Robotics and Intelligent Systems Lab II Report 6

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Task 1.25. Show that under the assumption of negligible La,

$$H_{er}(s) = \frac{s^2 D(s)}{Q(s)}$$

$$Q(s) = R_a J s^3 + s^2 (R_a b + k_e k_t + k_t K_D) + k_t K_P s + k_t K_I$$

$$H_{er}(s) = \frac{1}{1 + H_{avv}(s)G(s)} = \frac{s^2 D(s)}{s^2 D(s) + k_t (K_D s^2 + K_P s + K_I)}$$

$$(1.49d)$$

By putting D(s)= $(R_a(Js + b) + k_e k_t)$ into the formula where $L_a = 0$, we can prove $H_{er}(s) = \frac{s^2 D(s)}{O(s)}$;

$$H_{er}(s) = \frac{s^{2}(R_{a}(Js+b) + k_{e}k_{t})}{s^{2}(R_{a}(Js+b) + k_{e}k_{t}) + k_{t}(K_{D}s^{2} + K_{p}s + K_{I})}$$

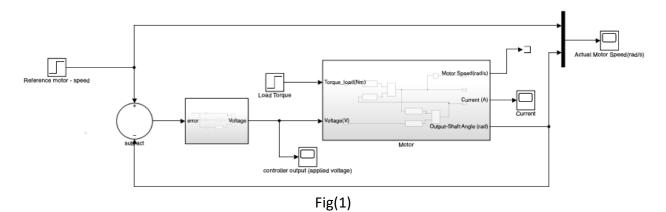
$$s^{2}(R_{a}(Js+b) + k_{e}k_{t}) + k_{t}(K_{D}s^{2} + K_{p}s + K_{I})$$

$$= R_{a}Js^{3} + s^{2}(R_{a}b + k_{e}k_{t} + k_{t}K_{D}) + k_{t}K_{P}s + k_{t}K_{I} = Q(s)$$

$$\therefore H_{er}(s) = \frac{s^{2}D(s)}{s^{2}(R_{a}(Js+b) + k_{e}k_{t}) + k_{t}(K_{D}s^{2} + K_{p}s + K_{I})}$$

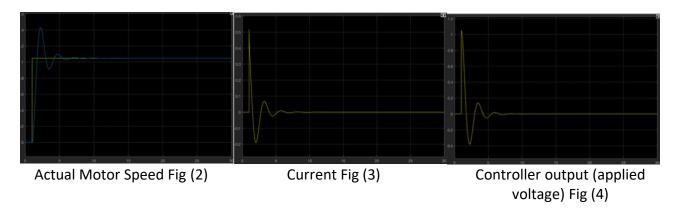
$$H_{er}(s) = \frac{s^{2}D(s)}{R_{a}Js^{3} + s^{2}(R_{a}b + k_{e}k_{t} + k_{t}K_{D}) + k_{t}K_{P}s + k_{t}K_{I}} = \frac{s^{2}D(s)}{Q(s)}$$

Task 1.26. Copy the model-file for the PID speed-controller to a new file. Now change the speed-controller to a servo-controller as shown in Fig. 1.19.



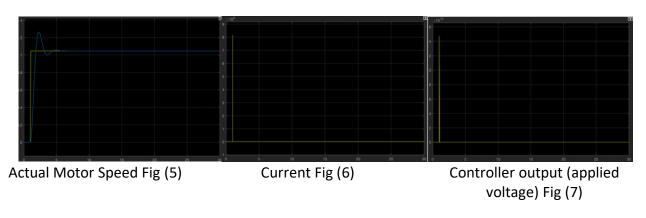
Task 1.27. *Proceed as follows:*

1. Start with some relatively small value of KP such as 1, keeping KD and KI zero. Set the reference input to fi/3 rad and T_L © 0. Simulate the sytem for 30 seconds. Create a table with the following columns and jot down your observations: KP, KI, KD, max absolute value of current, max absolute value of voltage, max overshoot of the angle above the reference, settle-time (approx. time it takes for the angle to settle near its steady-state value).



K_p	K_I	K_D	Max abs	Max abs	Max	Settle-time
			Current	Voltage	overshoot	
					angle	
1	0	0	0.5169	1.047	0.372	8.006

2. Now add some damping by setting KD = 0.1. Enter your observations in the table.



K_{p}	K_{I}	K_D	Max abs	Max abs	Max	Settle-time
•			Current	Voltage	overshoot	
					angle	
1	0	0.11	8.174×10^6	1.474×10^{13}	0.207	4.911

3. Now add some integral control $K_I = 0.1$. Enter your observations in the table.



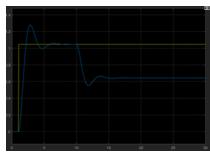
Actual Motor Speed Fig (8)

Current Fig (9)

Controller output (applied voltage) Fig (10)

K_{p}	K_{I}	K_D	Max abs	Max abs	Max	Settle-time
			Current	Voltage	overshoot	
					angle	
1	0.1	0.11	8.174×10^6	1.474×10^{13}	0.268	20.976

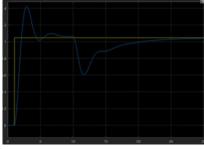
4. Now we will see what the controller can do if we add a step load torque. First reset $K_I = 0$. Reduce K_P to 0.5 and K_D to 0.001. Make a step load of $T_L = 0.01$ Nm at t = 10 seconds. Did the system reach its reference value?



Actual Motor Speed Fig (11)

The system did not reach its reference value, that is 1.047.

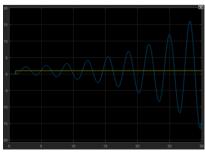
5. Now increase K_I to 0.1 and simulate again. Do you see any dierence in the steady-state error?



Actual Motor Speed Fig (12)

The steady-stat error decreased, leading the system to reach its reference value.

6. Although it is now tempting to increase K_I even more, we should be careful. Making K_I too big can easily make the closed-loop system unstable. Let us see how an unstable system reacts: set $K_I = 1$ and simulate.



Actual Motor Speed Fig (13)

The unstable system reacts in oscillations.

7. Does our model also predict this instability? Find the poles of the system by finding the roots of Q(s) for these controller parameters. Are they in LHP?

$$Q(s) = (2.4 \times 0.07)s^3 + (2.4 \times 0.00679 + 0.2154 \times 0.1186 + 0.001 \times 0.1186)s^2 + (0.1186 \times 0.5)s + 0.1186$$

$$Q(s) = 0.0168s^3 + 0.02729464s^2 + 0.0593s + 0.1186 = 0$$

$$Roots = 0.0969 + 1.9679i, 0.0969 - 1.9679i, -1.8185 + 0.0000i$$

Our model predicts instability because there's 1 pole in LHS and 2 poles in RHS.