

# GRAVITATIONAL LENSING

## 18 – SOFTENED LENSES

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*Massimo Meneghetti*  
*AA 2017-2018*

# SOFTENED PROFILES: THE NON-SINGULAR ISOTHERMAL SPHERE

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*The profiles considered so far have surface density profiles with a singularity at  $x=0$ . We consider another class of lenses which have a flat core.*

*Given the simplicity of the model, we investigate the effects of the core by modifying the SIS lens:*

$$\Sigma(\xi) = \frac{\sigma_v^2}{2G} \frac{1}{\sqrt{\xi^2 + \xi_c^2}} = \frac{\Sigma_0}{\sqrt{1 + \xi^2/\xi_c^2}}$$

$$\Sigma_0 = \frac{\sigma_v^2}{2G\xi_c}$$

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*Choosing*  $\xi_0 = 4\pi \left( \frac{\sigma_v}{c} \right)^2 \frac{D_L D_{LS}}{D_S}$

$$\Sigma(\xi) = \frac{\sigma_v^2}{2G} \frac{1}{\sqrt{\xi^2 + \xi_c^2}} = \frac{\Sigma_0}{\sqrt{1 + \xi^2/\xi_c^2}}$$

$$\kappa(x) = \frac{1}{2\sqrt{x^2 + x_c^2}}$$

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*The mass profile is computed as follows*

$$m(x) = 2 \int_0^x \kappa(x') x' dx' = \sqrt{x^2 + x_c^2} - x_c$$

*The deflection angle is*

$$\alpha(x) = \frac{m(x)}{x} = \sqrt{1 + \frac{x_c^2}{x^2}} - \frac{x_c}{x}$$

*The shear is*

$$\gamma(x) = \frac{\sqrt{x^2 + x_c^2} - x_c}{x^2} - \frac{1}{2\sqrt{x^2 + x_c^2}}$$

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*We can search for the tangential critical line:*

$$m(x) = 2 \int_0^x \kappa(x') x' dx' = \sqrt{x^2 + x_c^2} - x_c \qquad m(x)/x^2 = 1$$

$$\sqrt{x^2 + x_c^2} - x_c = x^2$$

$$x^2(x^2 + 2x_c - 1) = 0$$

$$x_t = \sqrt{1 - 2x_c}$$

*Note that the tangential critical line exists only if  $x_c < 1/2$*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*and the radial critical line:*

$$\left(1 - \frac{d\alpha(x)}{dx}\right) = 1 + \frac{m(x)}{x^2} - 2\kappa(x) = 0.$$

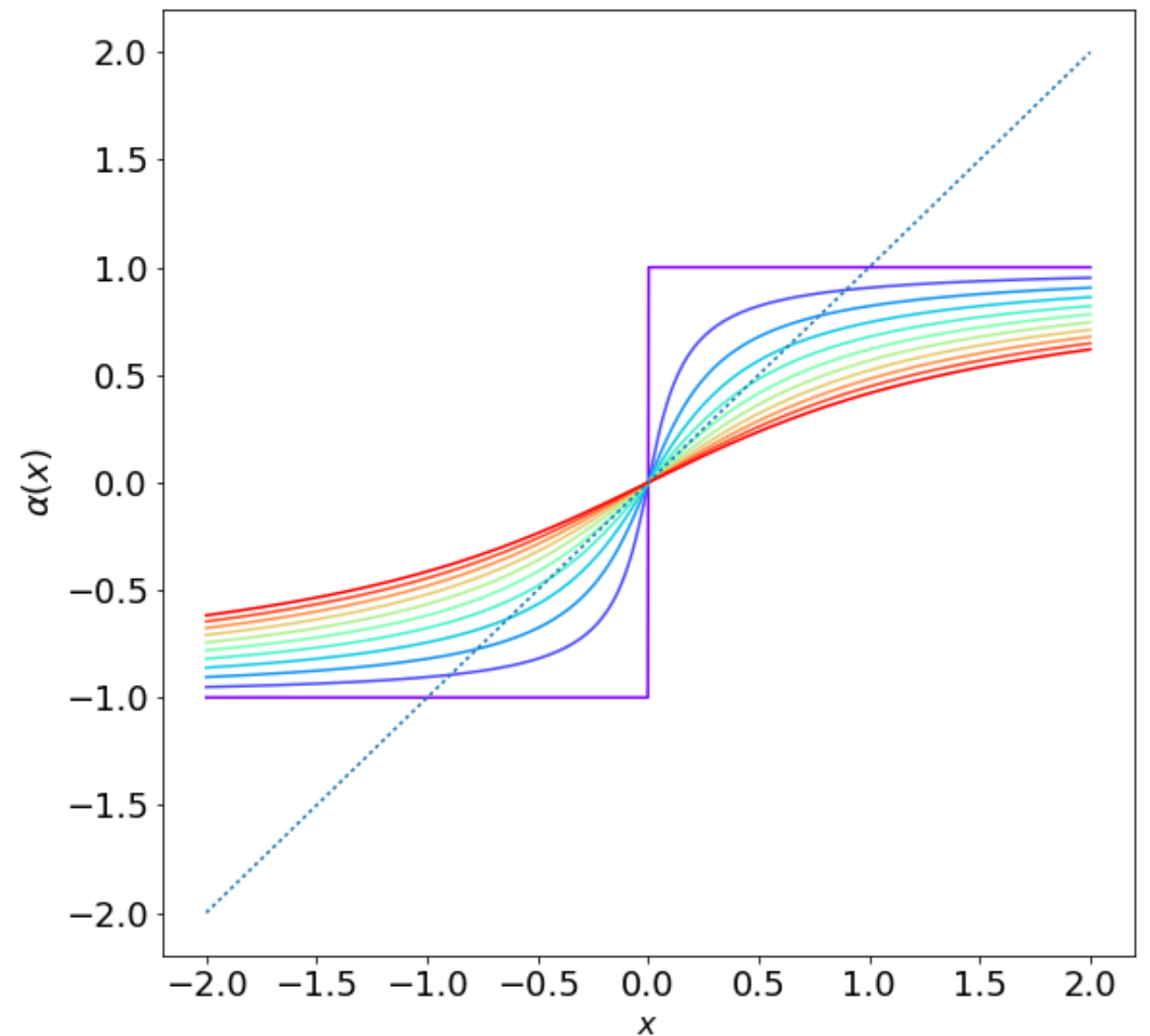
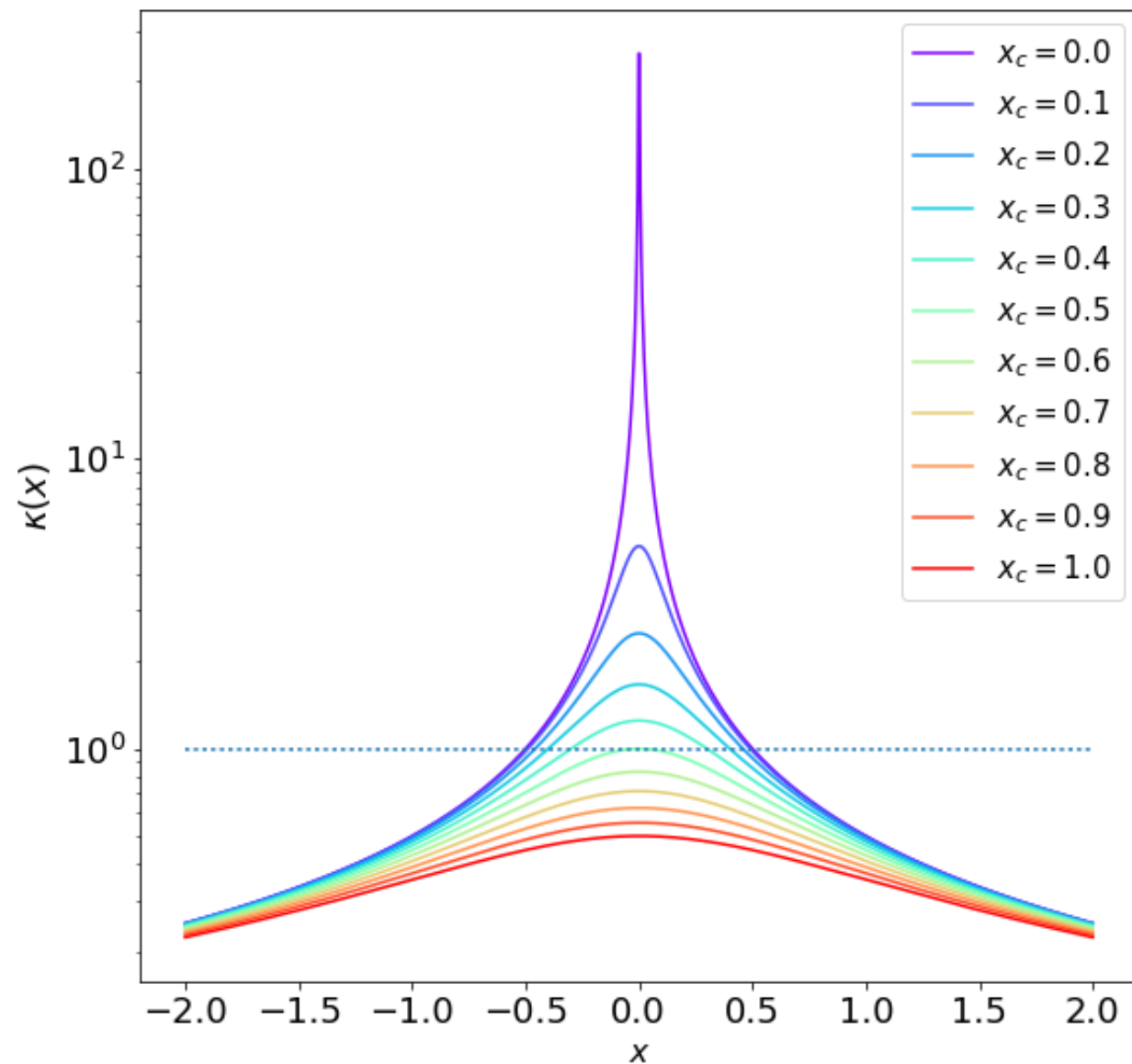
$$1 + \frac{\sqrt{x^2 + x_c^2} - x_c}{x^2} - \frac{1}{\sqrt{x^2 + x_c^2}} = 0$$

$$x_r^2 = \frac{1}{2} \left( 2x_c - x_c^2 - x_c \sqrt{x_c^2 + 4x_c} \right)$$

$$x_r^2 \geq 0 \text{ for } x_c \leq 1/2.$$

*Thus, the existence condition for the radial critical is the same as for the tangential critical line*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

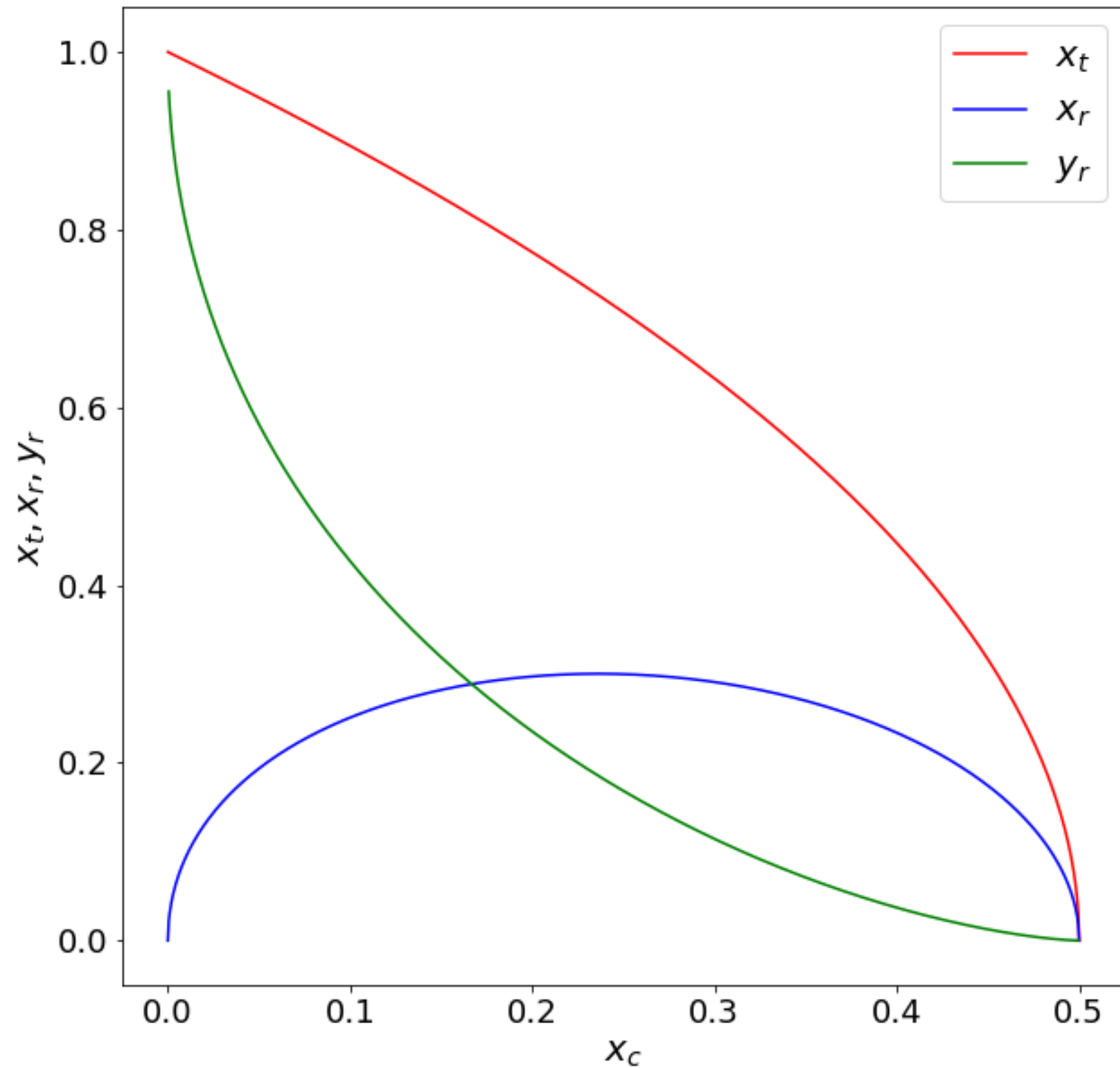


*If the core is too large, the convergence does not exceed 1 and the derivative of the deflection angle is never larger than 1...*

*No critical lines! No multiple images!*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

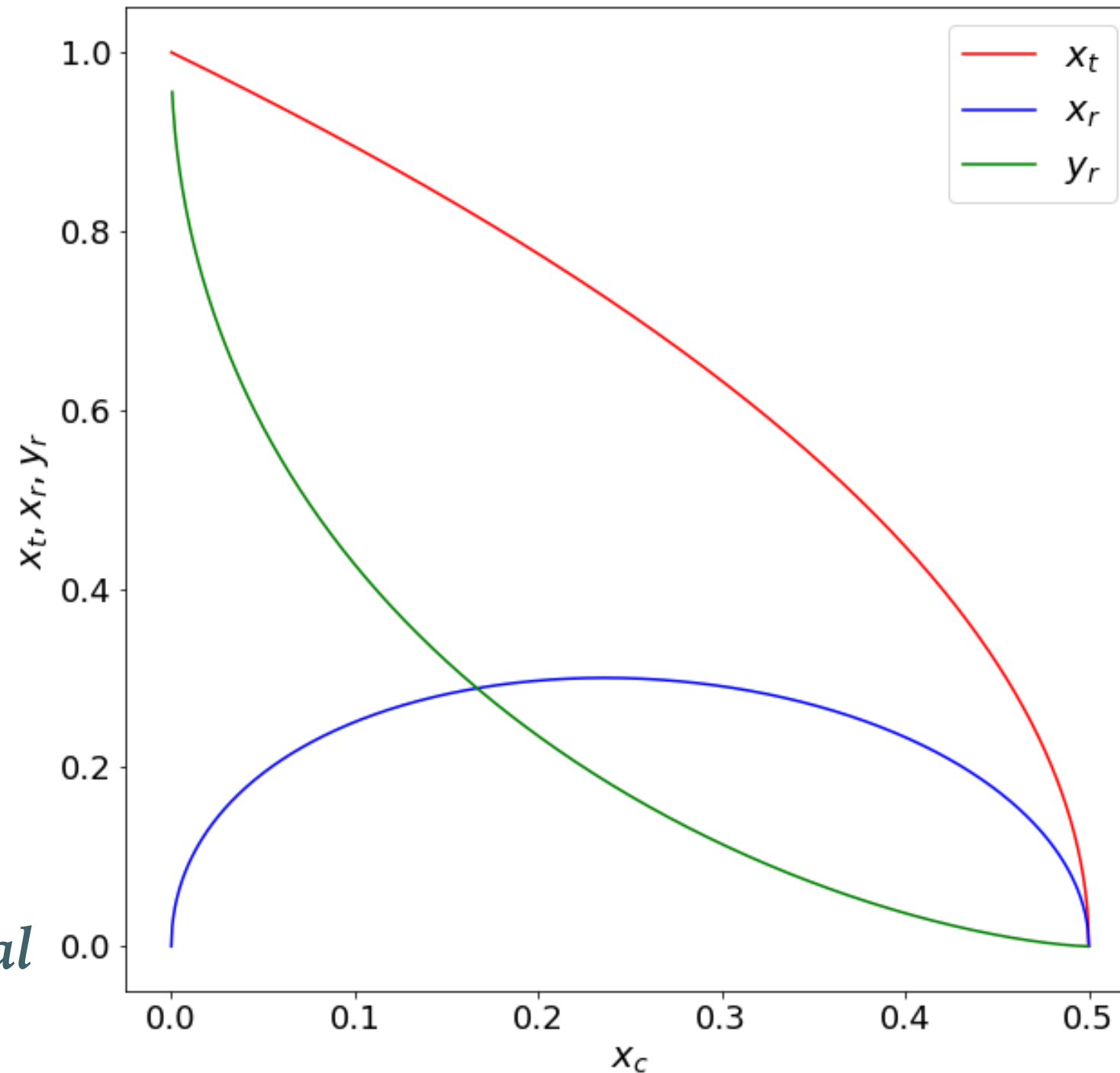
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# NON SINGULAR ISOTHERMAL SPHERE (NIS)

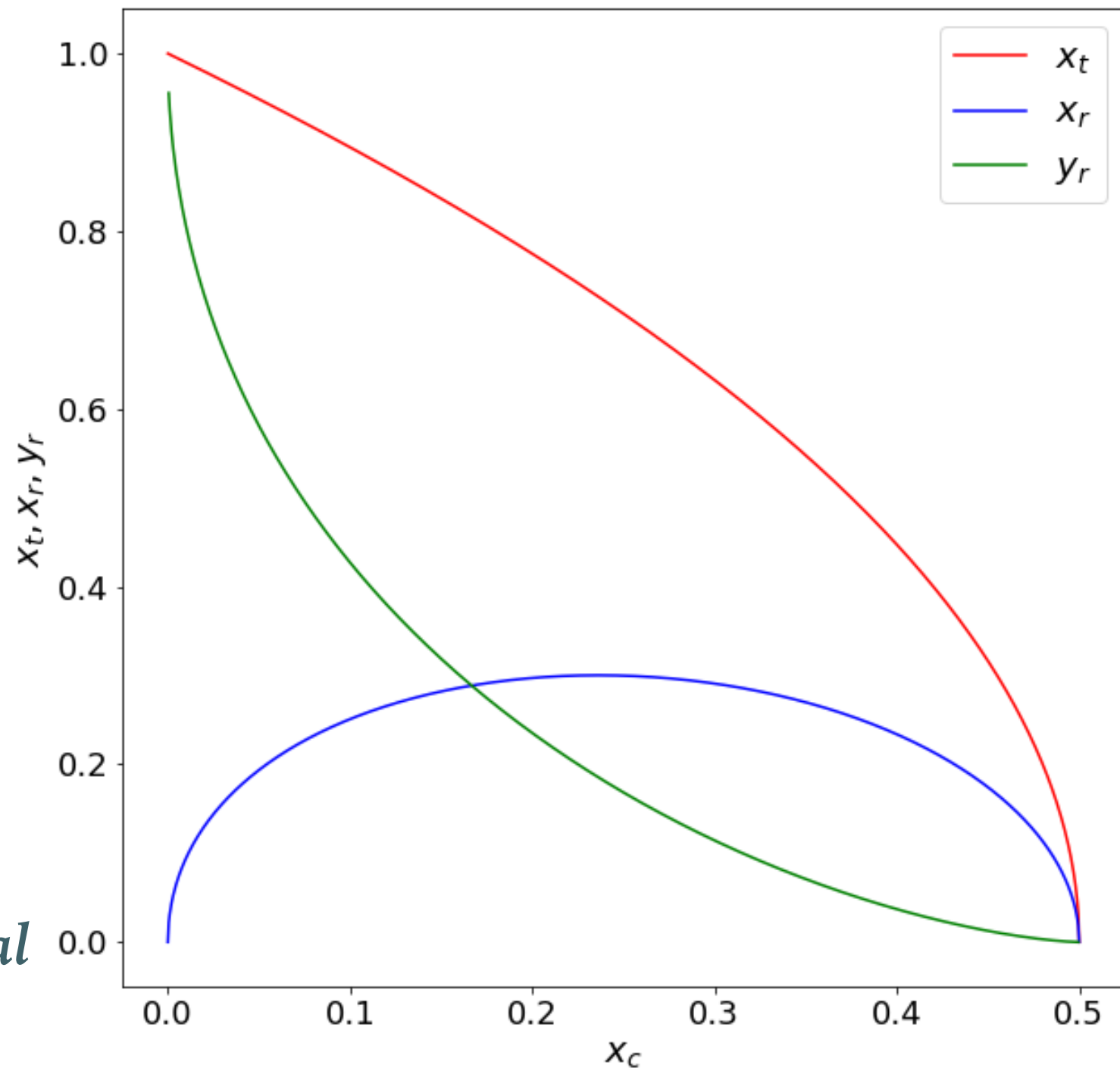
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*Small core,  
small radial  
critical line,  
large tangential  
critical line*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*Small core,  
small radial  
critical line,  
large tangential  
critical line*

*large core, small  
radial critical  
line, small  
tangential  
critical line*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*The lens equation can be reduced to the form:*

$$y = x - \frac{m(x)}{x} = x - \sqrt{1 + \frac{x_c^2}{x^2}} - \frac{x_c}{x}$$

$$x^3 - 2yx^2 + (y^2 + 2x_c - 1)x - 2yx_c = 0 .$$

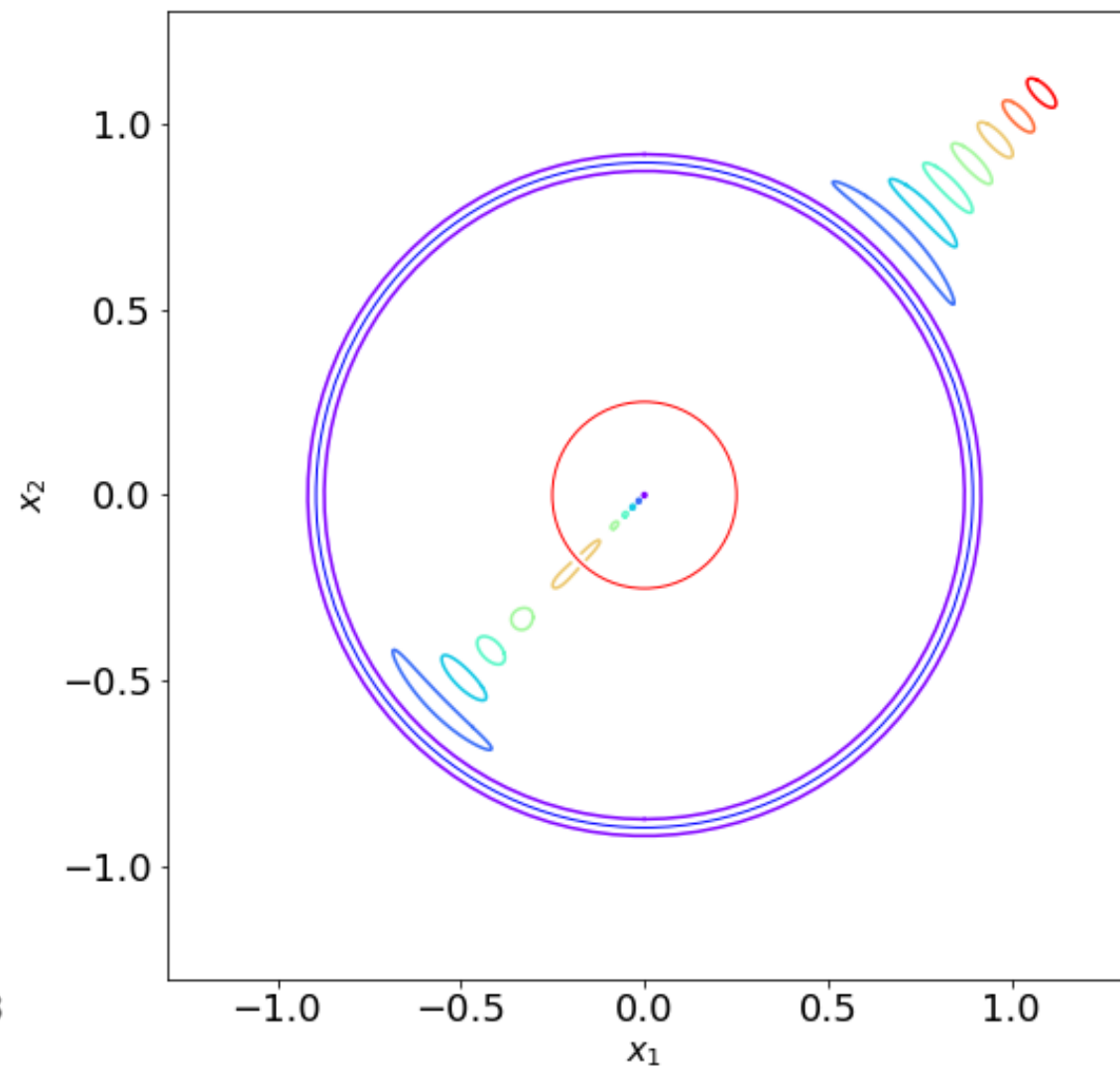
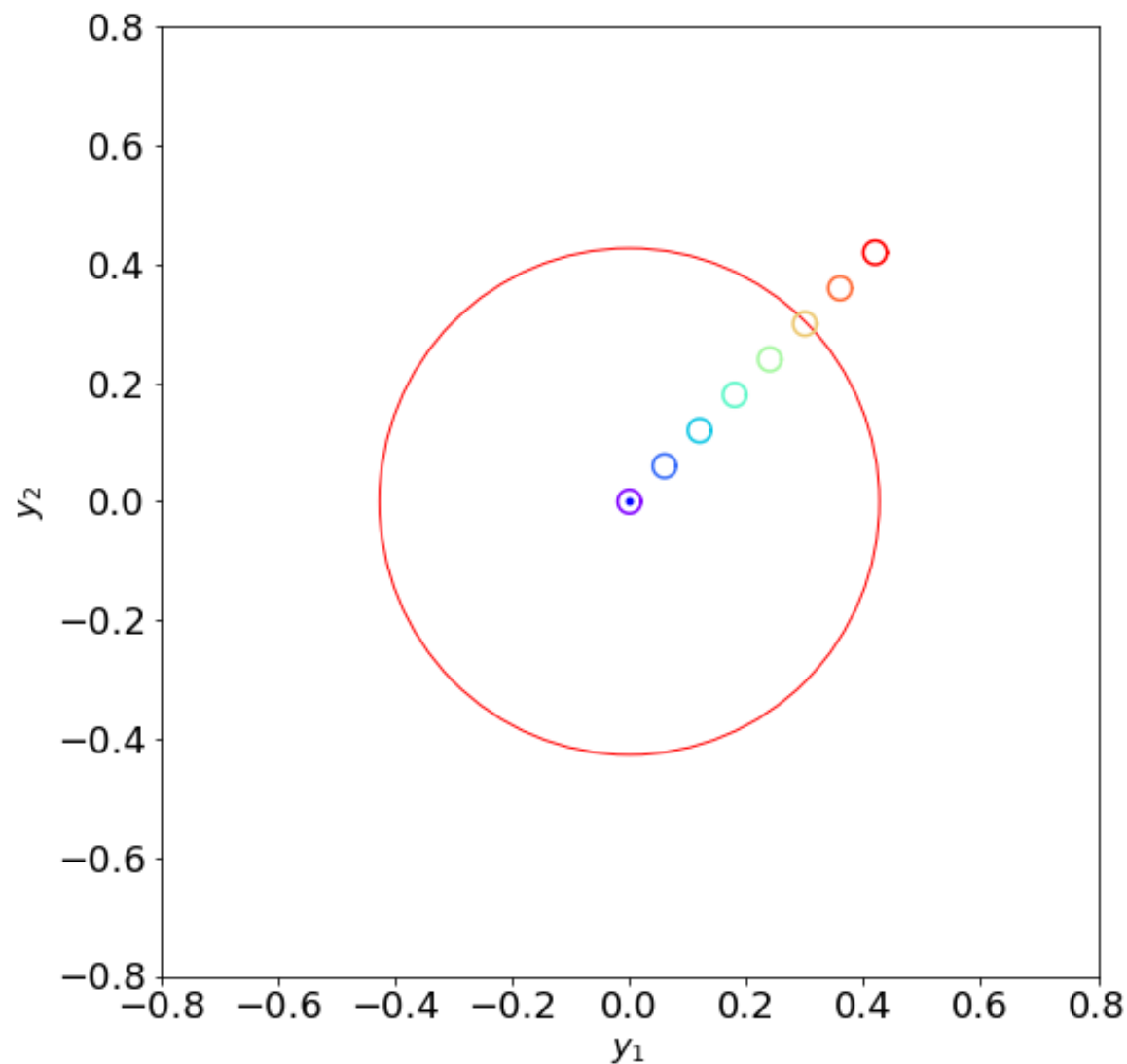
*There are up to three solutions, but, again the existence of multiple images depends on  $y$  and  $x_c$ ...*

*In particular on whether:*

- *the radial caustic exist*
- *the source is inside or outside the radial caustic*

# NON SINGULAR ISOTHERMAL SPHERE (NIS)

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*Three images if the source is inside the radial caustic; One image otherwise.*

*Parity: changes at each critical line (remember: maxima, minima, saddle points of TDS).*

# SINGULAR ISOTHERMAL ELLIPSOID

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*Now we make the surface density contours of the SIS elliptical:*

$$\xi \Rightarrow \sqrt{\xi_1^2 + f^2 \xi_2^2}$$

$$\Sigma(\xi) = \frac{\sigma_v^2}{2G\xi} \quad \rightarrow \quad \Sigma(\vec{\xi}) = \frac{\sigma_v^2}{2G} \frac{\sqrt{f}}{\sqrt{\xi_1^2 + f^2 \xi_2^2}}$$

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*Surface density is  
constant on ellipses  
with minor axis  $\xi$  and  
major axis  $\xi/f$*

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*Elliptical contours  
with their major axis  
along the  $\xi_2$  axis*

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*Ensures that the mass inside elliptical iso-contours is independent on  $f$*

*Elliptical contours with their major axis along the  $\xi_2$  axis*

*Surface density is constant on ellipses with minor axis  $\xi$  and major axis  $\xi/f$*



# SINGULAR ISOTHERMAL ELLIPSOID

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$$\Sigma(\vec{\xi}) = \frac{\sigma_v^2}{2G} \frac{\sqrt{f}}{\sqrt{\xi_1^2 + f^2 \xi_2^2}}$$

*Let's derive the convergence in  
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# SINGULAR ISOTHERMAL ELLIPSOID

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$$\Sigma(\vec{\xi}) = \frac{\sigma_v^2}{2G} \frac{\sqrt{f}}{\sqrt{\xi_1^2 + f^2 \xi_2^2}} \frac{\xi_0}{\xi_0}$$

$$\xi_0 = 4\pi \left( \frac{\sigma_v}{c} \right)^2 \frac{D_L D_{LS}}{D_S}$$

$$\kappa(\vec{x}) = \frac{\sqrt{f}}{2\sqrt{x_1^2 + f^2 x_2^2}}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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*In polar coordinates:*

$$\Delta(\varphi) = \sqrt{\cos^2 \varphi + f^2 \sin^2 \varphi}$$

$$\kappa(x, \varphi) = \frac{\sqrt{f}}{2x\Delta(\varphi)}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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$$\Delta(\varphi) = \sqrt{\cos^2 \varphi + f^2 \sin^2 \varphi} \qquad \kappa(x, \varphi) = \frac{\sqrt{f}}{2x\Delta(\varphi)}$$

*The lensing potential can be obtained by solving the Poisson equation:*

$$\frac{\partial^2 \Psi}{\partial x^2} + \frac{1}{x} \frac{\partial \Psi}{\partial x} + \frac{1}{x^2} \frac{\partial^2 \Psi}{\partial \varphi^2} = 2\kappa = \frac{\sqrt{f}}{x\Delta(\varphi)}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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*With the ansatz*  $\Psi(x, \varphi) := x\tilde{\Psi}(\varphi)$

$$\tilde{\Psi}(\varphi) + \frac{d^2}{d\varphi^2} \tilde{\Psi}(\varphi) = \frac{\sqrt{f}}{\Delta(\varphi)}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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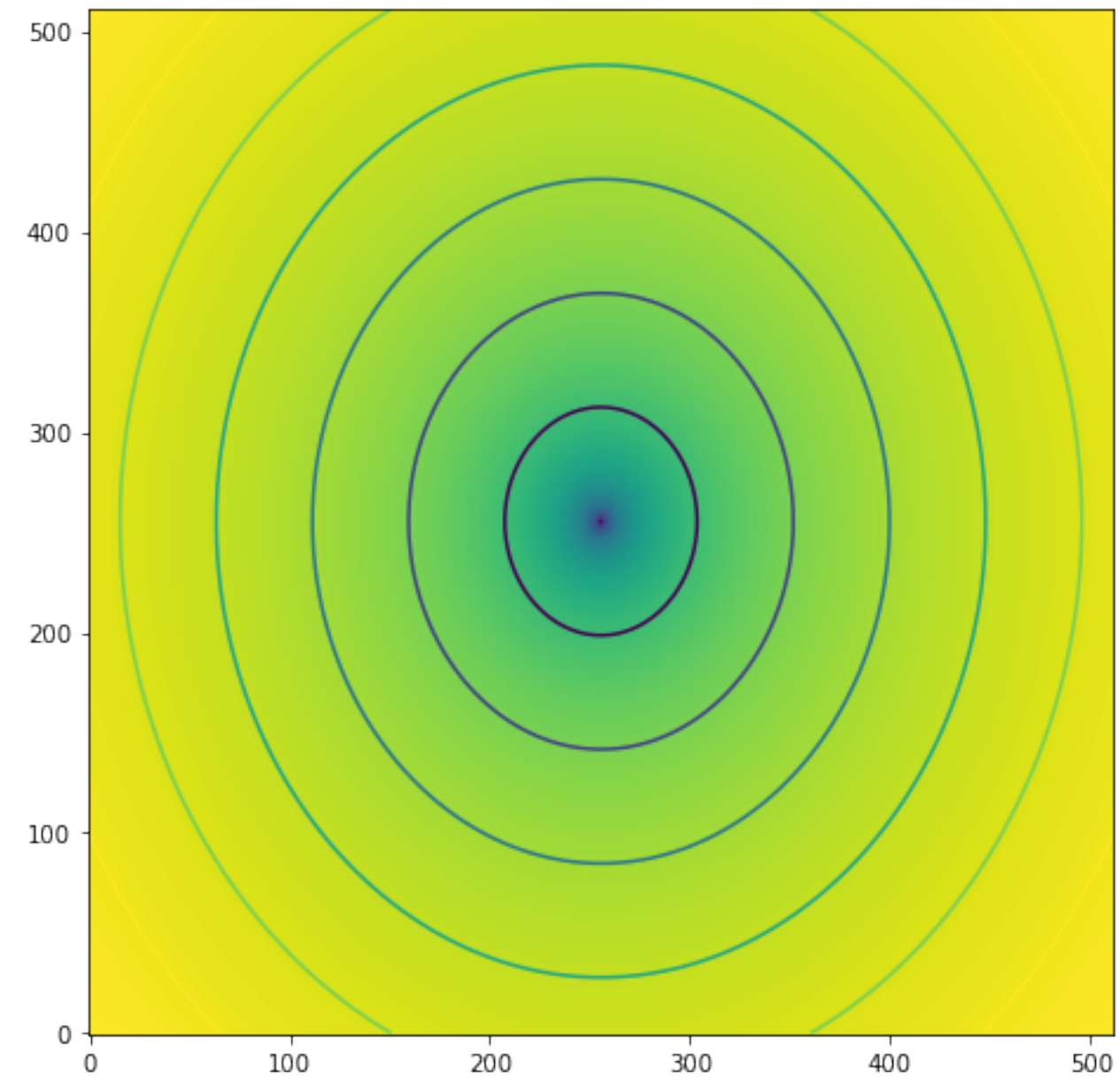
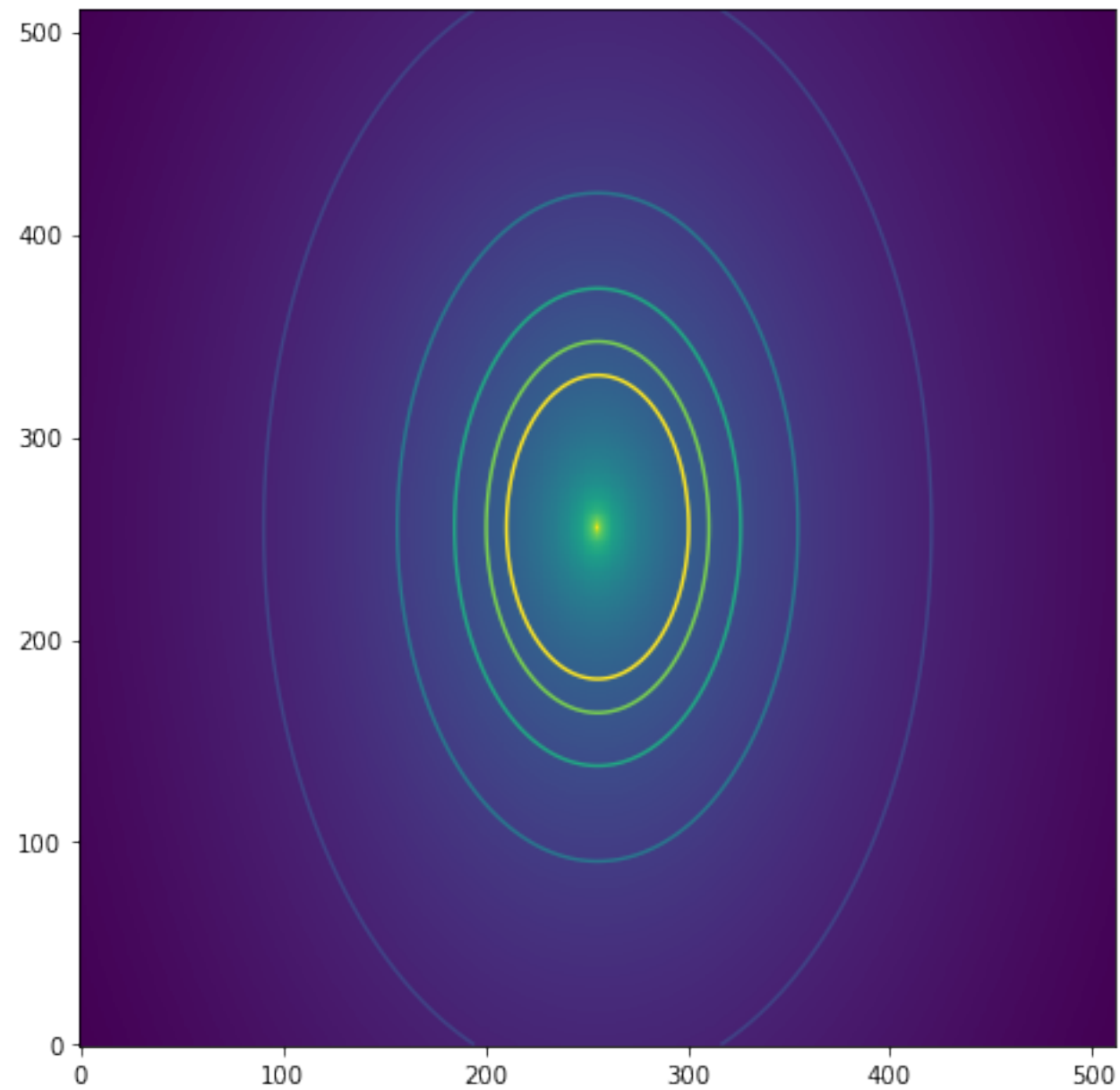
$$\tilde{\Psi}(\varphi) + \frac{d^2}{d\varphi^2} \tilde{\Psi}(\varphi) = \frac{\sqrt{f}}{\Delta(\varphi)}$$

*Solved with Green's method (Kormann et al. 1994):*

$$\Psi(x, \varphi) = x \frac{\sqrt{f}}{f'} \left[ \sin \varphi \arcsin(f' \sin \varphi) + \cos \varphi \operatorname{arcsinh}(f' / f \cos \varphi) \right] \qquad f' = \sqrt{1 - f^2}$$

# CONVERGENCE AND POTENTIAL

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# SINGULAR ISOTHERMAL ELLIPSOID

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$$\frac{\partial}{\partial x_1} = \cos \varphi \frac{\partial}{\partial x} - \frac{\sin \varphi}{x} \frac{\partial}{\partial \varphi}$$

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# SINGULAR ISOTHERMAL ELLIPSOID

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$$\alpha_1(\vec{x}) = \frac{\sqrt{f}}{f'} \operatorname{arcsinh} \left( \frac{f'}{f} \cos \varphi \right)$$

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# SINGULAR ISOTHERMAL ELLIPSOID

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*Analogy with the SIS: the deflection angle does not depend on  $x$ !*

# SINGULAR ISOTHERMAL ELLIPSOID

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*The component of the shear:*

# SINGULAR ISOTHERMAL ELLIPSOID

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$$\alpha_2(\vec{x}) = \frac{\sqrt{f}}{f'} \arcsin(f' \sin \varphi)$$

*The component of the shear:*

$$\gamma_1 = \frac{1}{2} \left( \frac{\partial \alpha_1}{\partial x_1} - \frac{\partial \alpha_2}{\partial x_2} \right) \qquad \gamma_1 = -\frac{\sqrt{f}}{2x\Delta(\varphi)} \cos 2\varphi = -\kappa \cos 2\varphi$$
$$\gamma_2 = \frac{\partial \alpha_1}{\partial x_2} \qquad \gamma_2 = -\frac{\sqrt{f}}{2x\Delta(\varphi)} \sin 2\varphi = -\kappa \sin 2\varphi$$

# SINGULAR ISOTHERMAL ELLIPSOID

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$$\gamma_2 = \frac{\partial \alpha_1}{\partial x_2} \qquad \gamma_2 = -\frac{\sqrt{f}}{2x\Delta(\varphi)} \sin 2\varphi = -\kappa \sin 2\varphi$$

*Similarly to the SIS:  $\gamma = \kappa$*

# SINGULAR ISOTHERMAL ELLIPSOID

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$$\begin{aligned}\gamma_1 &= -\frac{\sqrt{f}}{2x\Delta(\varphi)} \cos 2\varphi = -\kappa \cos 2\varphi \\ \gamma_2 &= -\frac{\sqrt{f}}{2x\Delta(\varphi)} \sin 2\varphi = -\kappa \sin 2\varphi\end{aligned}$$

*We have now the ingredients to compute the lensing Jacobian matrix*

$$A = \begin{bmatrix} 1 - \kappa - \gamma_1 & -\gamma_2 \\ \gamma_2 & 1 - \kappa + \gamma_1 \end{bmatrix} = \begin{bmatrix} 1 - 2\kappa \sin^2 \varphi & \kappa \sin 2\varphi \\ \kappa \sin 2\varphi & 1 - 2\kappa \cos^2 \varphi \end{bmatrix}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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*whose eigenvalues are:*

$$\begin{aligned}\lambda_t &= 1 - \kappa - \gamma = 1 - 2\kappa \\ \lambda_r &= 1 - \kappa + \gamma = 1.\end{aligned}$$



# SINGULAR ISOTHERMAL ELLIPSOID

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$$\lambda_t = 1 - \kappa - \gamma = 1 - 2\kappa$$

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*As the SIS, the SIE does not have a radial critical line!*

# SINGULAR ISOTHERMAL ELLIPSOID

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*As the SIS, the SIE does not have a radial critical line!*

*The tangential critical line is an ellipse, along which*

$$\kappa = \frac{1}{2}$$

# SINGULAR ISOTHERMAL ELLIPSOID

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As the SIS, *the SIE does not have a radial critical line!*

The tangential critical line is an ellipse, along which

$$\kappa = \frac{1}{2}$$

$$\kappa(x, \varphi) = \frac{\sqrt{f}}{2x\Delta(\varphi)} \quad \rightarrow \quad \vec{x}_t(\varphi) = \frac{\sqrt{f}}{\Delta(\varphi)} [\cos \varphi, \sin \varphi]$$

# SINGULAR ISOTHERMAL ELLIPSOID

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$$\vec{x}_t(\varphi) = \frac{\sqrt{f}}{\Delta(\varphi)} [\cos \varphi, \sin \varphi]$$

*The corresponding caustic can be found using the lens equation:*

$$\begin{aligned} y_{t,1} &= \frac{\sqrt{f}}{\Delta(\varphi)} \cos \varphi - \frac{\sqrt{f}}{f'} \operatorname{arcsinh} \left( \frac{f'}{f} \cos \varphi \right) \\ y_{t,2} &= \frac{\sqrt{f}}{\Delta(\varphi)} \sin \varphi - \frac{\sqrt{f}}{f'} \operatorname{arcsin}(f' \sin \varphi) . \end{aligned}$$

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*There is no radial caustic, but there is the cut, which can be computed as*

$$\vec{y}_c = \lim_{x \rightarrow 0} \vec{y}(x, \varphi) = -\vec{\alpha}(\varphi)$$

# SINGULAR ISOTHERMAL ELLIPSOID

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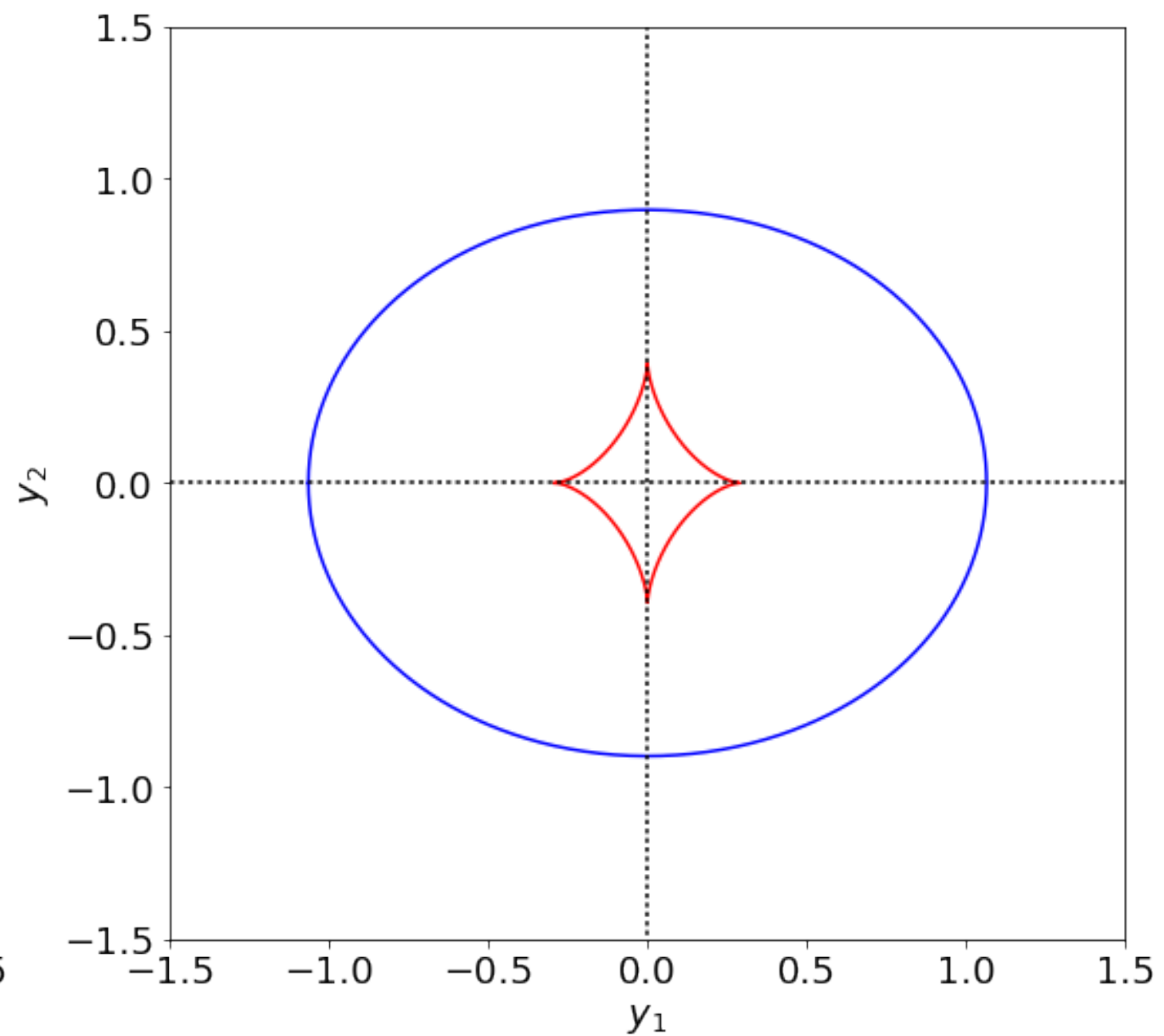
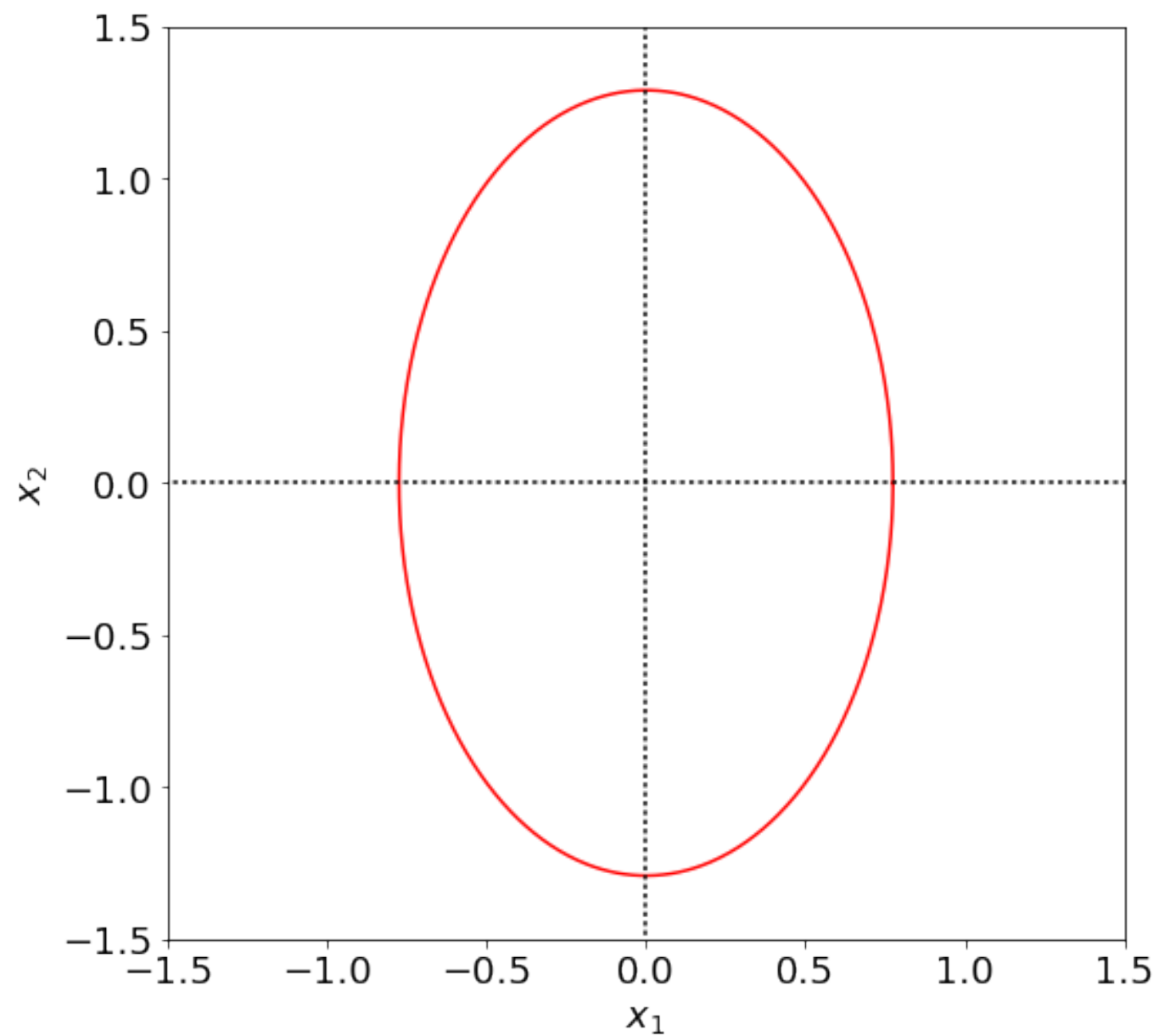
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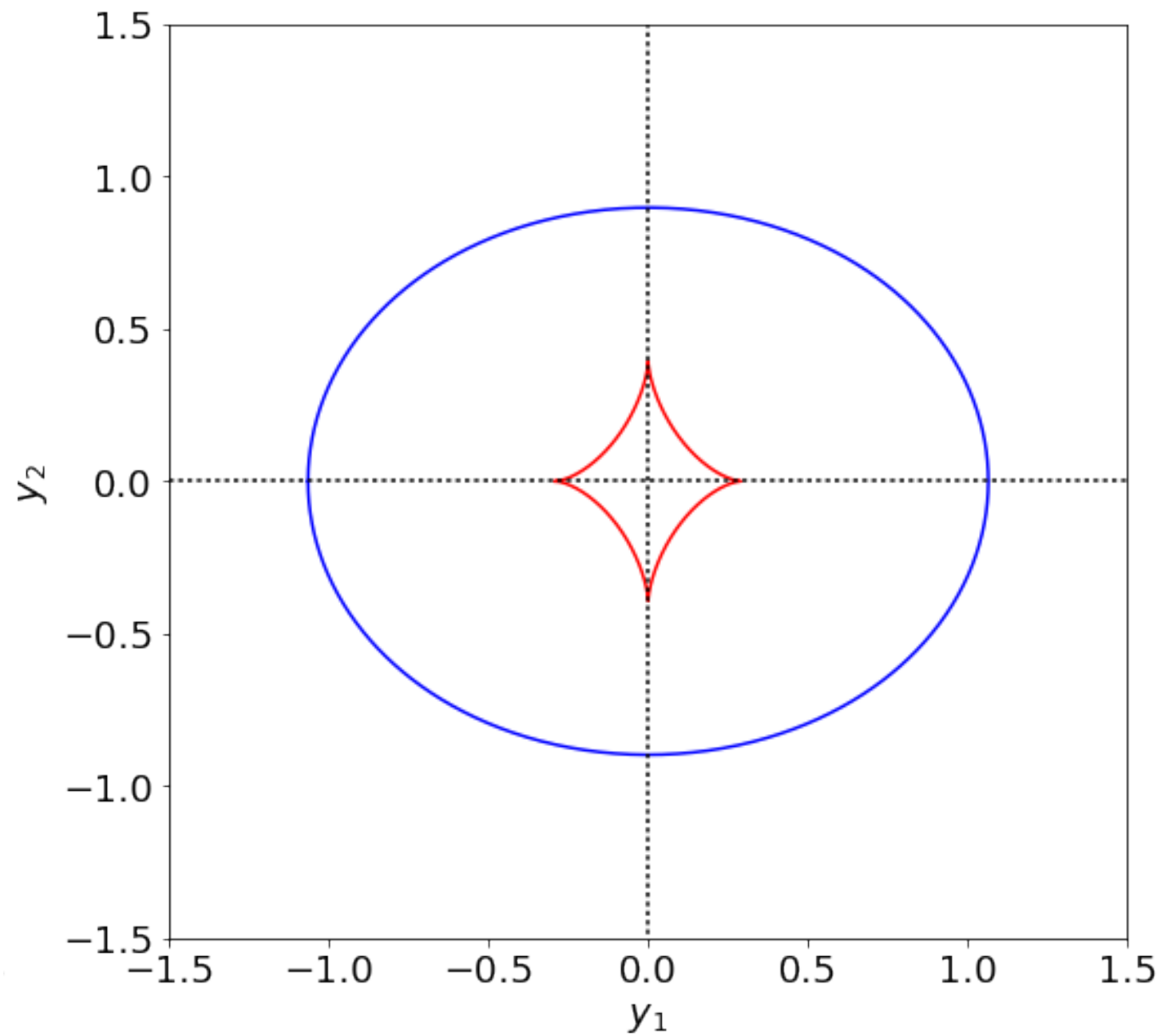
# CRITICAL LINE, CUT, CAUSTIC

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# CRITICAL LINE, CUT, CAUSTIC

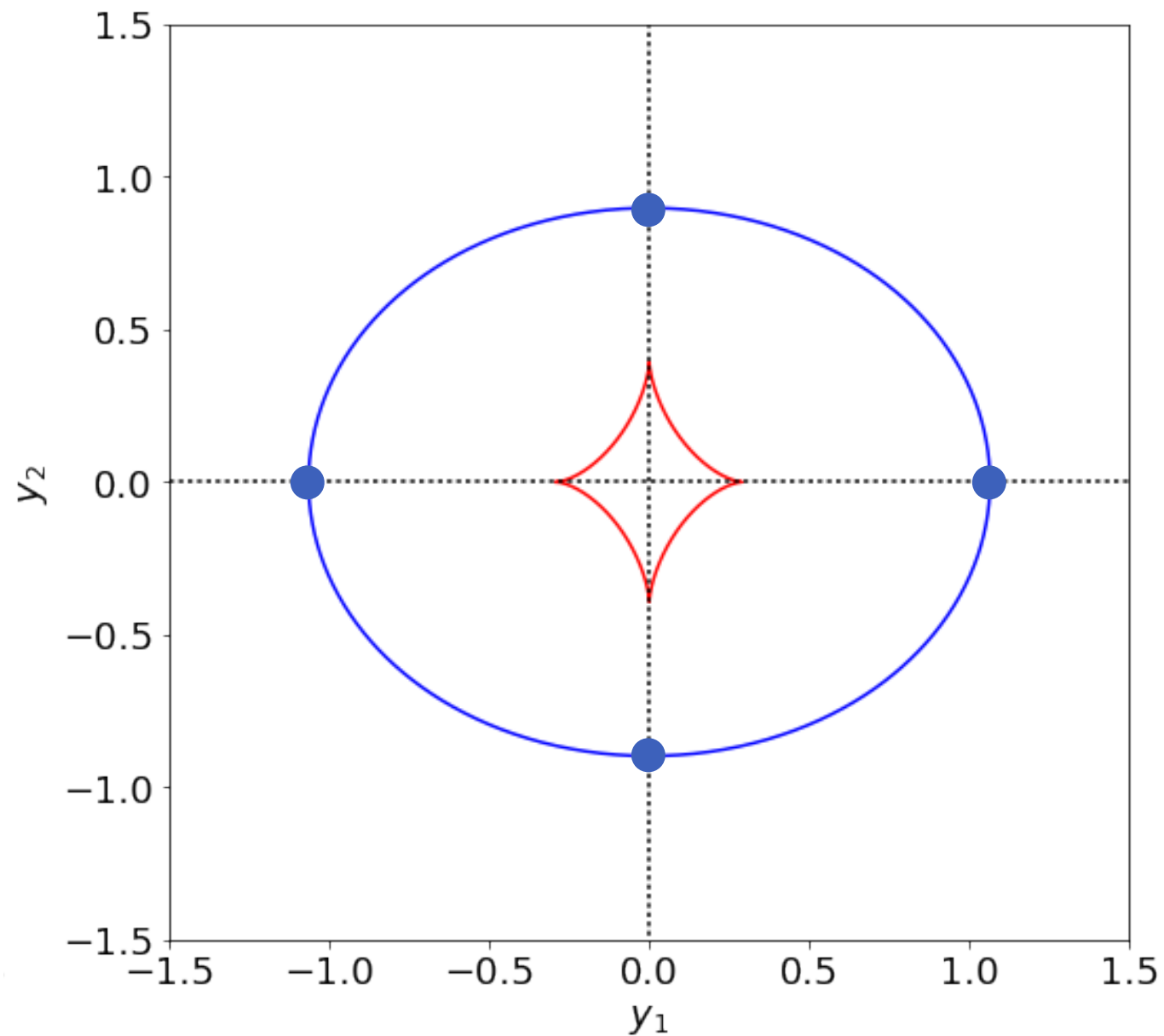
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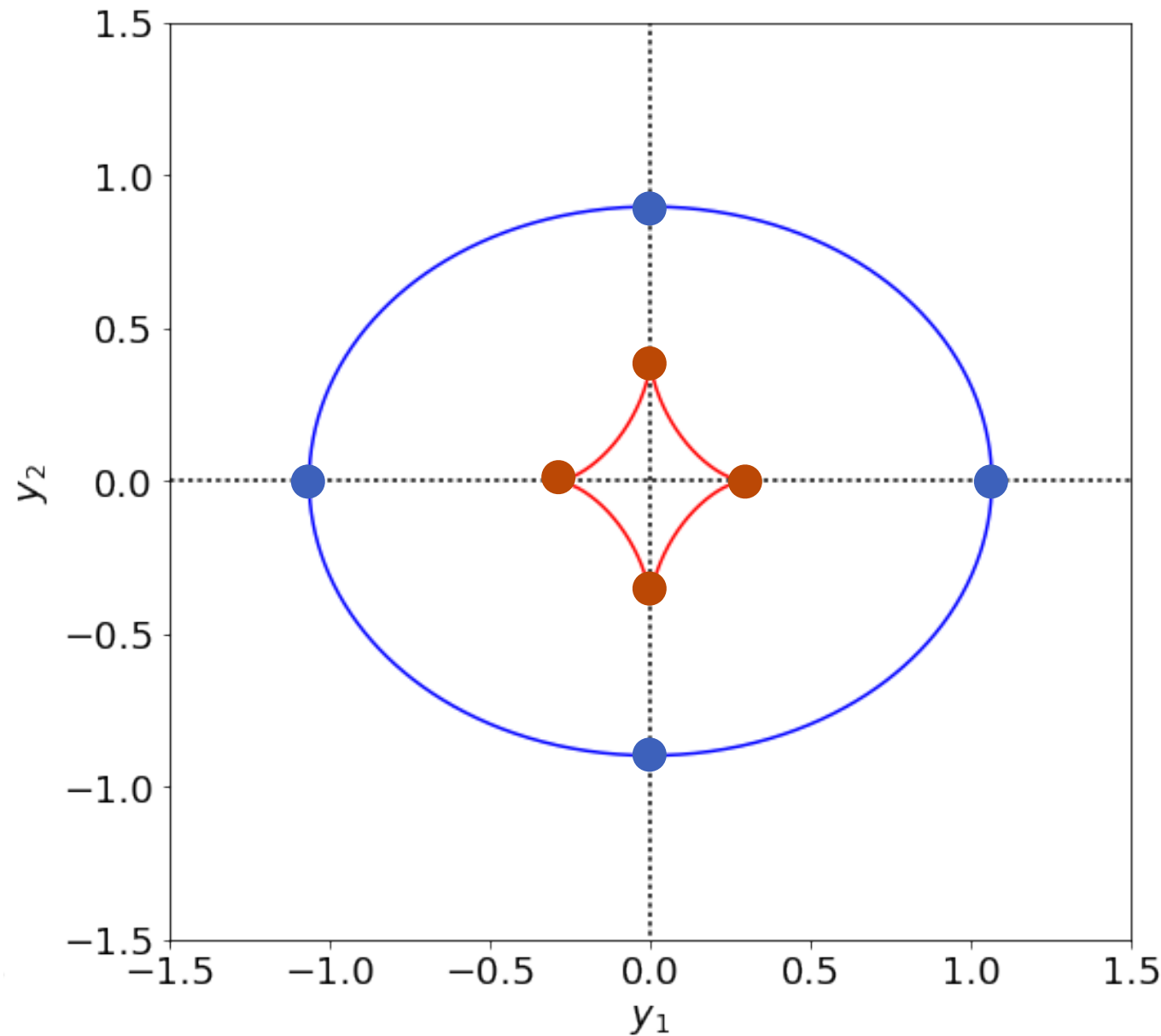
# CRITICAL LINE, CUT, CAUSTIC

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$$s_{1,\pm,c} = [y_{c,1}(\varphi = 0, \pi), 0] ,$$
$$s_{2,\pm,c} = [0, y_{c,2}(\varphi = \pi/2, -\pi/2)]$$

# CRITICAL LINE, CUT, CAUSTIC



$$s_{1,\pm,c} = [y_{c,1}(\varphi = 0, \pi), 0] ,$$

$$s_{2,\pm,c} = [0, y_{c,2}(\varphi = \pi/2, -\pi/2)]$$

$$s_{1,\pm,t} = [y_{t,1}(\varphi = 0, \pi), 0] ,$$

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# CRITICAL LINE, CUT, CAUSTIC

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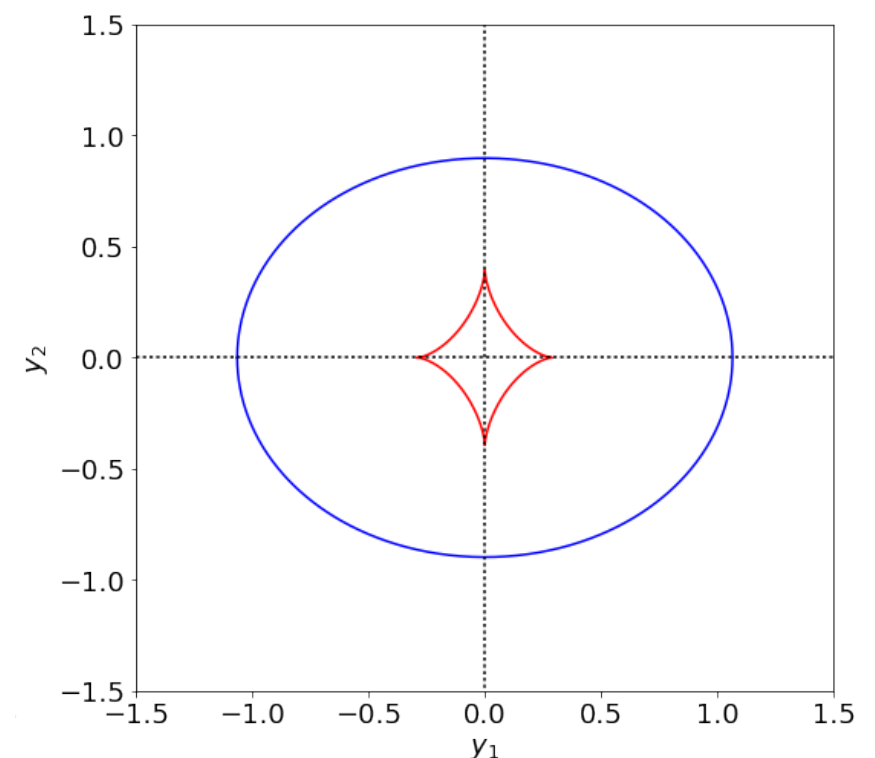
$$\begin{aligned} y_{c,1} &= -\frac{\sqrt{f}}{f'} \operatorname{arcsinh} \left( \frac{f'}{f} \cos \varphi \right) \\ y_{c,2} &= -\frac{\sqrt{f}}{f'} \arcsin(f' \sin \varphi) . \end{aligned}$$

$$\begin{aligned} y_{t,1} &= \frac{\sqrt{f}}{\Delta(\varphi)} \cos \varphi - \frac{\sqrt{f}}{f'} \operatorname{arcsinh} \left( \frac{f'}{f} \cos \varphi \right) \\ y_{t,2} &= \frac{\sqrt{f}}{\Delta(\varphi)} \sin \varphi - \frac{\sqrt{f}}{f'} \arcsin(f' \sin \varphi) . \end{aligned}$$

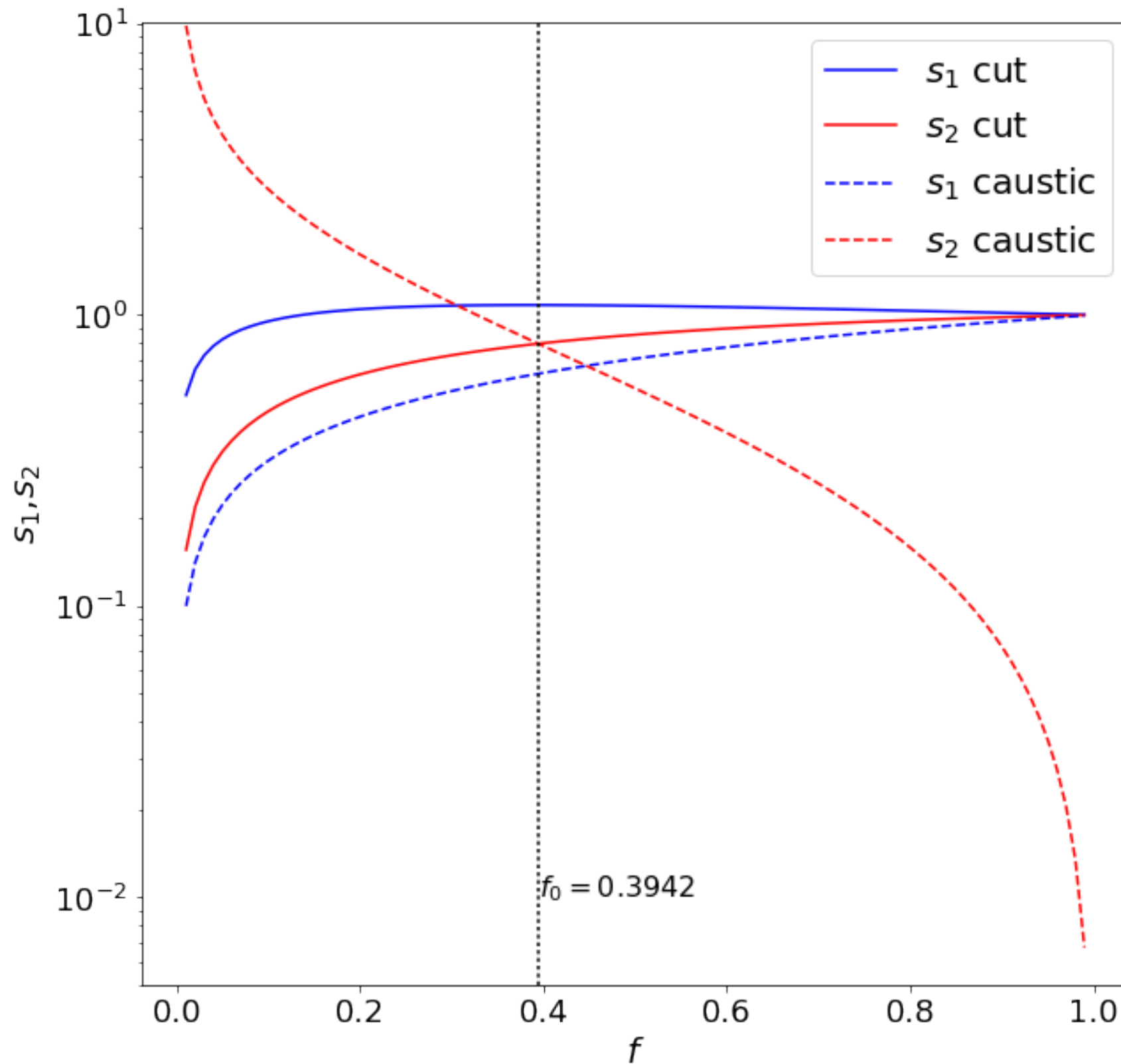
*We can easily see that*

$$s_{1,c} > s_{1,t}$$

*independent on  $f$ .*

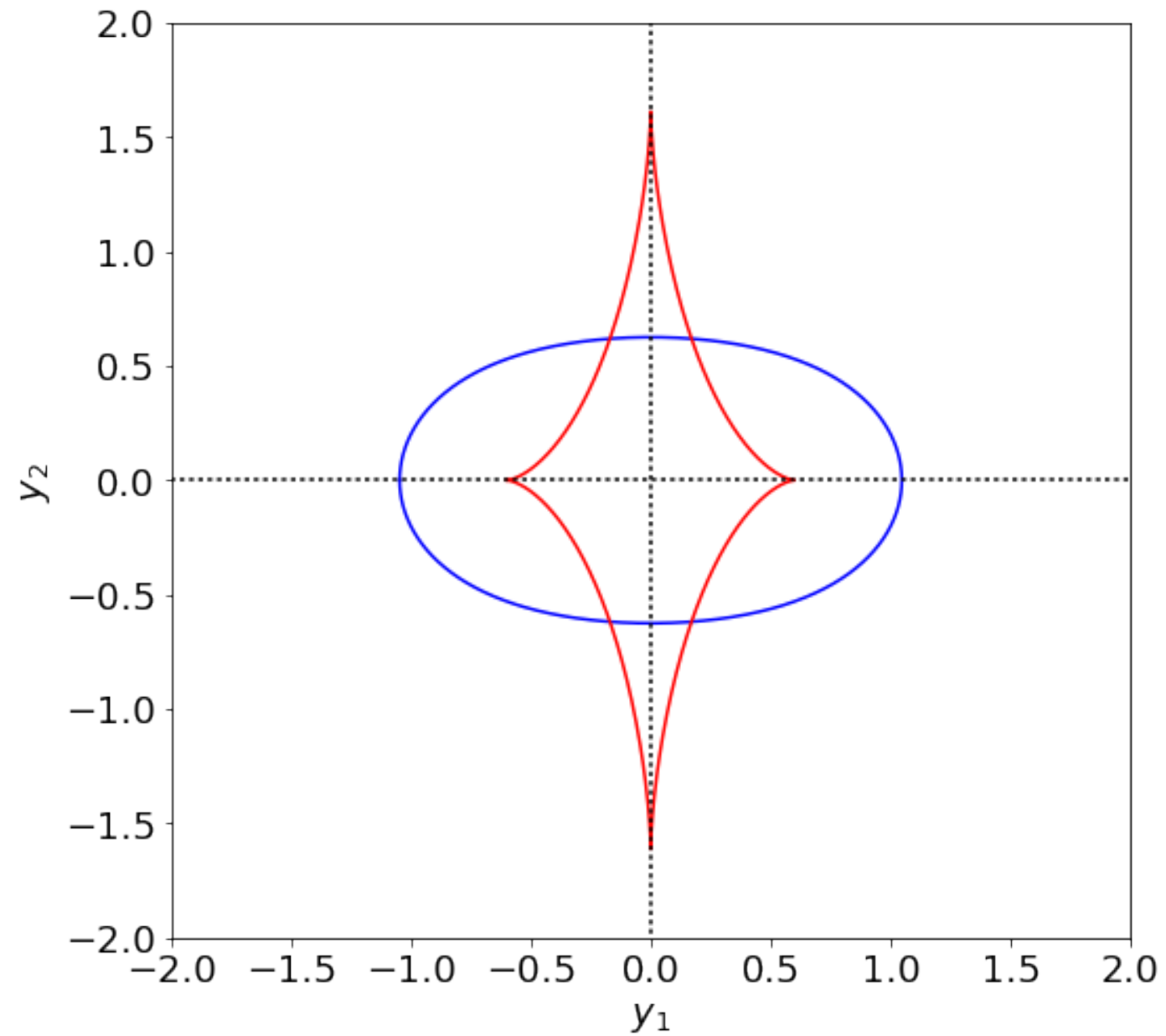
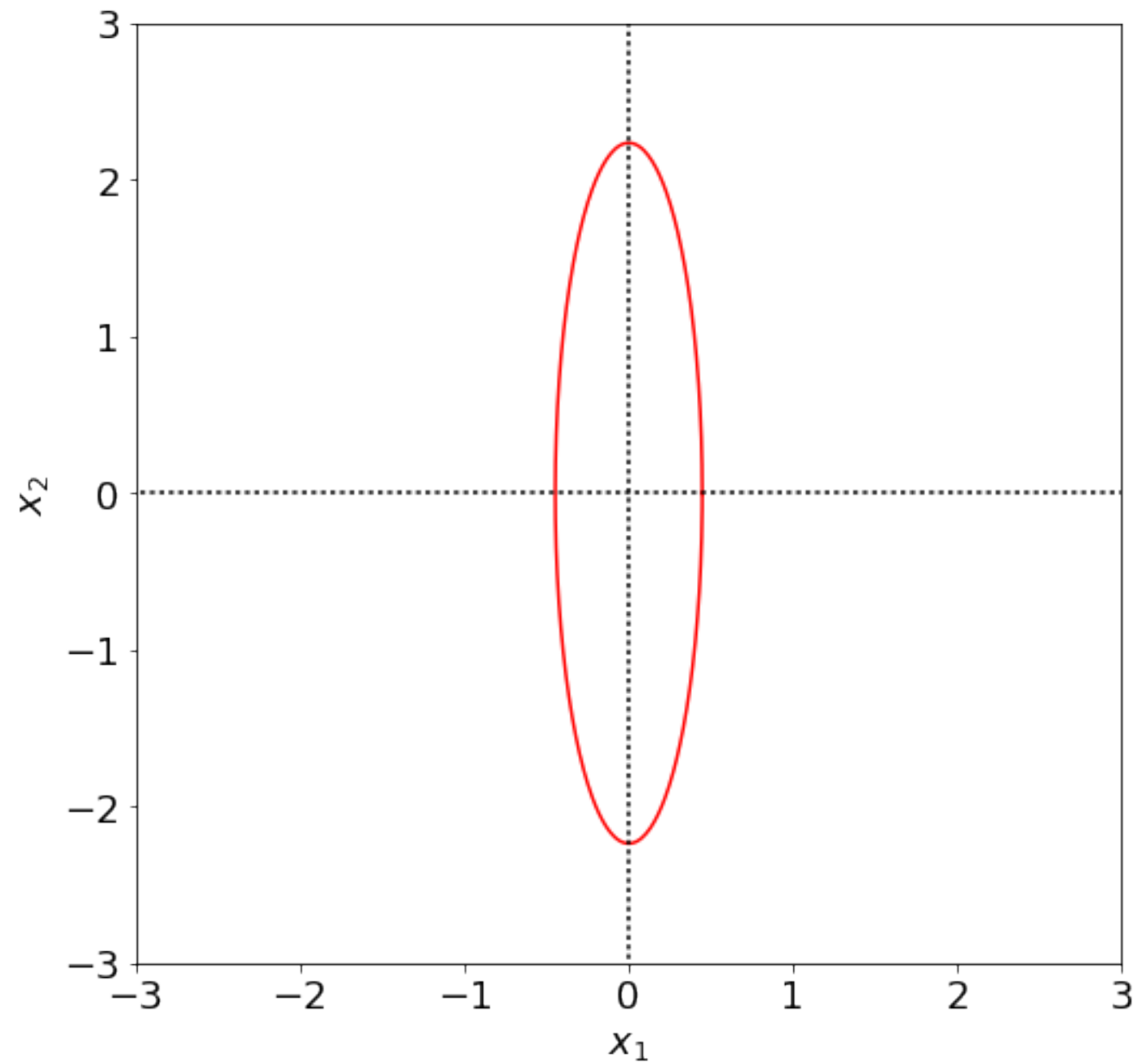


# CRITICAL LINE, CUT, CAUSTIC



# CRITICAL LINE, CUT, CAUSTIC

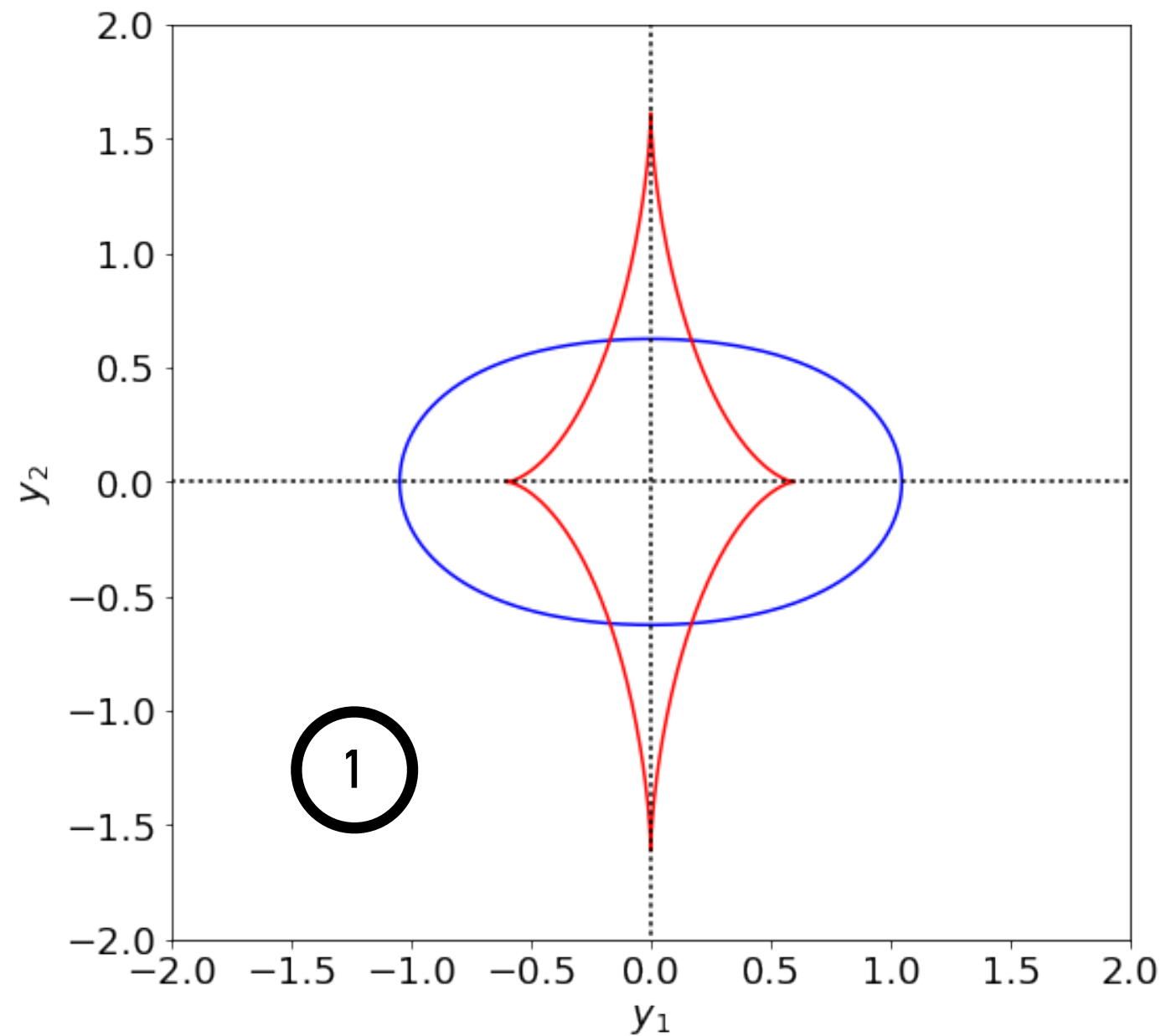
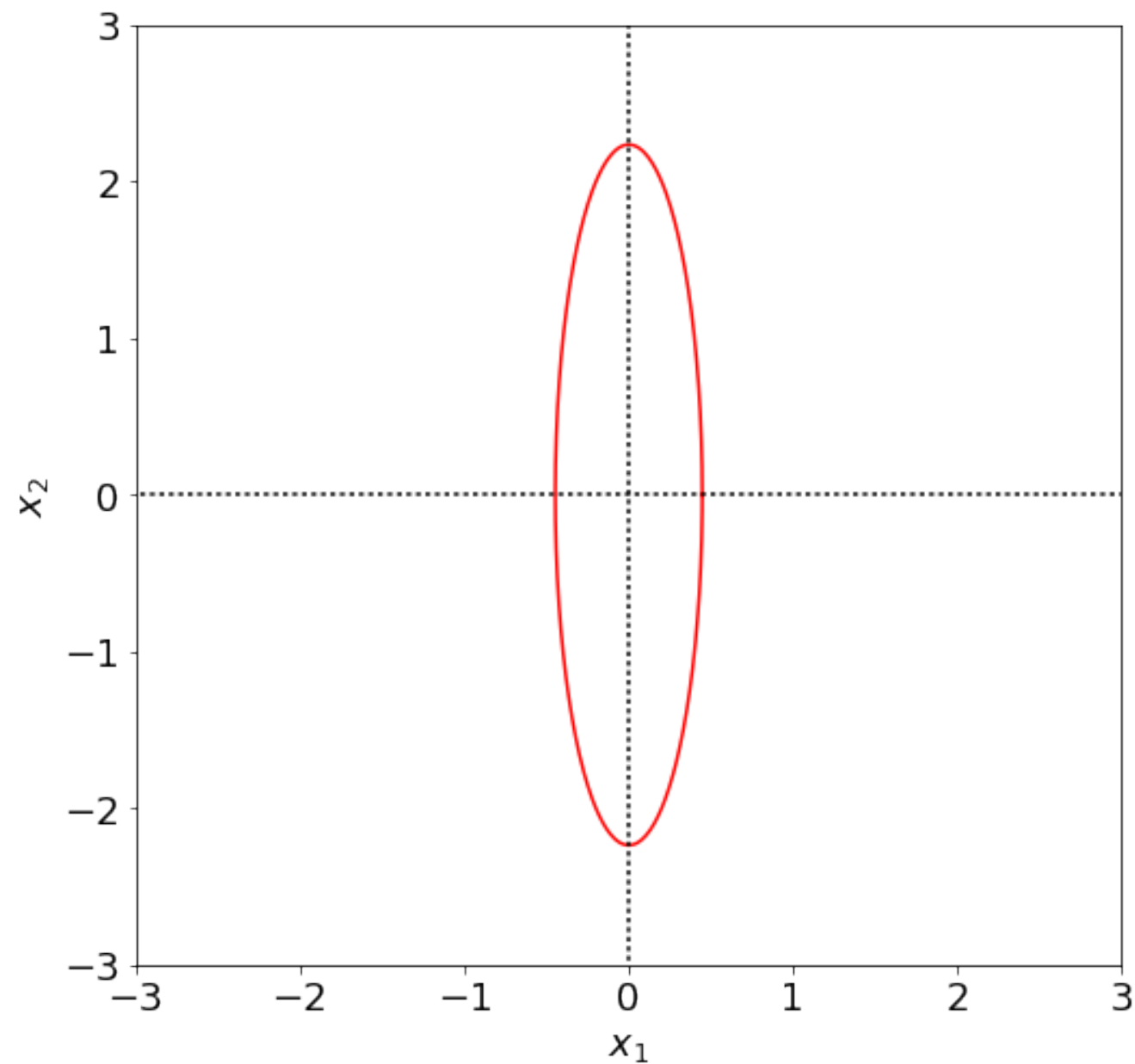
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*This is important for the image multiplicity...*

# CRITICAL LINE, CUT, CAUSTIC

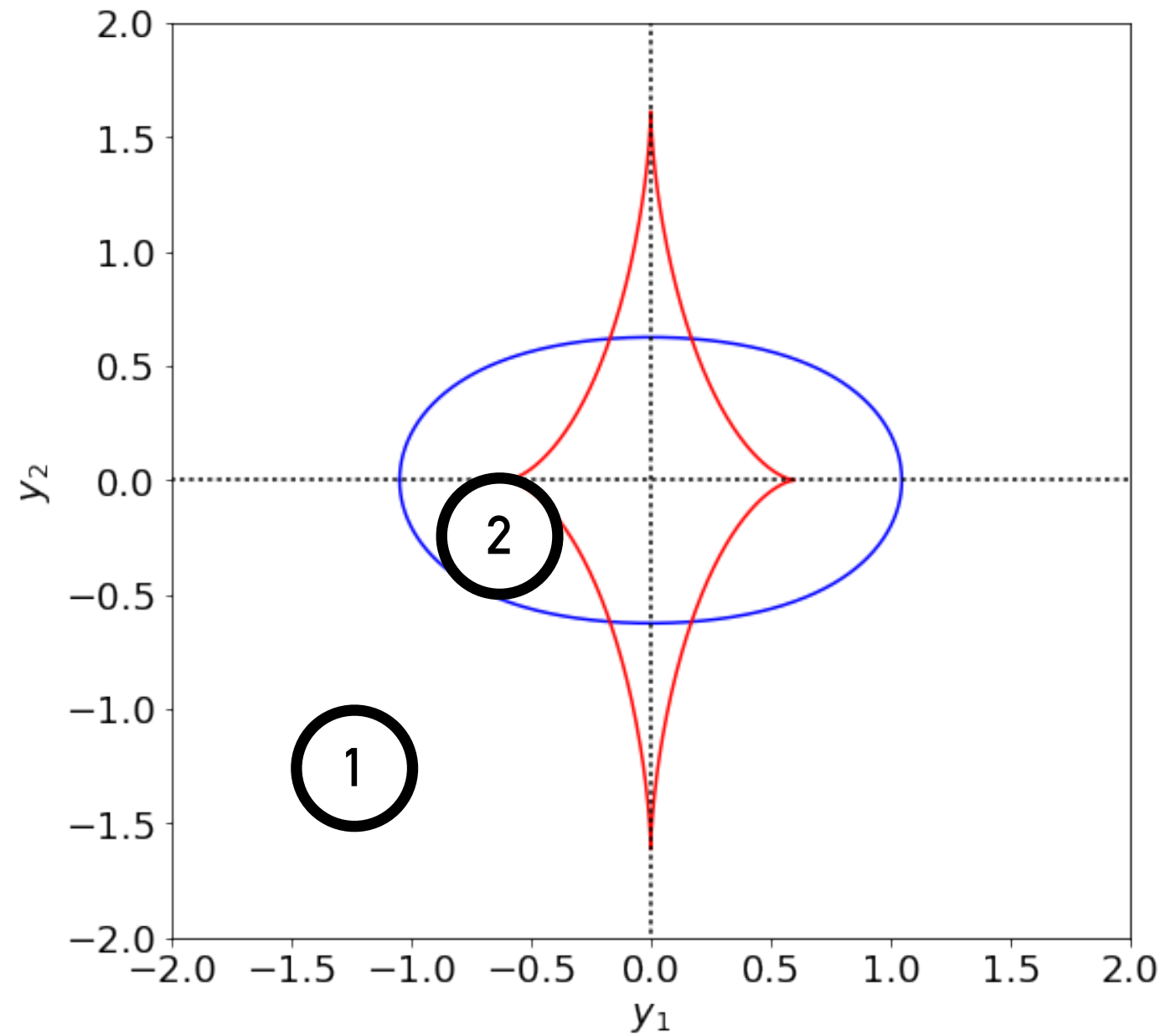
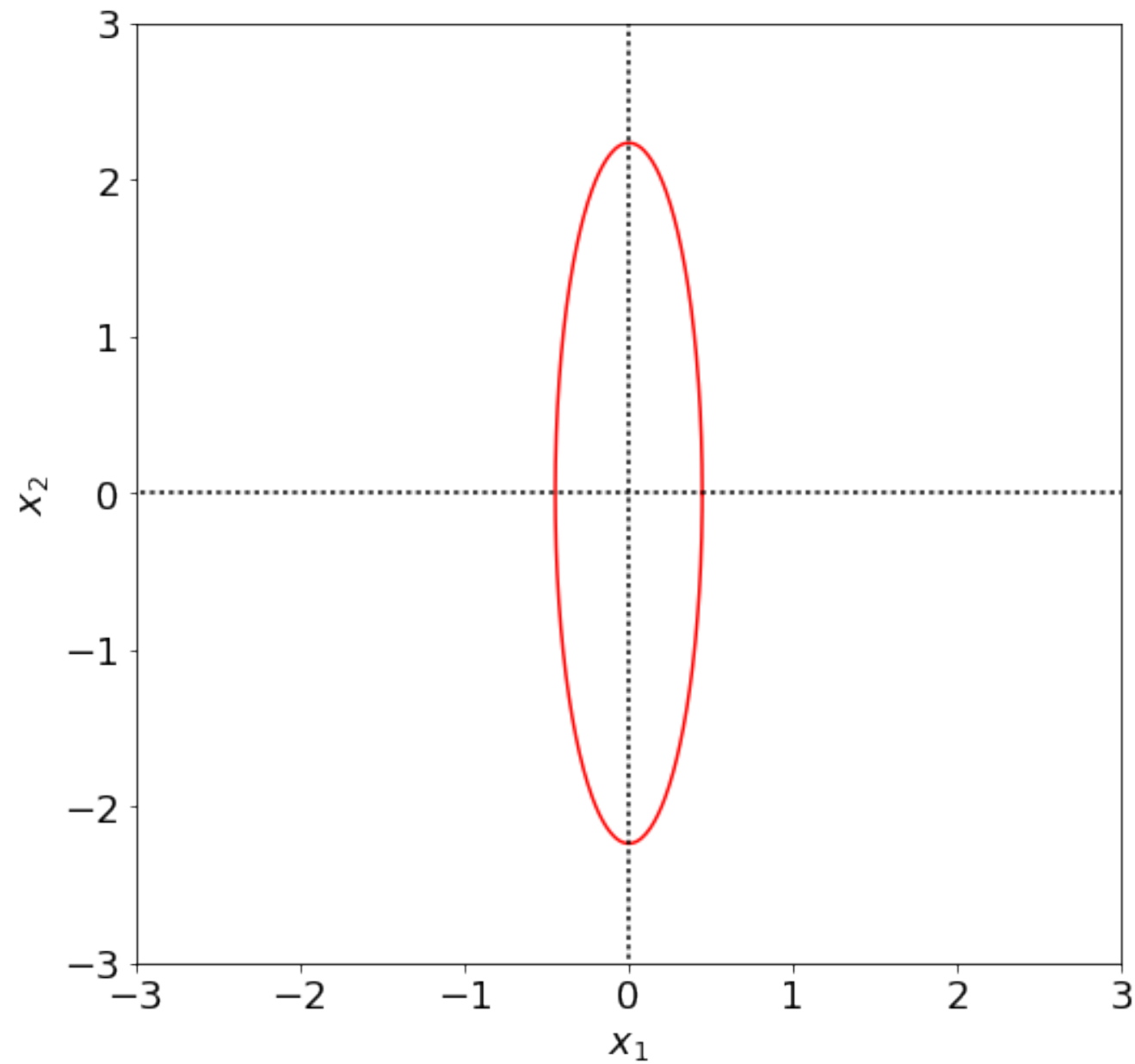
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*This is important for the image multiplicity...*

# CRITICAL LINE, CUT, CAUSTIC

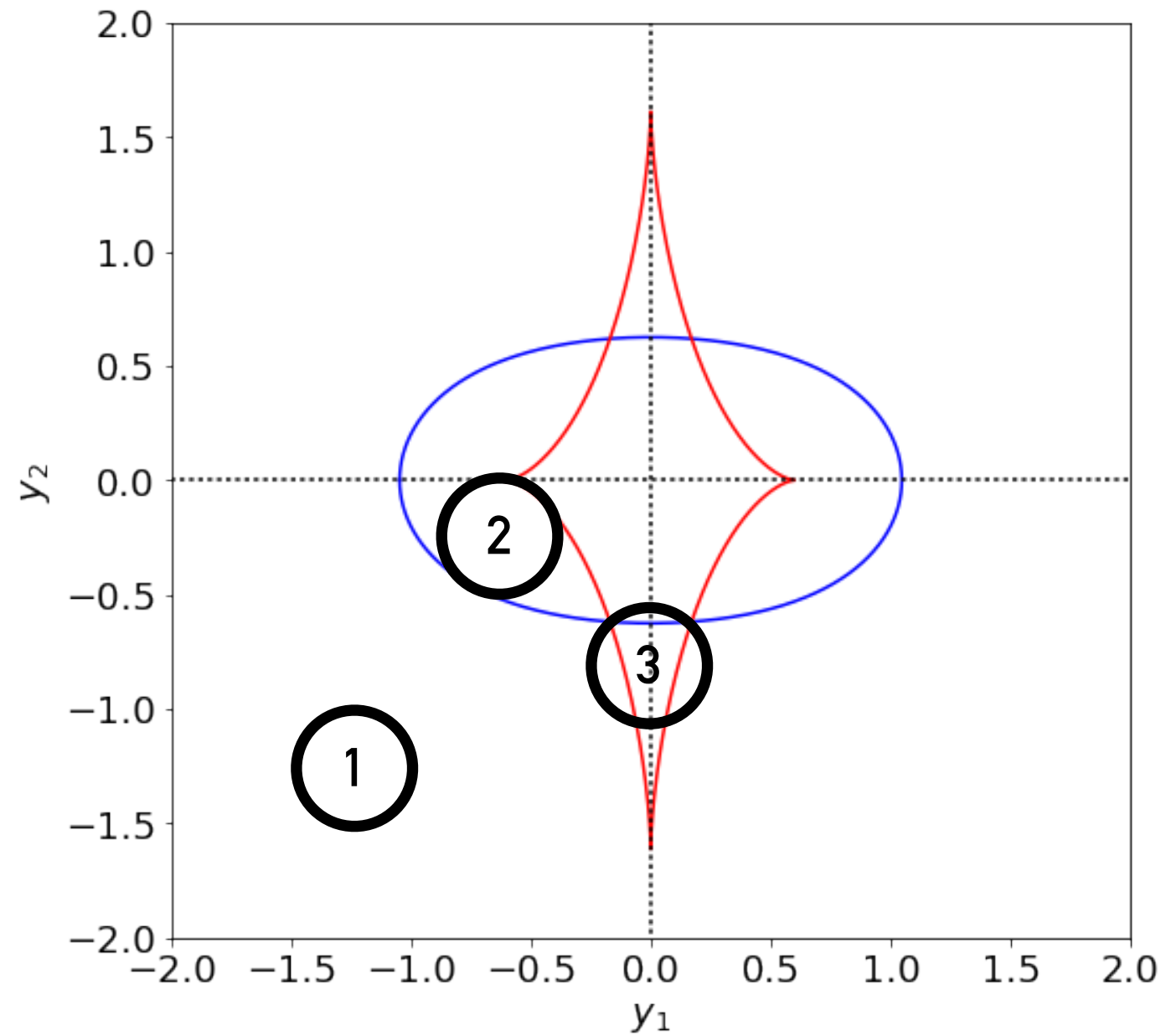
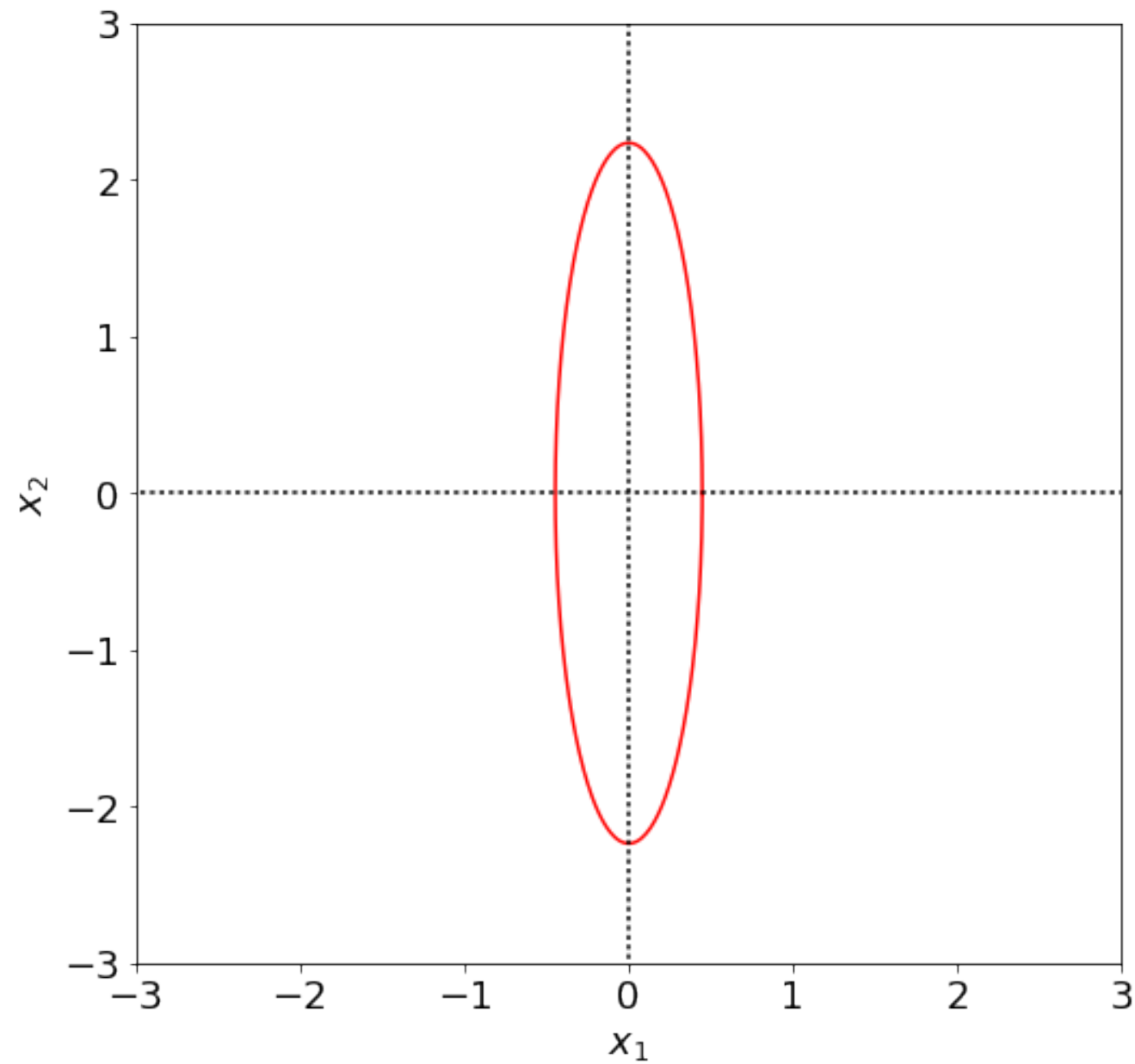
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*This is important for the image multiplicity...*

# CRITICAL LINE, CUT, CAUSTIC

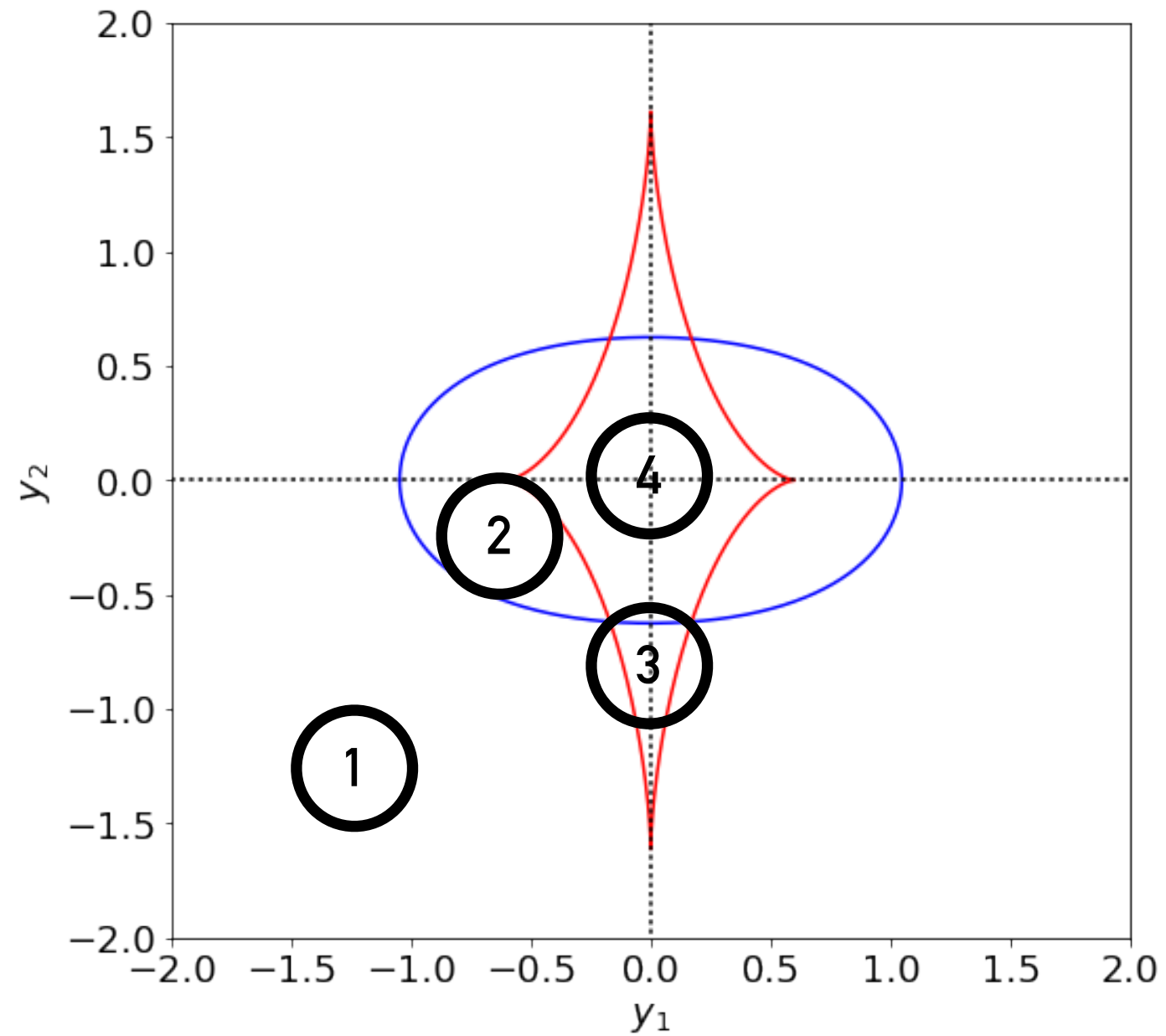
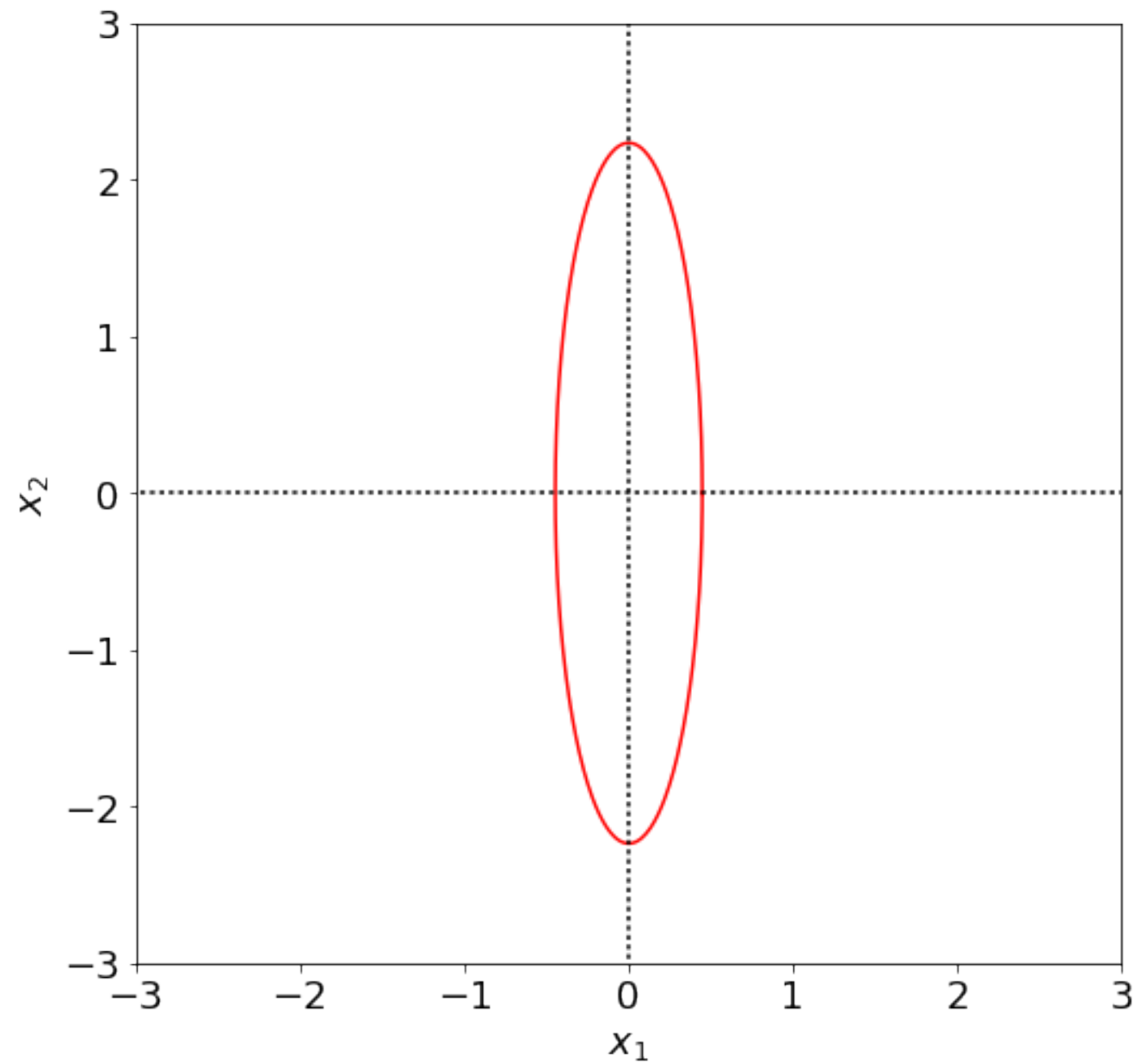
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*This is important for the image multiplicity...*



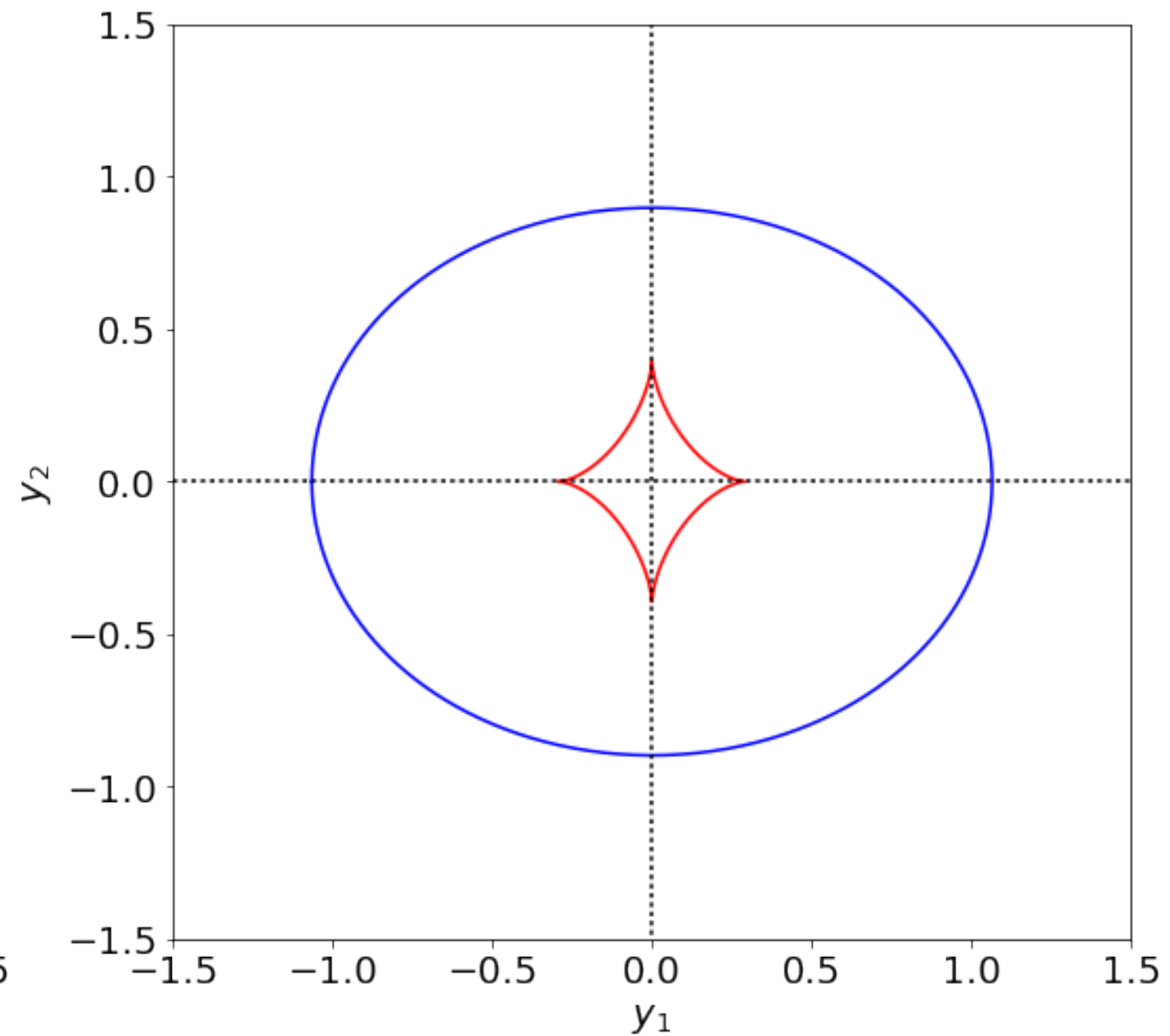
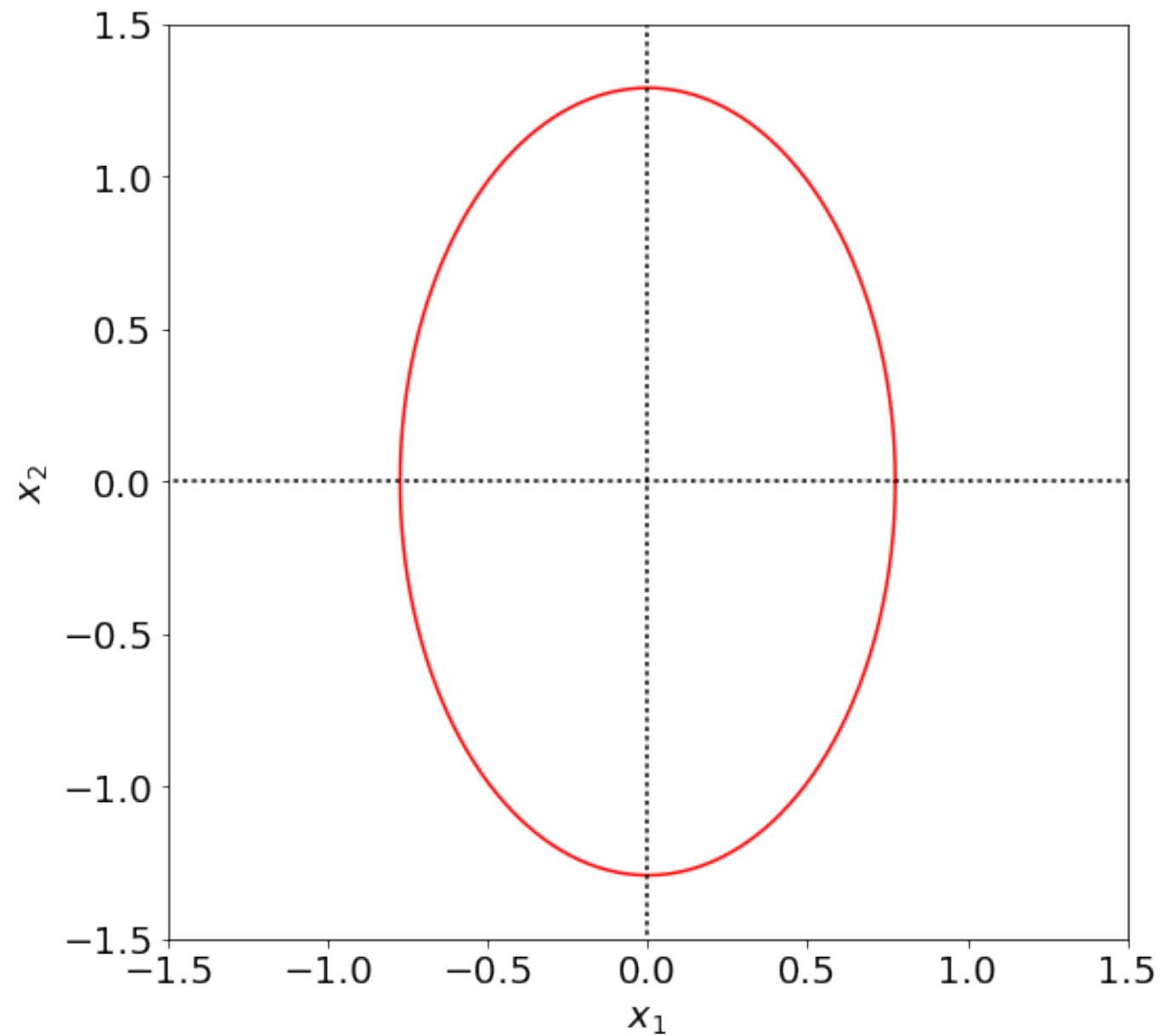
# CRITICAL LINE, CUT, CAUSTIC



*This is important for the image multiplicity...*

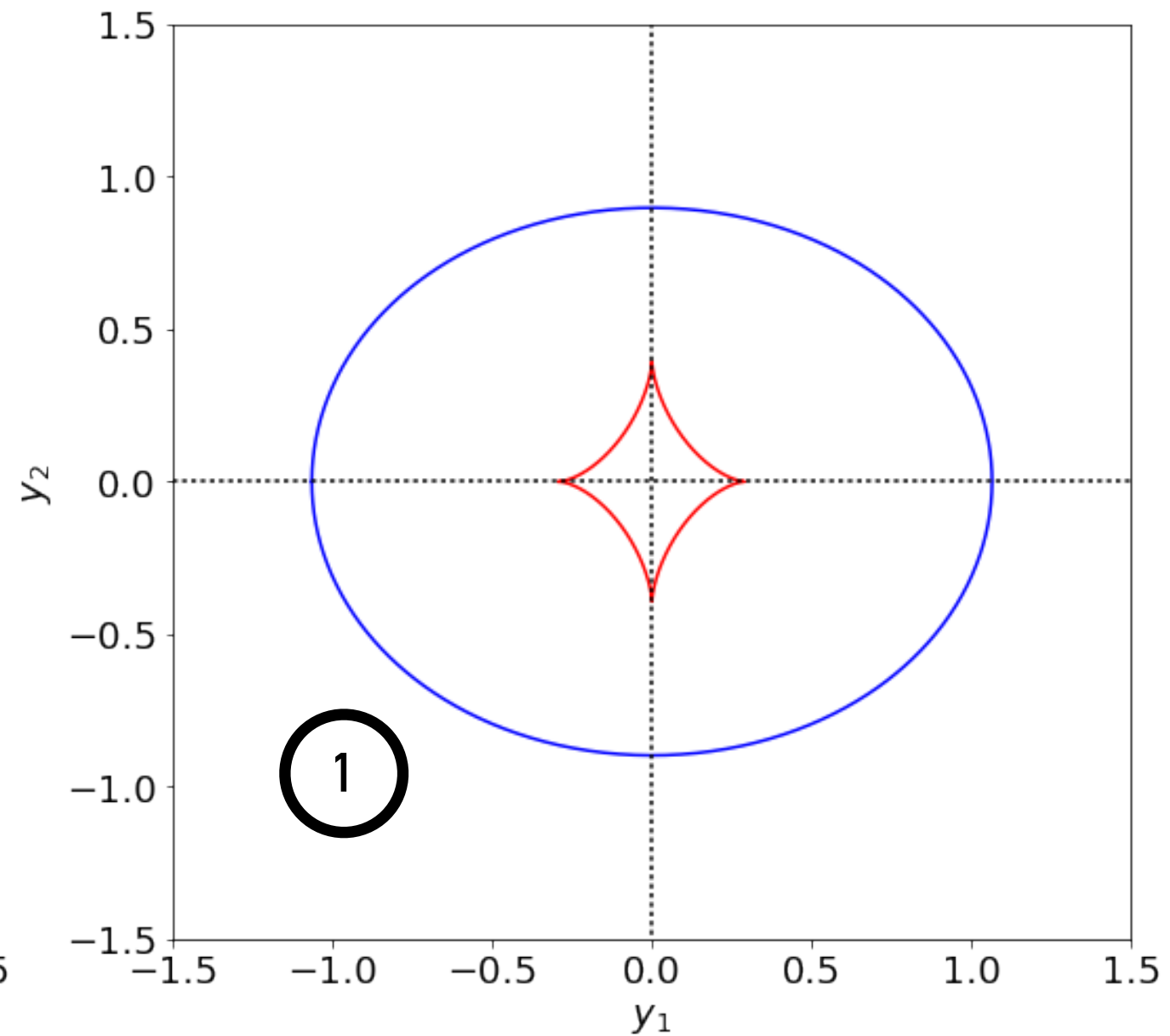
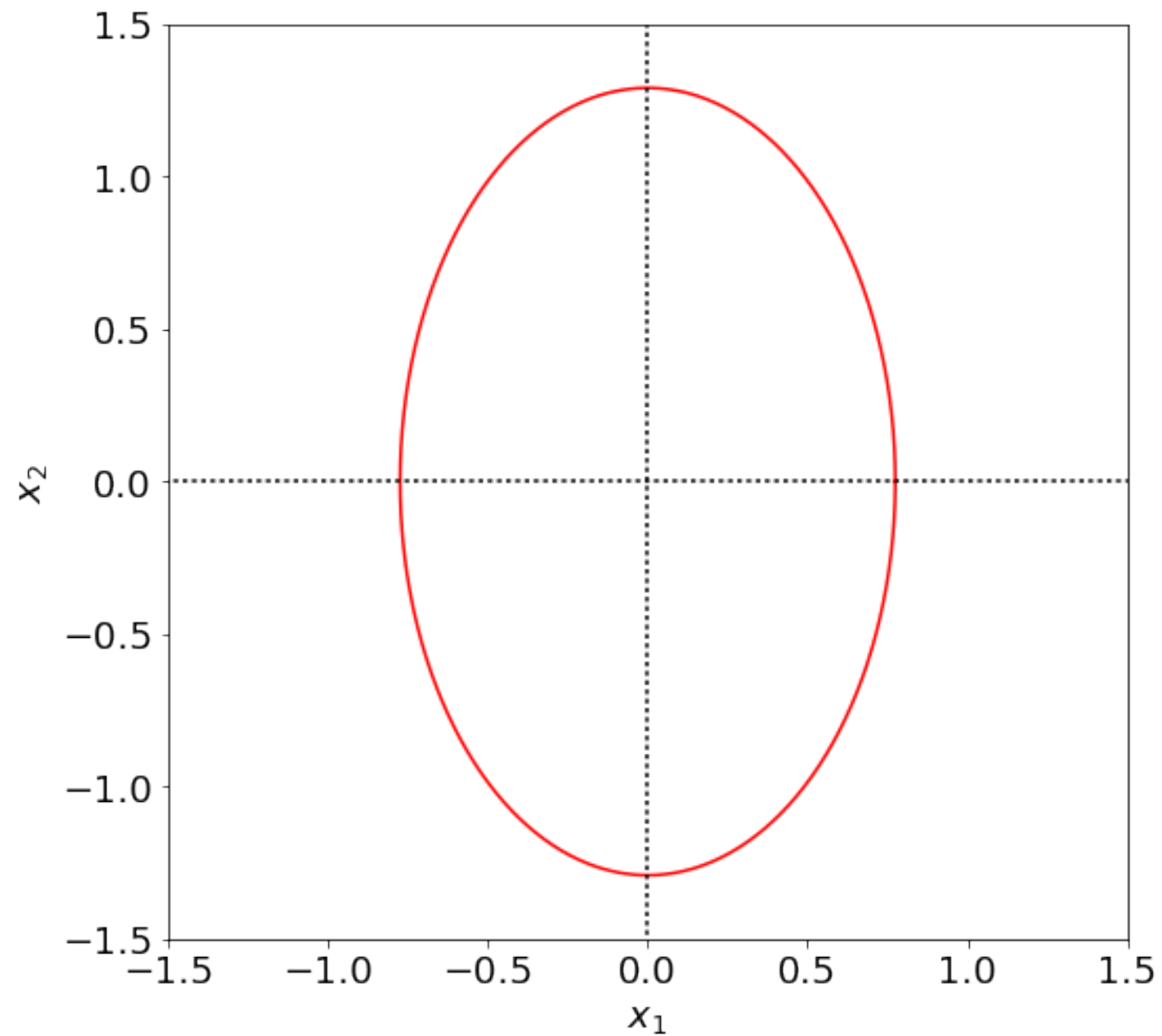
# CRITICAL LINE, CUT, CAUSTIC

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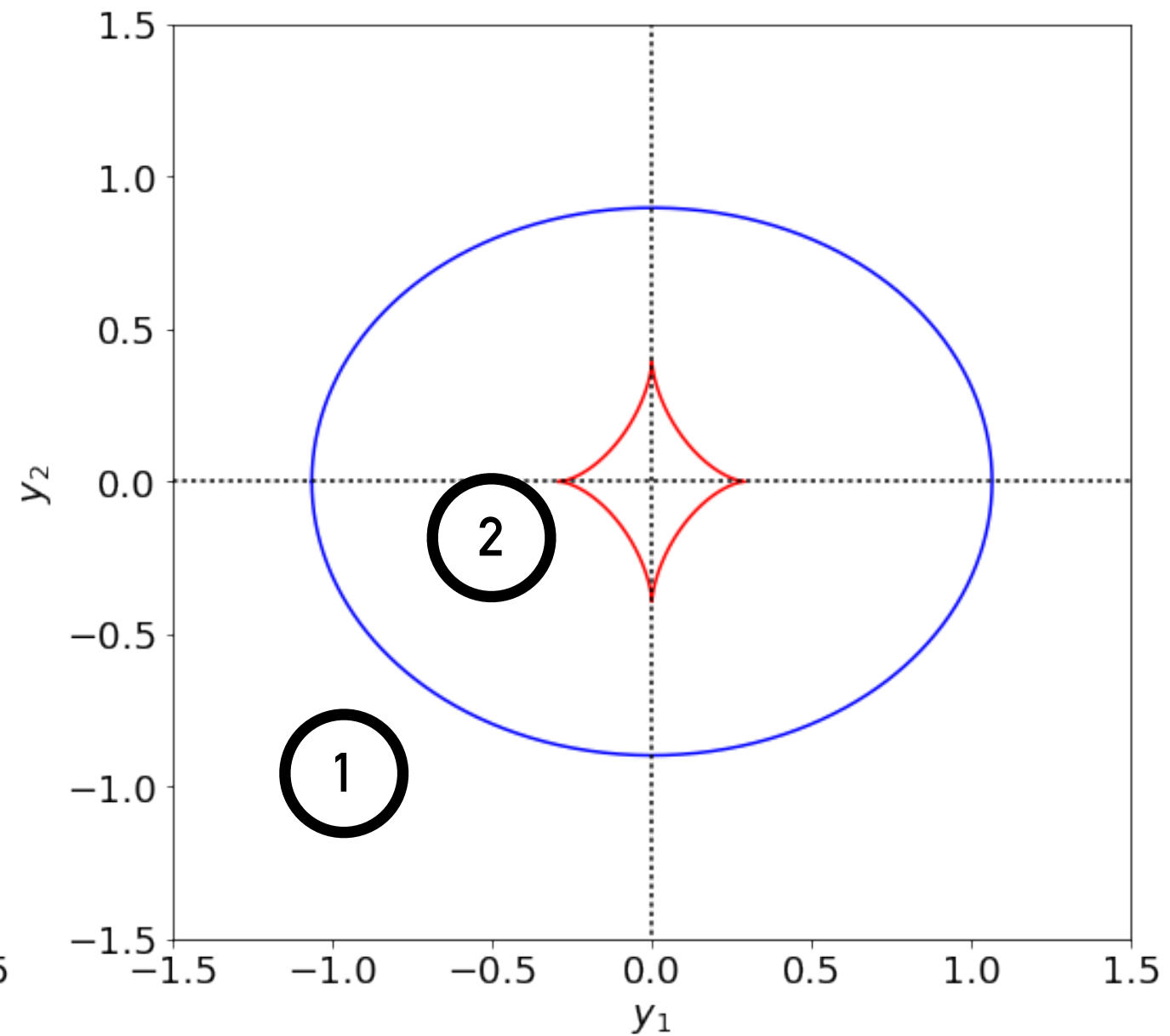
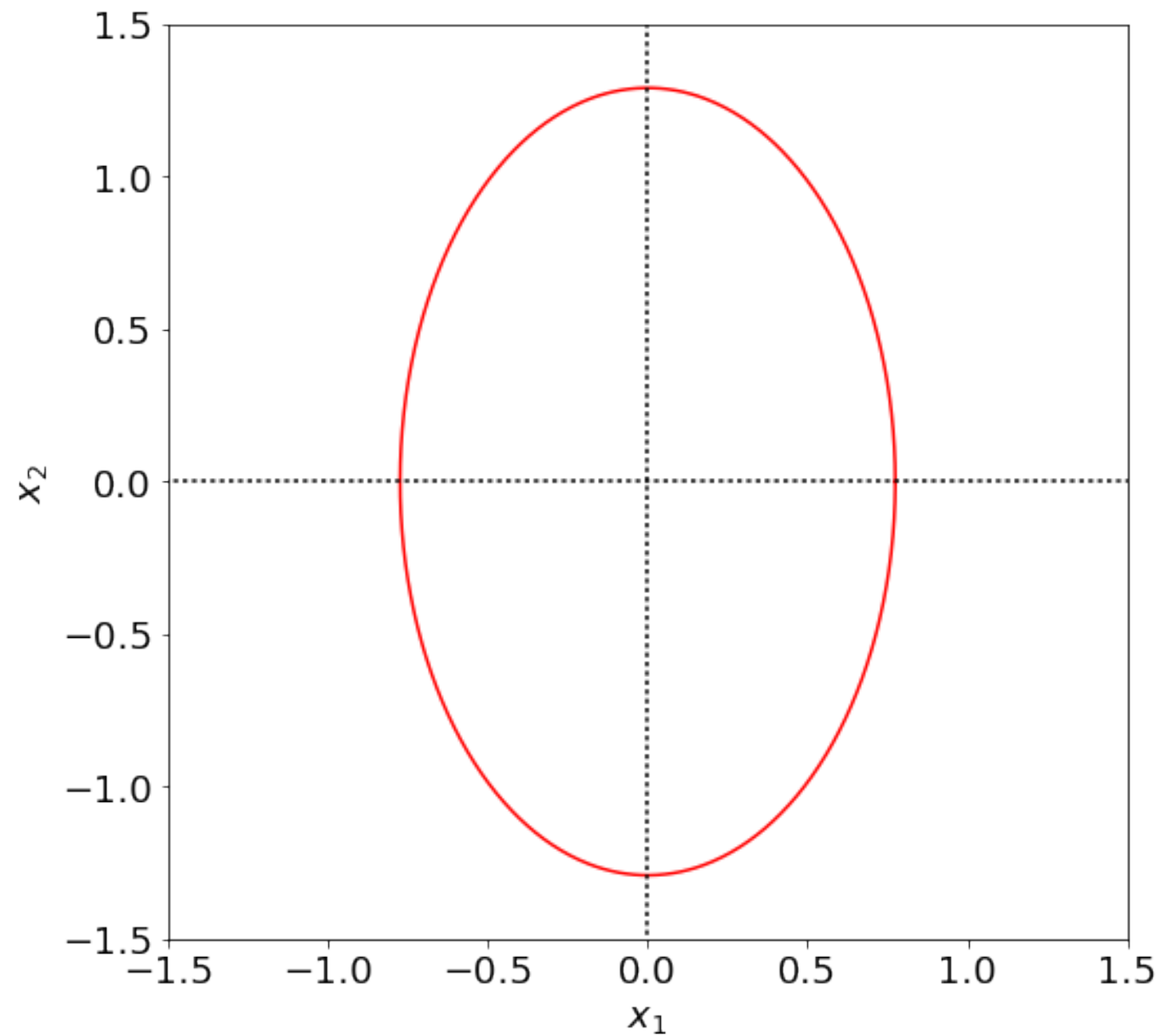
# CRITICAL LINE, CUT, CAUSTIC

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# CRITICAL LINE, CUT, CAUSTIC

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# CRITICAL LINE, CUT, CAUSTIC

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