

# **ELL 100 - Introduction to Electrical Engineering**

## **LECTURE 31: MAGNETIC CIRCUITS**

# INTRODUCTION

- A **magnetic circuit** is made up of one or more **closed loop** paths containing a **magnetic flux  $\phi$**  (= **magnetic field/flux density  $B$   $\times$  cross-sectional area  $A$** ).
- The **flux** is usually **generated** by **permanent magnets** or **electromagnets** and confined to a **path** by **magnetic cores** consisting of **ferromagnetic materials** like **iron**, although there **may be air gaps** or other materials in the path.
- Magnetic circuits are employed to efficiently channel magnetic fields in many **devices** such as **electric motors, generators, transformers, relays, solenoids, loudspeakers, hard disks, MRI machines**.

# APPLICATIONS

Motors



Generators



Transformers



Circuit  
Breakers

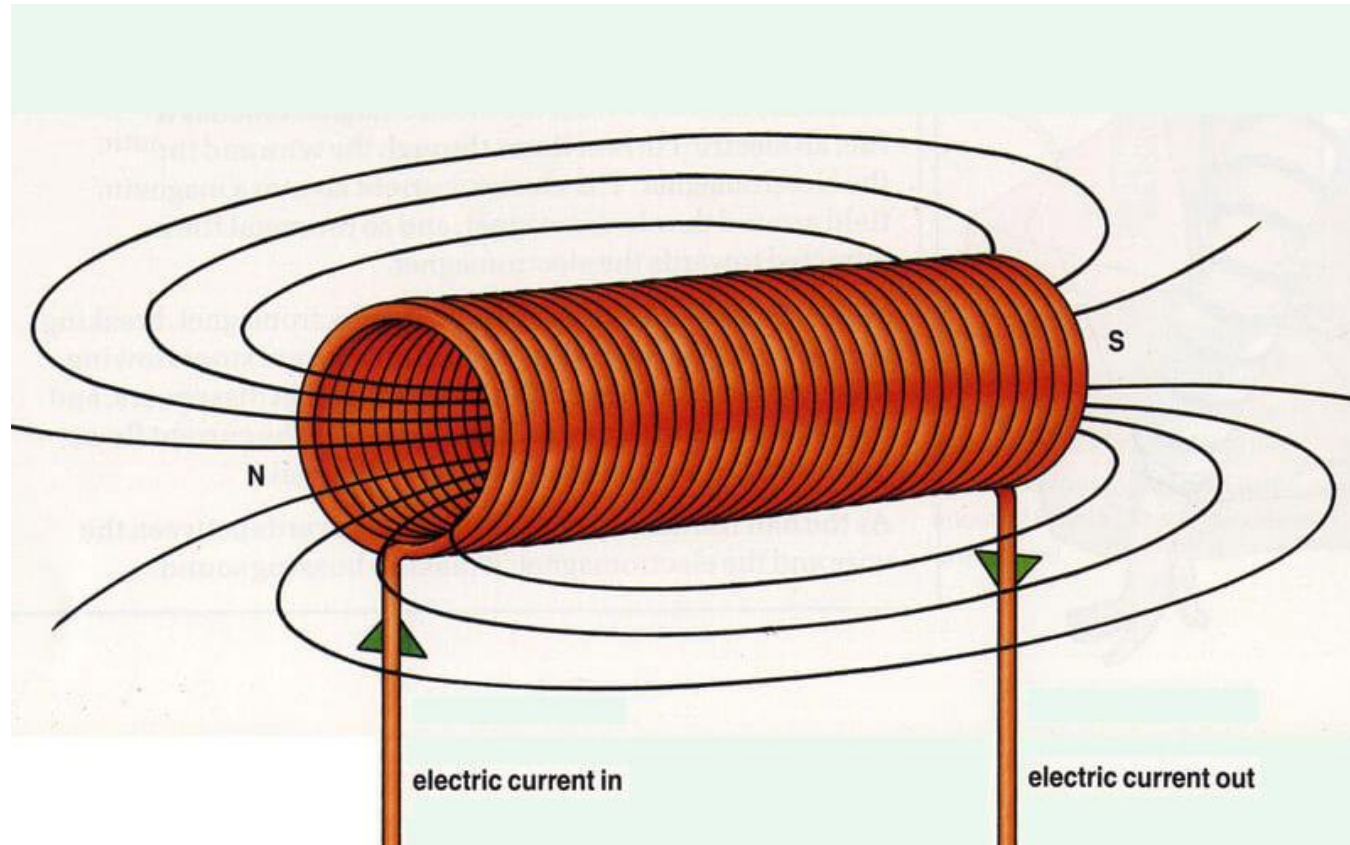


Relay  
Switches



# APPLICATIONS

## Solenoids



## Hard Disks



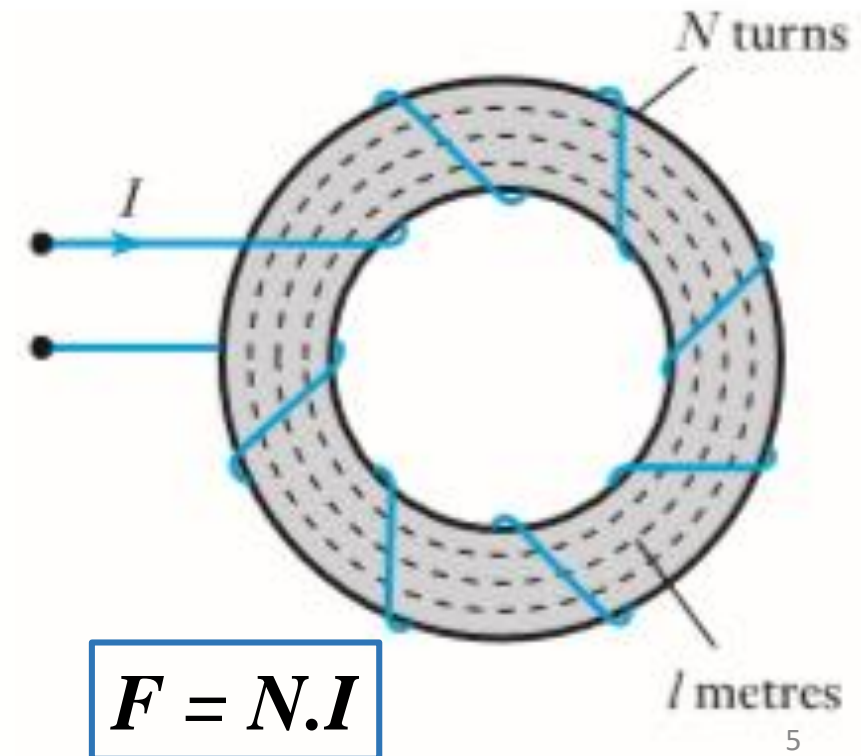
## MRI Machines





## Magnetomotive force (*mmf*)

- In an electric circuit, the current is induced due to the existence of an electromotive force (*emf*  $E$ , battery voltage). By analogy, we say that in a **magnetic circuit** the **magnetic flux** is **induced** due to the existence of a **magnetomotive force** (*mmf*  $F$ ) caused by a **current flowing through one or more turns of coil**.
- The value of the *mmf*  $F$  is **proportional** to the **current** flowing through the coil and to the **number of turns** in the coil, and is expressed in units of “**ampere-turns**” or just **amperes** (number of turns is dimensionless).



# Magnetic field strength/intensity ( $H$ )

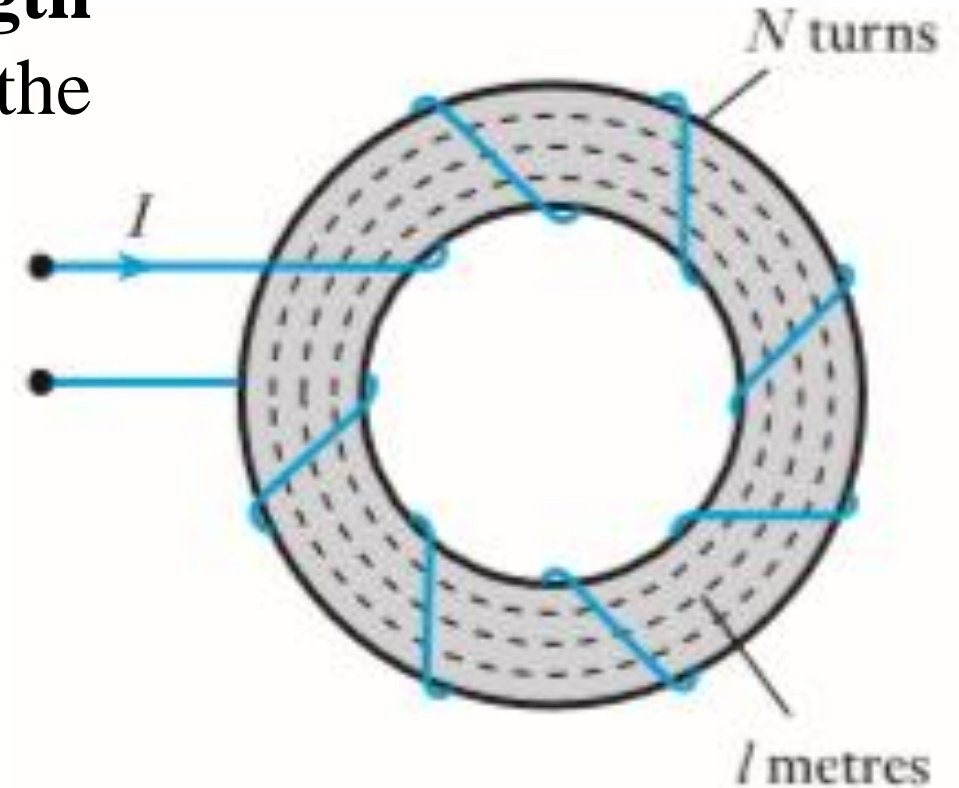
- The magnetomotive force per unit length of the magnetic circuit is termed the **magnetic field strength/intensity ( $H$ )**.

$$H = \frac{F}{l}$$

where,  $F = NI$  amperes

where  $l$  is the length of the magnetic circuit or flux loop

- **Units of  $H$  are ampere-turns per metre (At/m) or just ampere per metre (A/m)**



$$H = \frac{NI}{l} \text{ amperes per metre}$$

# Permeability of free space $\mu_0$ (magnetic constant)

The permeability of free space or non-magnetic materials is

$$\mu_0 = \frac{B}{H} \text{ for a vacuum and non-magnetic materials}$$

$$\mu_0 = 4\pi * 10^{-7} \text{ H / m} \text{ (The units of } \mu_0 \text{ are H/m (Henry per meter))}$$

where  $B$  ( $= \phi/A$ ) is the **magnetic flux density** (units of Tesla, T),

$A$  is the **cross-sectional area** through which the flux passes,

$\phi$  is the **magnetic flux** (units of Weber (Wb)) and

$H$  is the **magnetic field strength** (units A/m).

## SOLVED EXAMPLE

**Q.** A coil of 200 turns is wound uniformly over a wooden ring having a mean circumference of 600 mm and a uniform cross-sectional area of 500 mm<sup>2</sup>. If the current through the coil is 4.0 A, calculate (a) the magnetic field strength; (b) the flux density; (c) the total flux.

**Ans:**  $N = 200$ ,  $I = 4 \text{ A}$ ,  $l = 600 \text{ mm} = 0.6 \text{ m}$ ,  $A = 500 \text{ mm}^2 = 5 \times 10^{-4} \text{ m}^2$

(a)  $H = N.I / l = 200 \times 4 / 0.6 = 1333.3 \text{ A/m}$

(b)  $B = \mu_0 H = 4\pi \times 10^{-7} \times 1333.3 = 1.6755 \times 10^{-3} \text{ T} = 1.6755 \text{ mT}$

(c)  $\phi = B.A = 1.6755 \times 10^{-3} \times 5 \times 10^{-4} = 8.376 \times 10^{-7} \text{ Wb} = 0.8376 \text{ } \mu\text{Wb}$



## SOLVED EXAMPLE

**Q.** Calculate the magnetomotive force required to produce a flux of 0.015 Wb across an air-gap 2.5 mm long, having an effective area of 200 cm<sup>2</sup>.

**Ans:**  $\phi = 0.015$  Wb,  $l = 2.5$  mm =  $2.5 \times 10^{-3}$  m,  $A = 200$  cm<sup>2</sup> =  $2 \times 10^{-2}$  m<sup>2</sup>

$$B = \phi / A = 0.015 / (2 \times 10^{-2}) = 0.75 \text{ T}$$

$$H = B / \mu_0 = 0.75 / (4\pi \times 10^{-7}) = 5.97 \times 10^5 \text{ A/m}$$

$$F \text{ (mmf)} = H.l = 5.97 \times 10^5 \times 2.5 \times 10^{-3} = 1.49 \times 10^3 \text{ A}$$

## Relative Permeability $\mu_r$

- The **ratio of the flux density  $B$**  produced in a **material** to the flux density produced in **vacuum** (or in a non-magnetic core) for a particular applied magnetic field strength  $H$ .
- For air and **non-magnetic materials**,  $\mu_r = 1$
- For **ferromagnetic materials**, e.g. some forms of nickel–iron alloys, the relative permeability can be as large as  $\sim 100000$  i.e.  $\sim 10^6$ .
- For a material having a relative permeability  $\mu_r$ ,

$$B = \mu_r \mu_0 = \mu H$$

where,  $\mu = \mu_0 \mu_r$  is the absolute permeability

# Reluctance $S$

It is the opposition that a magnetic circuit offers to the passage of magnetic flux through it (**ratio of  $mmf$  applied to the flux induced**).

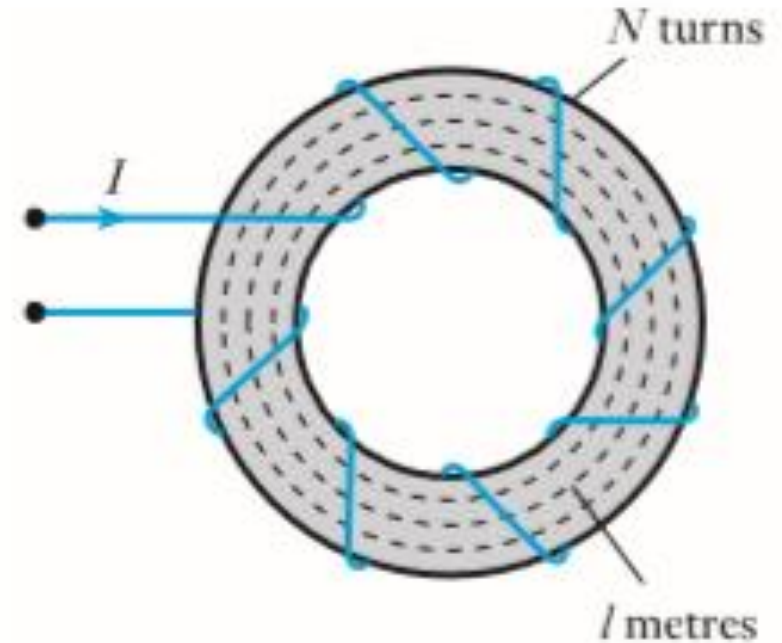
$$\phi = BA \quad (1)$$

$$mmf, F = Hl \quad (2)$$

Dividing (1) by (2),

$$\frac{\phi}{F} = \frac{BA}{Hl} = \frac{\mu_0 \mu_r HA}{Hl} = \mu_0 \mu_r \frac{A}{l}$$

Thus,  $S = F / \phi = l / (\mu A)$ , where  $\mu = \mu_0 \mu_r$  ( $S$  has units of A/Wb)



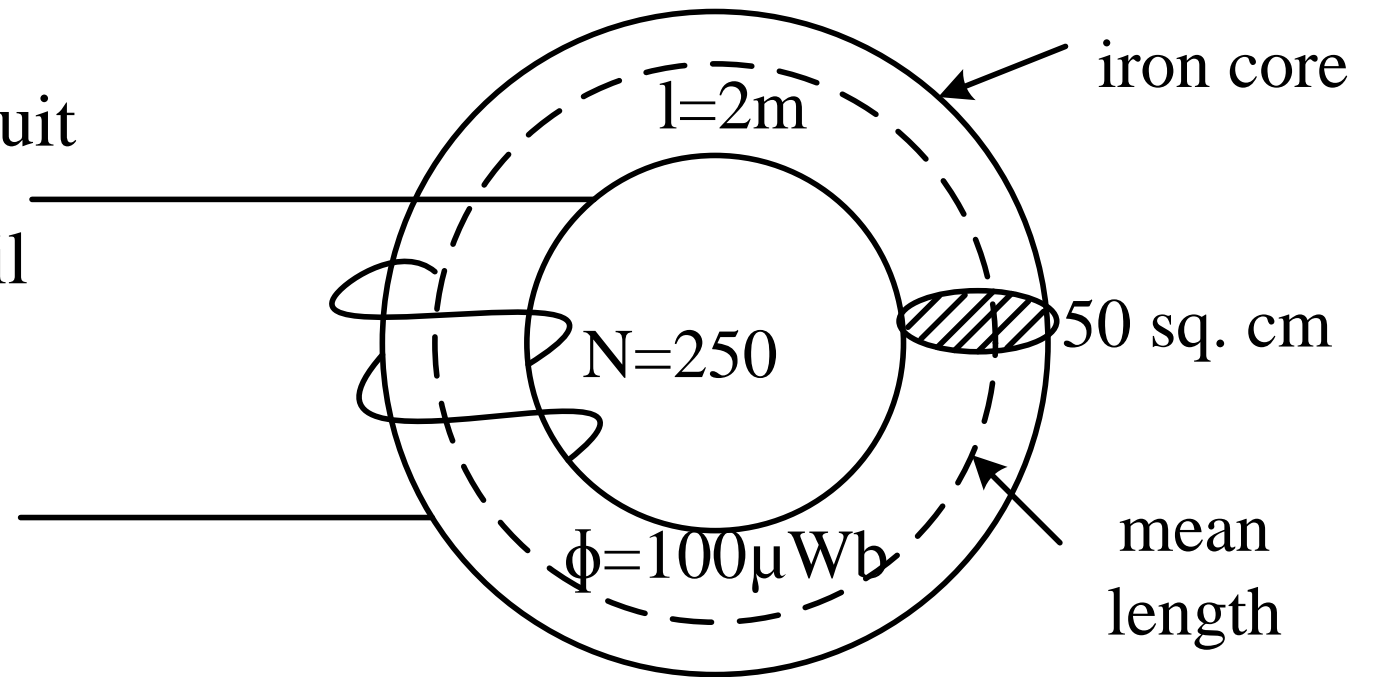
The **inverse** of reluctance is known as **permeance** (ease of flux passage)

## SOLVED EXAMPLE

**Q.** The simple magnetic circuit shown has a cross-sectional area of  $50 \text{ cm}^2$  and mean length of  $2 \text{ m}$ . The relative permeability of the core is  $100$ . The coil has  $250$  turns and the flux produced is  $100 \mu\text{Wb}$ .

Find:

- (a) Reluctance of the magnetic circuit
- (b) Current flowing through the coil



**Ans:**

(a) Reluctance,  $S = \frac{l}{\mu A}$

$$\mu = \mu_0 \mu_r = 4\pi * 10^{-7} * 100 = 4\pi * 10^{-5}$$

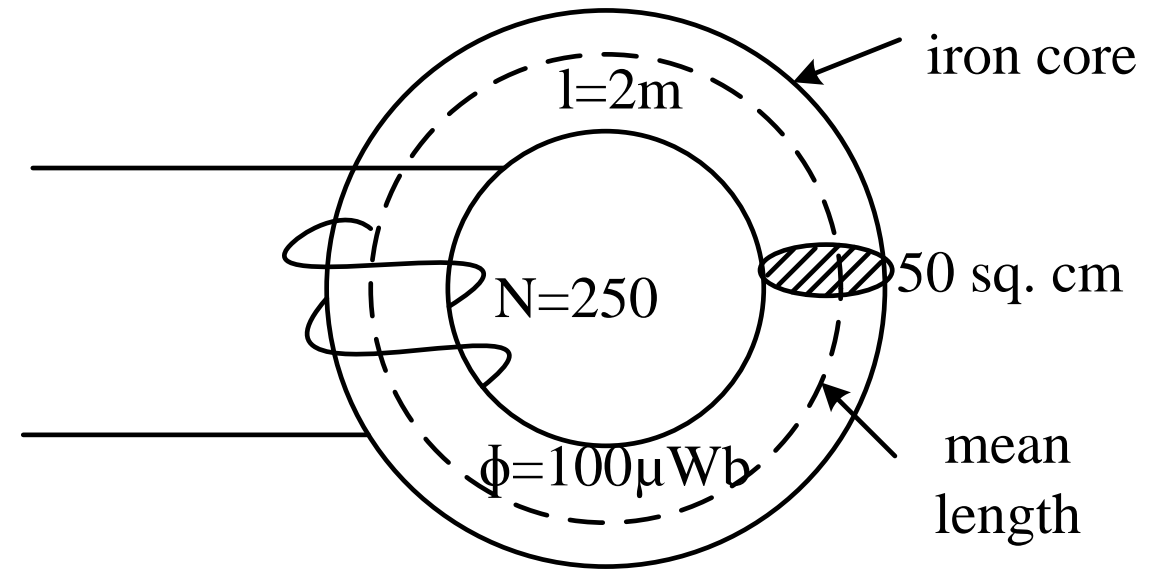
$$S = \frac{2}{4\pi * 10^{-5} * 50 * 10^{-4}} = 3.18 * 10^6 \text{ A / Wb}$$

(b) Magnetic field strength,  $H = \frac{mmf}{l} = \frac{NI}{l}$

$$I = \frac{Hl}{N}$$

$$H = \frac{B}{\mu} = \frac{\phi}{A\mu} = \frac{100 * 10^{-6}}{50 * 10^{-4} * 4\pi * 10^{-5}} = 159.15 \text{ A / m}$$

$$I = \frac{Hl}{N} = \frac{159.15 * 2}{250} = 1.27 \text{ A}$$





## SOLVED EXAMPLE

**Q.** The air gap in a magnetic circuit is 1.5 mm long and 2500 mm<sup>2</sup> in cross-sectional area. Calculate (a) The reluctance of the air gap (b) The *mmf* required to set up a flux of 800 μWb in the air gap.

**Ans:** (a) Reluctance,  $S = \frac{l}{\mu A}$

$$\mu = \mu_0 \mu_r = 4\pi * 10^{-7} * 1 = 4\pi * 10^{-7} \quad (\mu_r \text{ of air} = 1)$$

$$S = \frac{1.5 * 10^{-3}}{4\pi * 10^{-7} * 2500 * 10^{-6}} = 4.77 * 10^5 \text{ A / Wb}$$

$$(b) H = \frac{B}{\mu} = \frac{\phi}{A\mu} = \frac{800 * 10^{-6}}{2500 * 10^{-6} * 4\pi * 10^{-7}} = 2.55 * 10^5 \text{ A / m}$$

$$mmf = Hl = 2.55 * 10^5 * 1.5 * 10^{-3} = 382.5 \text{ A}$$

# EXERCISES

**Q.** A mild steel (relative permeability of 400) ring having a cross-sectional area of  $500 \text{ mm}^2$  and a mean circumference of 400 mm has a coil of 200 turns wound uniformly around it. Calculate (a) The reluctance of the ring  
(b) The current required to produce a flux of  $800 \mu\text{Wb}$  in the ring.

**Q.** A rectangular shaped core is made of mild steel (relative permeability of 940) plates  $15 \text{ mm} \times 20 \text{ mm}$  cross-section. The mean length of the magnetic path is 18 cm. The exciting coil has 300 turns with a current of 0.7 A flowing through it. Calculate:

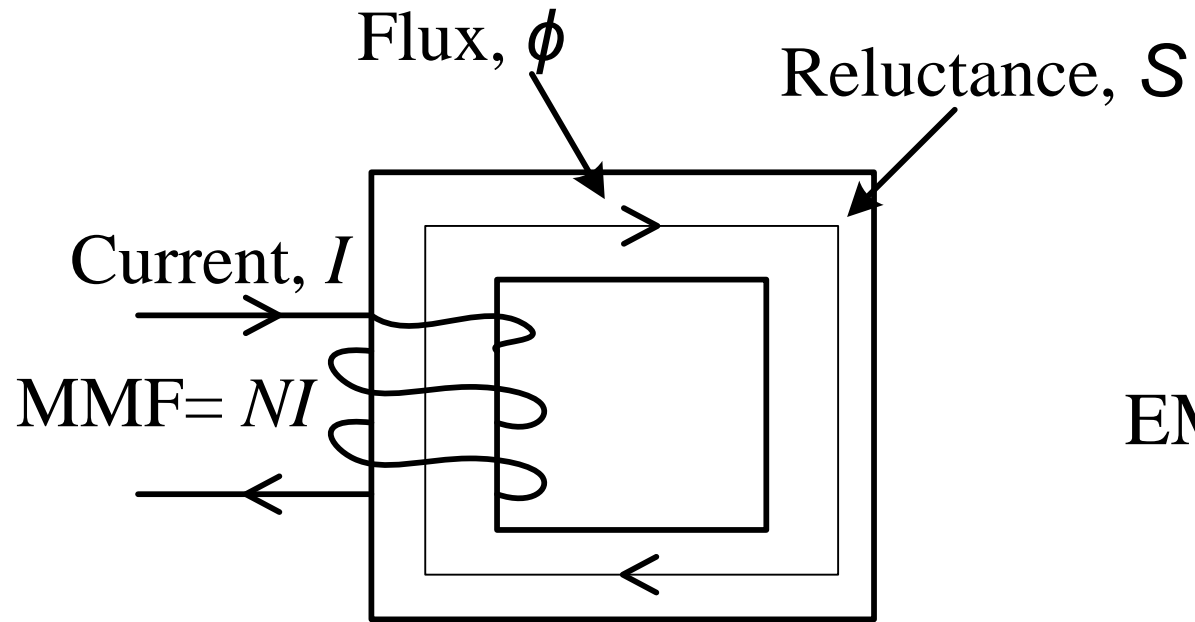
(a) Magneto-motive force

(b) Flux density

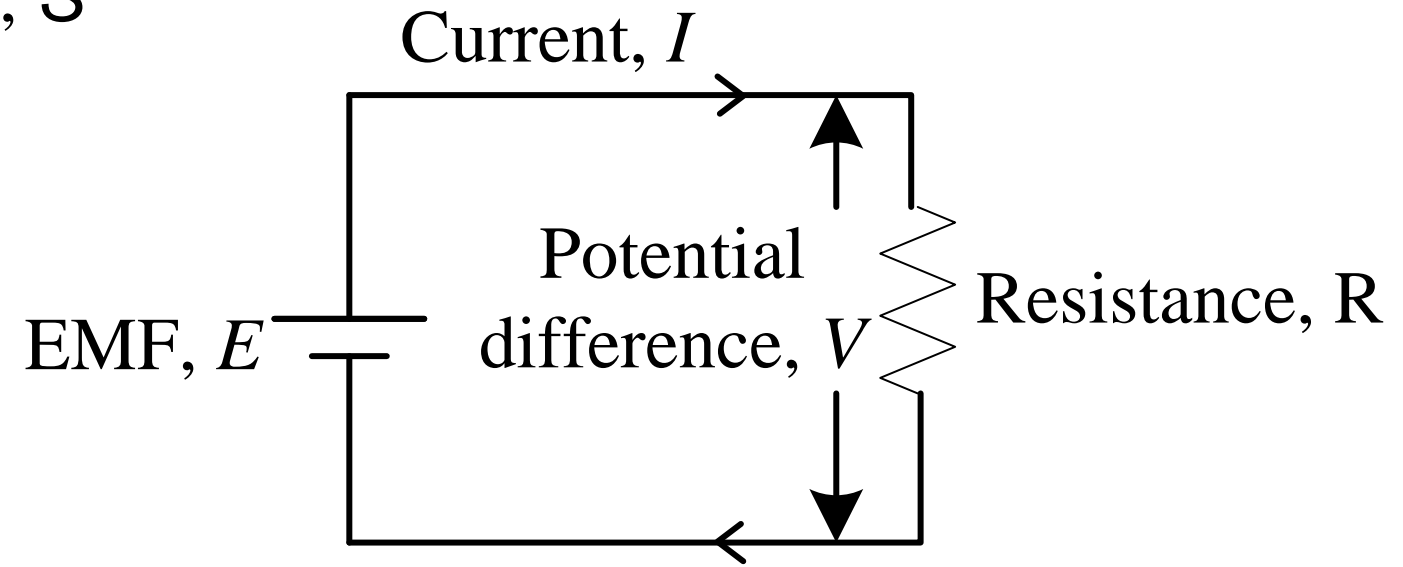
(c) Reluctance

(d) Magnetic flux

# MAGNETIC CIRCUIT ANALOGY WITH ELECTRICAL CIRCUIT



Magnetic circuit



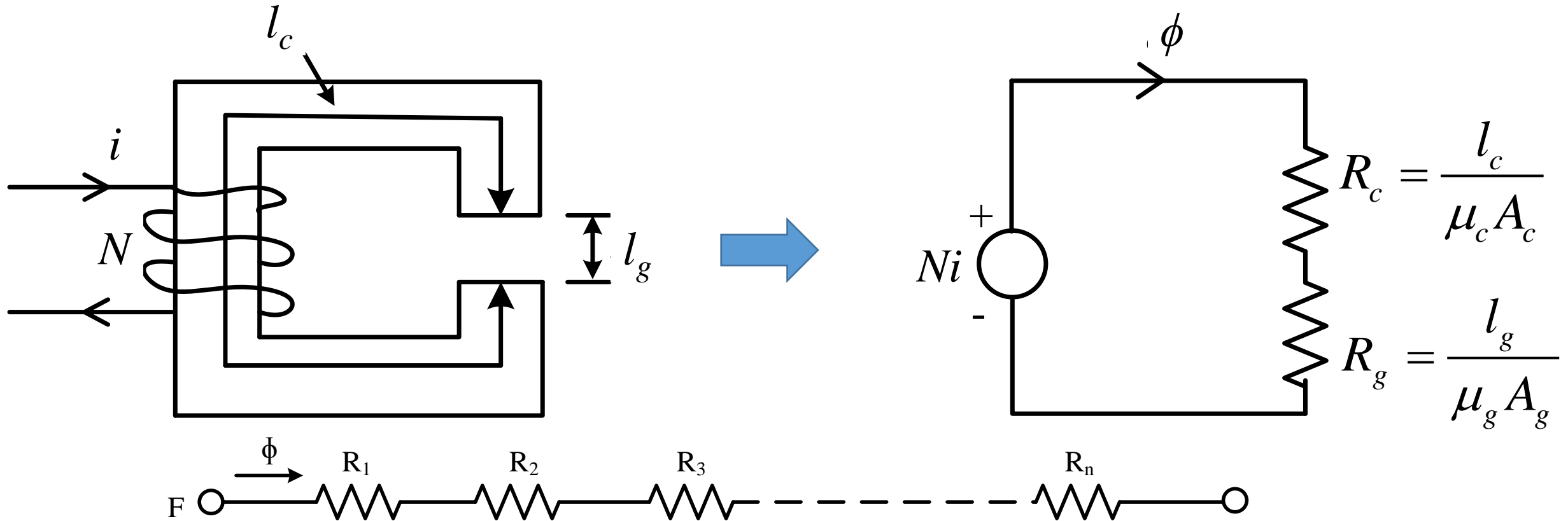
Analogous electrical circuit

# MAGNETIC CIRCUIT ANALOGY WITH ELECTRICAL CIRCUIT

S.No	Magnetic circuit quantity	Electrical circuit quantity
1	Magnetic flux density $\mathbf{B}$ (T = Wb/m <sup>2</sup> )	Current density $\mathbf{J}$ (A/m <sup>2</sup> )
2	Magnetic flux $\phi$ (Wb)	Current $\mathbf{I}$ (A)
3	Magnetic field intensity $\mathbf{H}$ (A/m)	Electric field intensity $\mathbf{E}$ (V/m)
4	m.m.f. $\mathbf{F}$ (A)	e.m.f. $\mathbf{E}$ (V)
5	Reluctance $\mathbf{S}$ (A/Wb)	Resistance $\mathbf{R}$ ( $\Omega$ = V/A)
6	Permeance (H = Wb/A)	Conductance (S = A/V)
7	Permeability $\mu$ (H/m)	Conductivity $\sigma$ (S/m)

# SERIES CONNECTION IN MAGNETIC CIRCUIT

The applied *mmf* is equal to the sum of the *mmfs* dropped across each series element, while the flux through each series element is the same.

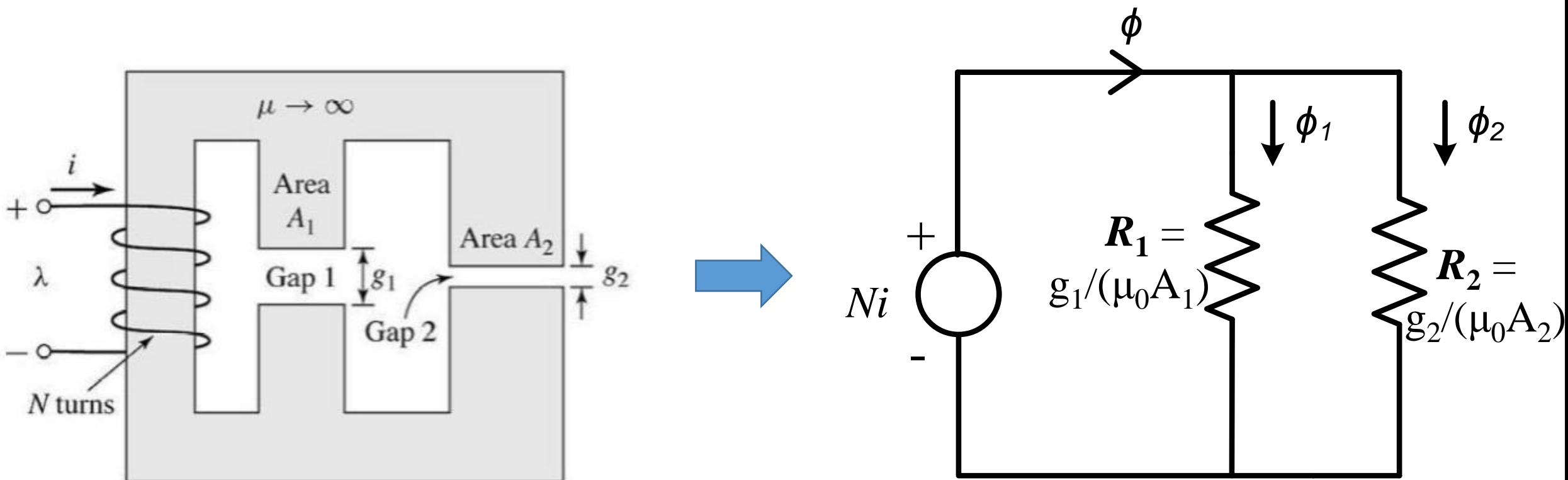


$$F = \phi R_{eq} = \phi (R_1 + R_2 + R_3 + \dots + R_n) \quad (R_i \text{ denote reluctances})$$



# PARALLEL CONNECTION IN MAGNETIC CIRCUIT

The same  $mmf$  appears across all the reluctances in parallel, while the total flux is the sum of the individual fluxes in each parallel element.



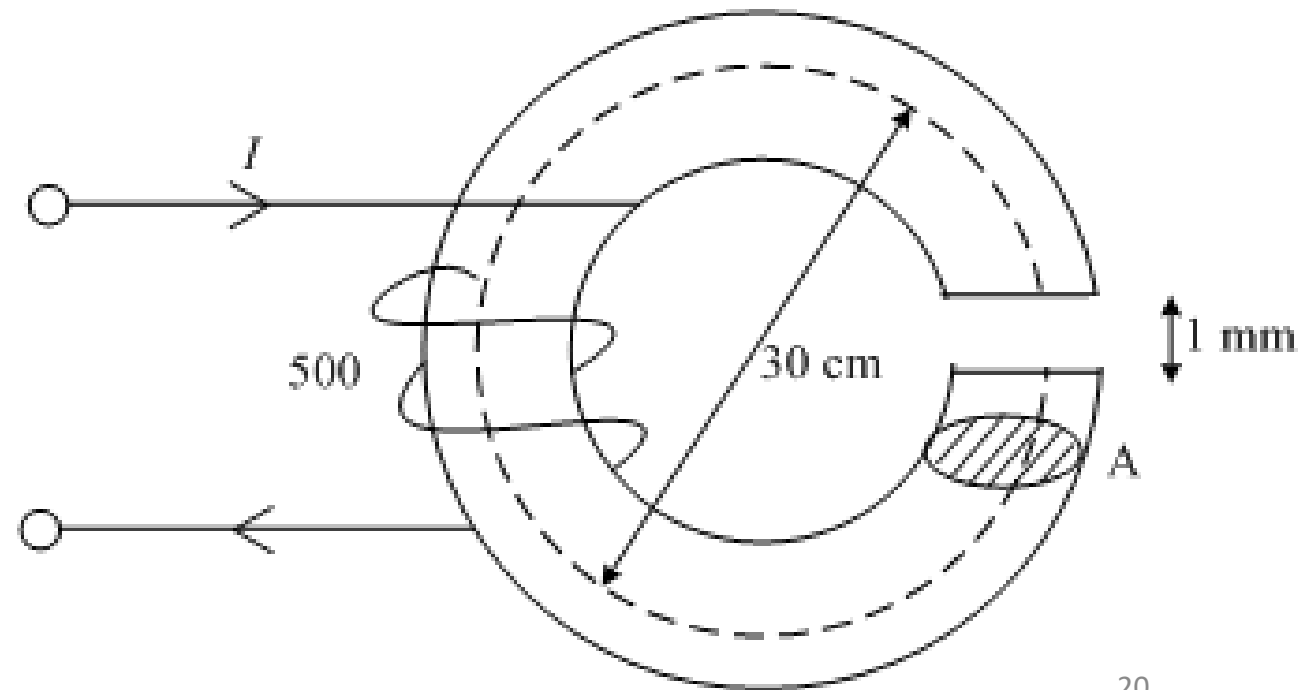
$$F = \phi R_{eq} \text{ where } R_{eq} = R_1 // R_2 = R_1 R_2 / (R_1 + R_2)$$

## SOLVED EXAMPLE

**Q.** A ring of 30-cm mean diameter is made using a cylindrical iron rod of diameter 2.5 cm. A saw-cut 1-mm wide is made through the ring to create an air-gap. A coil with 500 turns of wire is wound on the ring. Calculate the current required in the exciting coil to produce a flux of 4 mWb in the ring. Assume the relative permeability of iron at this flux density as 800. Neglect any leakage or fringing of the magnetic field.

**Ans:**  $A = \pi r^2 = 3.14 \times (0.025 \text{ m})^2$   
 $= 4.91 \times 10^{-4} \text{ m}^2$

$$\begin{aligned}\Rightarrow B &= \phi / A \\ &= (4 \times 10^{-3} \text{ Wb}) / (4.91 \times 10^{-4} \text{ m}^2) \\ &= 8.15 \text{ Wb/m}^2\end{aligned}$$



**First consider air gap:**

$$H_1 = B / \mu_0 = 8.15 / (4\pi \times 10^{-7}) \text{ A/m}$$
$$= 6.49 \times 10^6 \text{ A/m}$$

$$l_1 = 1 \text{ mm} = 10^{-3} \text{ m}$$

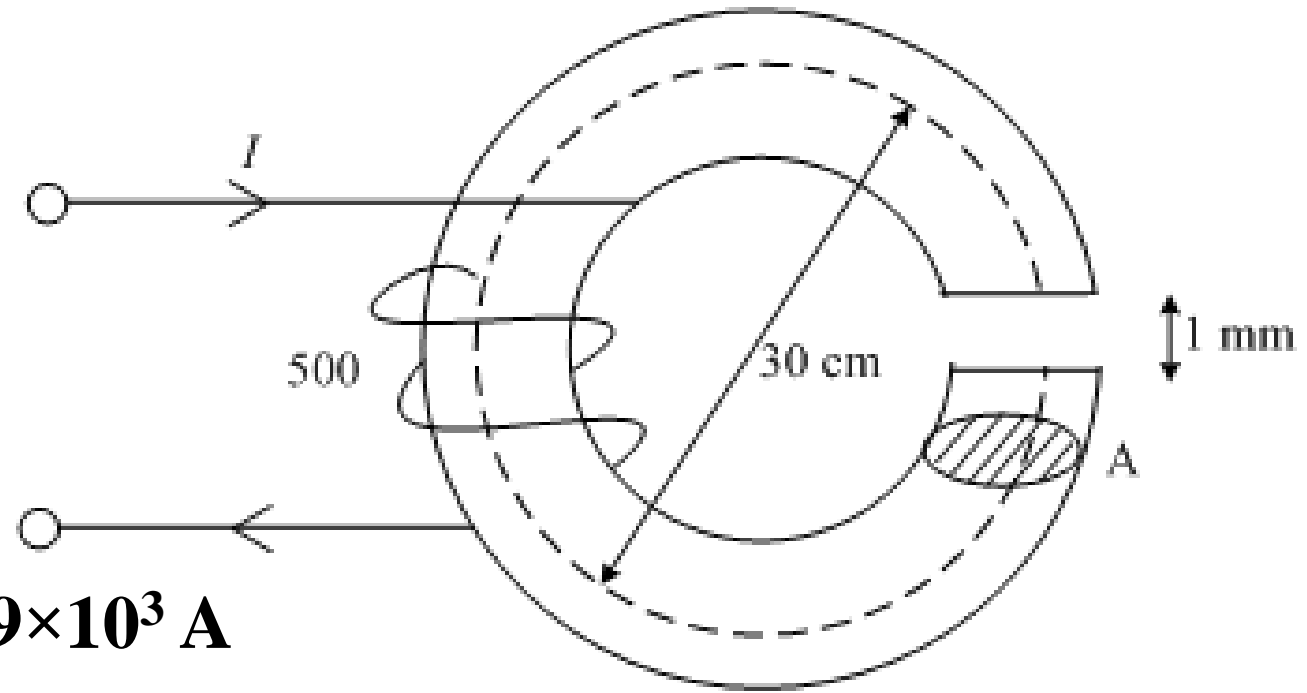
$$\Rightarrow \text{mmf across air gap } F_1 = H_1 l_1 = \mathbf{6.49 \times 10^3 \text{ A}}$$

**Now consider iron ring:**

$$H_2 = B / (\mu_r \mu_0) = 8.15 / (800 \times 4\pi \times 10^{-7}) \text{ A/m}$$
$$= 8.1 \times 10^3 \text{ A/m}$$

$$l_2 \sim 2\pi R = 2 \times 3.14 \times 0.15 \text{ m} = 0.94 \text{ m}$$

$$\Rightarrow \text{mmf across iron ring } F_2 = H_2 l_2 = \mathbf{7.63 \times 10^3 \text{ A}}$$



$$\text{Total mmf } F = F_1 + F_2$$
$$= \mathbf{1.41 \times 10^4 \text{ A}}$$

$$\Rightarrow \text{Current } I = F / N$$
$$= (1.41 \times 10^4) / 500 = \mathbf{28.24 \text{ A}}$$

## SOLVED EXAMPLE

**Q.** An iron ring of mean circumference 50-cm has an air gap of 0.1-cm length and a winding of 300 turns. If the relative permeability of iron is 400 when a current of 1 ampere flows through the coil, find the flux density in the air gap.

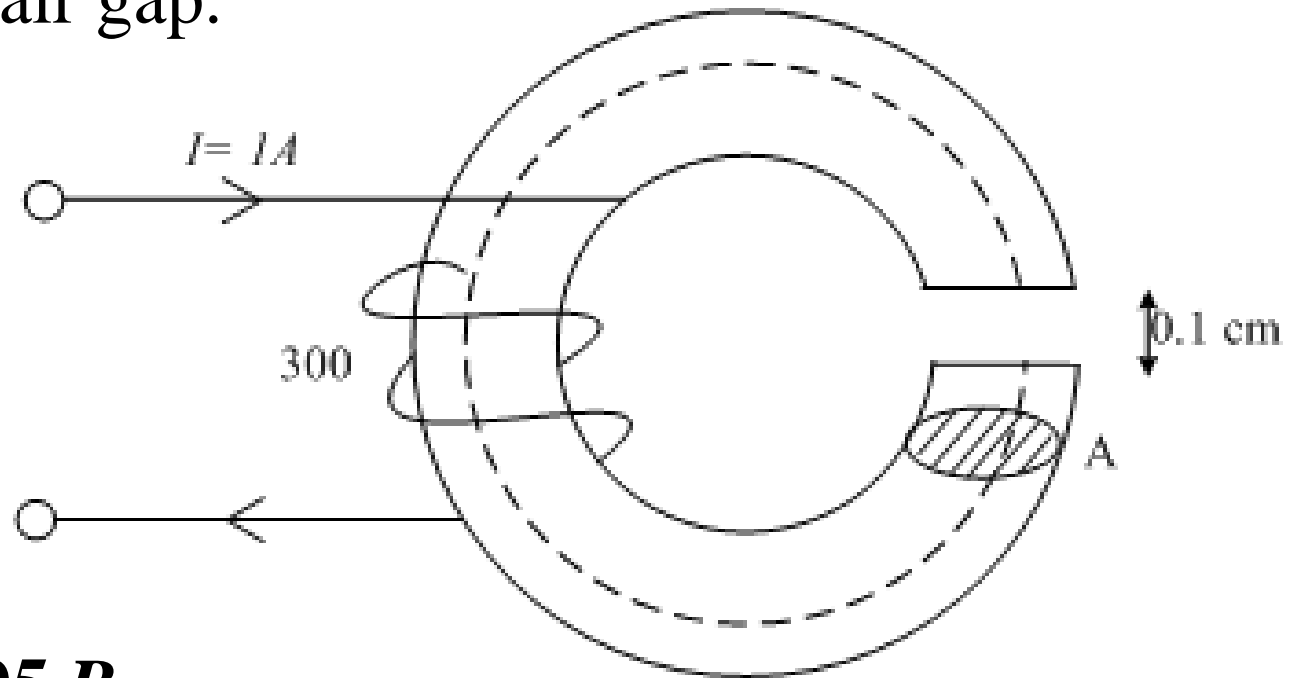
**Ans:** Let  $B$  be the flux density in the iron ring. Its value would also be the same in the air gap.

**First consider iron ring:**

$$H_1 = B / (\mu_r \mu_0) = B / (400 \times 4\pi \times 10^{-7})$$
$$= 1989.44 B$$

$$l_1 = 50 \text{ cm} = 0.5 \text{ m}$$

$$\Rightarrow \text{mmf across iron ring } F_1 = H_1 l_1 = \mathbf{995 B}$$



**Now consider air gap:**

$$H_2 = B / \mu_0 = B / (4\pi \times 10^{-7})$$
$$= 7.96 \times 10^5 B$$

$$l_2 = 0.1 \text{ cm} = 10^{-3} \text{ m}$$

$\Rightarrow$  *mmf* across air gap

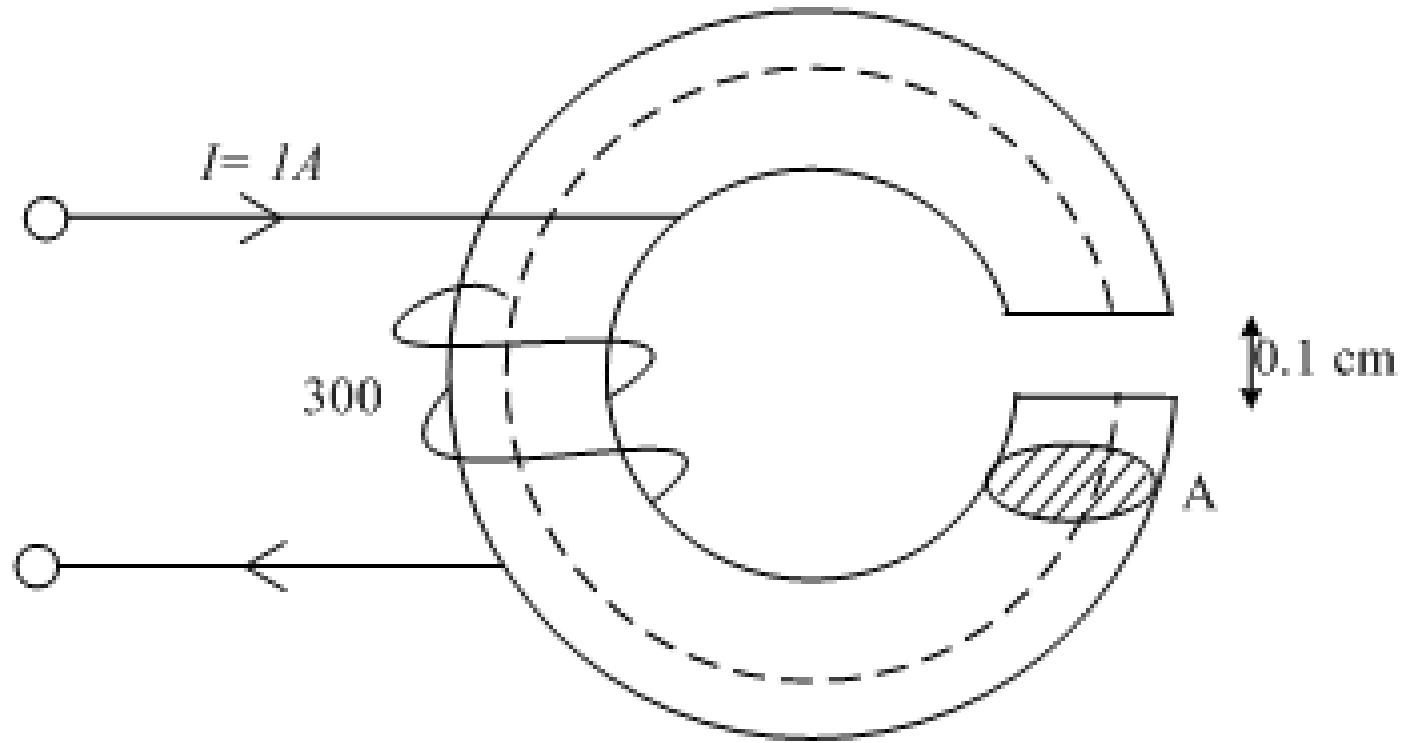
$$F_2 = H_2 l_2 = \mathbf{796 B}$$

**Total *mmf*  $F = F_1 + F_2$**

$$= (995 + 796)B = \mathbf{1791 B}$$

**But given total *mmf*  $F = N.I = 300 \times 1 = 300$**

$$\Rightarrow \boxed{B} = 300/1791 = \boxed{\mathbf{0.1675 \text{ Wb/m}^2}}$$





## EXERCISES

**Q.** An iron ring of mean circumference 50 cm has an air gap of 1 mm. It is uniformly wound with a coil having 200 turns. If the relative permeability of iron is 300 when a current of 1 A flows through the coil, calculate the flux density in the air gap. Neglect leakage and fringing.

**Q.** A current of 3 A flows through a coil of 1000 turns uniformly wound on an iron ring having a mean circumference of 40 cm and a cross-sectional area of 4 cm<sup>2</sup>. The relative permeability of the iron is 80. Calculate: (a) the magnetomotive force (b) the magnetic field strength (c) the flux density (d) the flux.

**Q.** A coil of wire wound up like a solenoid consists of 50 turns and carries a current of 5 A. If the length of the solenoid is 20 cm, calculate: (a) magnetic field intensity and (b) flux density within the solenoid coil.

## EXERCISES

**Q.** A coil having 200 turns and carrying a current of 3 A is wound uniformly over a toroidal ring with a mean circumference of 20 cm and cross-section of 5 cm<sup>2</sup>. The material of the ring has  $\mu_r = 1000$ . Calculate: (i) magnetic field strength (ii) flux density (iii) total flux.

**Q.** The mean length of a magnetic circuit is 40 cm with cross-sectional area 8 cm<sup>2</sup> and relative permeability of the core material being 200. When a magnetizing coil carries a current of 6 A, the magnetic flux produced in the core is 3 mWb. Find: (i) reluctance of the magnetic circuit (ii) flux density in the core (iii) magnetic field intensity (iv) number of turns of the coil.

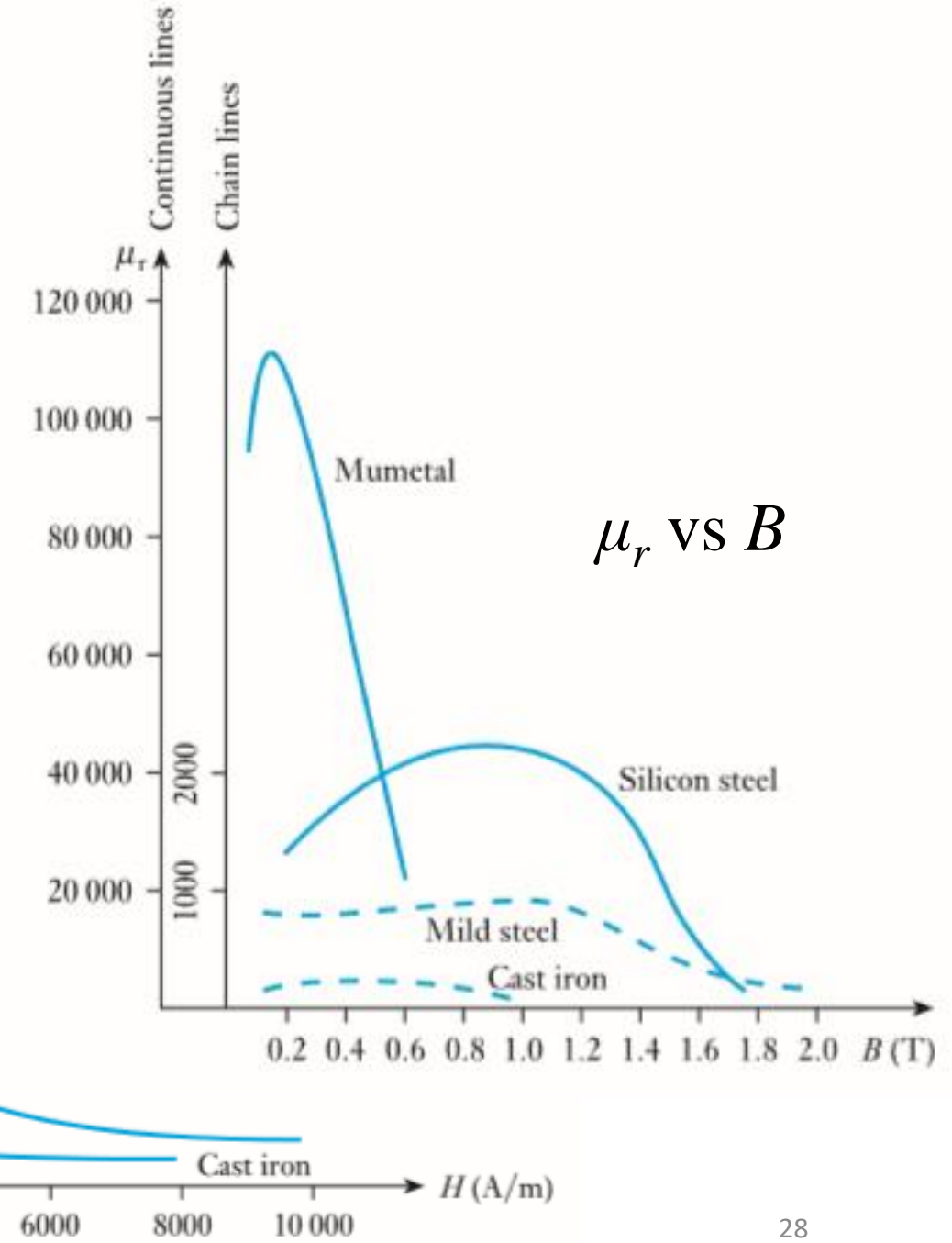
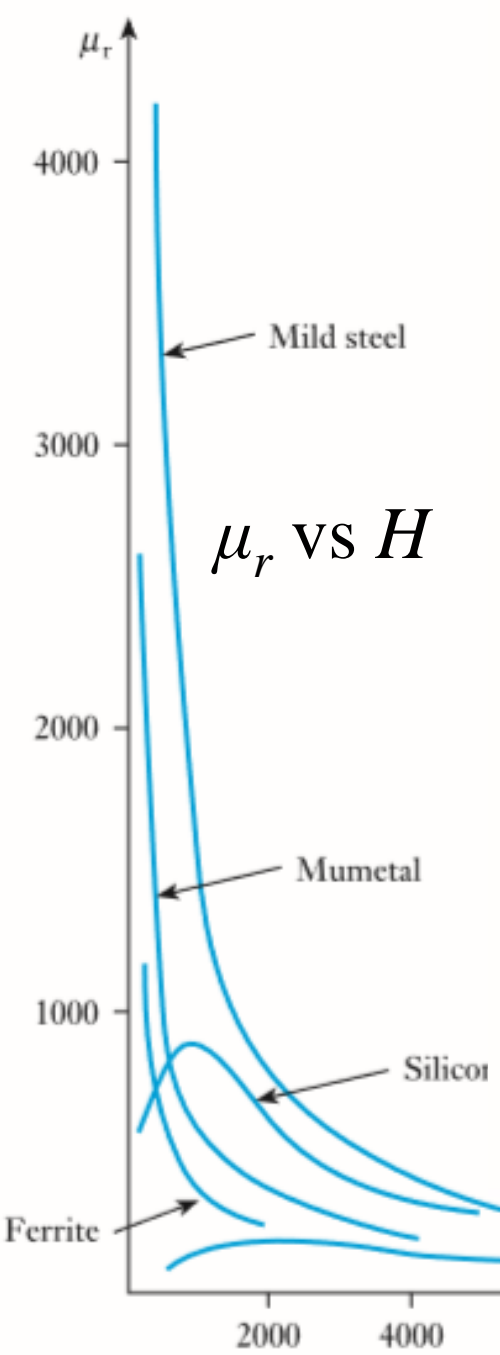
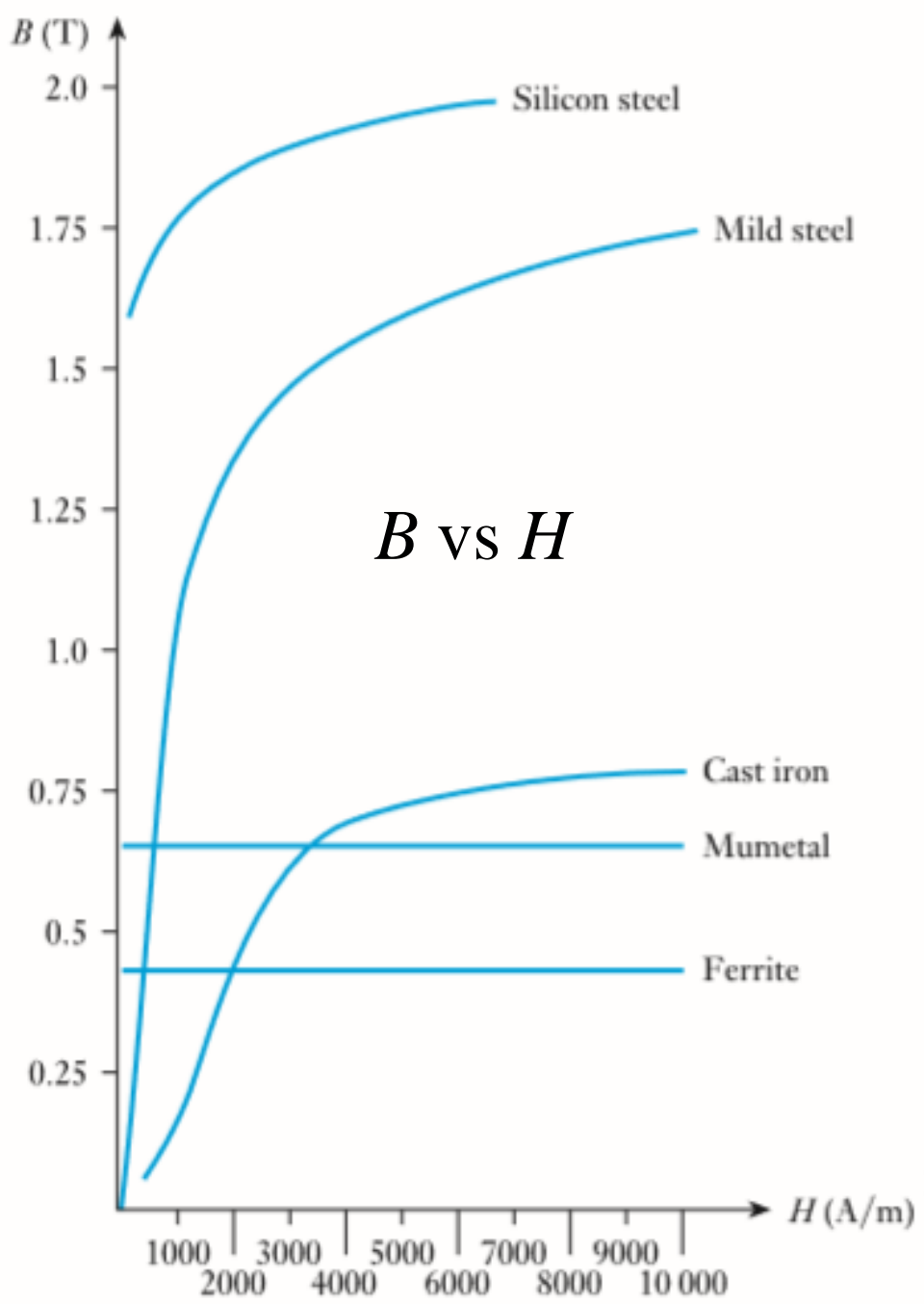
## EXERCISES

**Q.** A magnetic circuit has cross-sectional area of  $50 \text{ cm}^2$  and mean length of  $2 \text{ m}$ . The relative permeability of core material is  $80$ . Calculate the reluctance of the magnetic circuit if the magnetizing coil has  $150$  turns and the core flux is  $80 \text{ } \mu\text{Wb}$ . What is the value of the current flowing in the coil?

**Q.** A mild steel ring having a cross-sectional area of  $5 \text{ cm}^2$  and a mean circumference of  $40 \text{ cm}$  has a coil of  $200$  turns wound uniformly around it. Calculate (i) the reluctance of the ring (ii) the current required to produce a flux of  $800 \text{ } \mu\text{Wb}$  in the ring. Assume relative permeability of mild steel to be  $380$  at the flux density developed in the core.

# ***B-H* CURVE**

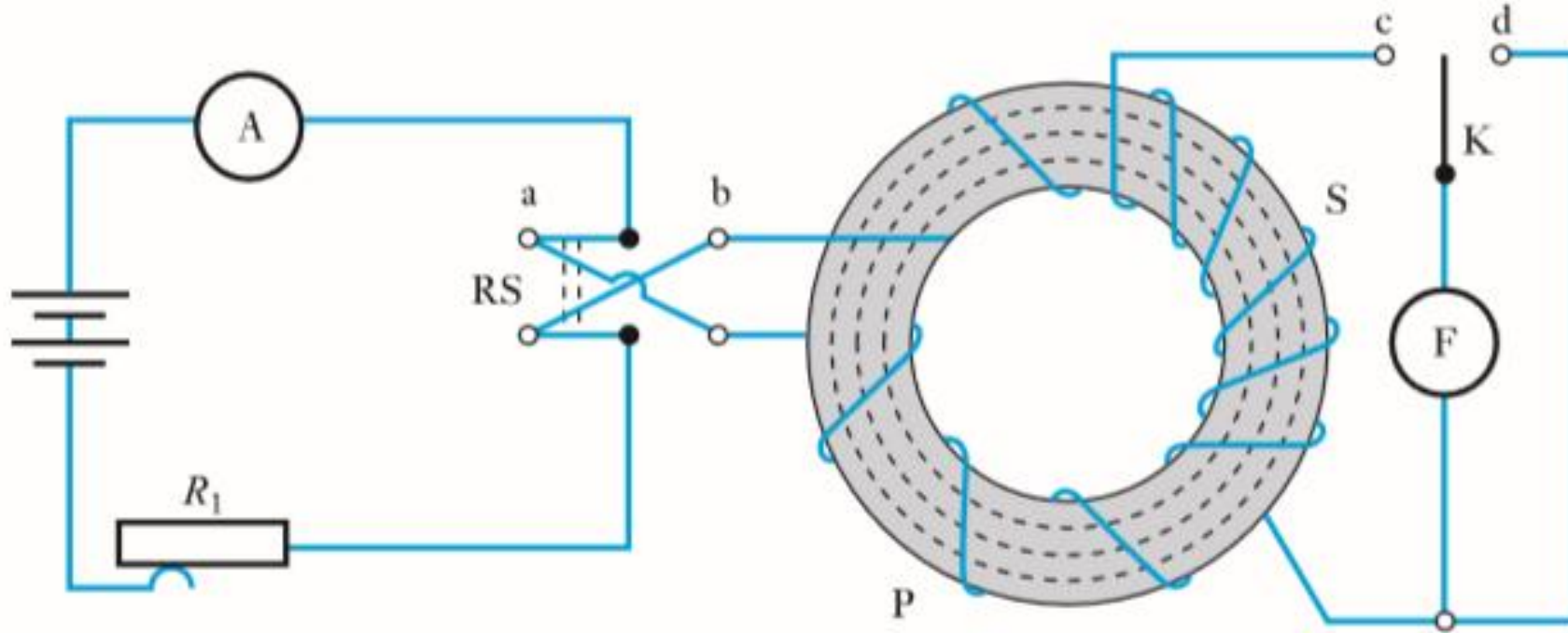
- The ***B-H*** or **magnetization curve** gives the **relation** between **flux density *B*** and **field intensity *H***.
- It is **not a straight line** (as naively expected from the relation  $B = \mu H$ ) and is actually **non-linear** as the permeability  $\mu$  typically **depends** on the applied field strength ***H***.
- The complete ***B-H* curve** is usually described as a **hysteresis loop**. The **area contained within** a hysteresis **loop** indicates the **energy required** to perform the '**magnetize - demagnetize**' process.





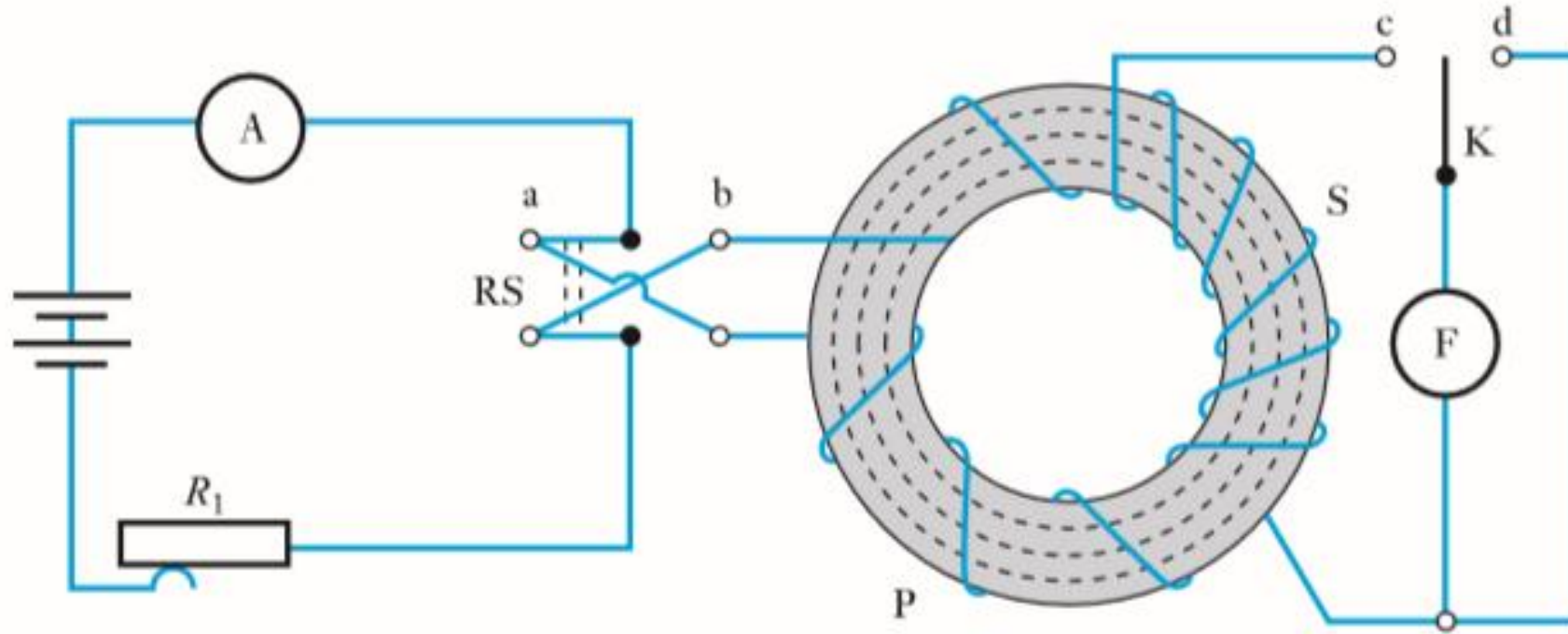
# Experimental Determination of $B$ - $H$ Curve

By means of a **fluxmeter**  $F$  to measure the induced flux  $\phi$  (and thus flux density  $B$ ), for a given applied field intensity  $H$  (through applied current  $I$ )



**Fluxmeter** is a special type of permanent-magnet moving-coil **instrument** that gives a **deflection** of its needle **proportional** to the **flux** measured through the **coil connected** to it.

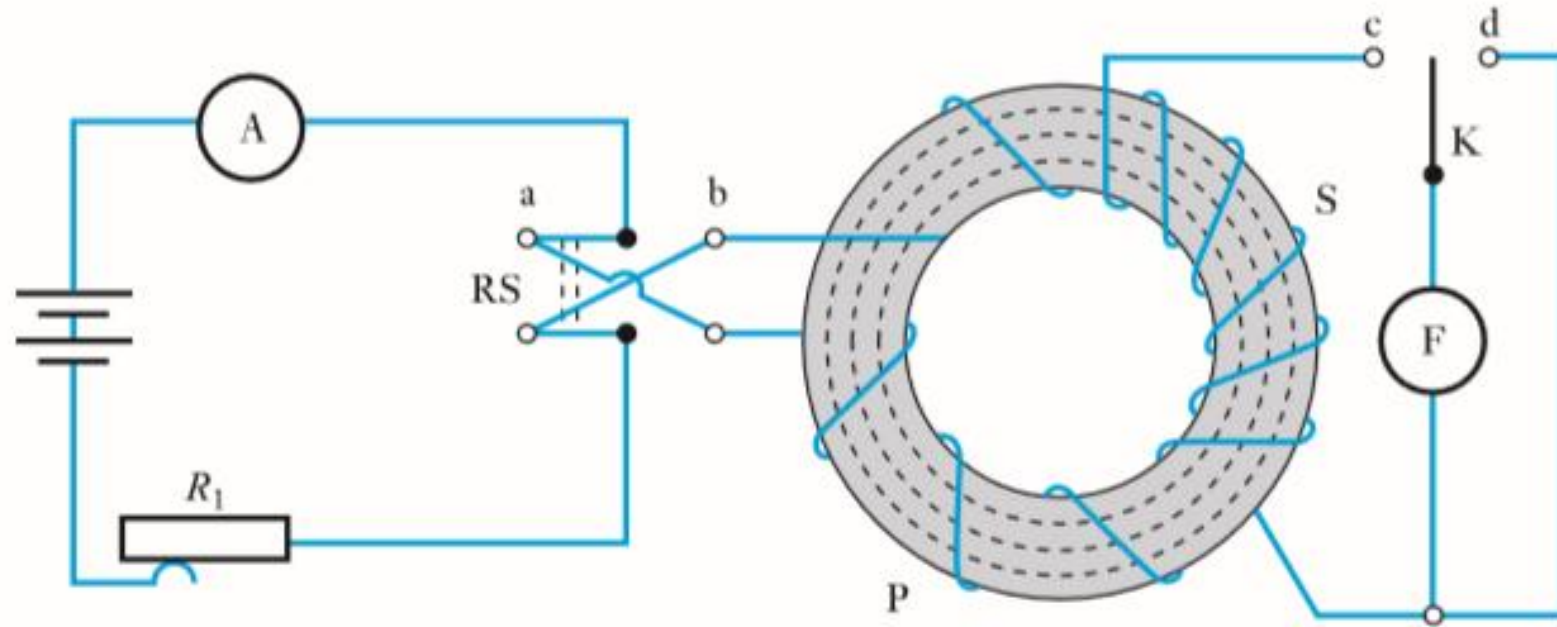
# Experimental Determination of $B$ - $H$ Curve



**Input coil  $P$**  is connected to a battery through a **reversing switch  $RS$** , an **ammeter  $A$**  (to **measure input current**) and a **variable resistor  $R_1$**  (to **vary the input current  $I$**  and hence the **applied field intensity  $H \propto I$** ).

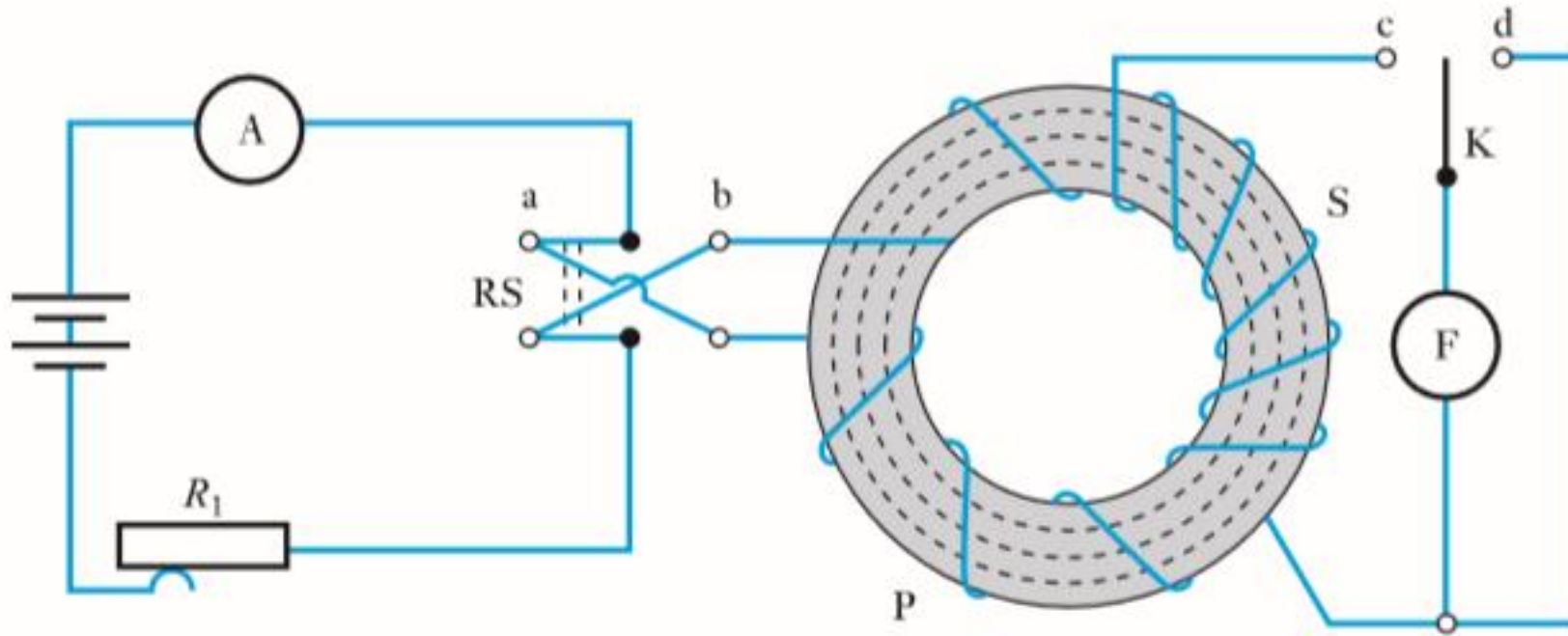
**Output coil  $S$**  is connected through a **two-way switch  $K$**  to fluxmeter  $F$ .

# Experimental Determination of $B$ - $H$ Curve



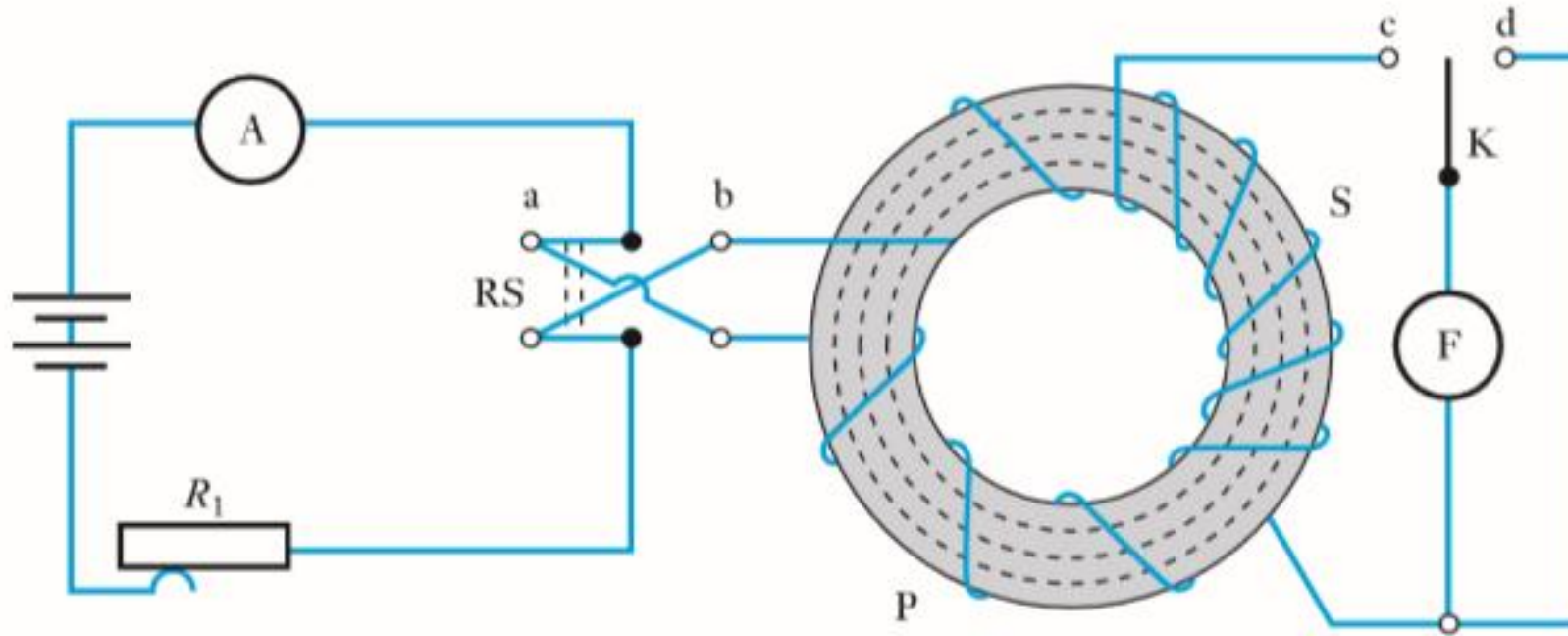
The **current** through input **coil P** is adjusted to a **desired value** by means of  $R_1$  and **switch RS** is then **reversed several times** to bring the core into a ‘**cyclic**’ steady-state condition, i.e. the **flux** in the ring **reverses** from a certain value in **one direction** to the same value in the **reverse direction**. During this cyclic operation, **switch K** is at position ‘**d**’, thereby **short-circuiting** the **fluxmeter**.

# Experimental Determination of $B-H$ Curve



Now, with switch **RS** initially at 'up' position, switch **K** is moved over to 'c', the **current** through **P** is **reversed** by moving **RS** quickly over to 'down' position. As the **flux** in the ring changes suddenly due to the **above process**, the **e.m.f. induced in S** (Lenz's law) sends a **current** through the **fluxmeter** and produces a **deflection** that is **proportional** to the **change of flux-linkages** in output **coil S**. This fluxmeter deflection  $\theta$  is noted.

# Experimental Determination of $B$ - $H$ Curve



If  $N_P$  is the **number of turns** on coil **P**,  $l$  the mean **circumference** of the **ring**, and  $I$  is the **input current** through **P**, the applied magnetic field strength is

$$H = \frac{IN_P}{l} \quad (1)$$

- If ' $\theta$ ' is the **fluxmeter deflection** when current through coil P is reversed and ' $c$ ' is the **fluxmeter constant** (flux change per unit deflection),

$$\text{Change of flux linkages with the coil } S = c\theta \quad (2)$$

- If the **flux** in the ring **changes** from  $\phi$  to  $-\phi$  when the current through input coil P is reversed, and if  $N_s$  is the **number of turns** of output coil S, the change of flux linkages ( $\propto$  emf induced) with coil S is

$$\text{Change of flux*number of turns on } S = 2\phi N_s \quad (3)$$

- Equating (2) and (3), we get  $2\phi N_s = c\theta \Rightarrow$

$$\phi = \frac{c\theta}{2N_s}$$

- If  $A$  is the **cross-sectional area** of the ring,

Flux density

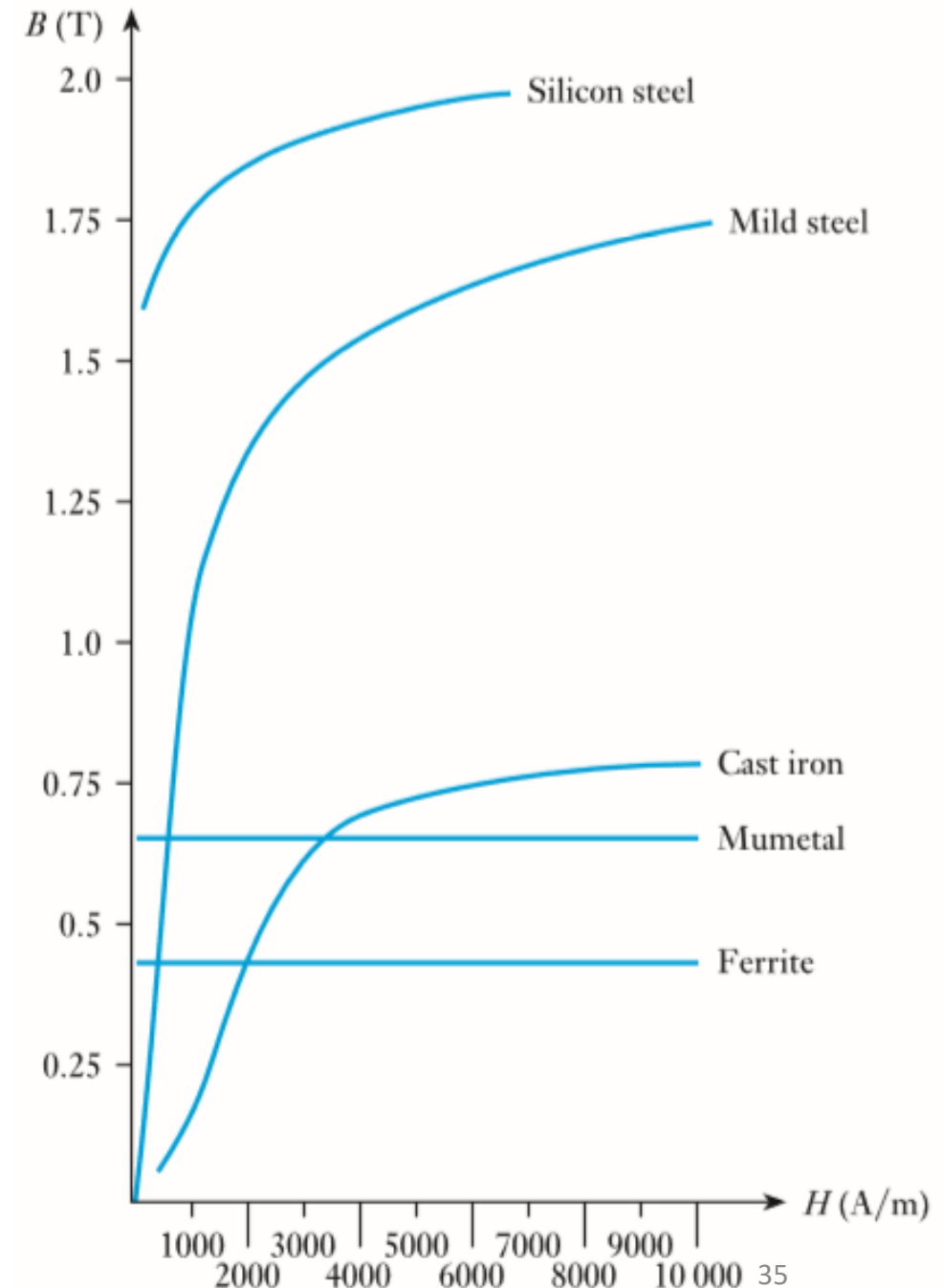
$$B = \frac{\phi}{A} = \frac{c\theta}{2AN_s}$$



# Experimental Determination of $B$ - $H$ Curve

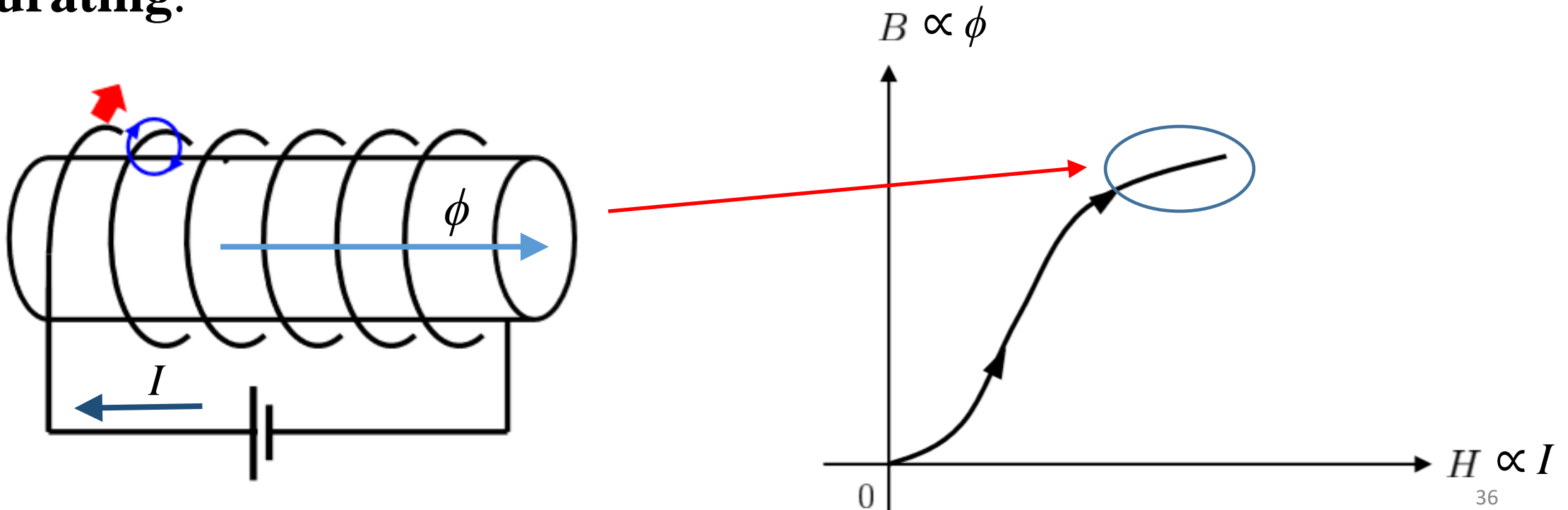
The test is performed with different values of the current  $I$  (hence different values of applied field strength  $H$ ); and the corresponding values of flux density  $B$  are determined (by measuring the fluxmeter deflection  $\theta$ ).

The  $B$ - $H$  data when plotted yield graphs like the ones shown.



# Magnetization and Hysteresis

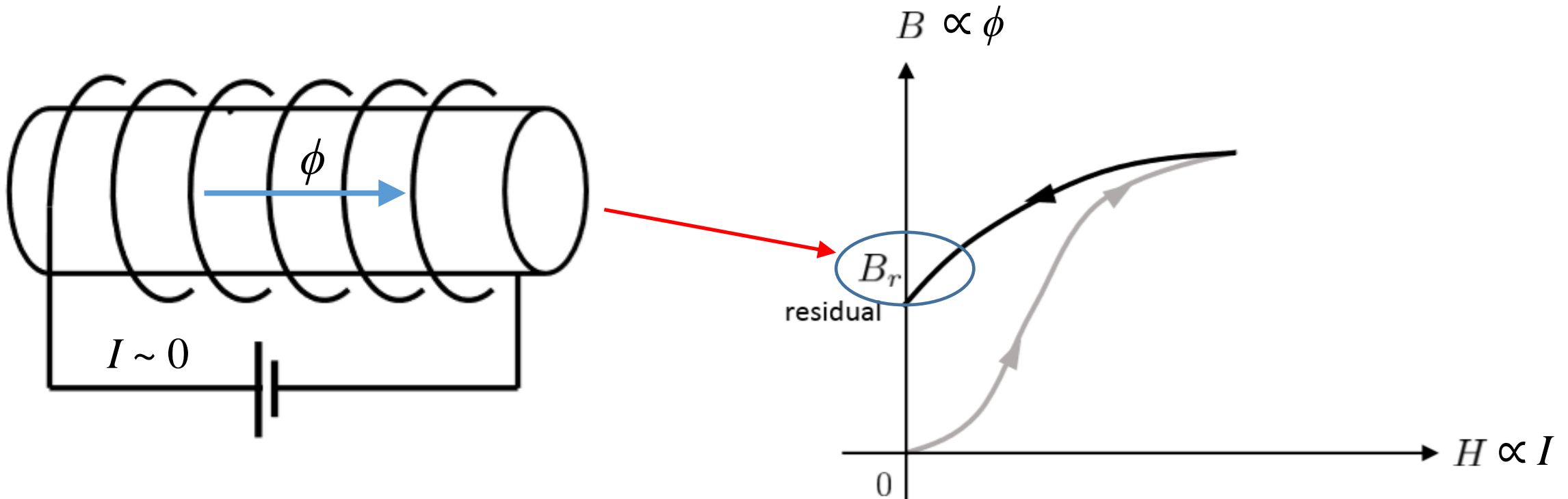
- A demagnetized magnetic material has  $B = 0$  when  $H = 0$ . As the applied magnetic field strength  $H$  is increased, the typical  $B$ - $H$  relationship observed is of the type shown below.
- For **large** values of  $H$ , the induced flux density  $B$  in the **material** starts **saturating**.





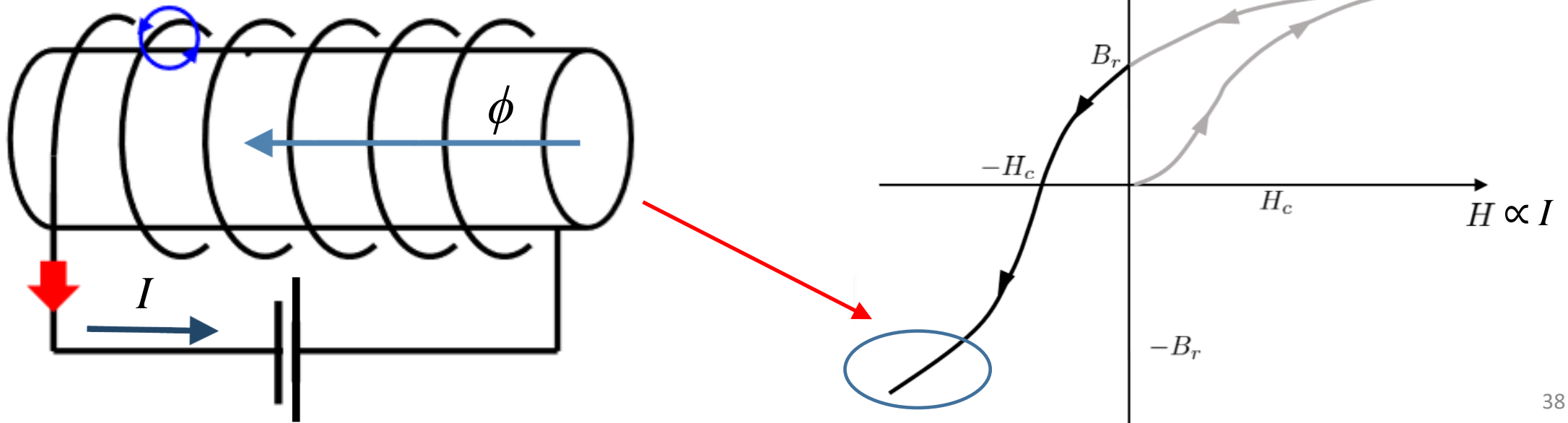
# Magnetization and Hysteresis

- Now if  $H$  is reduced back to 0 (by ramping the current back to zero), the induced flux density  $B$  does not follow the same path. There is **residual magnetism** ( $B_r$ ) leftover in the material even at  $H = 0$ .



# Magnetization and Hysteresis

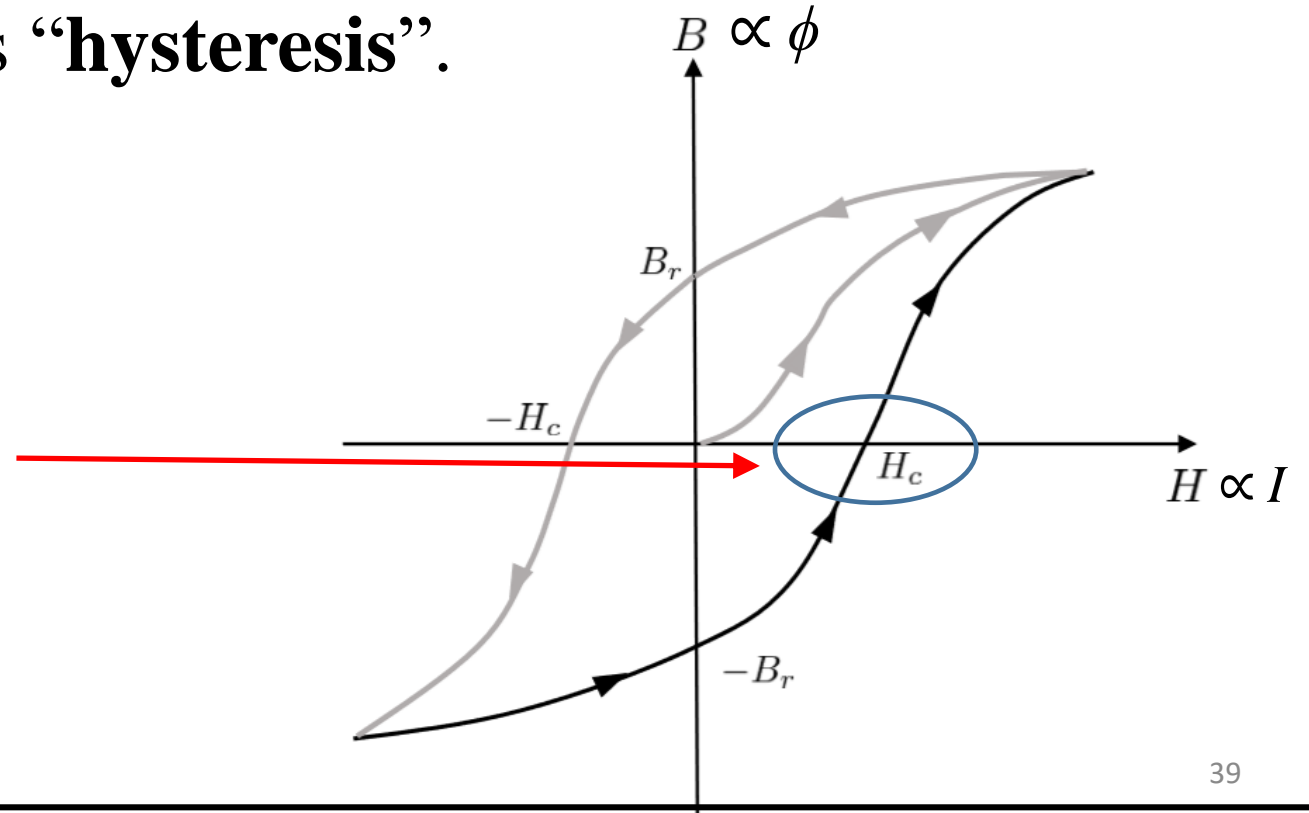
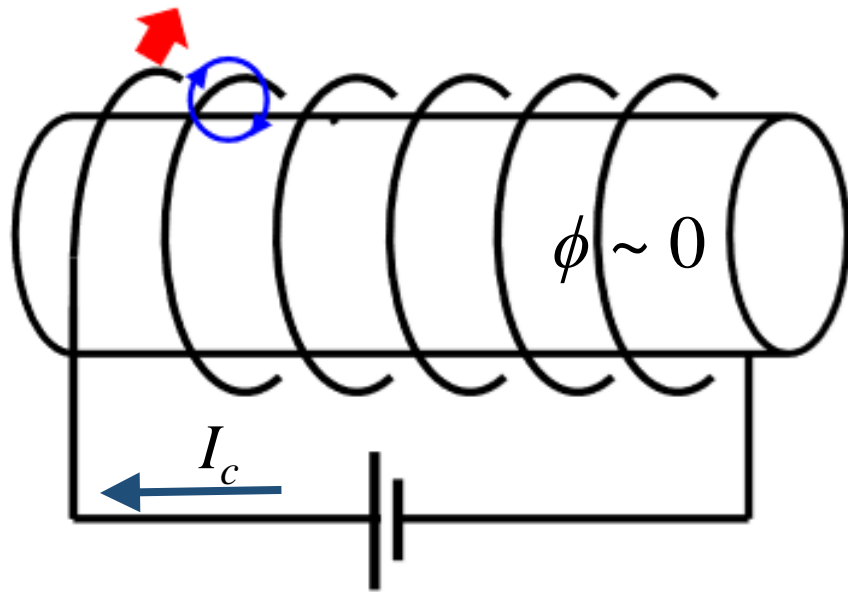
- As  $H$  is further reduced to negative values (by reversing the direction of applied current),  $B$  returns to zero only when  $H = -H_c$ . The value of  $H_c$  is called “coercive force/field”.
- As  $H$  is made even **more negative**, the flux density  $B$  in the material **saturates** in the **negative** direction.



# Magnetization and Hysteresis

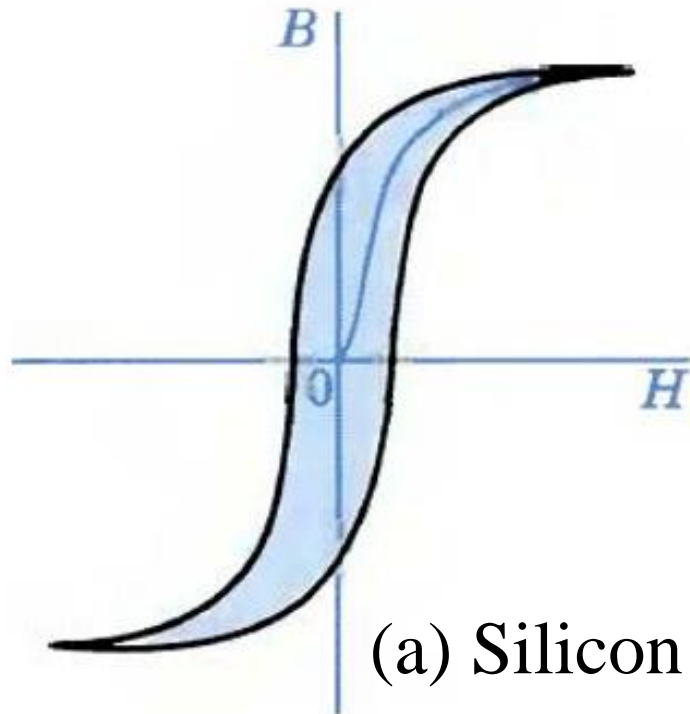
Now as  $H$  is **increased** again towards positive values, a **residual magnetism**  $-B_r$  remains at  $H = 0$ . Then  $B = 0$  is again reached at  $H = +H_c$ , and finally positive saturation occurs, but arrived via a **different path**.

This phenomenon of **non-conformity** (i.e. non-overlapping) of ‘**increase**’ and ‘**decrease**’ curves, is called as ‘**hysteresis**’.

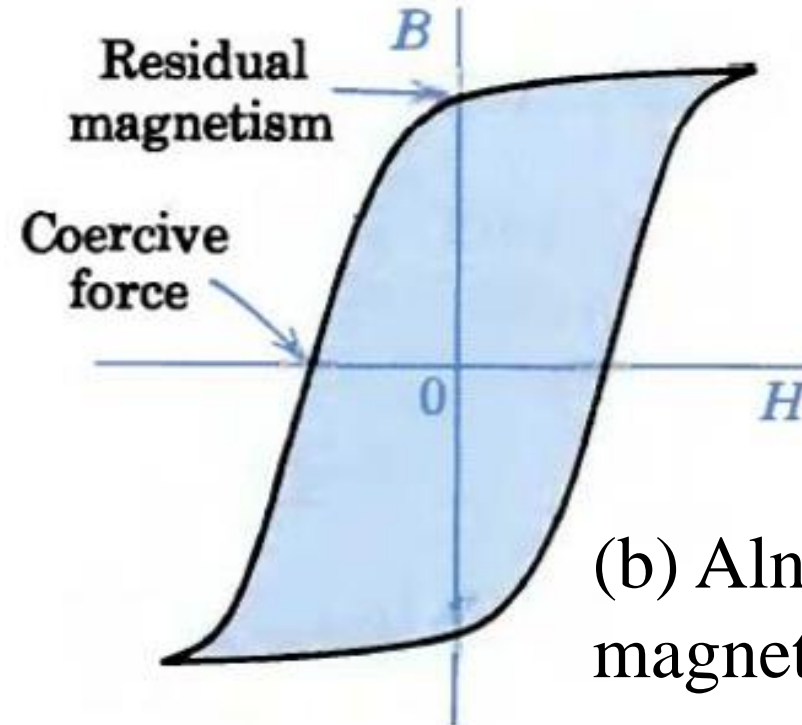


# Hysteresis Loop

- Thus, when a magnetic material is magnetized (flux induced), the original state is not returned to when applied magnetizing force/field is removed.
- If the magnetizing force is due to an applied AC current, a hysteresis loop results in every cycle/time period.



(a) Silicon steel



(b) Alnico (ferromagnetic alloy)

# Hysteresis Loss

- The **hysteresis** caused by **cyclic magnetization-demagnetization** leads to some magnetizing **energy** to be **lost**.
- The **area** of the  **$B$ - $H$  loop** gives the amount of **power lost** as heat in the cyclic magnetization-demagnetization process (less area => less loss)
- Empirical formula for power loss due to hysteresis:  $P_h = K_h f B_m^n$

The constants  $K_h$  and  $n$  **depend** on core **material**.

$f$  is the **frequency** of **AC** magnetizing current.

Typically  $n \sim 1.6 - 2$  (called the “**Steinmetz Exponent**”)

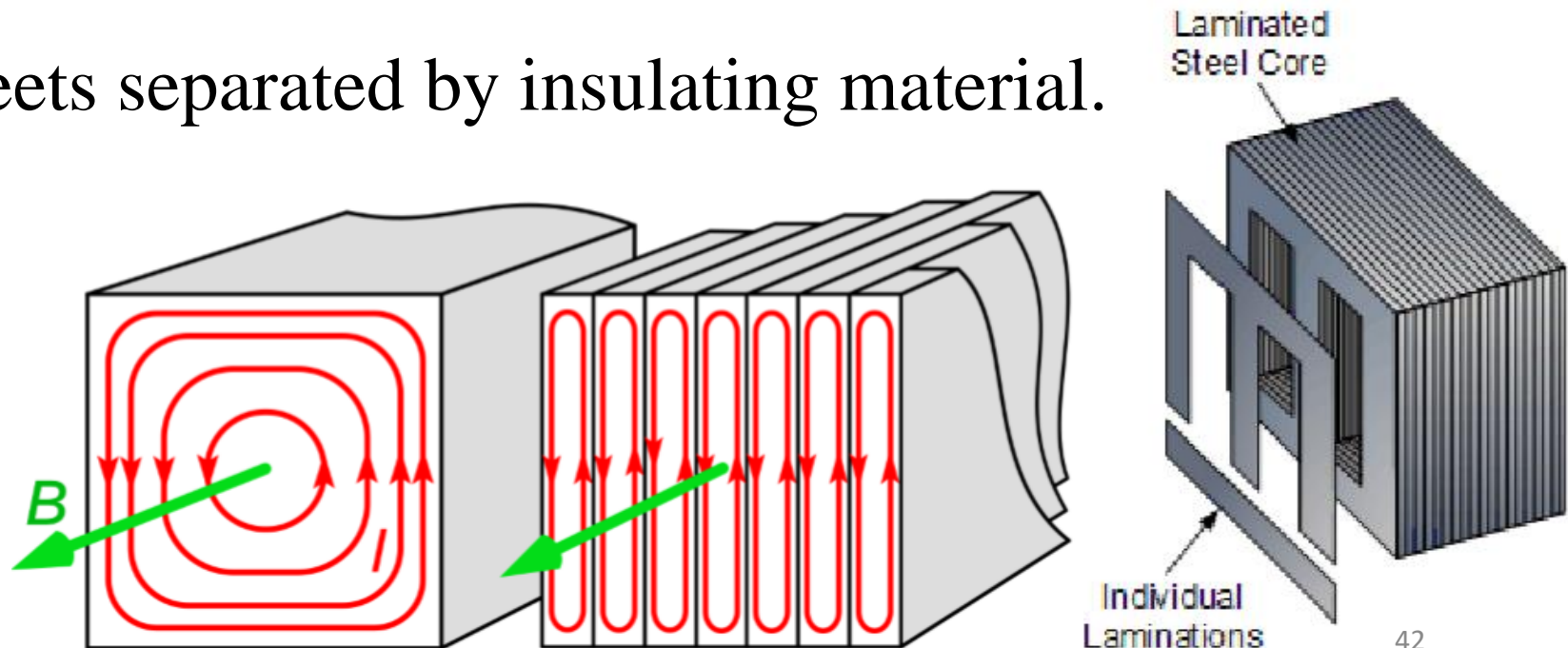
$B_m$  is the **maximum**/saturated induced **flux density** per cycle

# Eddy Current Loss

- If the magnetic core is solid, there can also be Eddy current loss.
- Localized Eddy currents excited by AC magnetic flux induced voltages (Lenz's law) result in  $I^2R$  losses.
- Loss can be reduced by using laminated core designs.
- Core in the form of sheets separated by insulating material.

➤ Loss:  $P_e = K_e (fB_m)^2$

( $K_e$  lower for laminated as compared to bulk material)



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