorem)

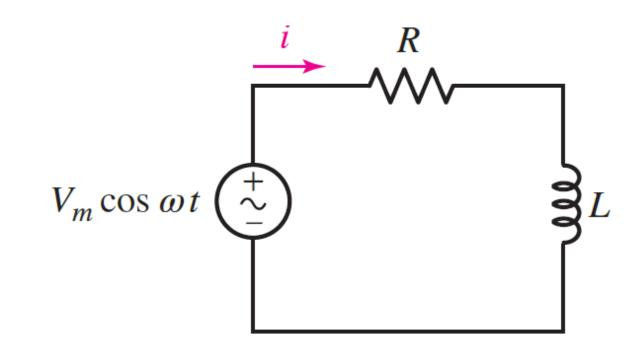


• For AC input, Let us see if we can perform that analysis in the s-domain

$$I(s) = \frac{\left(\frac{V_m s}{s^2 + \omega^2}\right)}{R + sL}$$

$$I(s) = V_m \left[\frac{s}{(s^2 + \omega^2)(R + sL)} \right]$$

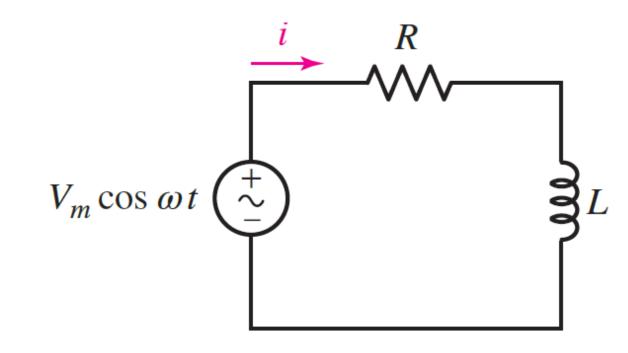
$$I(s) = V_m \left[\frac{s}{(s+j\omega)(s-j\omega)(R+sL)} \right]$$



$$I(s) = V_m \left[\frac{s}{(s+j\omega)(s-j\omega)(R+sL)} \right]$$

$$I(s) = V_m \left[\frac{1}{2(R - j\omega L)(s + j\omega)} + \frac{1}{2(R + j\omega L)(s - j\omega)} + \frac{\left(-\frac{R}{L}\right)}{(R^2/L^2 + \omega^2)(R + sL)} \right]$$

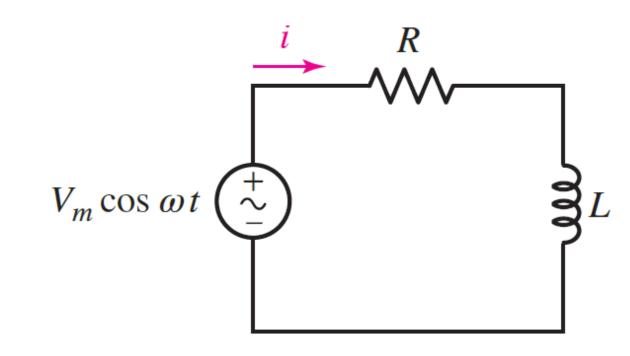
$$I(s) = V_m \left[\frac{1}{2(R - j\omega L)(s + j\omega)} + \frac{1}{2(R + j\omega L)(s - j\omega)} + \frac{\left(-\frac{R}{L}\right)}{(R^2/L^2 + \omega^2)(R + sL)} \right]$$



$$I(s) = V_m \left[\frac{sR + \omega^2 L^2}{(R^2 + \omega^2 L^2)(s^2 + \omega^2)} + \frac{\left(-\frac{R}{L}\right)}{(R^2/L^2 + \omega^2)(R + sL)} \right]$$

• Thus, the response of the circuit is:
$$i(t) = \left(A\sin\omega t + B\cos\omega t + Ce^{-\frac{R}{L}t}\right)u(t)$$

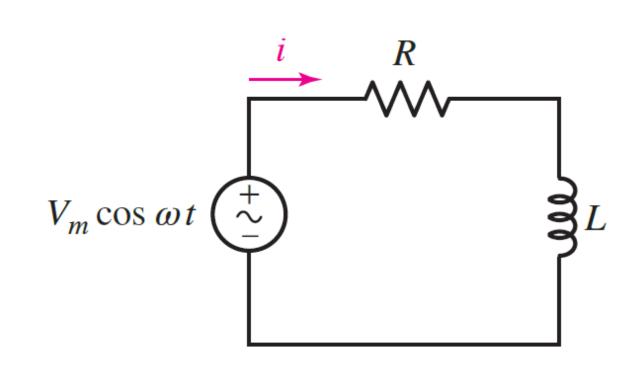
What is the initial current?



$$i(0^{+})$$

$$= \lim_{s \to \infty} \{ sV_{m} \left[\frac{sR + \omega^{2}L^{2}}{(R^{2} + \omega^{2}L^{2})(s^{2} + \omega^{2})} + \frac{\left(-\frac{R}{L}\right)}{\left(\frac{R^{2}}{L^{2}} + \omega^{2}\right)(R + sL)} \right] \}$$

$$i(0^+) = \frac{R}{R^2 + \omega^2 L^2} - \frac{R}{R^2 + \omega^2 L^2} = 0$$



Transfer function

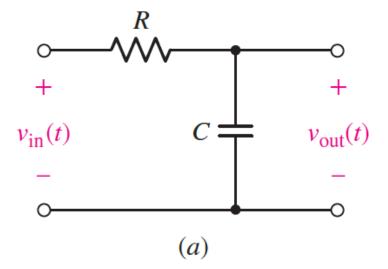
- We can convert any circuit in the sdomain and analyse its response to various input stimuli
- For this, a common technique is to detach the forcing function and obtain a "transfer function" for the circuit for any arbitrary forcing function

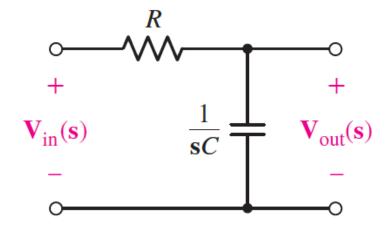
In the given circuit

$$\frac{V_{in} - V_{out}}{R} = \frac{V_{out}}{1/sC}$$

$$V_{out} \left(\frac{1}{R} + sC\right) = \frac{V_{in}}{R}$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{1 + sRC} \equiv H(s)$$





Transfer function

$$\frac{V_{out}}{V_{in}} = \frac{1}{1 + sRC} \equiv H(s)$$

- We could just as easily specify a particular current as either the input or output quantity, leading to a different transfer function for the same circuit
- Thus, for any input, the output of the circuit is V(s)H(s)
- The inverse Laplace of this provides the response
- However, stability, frequency response etc. can be directly inferred from the poles and zeros of the transfer function

