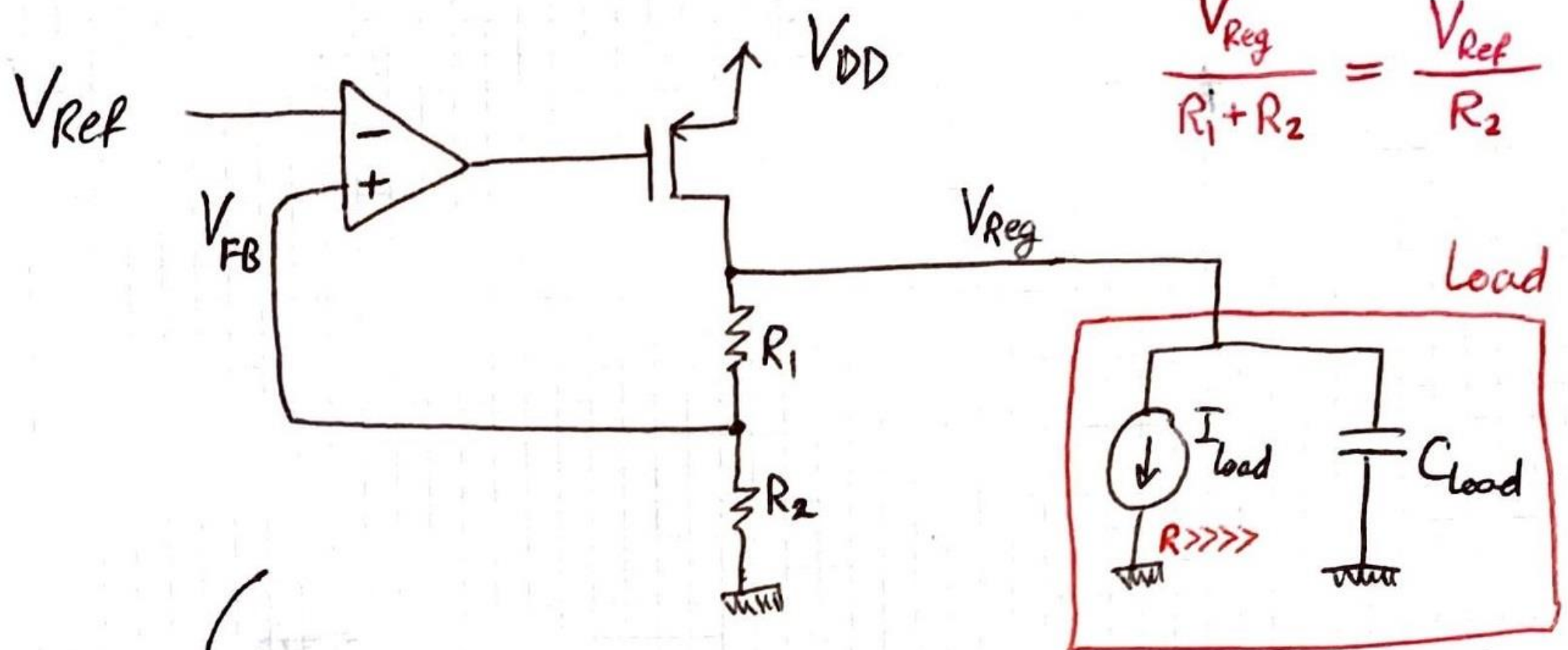
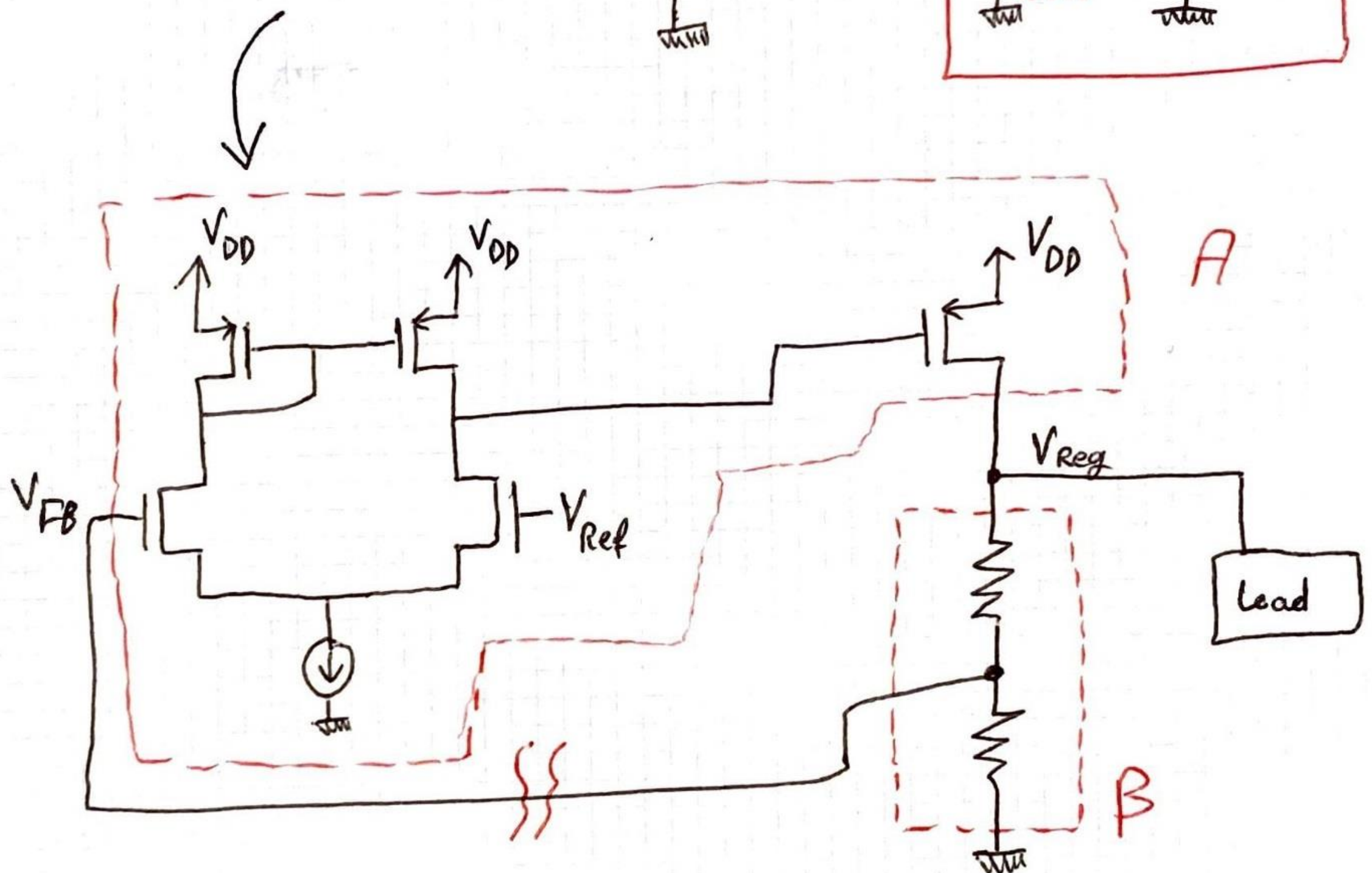


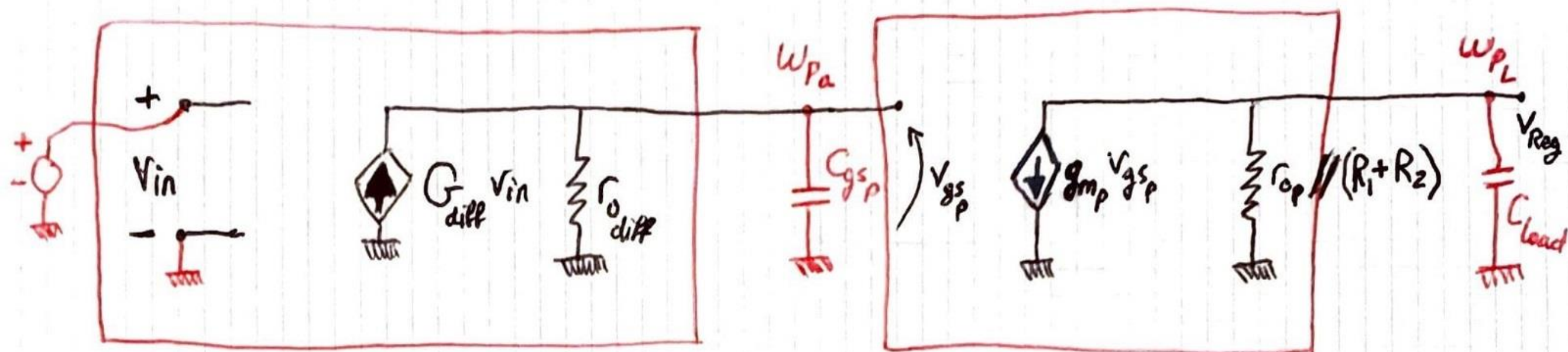
LDO Analysis



$$\frac{V_{Reg}}{R_1 + R_2} = \frac{V_{Ref}}{R_2}$$



$$A_{cl} = \frac{A}{1 + AB} = \frac{A}{1 + L}$$



Diff Amp

Pass Device

$$L = \text{Loop Gain} = \frac{G_{\text{diff}} r_{o\text{diff}} \cdot g_{\text{mp}} R_{\text{load}}}{\left(1 + \frac{s}{\omega_{Pa}}\right) \left(1 + \frac{s}{\omega_{PL}}\right)}$$

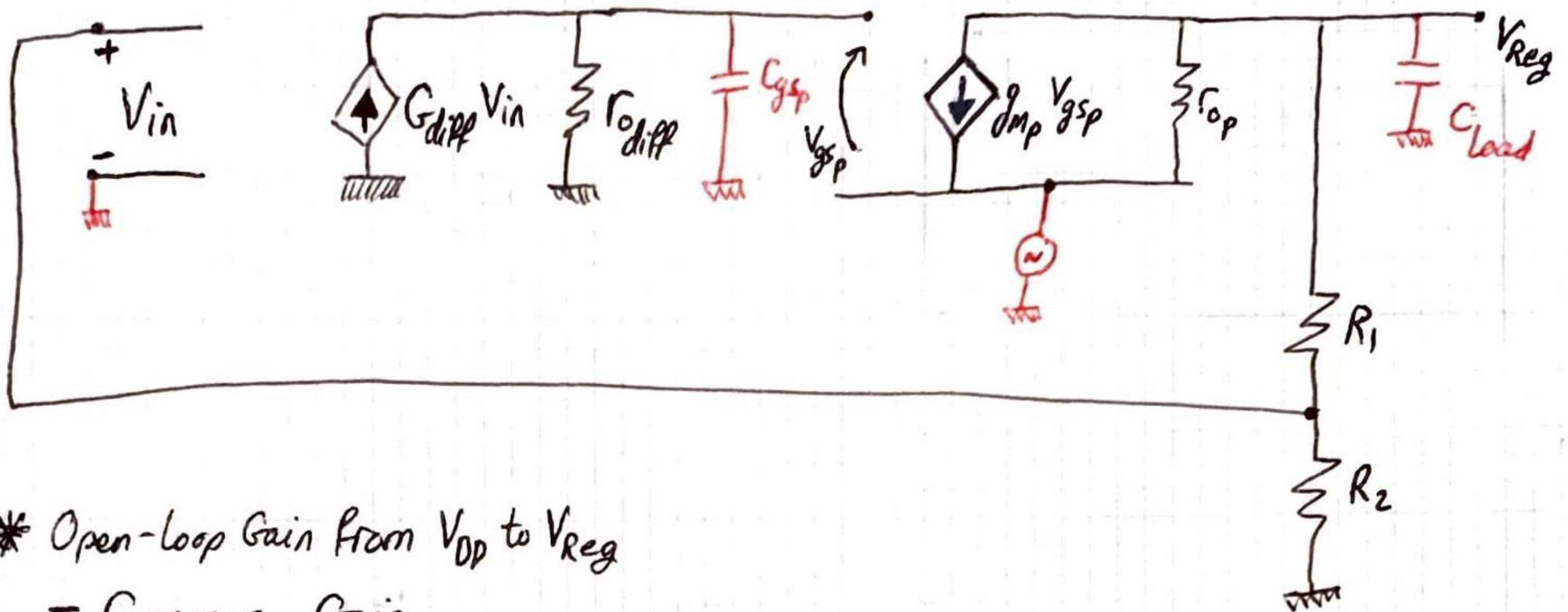
$$R_{\text{load}} = r_{oP} \parallel (R_1 + R_2)$$

➔ For PM

$$\omega_{Pa} = \frac{1}{r_{o\text{diff}} \cdot C_{gsP}}$$

$$\omega_{PL} = \frac{1}{R_{\text{load}} \cdot C_{\text{load}}}$$

➔ $\omega_{Pa} < \omega_{PL}$
↓
dominant



* Open-loop Gain from V_{DD} to V_{reg}
= Common-Gain

$$H_{CG} \approx g_{mp} R_{load} \cdot \frac{1}{(1 + \frac{s}{\omega_{out}})}$$

$$R_{load} = r_{dp} \parallel (R_1 + R_2)$$

$$\omega_{out} = \frac{1}{C_{load} \cdot R_{load}}$$

* Closed-loop Gain from V_{DD} to V_{reg}

$$H = \frac{V_{reg}}{V_{DD}} = PSRR^{-1} = \frac{H_{CG}(s)}{1 + L(s)}$$



For PSRR

* Usually: @ low $I_{load} \rightarrow PM_{min}$
@ high $I_{load} \rightarrow PSRR_{min}$

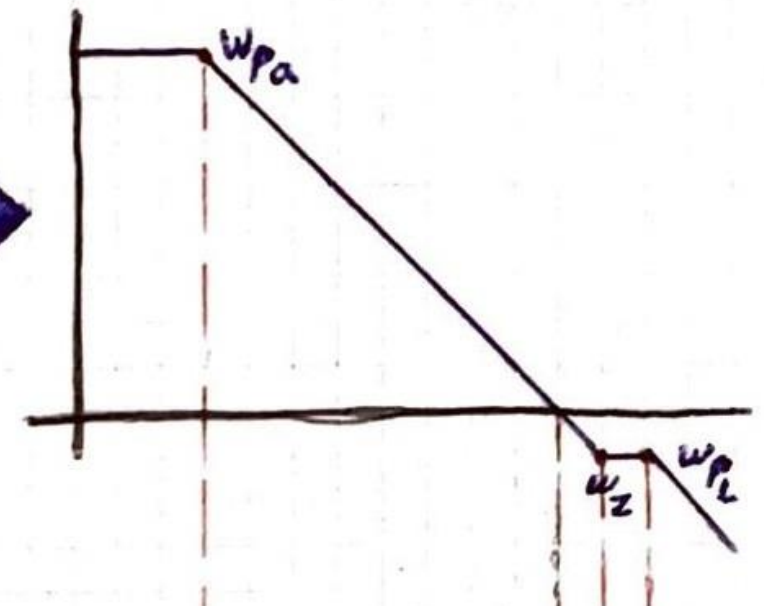
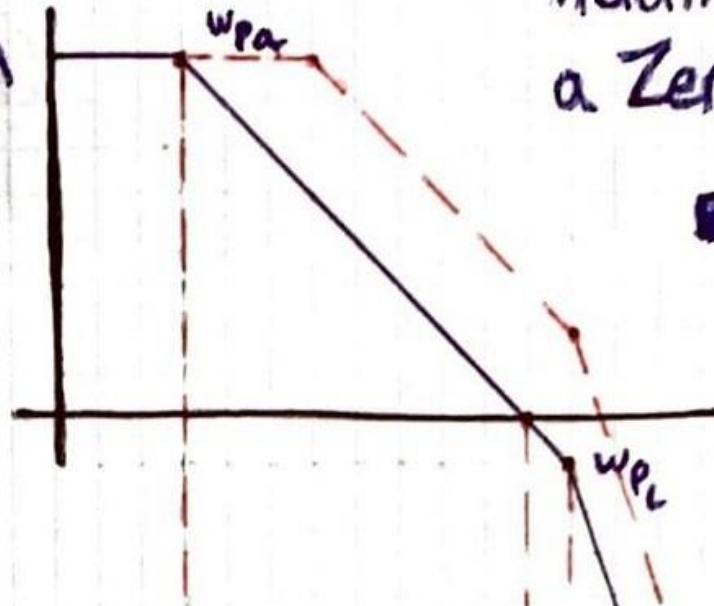
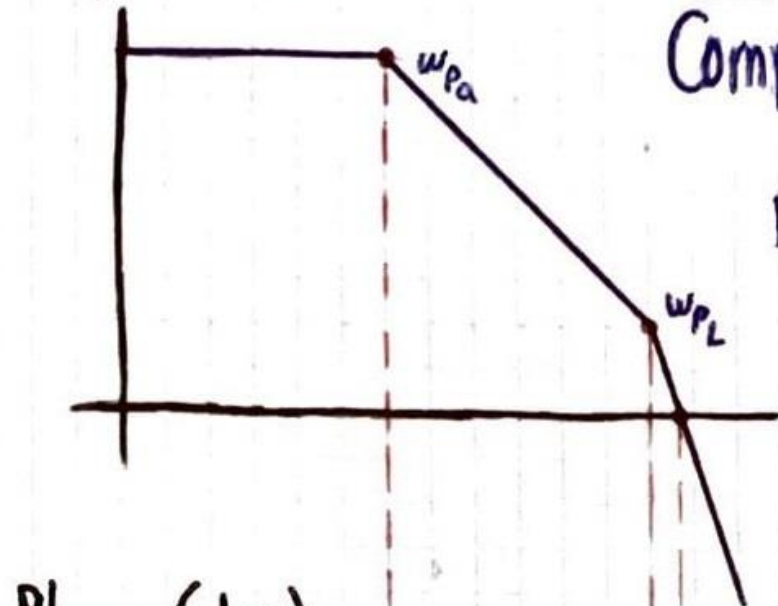
Loop Gain & PSRR

(Assume ω_p dominant)

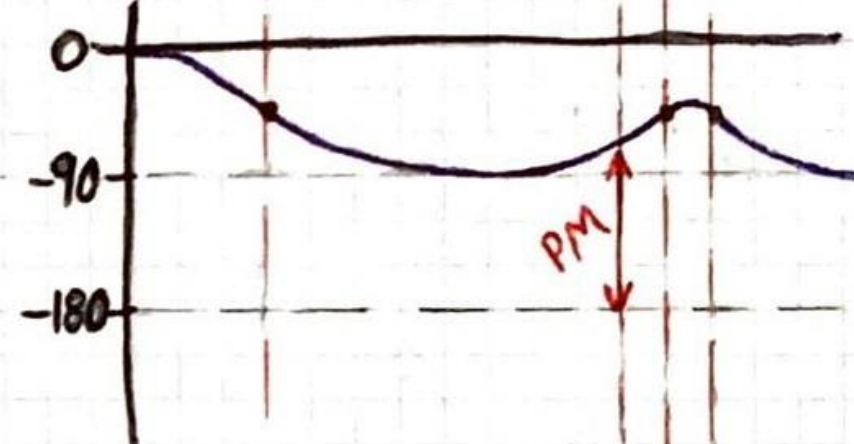
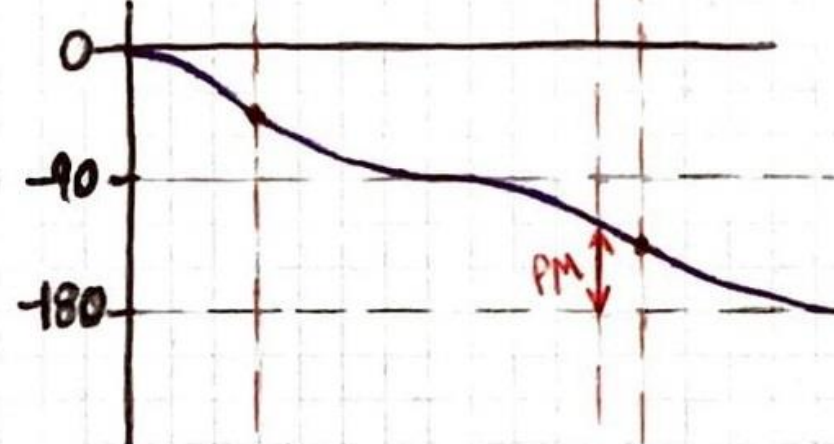
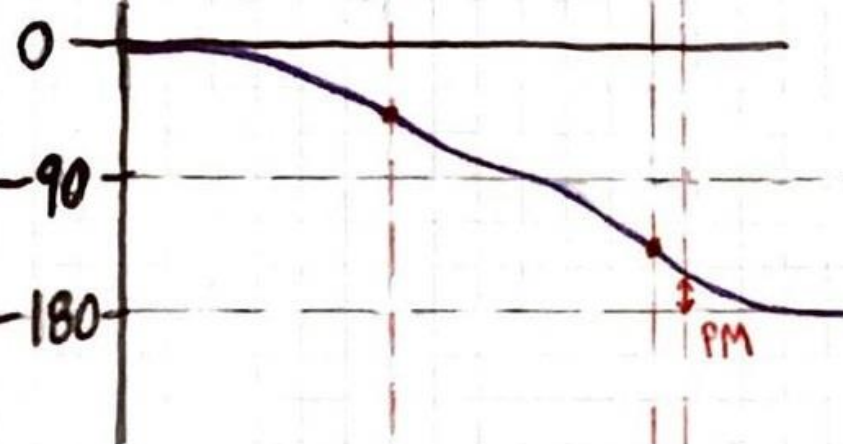
Loop Gain (dB)

With Miller Compensation

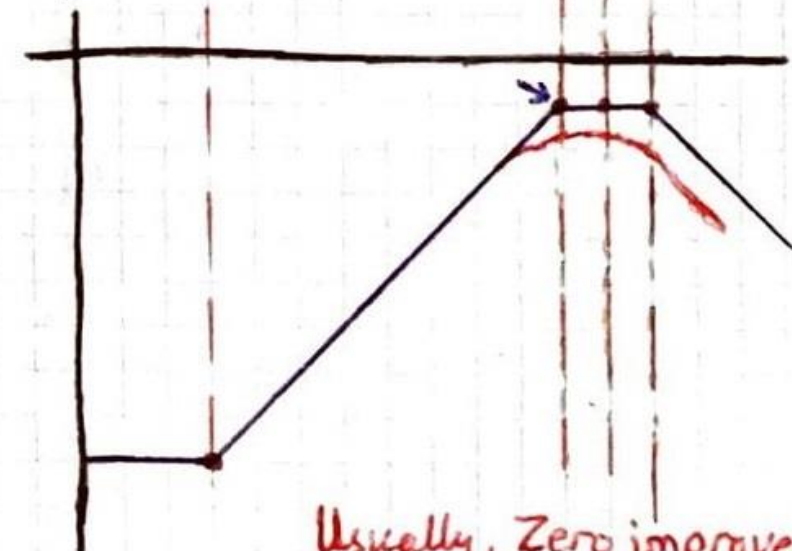
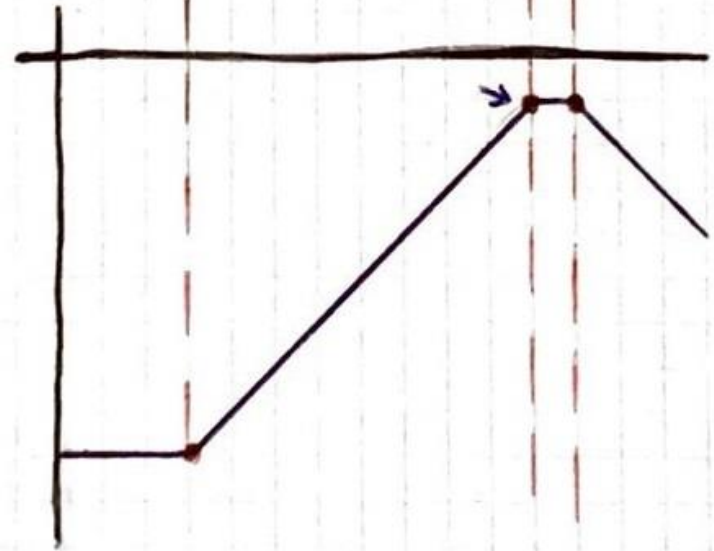
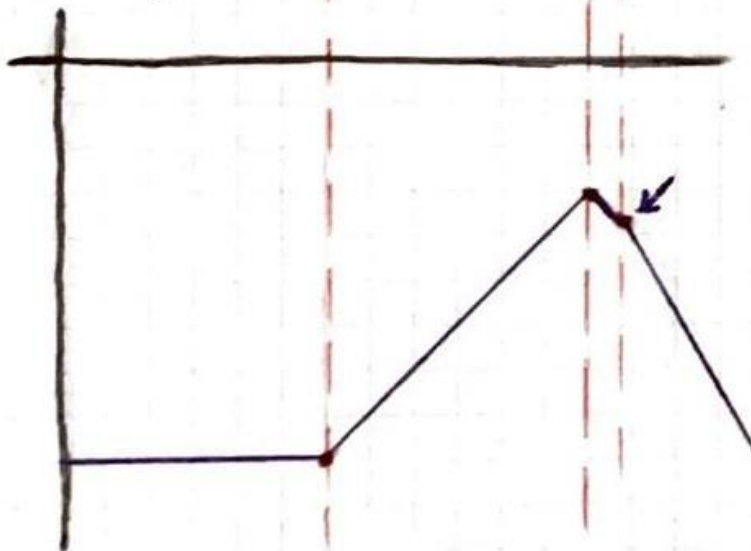
Adding a Zero



Phase (deg)



PSRR⁻¹ (dB)



Usually, Zero improves both PM & PSRR



Phase Margin Improves

PSRR Worsens (Max PSRR⁻¹ Increases)

} Tradeoff

* Note: ① $\omega_{pL} < UGB \rightarrow PM \ll$ (Unstable loop)
② As $\omega_{pL} \gg UGB \rightarrow PM \uparrow$ but $PSRR^{-1} \uparrow$

LDO Compensation

① Miller Compensation:

Assuming $R_c = 0$ for now:

① dominant pole

$$\omega_{p_d} = \frac{1}{r_{o_{diff}} (g_{mp} R_L) C_c + C_{GBP}}$$

② Non dominant pole

$$\omega_{p_L} = \frac{g_{mp}}{C_{gsP} + C_L}$$



③ Zero

$$\omega_z = \frac{g_{mp}}{C_c}$$

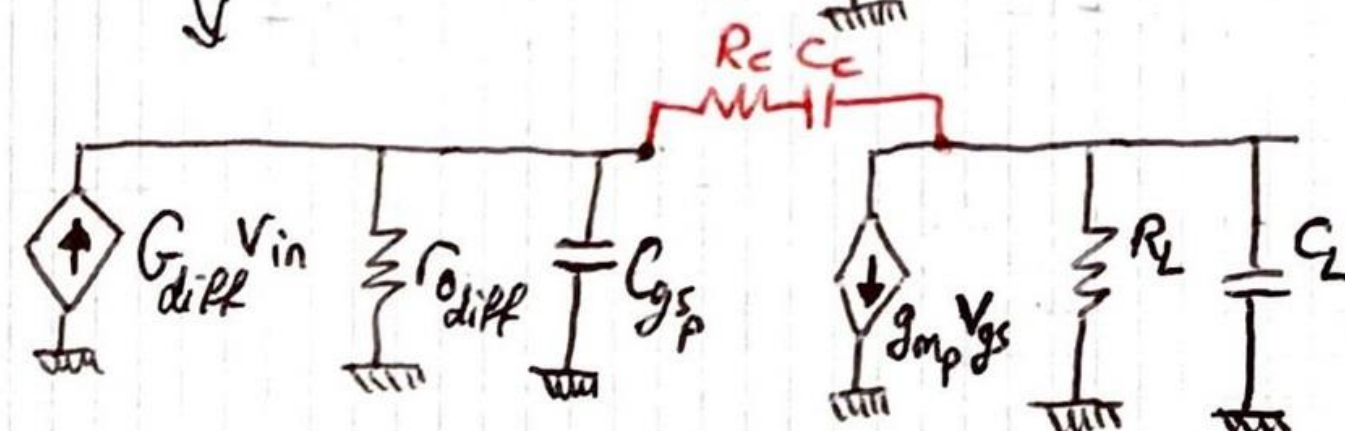
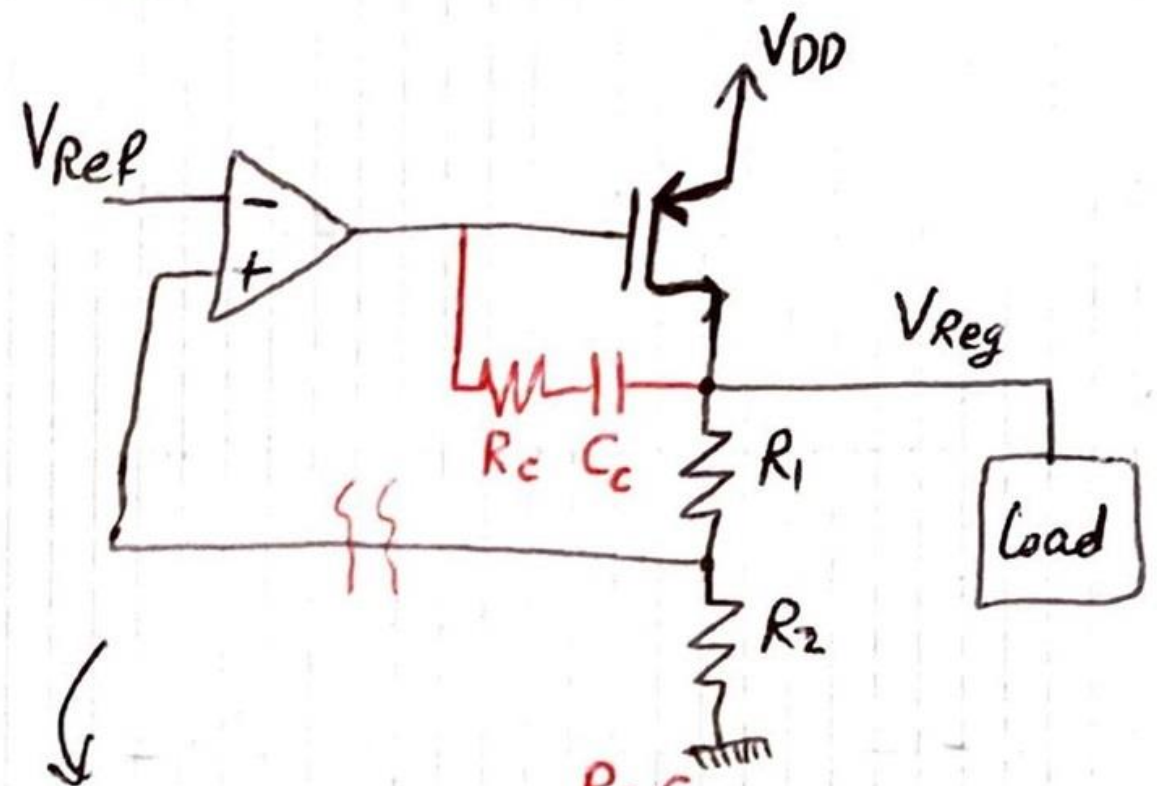
↓ RHP zero, reduces PM (undesirable)

if $R_c \neq 0$

$$\omega_z = \frac{1}{C_c \left(\frac{1}{g_{mp}} - R_c \right)}$$

→ $R_c > \frac{1}{g_{mp}}$
to give phase lead (improve PM)

→ $U_{GB} = \omega_o = \frac{G_{diff}}{C_c}$



② RC Compensation:

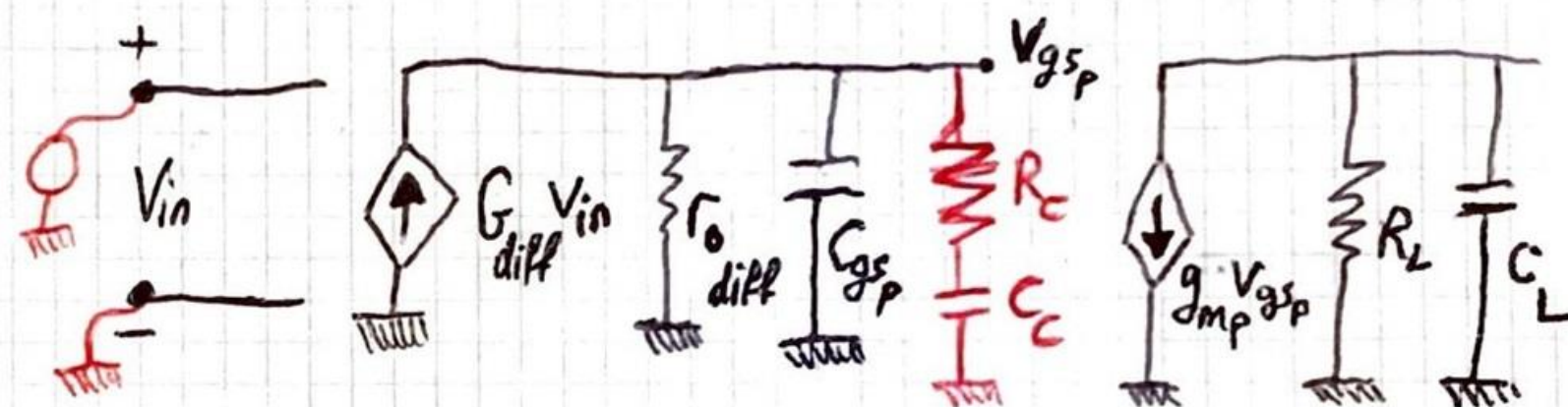
Assume $C_c \gg C_{gs_p}$ (ignore C_{gs_p} for now)

→ To find the zero, find the condition where $V_{gs_p} = 0$:

$$V_{gs_p} = G_{diff} V_{in} \left(r_o \parallel R_c + \frac{1}{sC_c} \right) = 0$$

$$\therefore \frac{r_o \cdot \left(R_c + \frac{1}{sC_c} \right)}{r_o + R_c + \frac{1}{sC_c}} = 0$$

$$\frac{(1 + sR_cC_c)}{(1 + s(r_o + R_c)C_c)} = 0$$



→ ① dominant pole

$$\omega_{p1} = \frac{1}{(r_o + R_c)C_c}$$

② Zero

$$\omega_z = \frac{1}{R_cC_c}$$

③ Non dominant poles

$$\omega_2 = \frac{1}{C_{gs_p} (r_o \parallel R_c)}$$

$$\omega_3 = \frac{1}{C_L R_L}$$

at higher frequencies,
 $C_c \sim$ as a short

