

Group Assignment 1

With Collective Effort

AE 616: Gas Dynamics
Group 5



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by

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Nomenclature

Abbreviations

Symbols

Symbol	Definition	Unit
T_0	Stagnation Temperature	[K]
X^*	Parameter X in the Starred (Diabatic-Sonic) state	[unit(X)]
M	Mach Number	[]
c_p	Specific Heat at Constant Pressure	[J· Kg ⁻¹ · K ⁻¹]
γ	Ratio of Specific Heats	[]

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Question 1

Derive a closed-form analytical expression for the Mach number in terms of the ratio of the total temperature to its diabatic sonic counterpart (i.e., T_0/T_0^*). Clearly identify the subsonic and supersonic solutions, with proper justification. Also, determine the ranges of T_0/T_0^* in which your equations are valid.

Solution:

As already derived in class,

$$\frac{T_{0,2}}{T_{0,1}} = \frac{(1 + \gamma M_1^2)^2 M_2^2 (1 - \frac{\gamma-1}{2} M_2^2)}{(1 + \gamma M_2^2)^2 M_1^2 (1 - \frac{\gamma-1}{2} M_1^2)} \implies \frac{T_0}{T_0^*} = \frac{2(1 + \gamma)M^2 (1 + \frac{\gamma-1}{2} M^2)}{(1 + \gamma M^2)^2}$$

$$\text{Let } a = \frac{T_0}{T_0^*}, \quad x = M^2$$

$$\text{Then } (1 - \gamma^2(1 - a))x^2 - (1 + \gamma(1 - a))x + a = 0$$

This simplifies to

$$x = \frac{1 + \gamma - a\gamma \pm \sqrt{(1 + \gamma - a\gamma)^2 - (1 + a\gamma^2 - \gamma^2)}}{1 + a\gamma^2 - \gamma^2}$$

$$x = \frac{1 + \gamma - a\gamma}{1 + a\gamma^2 - \gamma^2} \pm \frac{\sqrt{\gamma^2(1 - a) + 2\gamma(1 - a) + 1 - a}}{1 - \gamma^2(1 - a)}$$

$$\text{Let } 1 - a = b \quad \frac{1 + \gamma*b}{1 - \gamma^2*b} = \frac{(\gamma+1)\sqrt{b}}{1 - \gamma^2*b}$$

$$M^2 = \frac{1 + \gamma(1 - \frac{T_0}{T_0^*})}{1 - \gamma^2(1 - \frac{T_0}{T_0^*})} \pm \frac{1 + \gamma}{1 - \gamma^2(1 - \frac{T_0}{T_0^*})} \sqrt{1 - \frac{T_0}{T_0^*}}$$

The + part of the solution would be the supersonic solution, and the - part would be the subsonic solution. This is because we know how a Rayleigh curve looks like, and that the only time we get a single Mach number here is at the starred state. Any other $\frac{T_0}{T_0^*}$ will give one subsonic and one supersonic solution. The above equations are only valid for the values of $\frac{T_0}{T_0^*}$ which give a positive M^2 , since M physically cannot be non-real. That is,

$$\frac{1 + \gamma(1 - \frac{T_0}{T_0^*})}{1 - \gamma^2(1 - \frac{T_0}{T_0^*})} \pm \frac{1 + \gamma}{1 - \gamma^2(1 - \frac{T_0}{T_0^*})} \sqrt{1 - \frac{T_0}{T_0^*}} \geq 0$$

Since M^2 has to be real, $\frac{T_0}{T_0^*} \leq 1$.

Let us rewrite the inequality again in terms of $b = 1 - \frac{T_0}{T_0^*}$ (always positive):

$$\frac{1 + \gamma b}{1 - \gamma^2 b} \geq \mp \frac{1 + \gamma}{1 - \gamma^2 b} \sqrt{b}$$

For $b > \frac{1}{\gamma^2}$, the denominator is negative. Thus our condition gets divided into four parts:

1.1. Supersonic and $b > \frac{1}{\gamma^2}$

$$1 + \gamma b \leq -(1 + \gamma)\sqrt{b}$$

Clearly, this is impossible.

1.2. Supersonic and $b < \frac{1}{\gamma^2}$

$$1 + \gamma b \geq -(1 + \gamma)\sqrt{b}$$

Clearly, this is always the case.

1.3. Subsonic and $b > \frac{1}{\gamma^2}$

$$\begin{aligned} 1 + \gamma b &\leq (1 + \gamma)\sqrt{b} \\ (1 + \gamma b)^2 &\leq (1 + \gamma)^2 b \\ 1 + 2\gamma b + \gamma^2 b^2 &\leq b + 2\gamma b + \gamma^2 b \\ \gamma^2 b^2 - (1 + \gamma^2)b + 1 &\leq 0 \\ (\gamma^2 b - 1)(b - 1) &\leq 0 \end{aligned}$$

$$b \in \left(\frac{1}{\gamma^2}, 1 \right]$$

1.4. Subsonic and $b < \frac{1}{\gamma^2}$

$$\begin{aligned} 1 + \gamma b &\geq (1 + \gamma)\sqrt{b} \\ (\gamma^2 b - 1)(b - 1) &\geq 0 \end{aligned}$$

$$b \in \left[0, \frac{1}{\gamma^2} \right)$$

1.5. Special case: $b = \frac{1}{\gamma^2}$

From our original quadratic equation, we get

$$\begin{aligned} -\left(1 + \frac{1}{\gamma}\right)x &= -\left(1 - \frac{1}{\gamma^2}\right) \\ x &= 1 - \frac{1}{\gamma} \\ M &= \sqrt{\frac{\gamma - 1}{\gamma}} \end{aligned}$$

Summary: In the subsonic regime, all values of $\frac{T_0}{T_0^*}$ except $1 - \frac{1}{\gamma^2}$ work, but for the supersonic regime, only those greater than $1 - \frac{1}{\gamma^2}$ work.

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Question 2

Write a code (and run it) to reproduce the graph flashed in class showing the ratios of thermodynamic properties to their respective diabatic sonic counterparts (e.g. $\frac{p}{p^*}$, $\frac{T}{T^*}$, $\frac{T_0}{T_0^*}$, etc.) versus Mach number. Also reproduce the T-s diagram flashed in class (with appropriate normalization).

Solution:

Code and graphs for this Problem is given in Google colab. **[Google Colab link](#)**

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Question 3

Code up your solution of the first question and reuse parts from the second solution to design and implement a function with appropriate arguments and outputs, such that you can solve typical Rayleigh flow problems. Make this function in such a way that you can use it to solve examples 3.13 and 3.14 of Anderson's textbook (2003 edition) (or any two examples of your choice that exercise both the subsonic and supersonic parts of your code). Hence validate your code, with the given solutions to these example problems.

Solution:

Solution for this problem is given in Google Colab with code. **[Google Colab link](#)**