

NUCLIDE ground state

Nuclide	Symbol	Z	N	A	Z range	N range	A range
		28	40				

Z N A Z N A
even odd

More fields : Q-values, separation energies, atomic masses, radius

LEVELS

Energy keV Decays B.R. % Only Ground State and Metastables
 Half Life fs T_{1/2} y Stable
 More fields : nuclear moments

Isospin J weak order π any

GAMMA transitions

Energy keV Final level keV J order π any
 More fields : conversion coefficients, multipolarity, mixing ratio

DECAY radiation emitted by the daughter

Type any α β- β+ γ e
 delayed n p α

Energy keV only 2 most intense lines
Intensity % Max En. keV log FT

Order by : Z, A

Z A N Q(β) Q(α) Q(EC) Q(β- n) Sn Sp R AM E T_{1/2} BR μ Q Erad Irrad
 Log ft HF Eγ α B(E) B(M) δ

PLOTTING

X axis: None Y axis: None

email: nds.contact-point@iaea.org

Reset Search Plot Show Chart Guide

You requested: 28 ≤ Z ≤ 40 Radiation type β+. Click on a column header to open the guide. Uncertainty for numeric values refers to the last digits of the value: 12.1 23 means 12.1 ± 2.3.

1678 rows retrieved

Comments Click on a nuclide symbol to show the decay schema

Electron Capture and Beta+ [CSV](#) [Data API](#)

#	$\frac{\Delta E_{\beta^+}}{[keV]}$	$I_{\beta^+}(\text{abs})$ [%]	E_{ec} [keV]	$I_{\text{ec}}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	$\log ft$	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
1			(13279)		170+X					⁵⁰ Ni ₂₂	18.5 ms 12	0	0+	ec β+ 100 %	14129 516	⁵⁰ Co ₂₃
2	3585 34	14 5	(8614)	0.015 5	4835 47	(0)+	3.42 16	super allowed		⁵⁰ Ni ₂₂	18.5 ms 12	0	0+	ec β+ 100 %	14129 516	⁵⁰ Co ₂₃
3			(7589)		2931 30	0+		super allowed		⁵² Ni ₂₄	40.8 ms 2	0	0+	ec β+ 100 %	11784 83	⁵² Co ₂₅
4			(13280)		0	(7/2-)		allowed		⁵³ Ni ₂₅	55.2 ms 7	0.0	(7/2-)	ec β+ 100 %	13029 25	⁵³ Co ₂₆
5	3697 89	45.0	(8890)	0.0 0	4390 ≈	(7/2-)	3.4	allowed		⁵³ Ni ₂₅	55.2 ms 7	0.0	(7/2-)	ec β+ 100 %	13029 25	⁵³ Co ₂₆
6	1144 24	0.020 10	(3588)	0.0005 3	5202.4 5	1+	4.88 22	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₆
7	1324 24	0.120 10	(3967)	0.00213 21	4822.8 7	1+	4.37 5	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
8	1457 24	0.15 5	(4246)	0.0020 7	4543.8 4	1+	4.46 15	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
9	1562 24	0.11 10	(4467)	0.0012 12	4323.0 7	1+	4.7 4	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
10	1577 24	0.21 3	(4497)	0.0023 4	4293.4 10	1+	4.46 7	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
11	1771 25	0.37 4	(4900)	0.0029 4	3889.6 2	1+	4.43 6	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
12	2019 25	0.37 3	(5414)	0.00199 18	3376.1 2	1+	4.67 5	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
13	2482 25	0.16 3	(6365)	0.00048 10	2424.6 3	1+	5.43 9	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
14	3211 25	19.8 12	(7853)	0.0288 19	936.7 1	1+	3.84 3	allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
15	3673 25	79.1 12	(8790)	0.0785 21	0.0	0+	3.501 15	super allowed		⁵⁴ Ni ₂₆	114.2 ms 3	0.0	0+	ec β+ 100 %	8732 5	⁵⁴ Co ₂₇
16	3624 6	≈ 100	(8692)	≈ 0.103	0.0	7/2-	≈ 3.6	allowed		⁵⁵ Ni ₂₇	203.7 ms 20	0.0	7/2-	ec β+ 100 %	8694.0 8	⁵⁵ Co ₂₈
17			(416)	100 0	1720.19 5	1+	4.4	allowed		⁵⁶ Ni ₂₈	6.075 d 10	0.0	0+	ec β+ 100 %	2132.9 6	⁵⁶ Co ₂₉
18			(685)	< 0.50	1450.69 5	0+	> 7.1	super allowed		⁵⁶ Ni ₂₈	6.075 d 10	0.0	0+	ec β+ 100 %	2132.9 6	⁵⁶ Co ₂₉
19	65 5	< 1.2E-3	(1166)	< 0.77	970.24 4	2+	> 7.4	2 nd non-unique		⁵⁶ Ni ₂₈	6.075 d 10	0.0	0+	ec β+ 100 %	2132.9 6	⁵⁶ Co ₂₉
20	408 5	< 5.8E-5	(1978)	< 4.8E-4	158.38 3	3+	> 11.4	2 nd unique		⁵⁶ Ni ₂₈	6.075 d 10	0.0	0+	ec β+ 100 %	2132.9 6	⁵⁶ Co ₂₉
21	478 5	< 6.0E-5	(2136)	< 2.2E-5	0.0	4+	> 12.5	4 th non-unique		⁵⁶ Ni ₂₈	6.075 d 10	0.0	0+	ec β+ 100 %	2132.9 6	⁵⁶ Co ₂₉
22			(87)	0.0208 11	3177.41 4	5/2-,7/2-	6.06 4			⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
23			(156)	0.060 3	3108.12 7	(3/2)-	6.13 3	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
24			(460)	0.291 8	2804.27 4	(3/2-,5/2)	6.41 1			⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
25			(533)	0.0199 7	2730.91 4	3/2-,5/2	7.70 2			⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
26			(1131)	0.0340 19	2133.08 5	5/2-	8.13 2	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
27	139.0 11	0.444 20	(1345)	11.9 4	1919.55 5	5/2-	5.74 2	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
28	206.5 11	0.80 4	(1507)	4.86 18	1757.58 3	3/2-	6.22 2	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
29	313.7 11	7.04 22	1734 15	10.0 3	1504.81 4	1/2-	6.05 1	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀
30	368.7 11	35.3 13	1871 10	29.2 11	1377.65 5	3/2-	5.64 2	allowed		⁵⁷ Ni ₂₉	35.60 h 6	0.0	3/2-	ec β+ 100 %	3261.7 8	⁵⁷ Co ₃₀

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
68	2201.4 7	< 0.28	(5789.4)	< 0.0013	2776.1 3	2+	> 6.4	allowed		$^{58}\text{Cu}_{29}$	3.204 s 7	0.0	1+	ec $\beta+$ 100 %	8561.0 7	$^{58}\text{Ni}_{30}$
69	2846.6 7	1.4 4	(7111.0)	0.00033 9	1454.56 15	2+	6.20 13	allowed		$^{58}\text{Cu}_{29}$	3.204 s 7	0.0	1+	ec $\beta+$ 100 %	8561.0 7	$^{58}\text{Ni}_{30}$
70	3561.6 7	81.1 5	(8565.5)	0.101 1	0.0	0+	4.870 3	allowed		$^{58}\text{Cu}_{29}$	3.204 s 7	0.0	1+	ec $\beta+$ 100 %	8561.0 7	$^{58}\text{Ni}_{30}$
71	470.4 4	0.026 5	(2117.2)	0.012 2	2681.2 7	(5/2-)	6.0 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
72	589.22 19	0.201 12	(2383.5)	0.044 3	2414.85 13	3/2-	5.5 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
73	900.21 19	1.88 4	(3063.7)	0.117 3	1734.67 6	3/2-	5.3 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
74	925.72 19	1.61 3	(3118.7)	0.0920 18	1679.70 7	5/2-	5.4 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
75	1085.2 3	0.055 11	(3460.3)	0.0020 4	1338.1 5	7/2-	7.2 1	2 nd non-unique		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
76	1102.47 19	18.9 3	(3497.0)	0.654 12	1301.41 7	1/2-	4.7 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
77	1155.38 20	0.110 18	(3609.4)	0.00033 6	1188.93 13	5/2-	7.0 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
78	1302.36 20	8.6 4	(3920.4)	0.18 1	878.00 6	3/2-	5.3 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
79	1499.05 20	3.35 15	(4333.4)	0.0481 22	464.92 7	1/2-	6.0 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
80	1559.10 20	5.89 10	(4459.0)	0.0756 15	339.37 5	5/2-	5.8 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
81	1721.99 20	57.5 4	(4798.4)	0.557 7	0.0	3/2-	5.0 1	allowed		$^{59}\text{Cu}_{30}$	81.5 s 5	0.0	3/2-	ec $\beta+$ 100 %	4798.4 6	$^{59}\text{Ni}_{31}$
82		(1079.4)		0.022 8	5048.6 6	1,2	6.4 2			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
83		(2941.6)			3186.4 6 ?					$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
84	111.6 9	0.0014 6	(1278.9)	0.11 4	4849.1 6	1,2,3	5.8 2			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
85	113.6 11	0.00036 14	(1283.8)	0.026 10	4844.2 13	1,2	6.5 2			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
86	148.3 10	0.0013 5	(1367.2)	0.033 11	4760.8 5	1,2	6.4 1			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
87	224.2 10	0.0076 18	(1548.9)	0.040 10	4579.1 6	2+	6.4 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
88	237.0 9	0.071 12	(1579.1)	0.31 5	4548.9 4	1+,2+	5.6 1			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
89	242.4 10	0.012 3	(1591.9)	0.050 12	4536.1 8	2+	6.4 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
90	260.5 9	0.185 13	(1634.5)	0.58 4	4493.5 3	1+,2+	5.3 1			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
91	328.4 10	0.027 7	(1793.3)	0.037 9	4334.7 7	2	6.6 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
92	335.2 10	0.072 9	(1809.0)	0.095 12	4319.0 4	2+	6.2 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
93	440.0 10	1.17 8	(2049.4)	0.64 5	4078.63 23	1+,2+	5.5 1			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
94	465.6 10	0.96 9	(2107.5)	0.44 4	4020.49 23	1+	5.7 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
95	471.2 10	0.15 3	(2120.2)	0.064 13	4007.8 6	2+	6.5 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
96	507.6 10	0.22 5	(2202.0)	0.075 16	3926.0 4	2+,3+	6.5 1			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
97	531.5 11	0.069 23	(2255.8)	0.021 7	3872.2 9	1+,2+	7.0 2			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
98	592.5 10	0.80 8	(2392.0)	0.172 16	3736.0 4	2+	6.2 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
99	748.0 10	0.86 7	(2734.5)	0.092 7	3393.5 3	2+	6.6 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
100	804.9 10	4.59 22	(2858.5)	0.396 19	3269.48 18	2+	6.0 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
101	839.6 10	11.6 4	(2933.8)	0.88 3	3194.16 16	1+,2+	5.6 2			$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
102	872.0 10	49.0 23	(3003.8)	3.34 16	3124.16 16	2+	5.1 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
103	1104.2 10	2.8 3	(3501.7)	0.096 10	2626.25 16	3+	6.8 1	allowed		$^{60}\text{Cu}_{31}$	23.7 min 4	0.0	2+	ec $\beta+$ 100 %	6128.0 17	$^{60}\text{Ni}_{32}$
104	1324.9 10	15.0 12	(3969.0)	0.31 3	2158.95 13	2+</										

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
164	470 7	0.09 3	(2114)	0.047 14	3521.2 15	1/2-,3/2-,5/2-	5.5 2			$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
165	662 7	0.098 20	(2543)	0.017 4	3092.4 13	3/2-	6.1 1	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
166	695 7	0.23 3	(2616)	0.035 4	3019.3 11	3/2-	5.80 6	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
167	735 7	0.73 6	(2702)	0.094 8	2932.91 16	3/2-	5.39 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
168	769 7	0.48 6	(2778)	0.054 7	2857.1 3	1/2-,3/2-	5.66 6			$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
169	777 7	0.50 5	(2794)	0.055 5	2840.53 14	1/2-,3/2-	5.66 5			$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
170	799 7	1.58 14	(2842)	0.160 14	2792.98 13	5/2-	5.21 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
171	849 7	1.37 9	(2951)	0.116 8	2683.96 20	3/2-	5.38 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
172	947 8	1.29 8	(3162)	0.079 6	2472.50 13	3/2-	5.60 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
173	1000 8	1.29 9	(3277)	0.068 5	2358.13 11	3/2-	5.70 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
174	1126 8	0.58 6	(3546)	0.022 2	2088.86 9	(1/2)-	6.27 5	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
175	1200 8	0.79 11	(3702)	0.024 3	1932.60 8	3/2-	6.25 6	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
176	1213 8	0.23 6	(3730)	0.0070 18	1904.5 3	5/2-	6.8 1	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
177	1295 8	< 0.16	(3903)	< 0.0027	1732.4 12 ?	7/2-	> 7.5	2 nd non-unique		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
178	1329 8	10.8 7	(3975)	0.252 17	1660.44 7	3/2-	5.30 3	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
179	1455 8	0.66 6	(4240)	0.012 1	1394.52 8	5/2-	6.69 4	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
180	1495 8	< 0.098	(4324)	< 0.002	1310.94 10 ?	7/2-	> 7.6	2 nd non-unique		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
181	1658 8	0.46 19	(4665)	0.0057 23	970.10 11	5/2-	7.1 2	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
182	1897 8	10.8 6	(5160)	0.091 5	474.98 7	1/2-	5.97 3	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
183	2127 8	66.3 17	(5635)	0.405 12	0.0	3/2-	5.40 2	allowed		$^{61}\text{Zn}_{31}$	89.1 s 2	0.0	3/2-	ec $\beta+$ 100 %	5635 16	$^{61}\text{Cu}_{32}$
184		(1071.2)		31 3	548.29 6	1+	4.64 5	allowed		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
185		(982.0)		28.6 22	637.45 5	1+	4.60 4	allowed		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
186		(189.9)		0.102 9	1429.57 7	1+	5.59 4	allowed		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
187		(704.2)		0.036 4	915.31 7	2+	> 7.2	2 nd non-unique		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
188		(93.6)		0.0091 16	1525.92 19	1+	5.98 8	allowed		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
189	255.4 3	8.2 10	(1619.5)	32 4	0.0	1+	4.99 6	allowed		$^{62}\text{Zn}_{32}$	9.193 h 15	0.0	0+	ec $\beta+$ 100 %	1619.5 9	$^{62}\text{Cu}_{33}$
190		(265.7)		0.00057 17	3100.8 8	1/2-,3/2-	7.0 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
191		(321.8)		0.0049 9	3044.7 8	(5/2-)	6.2 1	allowed		$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
192		(477.0)		0.0112 17	2889.5 5	1/2-,3/2,5/2-	6.2 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
193		(508.7)		0.0074 15	2857.8 4	(1/2-,3/2-)	6.5 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
194		(560.1)		0.0057 12	2806.4 4	3/2-	6.7 1	allowed		$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
195		(586.1)		0.030 3	2780.43 24	(1/2-,3/2-)	6.0 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
196		(649.7)		0.085 8	2716.76 10	3/2-,5/2-	5.6 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
197		(669.9)		0.119 9	2696.57 13	1/2-,3/2-	5.5 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
198		(830.7)		0.255 18	2535.82 7	(5/2-)	5.34 3	allowed		$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
199		(854.4)		0.0098 17	2512.1 5	1/2,3/2,5/2	6.8 1			$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
200		(869.3)		0.026 3	2497.2 4	(3/2-)	6.4 1	allowed		$^{63}\text{Zn}_{33}$	38.47 min 5	0	3/2-	ec $\beta+$ 100 %	3366.4 16	$^{63}\text{Cu}_{34}$
201		(1029.9)		0.1												

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
260	382.2 6	0.51 11	(1910.9)	0.59 12	1343.94 12	5/2-	5.36 9	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
261	512.8 6	1.9 5	(2207.5)	0.84 19	1047.43 13	5/2-	5.33 10	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
262	574.3 6	0.71 15	(2345.2)	0.23 5	909.70 10	3/2-	5.95 9	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
263	593.5 6	6.5 14	(2387.9)	1.9 4	866.93 12	1/2-	5.05 9	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
264	594.5 6	0.035 8	(2390.2)	0.0099 22	864.7 4	7/2-	7.32 10	2 nd non-unique		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
265	637.8 6	1.8 4	(2486.0)	0.41 10	768.84 12	5/2-	5.74 10	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
266	895.0 6	10.2 22	(3047.9)	0.85 18	206.95 10	3/2-	5.60 9	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
267	937.6 6	58 14	(3139.7)	4.2 11	115.126 14	3/2-	4.94 11	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
268	966.0 6	10 6	(3200.9)	0.7 4	53.928 10	(1/2)-	5.74 24	allowed		$^{65}\text{Ga}_{34}$	15.2 min 2	0.0	3/2-	ec $\beta+$ 100 %	3254.5 10	$^{65}\text{Zn}_{35}$
269		(169)		0.00122 18	5005.8 3	1+	7.47 7	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
270		(217)		0.0020 5	4958.2 4	1+	7.48 11	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
271		(309)		0.047 6	4866.056 16	1+	6.42 6	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
272		(714)		1.96 17	4461.409 5	1+	5.54 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
273		(537)		0.0042 10	4638.24 14	1	7.96 11	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
274		(499)		0.0015 5	4675.6 5	1+	8.35 15	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
275		(369)		2.30 19	4806.199 5	1+	4.89 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
276		(325)		0.033 4	4849.93 3	1+	6.62 6	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
277		(880)		6.2 5	4295.339 4	1+	5.23 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
278		(1089)		1.67 14	4085.983 4	1+	5.99 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
279	118.9 13	0.000016 11	(1293)	0.0014 9	3882.424 10	(2)+	9.2 3	2 nd non-unique		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
280	142.9 13	0.000073 15	(1350)	0.0029 6	3825.0 3	0+	8.93 9	super allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
281	157.0 13	0.94 8	1420 50	26.0 21	3791.123 3	1+	5.00 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
282	179.2 13	0.00041 9	(1437)	0.0068 15	3738.207 21	+	8.62 10			$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
283	308.9 13	0.16 2	(1743)	0.39 4	3432.408 4	1-	7.03 4	1 st non-unique		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
284	311.1 13	0.0020 5	(1748)	0.0047 11	3427.406 18	1,2-	8.95 11			$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
285	331.1 13	0.70 6	(1794)	1.31 11	3380.944 4	1-	6.53 4	1 st non-unique		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
286	397.1 14	3.7 3	1920 50	3.7 3	3228.885 3	1+	6.14 4	allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
287	575.3 14	0.0053 8	(2348)	0.0017 3	2826.69 5	3-	9.66 7	3 rd non-unique		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
288	781.6 14	0.30 3	2860 50	0.038 3	2372.353 4	0+	8.46 4	super allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
289	1904.1 15	51 4	5175 3	0.48 4	0	0+	7.88 4	super allowed		$^{66}\text{Ga}_{35}$	9.49 h 3	0.0	0+	ec $\beta+$ 100 %	5175.5 13	$^{66}\text{Zn}_{36}$
290		(113.1)		0.281 4	887.693 9	5/2-	5.646 12	allowed		$^{67}\text{Ga}_{36}$	3.2617 d 5	0	3/2-	ec 100 %	1001.2 14	$^{67}\text{Zn}_{37}$
291		(607.3)		23.6 3	393.527 7	3/2-	5.239 6	allowed		$^{67}\text{Ga}_{36}$	3.2617 d 5	0	3/2-	ec 100 %	1001.2 14	$^{67}\text{Zn}_{37}$
292		(816.2)		22.71 9	184.576 6	3/2-	5.5153 22	allowed		$^{67}\text{Ga}_{36}$	3.2617 d 5	0	3/2-	ec 100 %	1001.2 14	$^{67}\text{Zn}_{37}$
293		(907.5)		52.5 11	93.310 5	1/2-	5.244 10	allowed		$^{67}\text{Ga}_{36}$	3.2617 d 5	0	3/2-	ec 100 %	1001.2 14	$^{67}\text{Zn}_{37}$
294		(1000.8)		0.9 9	0.0	5/2-	7.1 5	allowed		$^{67}\text{Ga}_{36}$	3.2617 d 5	0	3/2-	ec 100 %	1001.2 14	$^{67}\text{Zn}_{37}$
295		(99.2)		0.0104 5	2821.86 6	2+	5.113 24	allowed		$^{68}\text{Ga}_{37}$	6.71 min 8	0.0	1+	ec $\beta+$ 100 %	2921.1 16	$^{68}\text{Zn}_{38}$
296		(582.6)		0.0955 22	2338.48 5	2+	5.754 11	allowed		$^{68}\text{Ga}_{37}$	6.71 min 8	0.0	1+	ec $\beta+$ 100 %	2921.1 16	$^{68}\text{Zn}_{38}$

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
356	418 14	0.7 6	(1991)	0.6 6	108.874 21 ?	1+	6.4 4	allowed		$^{66}\text{Ge}_{34}$	2.26 h 5	0.0	0+	ec $\beta+$ 100 %	2116.7 3	$^{66}\text{Ga}_{35}$
357	437 14	0.7 6	(2034)	0.6 6	66.14 4 ?	(2)+	6.4 4	2 nd non-unique		$^{66}\text{Ge}_{34}$	2.26 h 5	0.0	0+	ec $\beta+$ 100 %	2116.7 3	$^{66}\text{Ga}_{35}$
358	446 14	7.2 12	(2056)	5.7 9	43.81 3	1+	5.43 8	allowed		$^{66}\text{Ge}_{34}$	2.26 h 5	0.0	0+	ec $\beta+$ 100 %	2116.7 3	$^{66}\text{Ga}_{35}$
359		(494)		0.030 4	3728.0 9	(1/2-,3/2-)	5.60 6			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
360		(567)		0.040 6	3655.4 7	(1/2-,3/2-)	5.60 7			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
361		(590)		0.014 3	3632.2 15		6.09 10			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
362		(820)		0.186 18	3401.6 5	(1/2-,3/2-)	5.26 5			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
363		(997)		0.45 4	3225.1 3	3/2-	5.04 4	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
364		(1060)		0.134 12	3162.0 8		5.62 4			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
365	202.9 22	0.024 3	(1491)	0.30 3	2730.7 4	(1/2-,3/2-)	5.58 5			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
366	249.9 22	0.0183 20	(1602)	0.105 11	2619.6 5		6.09 5			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
367	289.5 22	0.047 6	(1695)	0.159 17	2526.7 5	(1/2-,3/2-)	5.96 5			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
368	530.5 23	0.086 11	(2246)	0.040 5	1976.1 5		6.81 6			$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
369	605.0 23	4.1 3	(2412)	1.27 10	1809.84 18	3/2-	5.36 4	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
370	681.8 23	7.5 5	(2582)	1.60 9	1639.92 17	3/2-	5.32 3	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
371	720.0 24	0.024 4	(2666)	0.0043 7	1555.9 11	5/2-	7.92 7	2 nd non-unique		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
372	882.0 24	0.012 3	(3019)	0.0012 3	1203 1	7/2-	8.60 10	2 nd unique		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
373	938.2 24	3.5 4	(3140)	0.29 3	1081.64 18	1/2-	6.24 5	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
374	1056.2 24	1.0 3	(3394)	0.061 17	828.33 15	3/2-	6.98 12	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
375	1367.9 24	74 5	(4055)	2.05 14	167.01 5	1/2-	5.61 4	allowed		$^{67}\text{Ge}_{35}$	18.9 min 3	0	1/2-	ec $\beta+$ 100 %	4205 4	$^{67}\text{Ga}_{36}$
376		(106.9)		100 0	0.0	1+	5.006 22	allowed		$^{68}\text{Ge}_{36}$	270.93 d 13	0	0+	ec 100 %	107.3 24	$^{68}\text{Ga}_{37}$
377		(739.1)		0.18 3	1487.96 10	7/2-	7.28 8	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
378		(701.2)		0.77 10	1525.86 6	3/2-	6.60 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
379		(503.7)		0.079 11	1723.35 22	5/2-	7.30 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
380		(335.6)		0.71 9	1891.51 8	3/2-	5.98 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
381		(303.1)		1.26 16	1924.02 8	7/2-	5.64 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
382		(203.4)		0.63 8	2023.68 10	5/2-	5.58 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
383		(182.2)		0.047 8	2044.9 4	5/2-	6.61 8	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
384		(890.5)		4.4 7	1336.61 8	7/2-	6.05 7	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
385	46.64 22	0.0055 6	(1120.3)	37 4	1106.78 6	5/2-	5.33 5	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
386	145.69 21	0.26 4	(1355.1)	11.5 16	872.00 6	3/2-	6.00 6	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
387	271.45 22	2.3 3	(1653.0)	10.0 15	574.12 6	5/2-	6.24 7	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
388	522.10 23	21 5	(2227.1)	10 3	0.0	3/2-	6.49 12	allowed		$^{69}\text{Ge}_{37}$	39.05 h 10	0	5/2-	ec $\beta+$ 100 %	2227.1 18	$^{69}\text{Ga}_{38}$
389		232.47 9		100 0	0.0	3/2-	4.349 1	allowed		$^{71}\text{Ge}_{39}$	11.43 d 3	0.0	1/2-	ec 100 %	232.5 12	$^{71}\text{Ga}_{40}$
390		(10100)		0.0	0+			super allowed		$^{66}\text{As}_{33}$	95.77 ms 23	0.0	[0+]	ec $\beta+$ 100 %	9582 6	$^{66}\text{Ge}_{34}$
391	1100 47	0.27 17	(3486)	0.016 11	2523.7 11		6.2 3			$^{67}\text{As}_{34}$	42.5 s 12	0	(5/2-)	ec $\beta+$ 100 %	6086 4	$^{67}\text{Ge}_{35}$
392	1228 48	0.36 19	(3759)	0.016 8	2251.1 11		6.29 23			$^{67}\text{As}_{34}$	42.5 s 12	0	(5/2-)	ec $\beta+$ 100 %	6086 4	$^{67}\text{Ge}_{35}$
393	1244 48	3.6 14	(3792)	0.15 6	2218.2 10		5.31 18			$^{67}\text{As}_{34}$	42.5 s 12	0	(5/2-)	ec $\beta+$ 100 %	6086 4	$^{67}\text{Ge}_{35}$
394	130															

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
452	1349.15	73.3 9	(3990)	2.47 8	0	5/2-	5.49 2	allowed		$^{69}\text{As}_{36}$	15.2 min 2	0.0	5/2-	ec $\beta+$ 100 %	3988.32	$^{69}\text{Ge}_{37}$
453		(850)		0.84 6	5370.07 5		5.13 7		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
454		(954)		0.164 19	5265.81 14		5.94 7		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
455	226.22	0.008 3	(1545)	0.077 11	4675.41 21	(3,4+)	6.69 8		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
456	268.22	0.034 10	(1643)	0.18 3	4577.23 16	(3,4+)	6.39 8		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
457	413.22	0.12 3	(1977)	0.14 3	4243.11 15		6.64 11		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
458	475.23	0.59 7	(2119)	0.45 6	4101.45 5	(3-)	6.20 7	1 st non-unique		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
459	666.23	1.03 14	(2544)	0.27 4	3675.75 7	3+,4+	6.58 8		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
460	713.23	0.35 4	(2649)	0.075 11	3570.51 7	(2,3)-	7.17 8		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
461	751.23	6.0 4	(2732)	1.1 1	3488.234 24	(3,4+)	6.04 6		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
462	804.23	0.17 3	(2848)	0.026 6	3371.64 10	(3,4)	7.70 10		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
463	840.23	0.63 12	(2925)	0.082 17	3294.76 8	3+,4+	7.22 10		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$	
464	949.24	35.6 19	(3161)	3.2 3	3058.720 24	4+	5.69 5	allowed		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
465	954.24	31.9 19	(3174)	2.8 3	3046.43 3	3+	5.75 5	allowed		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
466	1066.24	1.2 4	(3414)	0.08 3	2806.25 3	4+	7.37 14	allowed		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
467	1181.24	1.6 4	(3658)	0.078 19	2562.05 3	3-	7.44 11	1 st non-unique		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
468	1194.24	0.80 16	(3685)	0.037 8	2534.93 4	2+	7.76 10	2 nd non-unique		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
469	1233.24	5.66 19	(3769)	0.241 16	2451.30 3	3+	6.97 4	allowed		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
470	1372.24	0.8 3	(4063)	0.02 1	2156.73 3	2+	8.04 17	2 nd non-unique		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
471	1374.24	4.3 15	(4067)	0.13 5	2153.17 3 ?	4+	7.30 16	allowed		$^{70}\text{As}_{37}$	52.6 min 3	0.0	4+	ec $\beta+$ 100 %	6228.1.16	$^{70}\text{Ge}_{38}$
472		(48)		0.0012 3	1965.06 7	3/2-	7.18 14	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
473		(76)		0.0196 6	1937.45 3	(3/2+,5/2-)	6.42 6			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
474		(212)		0.035 3	1801.13 7	(5/2+,7/2)	7.14 5			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
475		(221)		0.105 4	1792.098 9	(3/2+,5/2-)	6.71 3			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
476		(232)		0.0292 23	1780.746 19	5/2-,7/2-	7.31 4			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
477		(270)		0.076 4	1743.409 18	3/2-	7.03 3	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
478		(384)		0.102 9	1629.178 12	(3/2+,5/2-)	7.21 4			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
479		(414)		0.232 18	1598.535 17	3/2-	6.93 4	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
480		(454)		0.251 7	1558.744 14	5/2+	6.97 2	1 st non-unique		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
481		(507)		0.176 6	1506.381 14	7/2-	7.22 2	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
482		(563)		0.033 17	1449.8 3		8.04 23			$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
483		(591)		0.0007 3	1421.97 10 ?	9/2-	9.74 15	2 nd non-unique		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
484		(606)		0.215 7	1406.651 10	7/2-	7.30 2	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
485		(634)		0.0009 4	1379.0 5 ?	(1/2-)	9.71 20	2 nd non-unique		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
486		(634)		0.21 3	1378.70 5	5/2-	7.35 7	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
487		(714)		0.222 11	1298.737 14	3/2-	7.43 2	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
488		(800)		1.09 6	1212.498 6	5/2-	6.84 3	allowed		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}$
489		(808)		0.730 19	1205.145 8	5/2+	7.02 2	1 st non-unique		$^{71}\text{As}_{38}$	65.30 h 7	0.0	5/2-	ec $\beta+$ 100 %	2013.4	$^{71}\text{Ge}_{39}</math$

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
548		(195)	0.00020 4	6485 33		5.4 3				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
549		(293)	0.00030 7	6387 33		5.62 18				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
550		(358)	0.00020 5	6322 33		5.97 17				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
551		(407)	0.00050 10	6273 33		5.69 14				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
552		(441)	0.00021 5	6239 33		6.14 14				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
553		(483)	0.00070 20	6197 33		5.69 16				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
554		(544)	0.00060 10	6136 33		5.87 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
555		(599)	0.0010 2	6081 33		5.73 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
556		(650)	0.00050 10	6030 33		6.10 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
557		(686)	0.00060 10	5994 33		6.07 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
558		(730)	0.00060 10	5950 33		6.13 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
559		(757)	0.00040 10	5923 33		6.33 13				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
560		(801)	0.0017 4	5879 33		5.76 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
561		(839)	0.0017 4	5841 33		5.80 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
562		(880)	0.0024 5	5800 33		5.69 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
563		(939)	0.0014 3	5741 33		5.98 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
564		(985)	0.00070 20	5695 33		6.32 13				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
565		(1023)	0.0026 6	5657 33		5.79 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
566		(1074)	0.00050 10	5606 33		6.55 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
567		(1110)	0.0016 4	5570 33		6.07 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
568		(1147)	0.0017 4	5533 33		6.07 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
569	82 19	0.0000015 23	(1200)	0.0011 2	5480 33	6.30 9				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
570	93 19	0.000003 4	(1228)	0.0012 3	5452 33	6.28 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
571	109 19	0.000005 5	(1264)	0.0011 2	5416 33	6.35 9				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
572	128 19	0.000010 7	(1311)	0.00097 22	5369 33	6.43 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
573	152 19	0.000029 17	(1366)	0.0015 3	5314 33	6.29 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
574	169 19	0.000028 15	(1407)	0.00095 19	5273 33	6.50 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
575	188 19	0.00016 8	(1452)	0.0036 8	5228 33	5.95 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
576	216 19	0.00017 7	(1519)	0.0022 5	5161 33	6.20 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
577	241 19	0.00018 6	(1578)	0.0015 4	5102 33	6.40 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
578	263 19	0.00015 4	(1630)	0.00095 18	5050 33	6.63 9				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
579	292 20	0.00019 5	(1696)	0.00081 17	4984 33	6.73 10				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
580	313 20	0.00056 16	(1745)	0.0019 5	4935 33	6.38 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
581	340 20	0.00027 8	(1809)	0.00070 18	4871 33	6.86 12				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
582	394 20	0.0009 3	(1933)	0.0014 4	4747 33	6.61 13				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
583	437 20	0.0011 3	(2031)	0.0012 3	4649 33	6.72 11				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
584	728 14	0.21 4	(2680)	0.048 10	3999.6 7	5.36 9				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
585	888 14	0.10 3	(3028)	0.012 3	3651.6 10	6.06 13				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
586	973 14	0.19 4	(3211)	0.018 4	3468.9 7	5.94 9				$^{69}\text{Se}_{35}$	27.4 s 2	0.0	1/2-	ec $\beta+$ 100 %	6677 32	$^{69}\text{As}_{36}$
587	1															

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
644		(875)	0.412 10	1850.30 12	(9/2)+	6.42 2	allowed			$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
645		(815)	0.060 7	1909.89 16	(9/2+, 11/2)	7.20 6				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
646		(750)	0.095 3	1975.09 15	(7/2, 9/2)	6.92 2				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
647		(545)	0.030 8	2180.31 14	(7/2, 9/2+)	7.1 1				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
648		(414)	0.157 6	2311.25 12	(7/2, 9/2+)	6.18 3				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
649		(243)	0.0087 17	2482.47 25	(7/2, 9/2+)	7.0 1				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
650		(141)	0.0155 20	2583.87 14	(7/2, 9/2-)	6.2 1				$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
651	165 3	0.0035 3	(1397)	0.130 4	1328.42 13	(7/2+)	7.34 2	allowed		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
652	180 3	0.016 1	(1432)	0.43 2	1292.81 13	(7/2+)	6.83 2	allowed		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
653	180 3	0.016 1	(1432)	0.43 2	1292.73 17	(11/2+)	6.83 2	allowed		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
654	186 3	0.0044 5	(1449)	0.100 9	1302.05 6	(5/2-)	6.45 4	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
655	187 3	0.0004 4	(1450)	0.010 10	1274.82 12 ?	(7/2+)	8.5 5	allowed		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
656	188 3	0.0049 6	(1451)	0.108 11	1299.41 9	(1/2-, 3/2)	6.41 5			$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
657	228 3	0.0167 8	(1547)	0.178 4	1177.80 10	(9/2-)	7.29 1	1 st non-unique		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
658	234 3	0.0027 4	(1562)	0.026 4	1188.72 10	(3/2-)	7.1 1	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
659	278 3	0.037 4	(1664)	0.191 18	1086.69 5	5/2-	6.29 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
660	282 3	0.130 10	(1673)	0.65 6	1077.57 4	(3/2-)	5.76 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
661	288 3	< 0.0020	(1688)	< 0.0090	1036.97 18 ?	(13/2+)	> 8.7	2 nd non-unique		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
662	307 3	0.0006 4	(1732)	0.0023 13	993.45 10	(7/2-)	9.3 3	1 st non-unique		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
663	380 3	0.097 9	(1901)	0.174 16	850.18 18	(5/2-)	6.44 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
664	415 3	0.104 9	(1981)	0.138 12	769.61 10	5/2-	6.58 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
665	466 3	0.97 8	(2095)	0.88 8	655.36 6	3/2-	5.82 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
666	500 3	0.57 5	(2173)	0.42 4	577.6 3	5/2-	6.18 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
667	501 3	0.80 7	(2176)	0.57 5	574.43 6	(1/2)-	6.04 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
668	530 3	0.090 8	(2241)	0.054 5	509.74 15	(5/2+)	7.09 4	1 st non-unique		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
669	555 3	63.9 8	(2297)	33.4 6	427.65 12	9/2+	5.36 1	allowed		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
670	582 3	0.84 8	(2357)	0.38 3	393.39 5	3/2-	6.29 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
671	645 3	0.05 3	(2497)	0.010 10	253.84 4	(1/2)-	7.8 3	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
672	722 3	1.26 14	(2666)	0.29 3	84.19 4	(1/2)-	6.51 5	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
673	730 3	2.4 3	(2684)	0.55 7	67.09 7	5/2-	6.24 6	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
674	745 3	0.63 6	(2658)	0.47 4	67.10 9	5/2-	8.77 4	1 st unique		$^{73}\text{Se}_{39}$	7.15 h 9	0.0	9/2+	ec $\beta+$ 100 %	2725 8	$^{73}\text{As}_{40}$
675	760 3	12.8 9	(2780)	2.56 19	0.0	3/2-	5.60 4	allowed		$^{73m}\text{Se}_{39}$	39.8 min 17	25.71 4	3/2-	ec $\beta+$ 27.4 3 %	2750.71 8	$^{73}\text{As}_{40}$
676		(864.7)		1.1 6	0.0	3/2-	8.6 3	1 st non-unique		$^{75}\text{Se}_{41}$	119.78 d 5	0.0	5/2+	ec 100 %	864.7 9	$^{75}\text{As}_{42}$
677		(666.1)		0.047 18	198.6063 8	1/2-	10.0 2	1 st unique		$^{75}\text{Se}_{41}$	119.78 d 5	0.0	5/2+	ec 100 %	864.7 9	$^{75}\text{As}_{42}$
678		(600.0)		0.5 5	264.6581 6 ?	3/2-	> 8.3	1 st non-unique		$^{75}\text{Se}_{41}$	119.78 d 5	0.0	5/2+	ec 100 %	864.7 9	$^{75}\text{As}_{42}$
679		(585.2)		2.1 4	279.5428 8	5/2-	8.0 1	1 st non-unique		$^{75}\text{Se}_{41}$	119.78 d 5	0.0	5/2+	ec 100 %	864.7 9	$^{75}\text{As}_{42}$
680		(464.0)		96												

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
740	1162 7	0.94 13	(3615)	0.06 1	3306.1 3	(2 TO 6)	7.57 7			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
741	1182 7	17.6 5	(3657)	1.10 4	3250.04 12	(1,2+)	6.07 2			$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
742	1187 7	0.69 10	(3667)	0.040 6	3253.3 4	(2 TO 6)	7.74 7			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
743	1188 7	2.3 3	(3670)	0.10 2	3250.97 22	(1,2+)	7.22 6			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
744	1211 7	0.78 10	(3720)	0.04 1	3200.9 4	(4)	7.74 6	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
745	1253 7	1.09 15	(3808)	0.05 2	3112.7 3	(2+,3,4+)	7.64 12			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
746	1269 7	< 4.5	(3843)	< 0.2	3078.19 17 ?	(4)+	> 7.0	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
747	1307 7	0.89 19	(3883)	0.11 2	3037.3 4	(2+)	9.14 10	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
748	1344 8	3.5 4	(4002)	0.10 2	2918.71 19	(2+,3,4+)	7.27 6			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
749	1386 8	0.53 10	(4089)	0.020 4	2831.87 23	4-	8.15 9	1 st non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
750	1392 8	2.2 3	(4102)	0.10 1	2818.61 19	(2+,3,4+)	7.54 7			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
751	1466 8	0.82 17	(4258)	0.030 6	2662.46 18	5+	8.06 10	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
752	1513 8	7.8 7	(4357)	0.20 3	2563.63 14	(2+,3,4+)	7.14 5			$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
753	1595 8	< 0.1	(4528)	< 0.003	2378.56 12 ?	(1,2+)	> 8.9			$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
754	1615 8	4.1 16	(4571)	0.10 8	2349.65 24	3-	7.6 4	1 st non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
755	1646 7	1.15 20	(4606)	0.08 1	2314.43 16	(2+)	9.65 8	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
756	1685 7	0.65 10	(4689)	0.04 1	2231.36 23	6+	9.95 7	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
757	1731 8	4.9 8	(4813)	0.10 2	2107.99 12	4+	7.60 8	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
758	1832 8	< 0.6	(5023)	< 0.01	1884.00 18 ?	3+	> 8.5	3 rd non-unique		$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
759	1838 8	6.7 11	(5036)	0.10 2	1884.39 12	3+	7.58 8	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
760	1853 8	2.9 4	(5068)	0.049 7	1838.69 10 ?	(2+)	7.70 6	1 st unique		$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
761	1871 8	1.8 6	(5082)	0.070 24	1838.74 17	(2+)	9.80 15	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
762	2089 8	8 3	(5558)	0.10 5	1363.25 11	4+	7.74 22	allowed		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
763	2128 8	6.5 21	(5638)	0.075 24	1268.89 8	2+	7.61 14	1 st unique		$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
764	2142 8	< 9	(5652)	< 0.2	1269.12 11 ?	2+	> 9.5	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
765	2330 8	3.8 13	(6053)	0.034 12	853.79 10	0+	8.02 15	1 st non-unique		$^{74m}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
766	2436 8	< 4.0	(6272)	< 0.03	634.79 8 ?	2+	> 8.1	1 st unique		$^{74}\text{Br}_{39}$	25.4 min 3	0.0	(0-)	ec $\beta+$ 100 %	6925 6	$^{74}\text{Se}_{40}$
767	2445 8	< 11	(6286)	< 0.2	634.80 9 ?	2+	> 9.7	2 nd non-unique		$^{74m}\text{Br}_{39}$	46 min 2	13.58 21	4(+)	ec $\beta+$ 100 %	6938.58 6	$^{74}\text{Se}_{40}$
768	209.3 17	0.040 4	(1501)	0.68 7	1561.04 14	(5/2,7/2-)	6.08 5			$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
769	286.3 18	0.018 3	(1681)	0.096 16	1380.5 3		7.03 8			$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
770	288.7 18	0.053 6	(1687)	0.28 3	1374.70 22	1/2,3/2,5/2	6.57 6			$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
771	344.6 18	0.72 7	(1817)	2.03 19	1245.26 12	3/2-	5.77 4	allowed		$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
772	364.8 18	0.48 5	(1863)	1.11 11	1198.61 12	5/2+	6.05 5	1 st non-unique		$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
773	371.0 18	0.29 3	(1878)	0.64 7	1184.38 14	1/2,3/2,5/2	6.30 5			$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
774	388.4 18	0.062 10	(1917)	0.12 2	1144.51 20	3/2+,5/2+	7.05 8			$^{75}\text{Br}_{40}$	96.7 min 13	0.0	3/2-	ec $\beta+$ 100 %	3062 4	$^{75}\text{Se}_{41}$
775	419.3 18	0.45 4	(1988)	0.66 6	1073.77 14	5/2-	6.34 4	allowed	</							

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
836		(676)		0.0049 11	2898.14 21	2+	6.3 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
837		(927)		0.0117 12	2647.39 15	(1,2)+	6.2 1			$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
838		(1037)		0.063 3	2537.18 14	2+	5.61 2	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
839	98.8 18	0.00013 1	(1240)	0.046 3	2334.43 21	0+	5.91 3	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
840	101.0 18	0.0000048 19	(1245)	0.0016 6	2329.4 9	2+	7.4 2	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
841	242.0 17	0.00071 12	(1578)	0.0071 12	1996.08 17	2+	6.9 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
842	344.1 18	0.0046 4	(1816)	0.0131 11	1758.31 21	0+	6.8 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
843	457.8 18	0.032 2	(2076)	0.036 2	1498.41 12	0+	6.5 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
844	542.0 18	0.047 5	(2266)	0.030 4	1308.48 11	2+	6.6 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
845	857.4 19	11.5 3	(2960)	1.81 6	613.71 7	2+	5.07 2	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
846	1142.7 19	80.9 4	(3574)	5.49 6	0.0	0+	4.75 1	allowed		$^{78}\text{Br}_{43}$	6.45 min 4	0.0	1+	ec $\beta+$ $\geq 99.99\%$	3574 4	$^{78}\text{Se}_{44}$
847		(420.5)		< 0.0200	1450	2+	> 5.7	allowed		$^{80}\text{Br}_{45}$	17.68 min 2	0.0	1+	ec $\beta+$ 8.3 2 %	1870.5 14	$^{80}\text{Se}_{46}$
848		(392.5)		0.050 20	1478.0 16	0+	5.3 3	allowed		$^{80}\text{Br}_{45}$	17.68 min 2	0.0	1+	ec $\beta+$ 8.3 2 %	1870.5 14	$^{80}\text{Se}_{46}$
849	84.3 9		(1204.7)	1.10 10	665.8 2	2+	4.94 5	allowed		$^{80}\text{Br}_{45}$	17.68 min 2	0.0	1+	ec $\beta+$ 8.3 2 %	1870.5 14	$^{80}\text{Se}_{46}$
850	368.2 10	2.20 21	(1882)	4.90 23	0.0	0+	4.67 5	allowed		$^{80}\text{Br}_{45}$	17.68 min 2	0.0	1+	ec $\beta+$ 8.3 2 %	1870.5 14	$^{80}\text{Se}_{46}$
851		(13679.8911607805544960)		0+X	(3/2-)			allowed		$^{69}\text{Kr}_{33}$	28 ms 1	0.0	(5/2-)	ec $\beta+$ 100 %	14119 303	$^{69}\text{Br}_{34}$
852	4520 200	52 6	(10527)	0.080 15	3153 55	(5/2-)	3.43 11	allowed		$^{69}\text{Kr}_{33}$	28 ms 1	0.0	(5/2-)	ec $\beta+$ 100 %	14119 303	$^{69}\text{Br}_{34}$
853	6090 200	2.4 5	(13679.8911607805544960)	0.0016 4	0	(5/2-)	> 5.4	allowed		$^{69}\text{Kr}_{33}$	28 ms 1	0.0	(5/2-)	ec $\beta+$ 100 %	14119 303	$^{69}\text{Br}_{34}$
854	4501.67	≤ 99.8	(10479.91780570591231200)	≤ 0.155	0.0	0+	≥ 3.3	super allowed		$^{70}\text{Kr}_{34}$	40 ms 6	0.0	0+	ec $\beta+$ 100 %	10326 201	$^{70}\text{Br}_{35}$
855		(8319)		1861+X						$^{71}\text{Kr}_{35}$	94.9 ms 4	0	(5/2-)	ec $\beta+$ 100 %	10175 129	$^{71}\text{Br}_{36}$
856	4152 65	4.4 4	(9773)	0.0086 9	407.12 24	(5/2-)	4.87 5	allowed		$^{71}\text{Kr}_{35}$	94.9 ms 4	0	(5/2-)	ec $\beta+$ 100 %	10175 129	$^{71}\text{Br}_{36}$
857	4251 65	1.0 8	(9972)	0.0018 15	207.97 16	(3/2-)	5.6 4	allowed		$^{71}\text{Kr}_{35}$	94.9 ms 4	0	(5/2-)	ec $\beta+$ 100 %	10175 129	$^{71}\text{Br}_{36}$
858	4353 65	91.3 9	(10180)	0.156 7	0.0	(5/2-)	3.65 3	allowed		$^{71}\text{Kr}_{35}$	94.9 ms 4	0	(5/2-)	ec $\beta+$ 100 %	10175 129	$^{71}\text{Br}_{36}$
859	349 4	0.038 5	(1824)	0.116 16	3304.9 10 ?	1+	4.53 6	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
860	941 5	0.022 4	(3141)	0.0030 6	1988.4 10 ?	1	6.60 9	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
861	959 5	0.036 7	(3179)	0.0046 9	1950.0 7 ?	1	6.41 9	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
862	962 5	0.054 11	(3185)	0.0068 14	1943.5 7 ?	1	6.25 9	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
863	1012 5	0.69 4	(3293)	0.076 4	1835.53 18	1+	5.23 3	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
864	1029 5	0.32 5	(3329)	0.033 5	1799.5 3	1+	5.60 7	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
865	1042 5	2.63 11	(3357)	0.263 12	1772.05 18	1+	4.708 21	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
866	1074 5	0.30 5	(3425)	0.028 4	1703.8 4	1+	5.70 7	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
867	1120 5	0.47 11	(3524)	0.038 9	1604.93 20	1+	5.59 11	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
868	1223 5	1.86 15	(3743)	0.117 10	1386.08 15	1+	5.15 4	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
869	1252 5	0.224 22	(3806)	0.0131 13	1322.8 4	1(+)	6.12 5	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
870	1323 5	0.31 4	(3956)	0.016 2	1173.2 3	1(+)	6.07 6	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
871	1332 5	0.13 6	(3975)	0.007 3	1154.30 19	1	6.46 19	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$
872	1392 5	1.60 13	(4101)	0.069 6	1027.80 18	1+	5.46 4	allowed		$^{72}\text{Kr}_{36}$	17.1 s 2	0.0	0+	ec $\beta+$ 100 %	5121 8	$^{72}\text{Br}_{37}$

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
932	678 5	0.0032 4	(2566)	0.0011 2	4530		7.0 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
933	692 5	0.00082 15	(2596)	0.00028 5	4500		7.7 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
934	710 5	0.0012 2	(2636)	0.00038 5	4460		7.5 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
935	723 5	0.0005 2	(2666)	0.0002 1	4430		7.9 2			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
936	746 5	0.0006 2	(2716)	0.0001 0	4380		8.0 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
937	769 5	0.0005 1	(2766)	0.0001 0	4330		8.1 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
938	792 5	0.0002 2	(2816)	0.00006 4	4280		8.4 3			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
939	1168 5	0.23 6	(3627)	0.017 4	3469.1 8	(1/2,3/2,5/2)	6.2 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
940	1171 5	0.47 11	(3634)	0.033 8	3462.3 6	(1/2,-3/2,5/2)	5.9 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
941	1255 5	0.33 9	(3811)	0.019 5	3285.1 8	(1/2,3/2,5/2)	6.2 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
942	1270 5	0.22 6	(3844)	0.012 3	3252.1 8	(1/2,-3/2,5/2)	6.4 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
943	1381 5	2.3 6	(4079)	0.10 3	3017.3 4	(1/2,3/2,5/2)-	5.5 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
944	1601 5	0.76 17	(4541)	0.022 5	2555.0 5	(1/2,-3/2,5/2)	6.3 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
945	1741 5	0.9 2	(4834)	0.02 0	2261.5 5	(1/2,3/2,5/2-)	6.4 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
946	1793 5	1.3 3	(4942)	0.027 6	2153.9 4	(1/2,-3/2,5/2)	6.2 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
947	2087 5	1.7 4	(5554)	0.023 5	1542.4 4	(1/2,3/2,5/2)	6.4 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
948	2121 5	0.9 2	(5623)	0.01 0	1473.0 4	(1/2,-3/2,5/2)	6.7 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
949	2283 5	4.5 10	(5958)	0.047 10	1137.52 21	(1/2,-3/2,5/2)	6.2 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
950	2489 5	2.9 7	(6383)	0.024 6	713.3 3	(1/2,-3/2,5/2-)	6.5 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
951	2505 5	2.0 10	(6415)	0.016 8	681.1 4	7/2-	6.7 2	2 nd non-unique		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
952	2527 5	5.6 14	(6461)	0.044 11	635.26 21	(1/2,-3/2,5/2-)	6.3 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
953	2602 5	4.3 12	(6615)	0.031 9	481.20 24	(5/2-)	6.4 1	allowed		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
954	2606 5	5.1 12	(6623)	0.037 9	473.4 3	(1/2,-3/2,5/2-)	6.4 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
955	2630 5	3.9 9	(6673)	0.027 6	423.40 23	(1/2,3/2,5/2-)	6.5 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
956	2633 5	4.5 10	(6677)	0.032 7	419.03 24	(1/2,-3/2,5/2)	6.4 1			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
957	2697 5	3.8 10	(6810)	0.025 7	286.09 17	(5/2)+	6.6 1	1 st non-unique		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
958	2720 5	5.0 16	(6855)	0.032 10	240.45 15	(3/2,5/2-)	6.5 2			$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
959	2750 5	9.3	(6918)	0.055 16	178.04 14	3/2-	6.2 1	allowed		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
960	2824 5	< 9.9	(7069)	< 0.058	26.94 9	(5/2)-	> 6.2	allowed		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
961	2837 5	36 9	(7096)	0.21 5	0.0	1/2-	5.7 1	allowed		$^{73}\text{Kr}_{37}$	27.3 s 10	0.0	(3/2)-	ec $\beta+$ 100 %	7094 9	$^{73}\text{Br}_{38}$
962	424 7	0.19 6	(1997)	0.31 9	978.3 8	(1)	5.8	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
963	428 7	0.39 12	(2005)	0.61 18	970.0 4	(1+)	5.5	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
964	489 7	0.20 7	(2143)	0.20 7	831.8 6	(1)	6.0	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
965	547 7	1.9 4	(2274)	1.3 3	701.28 17	(1+)	5.3	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
966	587 7	0.19 7	(2362)	0.11 4	612.9 7	(1)	6.4	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
967	588 7	2.0 5	(2366)	1.10 24	609.11 16	(1+)	5.4	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec $\beta+$ 100 %	2956 6	$^{74}\text{Br}_{39}$
968	622 7	0.61 18	(2440)	0.29 9	534.7 6	(1)	6.0	allowed		$^{74}\text{Kr}_{38}$	11.50 min 11	0.0	0+	ec <		

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught					
1028		(956)	10.4	11	355.28	11	1+	5.52	5	allowed	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1029		(994)	< 1.1		317.05	12 ?	(2+)	>	6.5	2 nd non-unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1030		(995)	55	6	315.68	11	1+	4.83	5	allowed	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1031		(1059)	< 1.2		252.06	12 ?	(2+)	>	6.5	2 nd non-unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1032		(1160)	< 0.10		150.51	13 ?	(≤ 3)	>	7.7	2 nd unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1033		(1266)	< 4		45.48	11 ?	(2)-	>	7.0	1 st unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1034	95	9	(1208)	< 0.40	102.64	20 ?	(4)+	>	7.1	4 th non-unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1035	139	9	(1311)	< 6	0.0	?	1-	>	6.0	1 st non-unique	⁷⁶ Kr ₄₀	14.8 h	1	0.0	0+	ec $\beta+$ 100 %	¹²⁷⁵ 10				
1036		(721)	0.030	4	2344.3	5	(3/2,5/2,7/2+)	6.7	1		⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3				
1037		(871)	0.017	3	2193.6	6	(3/2,5/2,7/2)	7.1	1		⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3				
1038		(936)	0.055	7	2129.1	4	(3/2)-	6.7	1	1 st non-unique	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3				
1039	204	9	13	0.027	2	(1489)	0.56	5	1576.15	14	(5/2-)	6.06	4	1 st non-unique	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1040	411	1	14	0.021	5	(1967)	0.037	10	1097.68	24	(5/2+,7/2)	7.5	1		⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1041	443	2	14	0.19	2	(2041)	0.27	2	1024.45	20	(5/2)+	6.66	4	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1042	468	5	14	0.17	1	(2098)	0.19	2	967.19	18	(7/2+)	6.83	4	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1043	514	0	14	0.33	3	(2200)	0.28	3	864.51	15	(3/2+)	6.71	5	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1044	714	9	14	2.7	4	(2647)	0.82	12	417.69	16	7/2(+)	6.4	1	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1045	779	5	14	33.6	16	(2789)	7.9	4	276.21	6	(3/2+)	5.46	2	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1046	829	7	14	0.11	3	(2898)	0.021	5	166.6	3	(3/2)-	8.1	1	1 st non-unique	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1047	831	8	14	0.19	3	(2903)	0.038	5	161.9	3	5/2-	7.8	1	1 st non-unique	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1048	846	7	14	41.8	19	(2935)	7.7	4	129.63	4	5/2+	5.521	21	allowed	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1049	906	4	14	< 5		(3065)	< 0.8	0.0	?	3/2-	>	6.6	1	1 st non-unique	⁷⁷ Kr ₄₁	71.25 min	42	0.0	5/2+	ec $\beta+$ 100 %	³⁰⁶⁵ 3
1050		(52)		< 0.0005		1573.7	5 ?	(5/2)+	>	7.5	1	1 st unique	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4		
1051		(124)		0.023	8	1501.6	3	1/2,3/2	6.7	2		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4			
1052		(294)	1.27	7	1332.31	6	3/2-	5.76	4	allowed	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1053		(494)	0.069	8	1131.67	14	1/2,3/2	7.48	6		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1054		(514)	0.22	4	1112.48	11	1/2-,3/2-	7.0	1		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1055		(794)	1.80	12	831.94	6	1/2-,3/2-	6.48	3		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1056		(1020)	12.1	5	606.02	6	3/2-	5.88	2	allowed	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1057		(1103)	< 0.18		523.22	10 ?	5/2-	>	7.8	2 nd non-unique	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4				
1058	95	3	0.021	4	(1229)	9.6	5	397.47	6	1/2-,3/2-	6.14	3		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4	
1059	134	3	0.005	2	(1319)	0.52	15	306.52	7	1/2-,3/2-	7.5	2		⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4	
1060	153	3	0.18	2	(1365)	11.6	5	261.32	6	3/2-	6.15	2	allowed	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4	
1061	264	3	6.8	3	(1626)	55.9	12	0.0		3/2-	5.62	12	allowed	⁷⁹ Kr ₄₃	35.04	h 10	0.0	1/2-	ec $\beta+$ 100 %	¹⁶²⁶ 4	
1062		(280.8)	99.70	2	0		3/2-			11.014	22	1 st unique	⁸¹ Kr ₄₅	2.29	x 10 ⁵	y 11	0.0	7/2+	ec 100 %	^{280.9} 15	
1063		(4.8)	0.30	2	275.991	11	5/2-	9.35	15	1 st non-unique	⁸¹ Kr ₄₅	2.29	x 10 ⁵	y 11	0.0	7/2+	ec 100 %	^{280.9} 15			
1064		(471.4)	0.0025	4	0		3/2-	4.89	7	allowed	^{81m} Kr ₄₅	13.10	s 3	190.64	4	1/2-	ec 2.5 x 10 ⁻³ 4 %	^{471.}			

#	$\leq E_{\beta^+} \geq$ [keV]	$I_{\beta^+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
1124	1706.6 12	< 0.09	(4762)	< 0.002	577.3 6 ?	(3/2-,5/2,7/2-)	> 8.2			$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1125	1743.9 12	1.6 4	(4839.4)	0.040 10	499.58 12 ?	7/2-	7.0 1	2 nd non-unique		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1126	1762.9 12	7.1 14	(4879.1)	0.18 3	459.88 9	1/2-	6.4 1	allowed		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1127	1865.8 12	12.6 24	(5093.7)	0.27 5	245.30 6	5/2-	6.2 1	allowed		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1128	1919.8 12	1.5 5	(5189.0)	0.069 22	149.94 9	7/2+	8.8 2	1 st unique		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1129	1951.8 12	27 5	(5272.5)	0.51 9	66.50 5	3/2-	6.0 1	allowed		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1130	1983.9 12	< 29	(5339.0)	< 0.52	0.0 ?	5/2+	> 5.9	1 st non-unique		$^{77}\text{Rb}_{40}$	3.78 min 4	0.0	3/2-	ec $\beta+$ 100 %	5339.0 24	$^{77}\text{Kr}_{41}$
1131	277 4	0.024 3	(1657)	0.19 3	5586.09 16	(1)	6.08 7	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1132	285 4	0.049 5	(1675)	0.35 4	5567.79 16	(1)	5.81 5	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1133	296 4	0.030 6	(1699)	0.19 3	5543.69 16	(1)	6.1 1	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1134	302 4	0.13 1	(1714)	0.73 5	5529.24 9	(1)	5.51 4	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1135	371 4	0.080 11	(1873)	0.23 3	5369.56 15	(1)	6.09 6	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1136	387 4	0.17 1	(1910)	0.41 4	5333.04 12	(1)	5.86 4	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1137	426 4	0.22 2	(1999)	0.39 4	5243.88 8	(1)	5.92 5	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1138	435 4	0.16 2	(2020)	0.26 3	5222.60 11	(1)	6.10 6	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1139	449 4	0.44 8	(2050)	0.66 12	5192.51 11	(1)	5.7 1	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1140	454 4	0.35 2	(2062)	0.52 3	5180.74 8	(1)	5.83 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1141	506 4	0.24 2	(2181)	0.24 2	5061.69 17	(1)	6.20 4	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1142	529 4	0.40 3	(2231)	0.35 2	5011.53 7	(1)	6.06 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1143	796 4	0.59 3	(2822)	0.15 1	4420.88 9	(1)	6.64 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1144	896 4	0.52 4	(3041)	0.091 8	4201.68 8	(1)	6.92 4	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1145	948 4	2.6 2	(3154)	0.39 3	4089.32 5	(1)	6.32 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1146	971 4	3.3 2	(3203)	0.46 3	4040.39 5	(1)	6.26 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1147	986 4	2.0 1	(3235)	0.27 1	4007.80 5	(1)	6.50 2	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1148	1019 4	3.0 2	(3305)	0.37 2	3937.58 4	(1)	6.39 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1149	1038 4	0.17 4	(3346)	0.019 4	4007.79 6 ?	(1)	7.2 1	2 nd unique		$^{78}\text{Rb}_{41}$	5.74 min 3	111.19 22	4(-)	ec $\beta+$ 91 2 %	7354.19 3	$^{78}\text{Kr}_{42}$
1150	1039 4	15.9 7	(3350)	1.80 8	3893.27 5	(1)	5.71 2	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1151	1069 4	2.70 15	(3414)	0.282 17	3829.45 6	(1)	6.53 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1152	1147 4	8.9 4	(3580)	0.76 3	3774.61 5	(3)-	5.65 2	allowed		$^{78}\text{Rb}_{41}$	5.74 min 3	111.19 22	4(-)	ec $\beta+$ 91 2 %	7354.19 3	$^{78}\text{Kr}_{42}$
1153	1147 4	3.59 20	(3581)	0.306 18	3662.18 5	(1)	6.54 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1154	1158 4	0.58 6	(3605)	0.047 5	3749.15 10	(3,4,-)	6.86 5			$^{78}\text{Rb}_{41}$	5.74 min 3	111.19 22	4(-)	ec $\beta+$ 91 2 %	7354.19 3	$^{78}\text{Kr}_{42}$
1155	1170 4	2.92 20	(3629)	0.234 16	3725.49 6	3+,4+	6.17 3			$^{78}\text{Rb}_{41}$	5.74 min 3	111.19 22	4(-)	ec $\beta+$ 91 2 %	7354.19 3	$^{78}\text{Kr}_{42}$
1156	1188 4	2.54 14	(3668)	0.196 11	3575.08 6	(1)	6.75 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1157	1196 4	3.38 18	(3685)	0.255 13	3669.22 7	3-,4-	6.15 3			$^{78}\text{Rb}_{41}$	5.74 min 3	111.19 22	4(-)	ec $\beta+$ 91 2 %	7354.19 3	$^{78}\text{Kr}_{42}$
1158	1205 4	6.5 4	(3704)	0.48 3	3539.07 4	(1)	6.37 3	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1159	1253 4	14.9 7	(3806)	0.98 4	3437.42 5	(1)	6.08 2	allowed		$^{78}\text{Rb}_{41}$	17.66 min 3	0.0	0(+)	ec $\beta+$ 100 %	7243.3	$^{78}\text{Kr}_{42}$
1160	1341 4	0.99 8	(3993)	0.054 4												

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
1220	878.7 19	1.2 4	(3003)	0.22 8	635.78 8	5/2+	6.64 16	allowed		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1221	925.9 19	< 0.3	(3106)	< 0.06	533.40 6 ?	1/2+	> 7.3	2 nd non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1222	964.6 19	< 0.05	(3189)	< 0.007	449.80 18 ?	7/2-	> 8.2	1 st non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1223	986.8 19	0.41 8	(3237)	0.054 11	401.86 7	5/2-	7.32 9	1 st non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1224	995.1 19	0.28 8	(3255)	0.037 10	384.10 6	3/2-	7.49 13	1 st non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1225	1038.6 19	14.2 7	(3348)	1.61 8	290.52 5	5/2+	5.87 3	allowed		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1226	1088.8 19	< 0.2	(3456)	< 0.02	182.77 5 ?	3/2-	> 7.8	1 st non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1227	1104.6 19	< 0.2	(3490)	< 0.02	148.87 7 ?	9/2+	> 7.9	2 nd non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1228	1105.5 19	0.8 5	(3492)	0.08 5	147.05 6	5/2-	7.2 3	1 st non-unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1229	1113.6 19	10.9 12	(3509)	1.01 11	129.76 5	7/2+	6.11 5	allowed		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1230	1193.9 19	< 1.1	(3639)	< 0.23	0.0 ?	1/2-	> 8.5	1 st unique		$^{79}\text{Rb}_{42}$	22.9 min 5	0.0	5/2+	ec $\beta+$ 100 %	3640 4	$^{79}\text{Kr}_{43}$
1231	1534.3	1.8 3	(4399)	0.068 11	1321.1 7	0+	5.88 9	allowed		$^{80}\text{Rb}_{43}$	33.4 s 7	0.0	1+	ec $\beta+$ 100 %	5718.0 20	$^{80}\text{Kr}_{44}$
1232	1564.3	2.0 3	(4463)	0.071 10	1256.5 7	2+	5.87 8	allowed		$^{80}\text{Rb}_{43}$	33.4 s 7	0.0	1+	ec $\beta+$ 100 %	5718.0 20	$^{80}\text{Kr}_{44}$
1233	1871.3	21 3	4880 350	0.44 5	616.8 5	2+	5.19 8	allowed		$^{80}\text{Rb}_{43}$	33.4 s 7	0.0	1+	ec $\beta+$ 100 %	5718.0 20	$^{80}\text{Kr}_{44}$
1234	2168.3	73 3	5630 160	1.01 4	0.0	0+	4.93 6	allowed		$^{80}\text{Rb}_{43}$	33.4 s 7	0.0	1+	ec $\beta+$ 100 %	5718.0 20	$^{80}\text{Kr}_{44}$
1235		(582)		0.33 12	1743.61 11	(7/2)+	5.15 16	allowed		$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1236		(544)		0.0063 24	1781.8 5	7/2,9/2,11/2(+)	6.80 17			$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1237		(423)		0.0055 21	1902.6 6	7/2,9/2,11/2(+)	6.64 17			$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1238		(637)		0.022 8	1687.9 3	7/2,9/2,11/2(+)	6.40 16			$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1239		(643)		0.021 8	1682.7 4	7/2,9/2,11/2(+)	6.43 17			$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1240		(1119)		0.019 8	1206.44 20	(7/2)	6.96 19	allowed		$^{81}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1241		(1139)		< 0.06	1100.3 5 ?	5/2+	> 7.4	1 st non-unique		$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1242		(1000)		0.38 8	1239.05 8	(3/2)+	6.52 10	1 st non-unique		$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1243		(681)		0.6 5	1558.4 4 ?	1/2,3/2,5/2	6.0 4			$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1244		(561)		1.26 6	1678.04 6	1/2,-3/2-	5.485 23			$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1245		(494)		0.106 7	1744.86 12	(1/2)-	6.45 3	allowed		$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1246		(174)		0.059 5	2064.69 14	(1/2,3/2)-	5.75 5			$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1247	89 3	0.0028 4	(1213)	2.29 14	1025.64 4	3/2-,5/2-	5.91 3			$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1248	102 3	0.0090 11	(1245)	3.91 20	994.34 5	(1/2,3/2,5/2)-	5.696 23			$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1249	134 3	0.00194 20	(1319)	0.264 17	919.83 6	3/2-	6.92 3	allowed		$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1250	144 3	0.00055 20	(1344)	0.054 20	981.74 13	(9/2+)	6.67 16	allowed		$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1251	164 3	0.00060 24	(1391)	0.035 14	934.51 22	(11/2)+	6.88 17	allowed		$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1252	190 3	0.0007 3	(1452)	0.022 9	873.8 3	(11/2)+	7.12 17	allowed		$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1253	227 3	0.28 6	(1538)	4.7 9	700.86 6	(5/2)-	5.80 9	allowed		$^{81}\text{Rb}_{44}$	4.572 h 4	0.0	3/2-	ec $\beta+$ 100 %	2239 5	$^{81}\text{Kr}_{45}$
1254	250 3	0.0043 16	(1593)	0.050 18	731.86 11	(5/2)+	6.85 16	2 nd non-unique		$^{81m}\text{Rb}_{44}$	30.5 min 3	86.31 7	9/2+	ec $\beta+$ 2.4 6 %	2325.31 5	$^{81}\text{Kr}_{45}$
1255	254 3	1.82 10	1597 35	19.9 8	636.85 5	3/2-	5.211 19	allowed		$^{81}\text{Rb}_{44}$	4.572 h 4</					

#	$\leq E_{\beta+} \geq$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^{π}	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
1316		(119.9)	0.90 11	799.49 3	5/2+	6.87 6	1 st non-unique			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1317		(228.9)	0.137 17	690.53 4	5/2-	8.30 6	allowed			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1318		(348.2)	29.4 23	571.1538 10	(3/2-)	6.35 4	allowed			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1319		(357.4)	61 4	561.9586 8	5/2-	6.05 3	allowed			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1320		(910.0)	6 3	9.4057 6	7/2+	7.86 21	1 st non-unique			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1321		(919.4)	< 5.0	0.0	9/2+	> 8.5	1 st unique			⁸³ Rb ₄₆	86.2 d 1	0.0	5/2-	ec 100 %	920.0 23	⁸³ Kr ₄₇
1322		(789)	1.09 5	1897.784 10	2+	8.085 17	1 st non-unique			⁸⁴ Rb ₄₇	32.82 d 7	0	2-	ec $\beta+$ 96.1 20 %	2680.4 22	⁸⁴ Kr ₄₈
1323	340.5 13	12.6 7	781.5 13	56 3	881.615 3	2+	7.114 11	1 st non-unique		⁸⁴ Rb ₄₇	32.82 d 7	0	2-	ec $\beta+$ 96.1 20 %	2680.4 22	⁸⁴ Kr ₄₈
1324	758.5 14	13.1 7	1657.8 8	13.4 7	0	0+	9.509 19	1 st unique		⁸⁴ Rb ₄₇	32.82 d 7	0	2-	ec $\beta+$ 96.1 20 %	2680.4 22	⁸⁴ Kr ₄₈
1325		(518.65)	0.0052 7	0	0+	9.78 5	1 st unique			⁸⁶ Rb ₄₉	18.642 d 18	0.0	2-	ec 0.0052 5 %	518.67 20	⁸⁶ Kr ₅₀
1326		(10900)		3.23E3 20	(1/2-)	≈ 3.3				⁷³ Sr ₃₅	≈ 25 ms	0		ec $\beta+$ 100 %	14062 403	⁷³ Rb ₃₆
1327	1900 1200	5.1 16	(5100)	0.1 14	55E2 23	(1/2-, 3/2-, 5/2-)	3.2 16			⁷⁵ Sr ₃₇	88 ms 3	0.0	(3/2-)	ec $\beta+$ 100 %	10600 220	⁷⁵ Rb ₃₈
1328	4490 110	5.2 11	(10456)	0.010 2	144	(5/2-)	4.9 1	allowed		⁷⁵ Sr ₃₇	88 ms 3	0.0	(3/2-)	ec $\beta+$ 100 %	10600 220	⁷⁵ Rb ₃₈
1329	4560 110	89.4 14	(10600)	0.169 12	0	3/2(-)	3.7 1	allowed		⁷⁵ Sr ₃₇	88 ms 3	0.0	(3/2-)	ec $\beta+$ 100 %	10600 220	⁷⁵ Rb ₃₈
1330	1732 144	< 11	(4815.0)	< 0.3	1275 1 ?	(1+)	> 4.8	allowed		⁷⁶ Sr ₃₈	7.89 s 7	0.0	0+	ec $\beta+$ 100 %	6231 34	⁷⁶ Rb ₃₉
1331	1872 145	< 25	(5107.09)	< 1	982.87 14	(1+)	> 4.5	allowed		⁷⁶ Sr ₃₈	7.89 s 7	0.0	0+	ec $\beta+$ 100 %	6231 34	⁷⁶ Rb ₃₉
1332	2097 145	< 4.5	(5573.96)	< 0.1	516.0 2 ?	(1+)	> 5.5	allowed		⁷⁶ Sr ₃₈	7.89 s 7	0.0	0+	ec $\beta+$ 100 %	6231 34	⁷⁶ Rb ₃₉
1333	2116 145	< 67	(5613.15)	< 1	476.81 14	(1+)	> 4.3	allowed		⁷⁶ Sr ₃₈	7.89 s 7	0.0	0+	ec $\beta+$ 100 %	6231 34	⁷⁶ Rb ₃₉
1334	2055 4	2.4 6	(5486)	0.042 11	1541.2 5		5.7			⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1335	2196 4	0.6 3	(5778)	0.009 4	1249 3 ?		6.5			⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1336	2419 4	0.7 4	(6239)	0.008 4	788 3 ?		6.6			⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1337	2653 4	8.3 9	(6720)	0.073 8	307.03 4	(7/2+)	5.7	allowed		⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1338	2731 4	77 4	(6880)	0.62 3	146.937 20	5/2(+)	4.8	allowed		⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1339	2732 4	6.3 6	(6882)	0.051 5	144.83 3	5/2-	5.9	1 st non-unique		⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1340	2802 4	< 6	(7027)	< 0.04	0.0 ?	3/2-	> 5.9	1 st non-unique		⁷⁷ Sr ₃₉	9.0 s 2	0.0	5/2(+)	ec $\beta+$ 100 %	7027 8	⁷⁷ Rb ₄₀
1341	1665 4	≈ 7	(4674)	≈ 0.2	651.75 13	1/2-, 3/2-	≈ 6.1			⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1342	1760 4	≈ 9	(4873)	≈ 0.2	452.8 1	1/2-, 3/2-	≈ 6.1			⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1343	1803 4	≈ 11	(4963)	≈ 0.28	363.42 7	(5/2-)	≈ 6.0	allowed		⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1344	1806 4	≈ 5	(4969)	≈ 0.1	357.17 8	(1/2, 3/2, 5/2)	≈ 6.4			⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1345	1840 4	≈ 5	(5041)	≈ 0.1	285.33 7	1/2-, 3/2-	≈ 6.4			⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1346	1894 4	≈ 3	(5152)	≈ 0.07	174.28 8	(5/2-)	≈ 6.7	allowed		⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1347	1908 4	≈ 16	(5182)	≈ 0.35	144.41 5	3/2-	≈ 6.0	allowed		⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1348	1959 4	≈ 23	(5287)	≈ 0.46	39.41 5	(3/2-)	≈ 5.8	allowed		⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1349	1978 4	≈ 21	(5326)	≈ 0.41	0.0	5/2+	≈ 5.9	1 st non-unique		⁷⁹ Sr ₄₁	2.25 min 10	0.0	3/2(-)	ec $\beta+$ 100 %	5323 8	⁷⁹ Rb ₄₂
1350	116 4	0.14 3	(1276)	42 5	589.0 4	1+	4.32 6	allowed		⁸⁰ Sr ₄₂	106.3 min 15	0.0	0+	ec $\beta+$ 100 %	1864 4	⁸⁰ Rb ₄₃
1351	131 4	0.070 13	(1311)	12.0 13	553.5 4	1+	4.89 5	allowed		⁸⁰ Sr ₄₂	106.3 min 15	0.0	0+	ec $\beta+$ 100 %	1864 4	⁸⁰ Rb ₄₃
1352	266 4	0.27 5	(1629)	2.8 5	236.1 8 ?		5.70 7			⁸⁰ Sr ₄₂	106.3 min 15	0.0	0+	ec $\beta+$ 100 %	1864 4	⁸⁰ Rb ₄₃
1353	293 4	0.32 15	(16													

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}$ (abs) [%]	E_{EC} [keV]	I_{EC} (abs) [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
1412	529 3	11 3	(2231)	12 4	42.0780 20	9/2+	6.63 14	allowed		$^{83}\text{Sr}_{45}$	32.41 h 3	0.0	7/2+	ec $\beta+$ 100 %	2273 7	$^{83}\text{Rb}_{46}$
1413	548 3	12.4 11	(2273)	11.1 10	0.0	5/2-	6.66 4	1 st non-unique		$^{83}\text{Sr}_{45}$	32.41 h 3	0.0	7/2+	ec $\beta+$ 100 %	2273 7	$^{83}\text{Rb}_{46}$
1414		(113)		≤ 0.00003	951.0 5 ?	5/2+	≥ 11.2	2 nd non-unique		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1415		(196)		0.0123 7	868.06 3	7/2-	9.12 3	1 st non-unique		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1416		(550)		96 4	514.0084 19	9/2+	6.16 2	allowed		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1417		(783)		≤ 0.0005	280.98 6 ?	1/2-	≥ 11.8	3 rd unique		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1418		(913)		< 0.0012	151.18 3 ?	3/2-	> 11.6	3 rd non-unique		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1419		(1064)		< 8	0.0 ?	5/2-	> 8.5	1 st unique		$^{85}\text{Sr}_{47}$	64.849 d 7	0.0	9/2+	ec 100 %	1064.1 3	$^{85}\text{Rb}_{48}$
1420		(383)		0.0004 3	919.8 7	(3/2,5/2)-	8.1 4			$^{85m1}\text{Sr}_{47}$	67.63 min 4	238.79 5	1/2-	ec 13.4 4 %	1302.89 3	$^{85}\text{Rb}_{48}$
1421		(571)		0.0261 15	731.803 14	3/2-	6.62 4	allowed		$^{85m1}\text{Sr}_{47}$	67.63 min 4	238.79 5	1/2-	ec 13.4 4 %	1302.89 3	$^{85}\text{Rb}_{48}$
1422		(1022)		0.15 5	281.011 23	1/2-	6.38 13	allowed		$^{85m1}\text{Sr}_{47}$	67.63 min 4	238.79 5	1/2-	ec 13.4 4 %	1302.89 3	$^{85}\text{Rb}_{48}$
1423		(1152)		13.3 9	151.191 14	3/2-	4.53 4	allowed		$^{85m1}\text{Sr}_{47}$	67.63 min 4	238.79 5	1/2-	ec 13.4 4 %	1302.89 3	$^{85}\text{Rb}_{48}$
1424		(106.3)		0.30 8	0.0	3/2-	4.40 12	allowed		$^{87m1}\text{Sr}_{49}$	2.815 h 12	388.5287 23	1/2-	ec 0.30 8 %	106.2547 8	$^{87}\text{Rb}_{50}$
1425		(9153.9355637578859484)			1496	6+	> 5.4	allowed	$^{78m}\text{Sr}_{39-39}$	5.8 s 6	0+X	(5+)	ec $\beta+$ 100 %	11001 298	$^{78m}\text{Sr}_{40}$	
1426		(9866.9305448546057082)			783	4+	> 5.4	allowed	$^{78m}\text{Sr}_{39-39}$	5.8 s 6	0+X	(5+)	ec $\beta+$ 100 %	11001 298	$^{78m}\text{Sr}_{40}$	
1427		(10649.92503321187299000)		0.0	0+		3.49 7	super allowed		$^{78}\text{Sr}_{39-39}$	53 ms 8	0	(0+)	ec $\beta+$ 100 %	11001 298	$^{78m}\text{Sr}_{40}$
1428	2224 220	< 24.5	(5837)	< 0.5	1283.4 10		> 5.1			$^{79}\text{Sr}_{39-40}$	14.8 s 6	0.0	(5/2+)	ec $\beta+$ 100 %	7677 80	$^{79}\text{Sr}_{41}$
1429	2686 220	< 14	(6790)	< 0.1	329.9 1	(7/2+)	> 5.7	allowed		$^{79}\text{Sr}_{39-40}$	14.8 s 6	0.0	(5/2+)	ec $\beta+$ 100 %	7677 80	$^{79}\text{Sr}_{41}$
1430	2761 220	< 60.5	6940 450	< 0.5	177.4 1	(5/2+)	> 5.1	allowed		$^{79}\text{Sr}_{39-40}$	14.8 s 6	0.0	(5/2+)	ec $\beta+$ 100 %	7677 80	$^{79}\text{Sr}_{41}$
1431	2009 87	3.6	(5392)	0.08 0	3697.6 3	(3,4,5)	6.0			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1432	2164 87	0.9	(5713)	0.02 0	3377.1 3		6.8			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1433	2196 87	0.6	(5778)	0.01 0	3311.6 4		7.0			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1434	2209 87	2.6	(5806)	0.04 0	3283.96 19	(3+,4,5)	6.4			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1435	2267 88	0.7	(5927)	0.01 0	3163.0 3		7.0			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1436	2301 88	0.5	(5995)	0.01 0	3094.6 4		7.2			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1437	2318 88	1.8	(6032)	0.02 0	3058.07 17	(3,4,5+)	6.6			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1438	2367 88	1.4	(6132)	0.02 0	2958.26 19	(3,4,5+)	6.8			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1439	2426 88	1.5	(6253)	0.02 0	2836.5 3	(4)	6.8	allowed		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1440	2628 88	4.3	(6671)	0.04 0	2418.87 12	(3,4+)	6.5			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1441	2686 88	1.7	(6789)	0.02 0	2301.15 13	(3,4+)	6.9			$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1442	2688 88	3.1	(6794)	0.03 0	2296.27 16	(5+)	6.7	1 st non-unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1443	2704 88	0.81 8	(6826)		2492.53 13 ?	(0,1,2)	6.4			$^{80m1}\text{Y}_{39-41}$	4.8 s 3	228.5 1	(1-)	ec $\beta+$ 19 2 %	9391.5 7	$^{80}\text{Sr}_{42}$
1444	2914 88	6.8	(7257)	0.05 0	1832.55 10	(4+)	6.5	1 st non-unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1445	2939 87	< 5.4	(7326)	< 0.08	1763.80 23 ?	6+	> 8.6	1 st unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1446	2992 87	1.7	(7436)	0.03 0	1653.59 12	(2+)	9.1	1 st unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1447	3042 88	5.2	(7519)	0.03 0	1571.05 10	(3+)	6.7	1 st non-unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1448	3239 87	5.0	(7948)	0.06 0	1142.13 8	(2+)	8.9	1 st unique		$^{80}\text{Y}_{39-41}$	30.1 s 5	0	(4-)	ec $\beta+$ 100 %	9163 7	$^{80}\text{Sr}_{42}$
1449	3331 89	< 31	(8109)	< 0.2	980.70 10 ?	4+	> 6.1	1 st								

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	Jp_order	Decay	Q_{decay} [keV] see the note	Daught
1508	1104.4 24	14.5 7	(3487)	1.73 9	3270.01 23	(4,5,6)+	6.2			84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1509	1184.9 24	2.6 3	(3659)	0.26 3	3097.8 5	6(+)	7.1	allowed		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1510	1321.4 24	28 4	(3950)	2.0 3	2807.28 20	6+	6.2	allowed		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1511	1339.9 24	2.4 3	(3989)	0.17 2	2768.2 3	(5-)	7.3	1 st non-unique		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1512	1355.7 24	5.8 5	(4022)	0.38 3	2734.7 3	(5+)	7.0	allowed		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1513	1420.2 24	1.9 7	(4159)	0.11 4	2598.22 22 ?	(4+)	7.6	2 nd non-unique		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1514	1678.3 24	4.7 8	(4701)	0.17 3	2055.52 19 ?	(3+)	7.5	2 nd unique		84 $_{\text{Y}}^{44}$ 39-45	39.5 min 8	0.0	(6+)	ec $\beta+$ 100 %	6755 4	$^{84}_{\text{Sr}} 46$
1515	2318.3	30 10	(6031)	0.42 14	793.0 3	2+	4.6 2	allowed		84 $_{\text{mY}}^{44}$ 39-45	4.6 s 2	67.0 2	1+	ec $\beta+$ 100 %	6822 4	$^{84}_{\text{Sr}} 46$
1516	2703 3	69 10	(6824)	0.64 9	0	0+	4.5 1	allowed		84 $_{\text{mY}}^{44}$ 39-45	4.6 s 2	67.0 2	1+	ec $\beta+$ 100 %	6822 4	$^{84}_{\text{Sr}} 46$
1517		(152)		0.017 5	3129.1 5	(7/2,9/2,11/2+)	6.3 2			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1518		(192)		0.067 11	3088.6 4	(7/2,9/2,11/2+)	5.9 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1519		(205)		0.038 5	3075.3 4	(7/2,9/2-)	6.2 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1520		(218)		0.025 4	3063.2 4	(7/2,9/2,11/2)	6.4 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1521		(250)		0.063 8	3031.2 3	(7/2,9/2-)	6.2 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1522		(263)		0.036 17	3018.1 5	(7/2,9/2,11/2+)	6.5 2			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1523		(290)		0.048 6	2990.7 3	(7/2,9/2-)	6.4 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1524		(301)		0.133 14	2980.27 24	(7/2,9/2)	6.0 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1525		(306)		0.163 19	2975.25 20	(7/2,9/2-)	5.9 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1526		(466)		0.146 15	2814.4 3	(7/2,9/2,11/2+)	6.37 6			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1527		(471)		0.213 23	2810.03 23	(7/2,9/2+)	6.21 6			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1528		(499)		0.69 6	2782.03 15	(7/2,+9/2+)	5.75 6			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1529		(513)		0.084 12	2768.2 3	(7/2,9/2,11/2+)	6.7 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1530		(563)		0.037 5	2717.6 4	(7/2,9/2,11/2+)	7.1 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1531		(639)		0.81 7	2642.21 17	(7/2,9/2-)	5.90 5			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1532		(810)		0.049 6	2471.0 3	(7/2,9/2,11/2+)	7.33 6			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1533		(929)		5.0 4	2351.73 9	(7/2)+	5.44 4	allowed		85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1534		(1109)		7.8 6	2172.02 10	(7/2)+	5.41 4	allowed		85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1535		(1115)		1.33 11	2165.83 12	(7/2,+9/2+)	6.18 4			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1536		(1195)		0.67 6	2086.19 14	(7/2,+9/2,11/2+)	6.54 5			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1537	65 9	0.0023 18	(1157)	11.7 10	2123.78 9	(7/2)+	5.27 5	allowed		85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1538	98 8	0.00016 7	(1234)	0.115 19	2046.61 24	(9/2+)	7.3 1	allowed		85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1539	126 8	0.00036 14	(1299)	0.086 20	1982.1 4	(7/2,+9/2+)	7.5 1			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1540	152 8	0.0030 8	(1361)	0.32 4	1919.74 20	(7/2,9/2,11/2+)	6.98 6			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47$
1541	206 8	0.0015 8	(1487)	0.048 23	1793.68 19	(5/2,-7/2,9/2+)	7.9 2			85 $_{\text{mY}}^{44}$ 39-46	4.86 h 20	19.68 17	(9/2+)	ec $\beta+$ 100 %	3280.68 19	$^{85}_{\text{Sr}} 47</math$

#	$\leq E_{\beta+}$ [keV]	$I_{\beta+}(\text{abs})$ [%]	E_{EC} [keV]	$I_{EC}(\text{abs})$ [%]	Daughter level [keV]	J^π	Logft	Transition type	Comments	Parent	$T_{1/2}$	E_x [keV]	J_p order	Decay	Q_{decay} [keV] see the note	Daught
1604	2032 10	4.6 4	(5438)	0.11 1	855.5 3	(3/2)	6.1 1	allowed		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1605	2096 10	0.51 11	(5572)	0.011 2	722.2 3	(3/2-,5/2)	7.10 10			83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1606	2134 10	1.7 4	(5652)	0.034 8	642.4 3	(3/2,5/2-)	6.62 11			83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1607	2171 10	0.08 5	(5724)	0.003 2	570.4 3	(3/2+,5/2)	9.7 3			83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1608	2171 10	1.8 2	(5728)	0.034 4	565.5 3	(1/2-,3/2,5/2-)	6.6 1			83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1609	2172 10	0.98 10	(5729)	0.019 2	564.6 3	(1/2-,3/2,5/2-)	6.9 1			83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1610	2185 10	3.4 7	(5758)	0.065 13	536.40 24	(7/2-)	6.4 1	2 nd unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1611	2234 10	0.60 12	(5857)	0.011 2	436.8 3	(5/2)	7.2 1	2 nd non-unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1612	2241 10	10.3 9	(5872)	0.181 16	421.80 24	(3/2-)	5.9 1	allowed		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1613	2284 10	0.58 16	(5962)	0.022 6	331.60 25	(5/2+)	8.99 13	1 st unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1614	2364 10	1.5 13	(6127)	0.022 19	167.03 24	5/2-	6.9 4	2 nd non-unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1615	2375 10	0.30 8	(6149)	0.0044 12	144.88 24	7/2+	7.58 12	3 rd non-unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1616	2388 10	8.2 18	(6176)	0.12 3	117.58 24	(1/2-)	6.14 10	allowed		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1617	2396 10	1.6 5	(6197)	0.053 16	97.1 3	5/2+	8.67 13	1 st unique		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1618	2415 10	59 6	(6232)	0.84 9	62.02 24	3/2-	5.3 1	allowed		83 $\frac{\gamma}{\tau}_{43}$	42 s 2	0.0	(1/2-)	ec $\beta+$ 100 %	6294 20	83 $\frac{\gamma}{\tau}_{39-44}$
1619	432 9	0.11 2	(2008)	0.27 4	2660.3 5	(5/2+,7/2,9/2)	5.86 7			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1620	465 9	0.14 2	(2082)	0.26 4	2586.2 5	(7/2+,9/2)	5.90 7			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1621	535 9	0.66 7	(2239)	0.82 9	2429.3 4	(7/2+,9/2+)	5.48 5			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1622	543 9	0.29 3	(2257)	0.35 3	2411.3 7	(5/2,7/2,9/2)	5.86 5			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1623	570 9	0.90 8	(2318)	0.90 8	2349.6 4	(7/2+,9/2+)	5.47 4			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1624	595 9	0.12 4	(2374)	0.10 3	2293.9 4	(5/2,7/2,9/2)	6.4 2			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1625	635 9	3.2 2	(2464)	2.2 1	2204.1 3	(5/2+)	5.12 3	allowed		85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1626	749 9	0.17 4	(2714)	0.072 15	1954.1 5	(5/2+,7/2,9/2+)	6.7 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1627	776 9	0.20 4	(2775)	0.078 17	1892.9 5	(7/2+,9/2)	6.7 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1628	808 9	0.12 10	(2844)	0.04 3	1824.3 5?		7.0 4			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1629	832 9	0.06 4	(2896)	0.02 1	1772.1 5	7/2+,9/2+	7.3 3			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1630	854 9	0.22 9	(2944)	0.06 3	1724.1 4	5/2+	6.8 2	allowed		85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1631	862 9	0.31 5	(2962)	0.087 13	1706.3 6	(5/2+,7/2,9/2+)	6.7 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1632	898 9	0.38 6	(3041)	0.095 16	1627.3 4	(5/2+,7/2,9/2+)	6.7 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1633	950 9	0.36 9	(3154)	0.076 19	1514.0 4	(5/2+,7/2,9/2)	6.8 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1634	993 9	0.19 4	(3245)	0.034 8	1422.5 5		7.2 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1635	1006 9	0.20 9	(3275)	0.036 15	1393.0 4	(5/2,7/2,9/2+)	7.2 2			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1636	1045 9	0.69 10	(3357)	0.11 2	1310.7 4	(5/2+,7/2,9/2+)	6.71 7			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1637	1062 9	0.83 19	(3394)	0.13 3	1274.0 4	(5/2,7/2,9/2+)	6.7 1			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 100 %	4667 20	85 $\frac{\gamma}{\tau}_{39-46}$
1638	1088 9	4.8 4	(3450)	0.68 5	1218.0 4	(5/2+,7/2,9/2+)	5.94 4			85 $\frac{\gamma}{\tau}_{45}$	7.86 min 4	0.0	(7/2+)	ec $\beta+$ 1		

